Received by UCD:S/24/2022 6:34:03 AM U.S. Department of the Interior BUREAU OF LAND MANAGEMENT		Sundry Print Report 05/24/2022
Well Name: BURTON FLAT 26-28 FED STATE COM	Well Location: T20S / R28E / SEC 26 / SESW /	County or Parish/State: /
Well Number: 623H	Type of Well: OIL WELL	Allottee or Tribe Name:
Lease Number: NMNM108513	Unit or CA Name: BURTON FLAT DEEP-EXPL	Unit or CA Number: NMNM70798X
US Well Number: 3001549256	Well Status: Drilling Well	Operator: DEVON ENERGY PRODUCTION COMPANY LP

Notice of Intent

Sundry ID: 2663401

Type of Submission: Notice of Intent

Date Sundry Submitted: 03/23/2022

Date proposed operation will begin: 02/09/2022

Type of Action: Casing Time Sundry Submitted: 06:52

Procedure Description: Devon Energy Production Company, L.P. respectfully requests approval for optional intermediate casing/drilling plan of 10-3/4" intermediate casing inside of 13-1/2" intermediate hole at previously permitted set depths. Devon Energy Production Company, L.P. will circulate class C cement to surface behind the 10-3/4" casing.

Surface Disturbance

Is any additional surface disturbance proposed?: No

NOI Attachments

Procedure Description

BURTON_FLAT_26_28_FED_COM_623H_final_drill_plan_20220513102927.pdf

MB_Wellhd_10M_4S_20_10.75_8.625_20220323065150.pdf

MB_Wellhd_10M_4S_20_13.375_9.625_20220323065150.pdf

R	eceived by OCD: 5/24/2022-6:34:03 AM Well Name: BURTON FLAT 26-28 FED STATE COM	Well Location: T20S / R28E / SEC 26 / SESW /	County or Parish/State: / Page 2 of 2
	Well Number: 623H	Type of Well: OIL WELL	Allottee or Tribe Name:
	Lease Number: NMNM108513	Unit or CA Name: BURTON FLAT DEEP-EXPL	Unit or CA Number: NMNM70798X
	US Well Number: 3001549256	Well Status: Drilling Well	Operator: DEVON ENERGY PRODUCTION COMPANY LP

Conditions of Approval

Specialist Review

26_20_28_N_Sundry_ID_2663401_Burton_Flat_26_28_Fed_State_Com_623H_Eddy_NM108513_13_22c_10_26_202 1_LV_Alt_20220513111259.pdf

26_20_28_N_Sundry_ID_2663401_Burton_Flat_26_28_Fed_State_Com_623H_Eddy_NM108513_13_22c_10_26_202 1_LV_Primary_20220513111259.pdf

Burton_Flat_26_28_Fed_Com_623H_Dr_COA_Sundry_ID_2663401_20220513111259.pdf

State: OK

State:

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CHELSEY GREEN

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Compliance Professional

Street Address: 333 West Sheridan Avenue

City: Oklahoma City

Phone: (405) 228-8595

Email address: Chelsey.Green@dvn.com

Field

Representative	Name:
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Street Address: City:

Phone:

i none.

Email address:

BLM Point of Contact

BLM POC Name: CHRISTOPHER WALLS

BLM POC Phone: 5752342234

Disposition: Approved

Signature: Chris Walls

Signed on: MAY 13, 2022 10:30 AM

BLM POC Title: Petroleum Engineer

Zip:

BLM POC Email Address: cwalls@blm.gov

Disposition Date: 05/20/2022

20	sur	face csg in a	26	inch hole.		Design I	Factors			Surface		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	94.00		j 55	stc	22.21	2.97	3.73	375	13	6.25	5.60	35,250
"B"			,	stc				0	- i -			0
_	w/8.4#/	g mud, 30min Sfc Csg Test psi	g. 1 313	Tail Cmt	does not	circ to sfc.	Totals:	375				35,250
omnarison o		nimum Required Cement					rotais.	010				00,200
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
26	1.5053	800	1152	565	104	9.00	338	2M				2.50
Proposed												
10 3/4		ng inside the	20			Design				Int 1		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	40.50		h 40	stc	7.47	2.46	0.57	1,038	4	1.08	4.11	42,039
"B"								0				0
	w/8.4#/	g mud, 30min Sfc Csg Test psi	g:				Totals:	1,038	-			42,039
				ded to achieve a top of	0	ft from su	rface or a	375				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
13 1/2	0.3637	375	906	753	20	10.50	2115	3M				0.88
	0.3037	575	900	755	20	10.50	2115	JIVI				0.00
lass 'C' tail cm		ent(s): A, B, C, D = 2.2, b, c	c, d All > 0.70, (ЭК.								
Class 'C' tail cm Burst Frac Grac 8 5/8	dient(s) for Segme casir	ng inside the	c, d All > 0.70, d 10 3/4			Design Fa				Int 2		
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment	dient(s) for Segme casir #/ft	ng inside the Grade	10 3/4	 Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	
Burst Frac Grac 8 5/8 Segment "A"	dient(s) for Segme casir	ng inside the Grade	· _ · _ · _ · _ · _ · _ ·		Joint 3.94			8,544	B@s 2		a-C 2.00	273,40
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment	dient(s) for Segme casir #/ft	ng inside the Grade	10 3/4	 Coupling		Collapse	Burst		-	a-B		
Burst Frac Grac 8 5/8 Segment "A"	dient(s) for Segme casir #/ft 32.00	ng inside the Grade	10 3/4 p 110	 Coupling		Collapse	Burst	8,544	-	a-B		273,40 0
Burst Frac Grac 8 5/8 Segment "A"	dient(s) for Segme casir #/ft 32.00	n g inside the Grade g mud, 30min Sfc Csg Test psi	10 3/4 p 110 g: 1,880	 Coupling	3.94	Collapse	Burst 1.79 Totals:	8,544 0	-	a-B	2.00	273,40 0
Burst Frac Grac 8 5/8 Segment "A"	dient(s) for Segme casir #/ft 32.00	n g inside the Grade g mud, 30min Sfc Csg Test psi	10 3/4 p 110 g: 1,880	Coupling tlw	3.94	Collapse 1.06	Burst 1.79 Totals:	8,544 0 8,544	-	a-B	2.00	273,40 0 273,40 overlap.
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B"	dient(s) for Segme casin #/ft 32.00 w/8.4#/	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo	10 3/4 p 110 g: 1,880 lume(s) are inter	Coupling tlw	3.94 838	Collapse 1.06 ft from su	Burst 1.79 Totals: rface or a	8,544 0 8,544 200	-	a-B	2.00	273,40 0 273,40 overlap. Min Dis
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B" Hole	dient(s) for Segme casir #/ft 32.00 w/8.4#/j Annular	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage	Coupling tlw nded to achieve a top of Min	3.94 838 1 Stage	Collapse 1.06 ft from su Drilling	Burst 1.79 Totals: Inface or a Calc	8,544 0 8,544 200 Req'd	-	a-B	2.00	273,40 0 273,40 overlap. Min Dis
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B" Hole Size	dient(s) for Segme casin #/ft 32.00 w/8.4#// Annular Volume 0.1261	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735	Coupling tiw nded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt	Burst 1.79 Totals: Inface or a Calc MASP 2971	8,544 0 8,544 200 Req'd BOPE 3M	-	a-B	2.00	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8	dient(s) for Segme casin #/ft 32.00 w/8.4#// Annular Volume 0.1261 Setti	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088	Coupling tiw nded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt	Burst 1.79 Totals: rface or a Calc MASP 2971 sum of sx	8,544 0 8,544 200 Req'd BOPE 3M Σ CuFt	-	a-B	2.00	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 Σ%exces
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8	dient(s) for Segme casin #/ft 32.00 w/8.4#// Annular Volume 0.1261 Setti s cmt by stage:	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735	Coupling tiw nded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt	Burst 1.79 Totals: Inface or a Calc MASP 2971	8,544 0 8,544 200 Req'd BOPE 3M	-	a-B	2.00	273,40 0 273,40 overlap. Min Dis Hole-Cpl 0.44
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces	dient(s) for Segme casin #/ft 32.00 w/8.4#// Annular Volume 0.1261 Setti s cmt by stage:	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088	Coupling tiw nded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt	Burst 1.79 Totals: rface or a Calc MASP 2971 sum of sx	8,544 0 8,544 200 Req'd BOPE 3M Σ CuFt	-	a-B	2.00	0 273,408 overlap. Min Dist Hole-Cpl 0.44 Σ%exces
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm	dient(s) for Segme casin #/ft 32.00 w/8.4#/r Annular Volume 0.1261 0.1261 s cmt by stage: it yld > 1.35	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088	Coupling tiw nded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt	Burst 1.79 Totals: rface or a Calc MASP 2971 <u>sum of sx</u> 1135	8,544 0 8,544 200 Req'd BOPE 3M Σ CuFt	-	a-B	2.00	273,400 0 273,400 overlap. Min Dis Hole-Cpl 0.44 Σ%exces
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt	dient(s) for Segme casin #/ft 32.00 w/8.4#/r Annular Volume 0.1261 0.1261 s cmt by stage: it yld > 1.35	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854	Coupling tiw nded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt 9.00	Burst 1.79 Totals: rface or a Calc MASP 2971 <u>sum of sx</u> 1135	8,544 0 8,544 200 Req'd BOPE 3M Σ CuFt	-	a-B 3.01	2.00	273,400 0 273,400 overlap. Min Dis Hole-Cpl 0.44 Σ%exces
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 1/2 Segment	dient(s) for Segme casir #/ft 32.00 w/8.4#/j Annular Volume 0.1261 Setti s cmt by stage: it yld > 1.35 casir #/ft	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 g inside the Grade	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CLFt Cmt 1735): 1088 1854 8 5/8	Coupling tiw nded to achieve a top of Min Cu Ft 976 Coupling	3.94 838 1 Stage % Excess 78 Body	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse	Burst 1.79 Totals: Inface or a Calc MASP 2971 <u>sum of sx</u> 1135 Factors Burst	8,544 0 8,544 200 Req'd BOPE 3M ∑ CuFt 2425	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 Σ%exces 149 Weigh
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 agment "A"	dient(s) for Segme casin #/ft 32.00 w/8.4#/f Annular Volume 0.1261 Setti s cmt by stage: it yld > 1.35 Casin	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 g inside the Grade	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854	Coupling tiw nded to achieve a top of Min Cu Ft 976	3.94 838 1 Stage % Excess 78	Collapse 1.06 ft from su Drilling Mud Wt 9.00 Design 1	Burst 1.79 Totals: rface or a Calc MASP 2971 <u>sum of sx</u> 1135 Factors	8,544 0 8,544 200 Req'd BOPE 3M Σ CuFt 2425	2	a-B 3.01	2.00	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 Σ%exces 149 Weigh 377,09
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 1/2 Segment	dient(s) for Segme casin #/ft 32.00 w/8.4#// Annular Volume 0.1261 Setti s cmt by stage: it yld > 1.35 casin #/ft 17.00	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 ng inside the Grade	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854 8 5/8 p 110	Coupling tiw nded to achieve a top of Min Cu Ft 976 Coupling	3.94 838 1 Stage % Excess 78 Body	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse	Burst 1.79 Totals: rface or a Calc MASP 2971 sum of sx 1135 Factors Burst 2.14	8,544 0 8,544 200 Reqd BOPE 3M ∑ <u>CuFt</u> 2425	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 <u>Σ%exces</u> 149 Weigh 377,09 0
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 agment "A"	dient(s) for Segme casin #/ft 32.00 w/8.4#// Annular Volume 0.1261 Setti s cmt by stage: it yld > 1.35 casin #/ft 17.00	ig inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 g inside the Grade g mud, 30min Sfc Csg Test psi	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854 8 5/8 p 110 g: 2,008	Coupling tlw ded to achieve a top of Min Cu Ft 976 Coupling btc	3.94 838 1 Stage % Excess 78 Body 3.52	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 1.5	Burst 1.79 Totals: rface or a Calc MASP 2971 <u>sum of sx</u> 1135 Factors Burst 2.14 Totals:	8,544 0 8,544 200 Req'd BOPE 3M ΣCuFt 2425 Length 22,182 0 22,182	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C 2.52	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 Σ%exces 149 Weigh 377,09 0 377,09
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 1/2 Segment "A" "B"	dient(s) for Segme casir #/ft 32.00 w/8.4#/r Annular Volume 0.1261 0.1261 s cnt by stage: it yld > 1.35 casir #/ft 17.00 w/8.4#/r	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854 8 5/8 p 110 g: 2,008 lume(s) are inter	Coupling tlw nded to achieve a top of Min Cu Ft 976 Coupling btc	3.94 838 1 Stage % Excess 78 Body 3.52 8344	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 1.5 ft from su	Burst 1.79 Totals: rface or a Calc MASP 2971 sum of sx 1135 Factors Burst 2.14 Totals: rface or a	8,544 0 8,544 200 Req'd BOPE 3M ∑ CuFt 2425 2425	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C 2.52	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 <u>2%exces</u> 149 Weigh 377,09 0 377,09 overlap.
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 1/2 Segment "A" "B" Hole	dient(s) for Segme casin #/ft 32.00 w/8.4#/f Annular Volume 0.1261 0.1261 Setti s cmt by stage: it yld > 1.35 casin #/ft 17.00 w/8.4#/f Annular	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854 8 5/8 p 110 g: 2,008 lume(s) are inter 1 Stage	Coupling tiw nded to achieve a top of Min Cu Ft 976 Coupling btc	3.94 838 1 Stage % Excess 78 Body 3.52 8344 1 Stage	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 1.5 ft from su Drilling	Burst 1.79 Totals: rface or a Calc MASP 2971 <u>sum of sx</u> 1135 Factors Burst 2.14 Totals: rface or a Calc	8,544 0 8,544 200 Req'd BOPE 3M ∑ CuFt 2425 2425 2425 0 22,182 200 Req'd	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C 2.52	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 <u>2%exces</u> 149 Weigh 377,09 0 377,09 overlap. Min Dis
Class 'C' tail cm Burst Frac Grad 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces Class 'C' tail cm Tail cmt 5 1/2 Segment "A" "B" Hole Size	dient(s) for Segme casin #/ft 32.00 w/8.4#/r Annular Volume 0.1261 Setti s cmt by stage: it yld > 1.35 casin #/ft 17.00 w/8.4#/r Annular Volume	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 g inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CLFt Cmt 1735): 1088 1854 8 5/8 p 110 g: 2,008 lume(s) are inter 1 Stage CLFt Cmt	Coupling tlw ded to achieve a top of Min Cu Ft 976 Coupling btc ded to achieve a top of Min Cu Ft	3.94 838 1 Stage % Excess 78 Body 3.52 8344 1 Stage % Excess	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 1.5 ft from su Drilling Mud Wt	Burst 1.79 Totals: rface or a Calc MASP 2971 sum of sx 1135 Factors Burst 2.14 Totals: rface or a	8,544 0 8,544 200 Req'd BOPE 3M ∑ CuFt 2425 2425	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C 2.52	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 Σ%exces 149 Weigh 377,09 0 377,09 0 377,09 0 377,09 0
Class 'C' tail cm Burst Frac Grac 8 5/8 Segment "A" "B" Hole Size 9 7/8 % exces class 'C' tail cm Tail cmt 5 1/2 Segment "A" "B" Hole	dient(s) for Segme casin #/ft 32.00 w/8.4#/f Annular Volume 0.1261 0.1261 Setti s cmt by stage: it yld > 1.35 casin #/ft 17.00 w/8.4#/f Annular	ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage Cmt Sx 760 ing Depths for D V Tool(s 84 ng inside the Grade g mud, 30min Sfc Csg Test psi The cement vo 1 Stage	10 3/4 p 110 g: 1,880 lume(s) are inter 1 Stage CuFt Cmt 1735): 1088 1854 8 5/8 p 110 g: 2,008 lume(s) are inter 1 Stage	Coupling tiw nded to achieve a top of Min Cu Ft 976 Coupling btc	3.94 838 1 Stage % Excess 78 Body 3.52 8344 1 Stage	Collapse 1.06 ft from su Drilling Mud Wt 9.00 <u>Design I</u> Collapse 1.5 ft from su Drilling	Burst 1.79 Totals: rface or a Calc MASP 2971 <u>sum of sx</u> 1135 Factors Burst 2.14 Totals: rface or a Calc	8,544 0 8,544 200 Req'd BOPE 3M ∑ CuFt 2425 2425 2425 0 22,182 200 Req'd	2 B@s	a-B 3.01 Prod 1 a-B	2.00 a-C 2.52	273,40 0 273,40 overlap. Min Dis Hole-Cp 0.44 <u>2%exces</u> 149 Weigh 377,09 0 377,09 overlap. Min Dis

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Burton Flat 26-28 Fed State Com 623H

20	Suria			inch hole. Design Factors						sign Factors			Surface		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh			
"A"	94.00		i 55	stc	22.21	2.97	3.73	375	13	6.25	5.60	35,250			
"B"			,	stc				0				0			
	w/8.4#/g	mud, 30min Sfc Csg Test	t psig: 1.313	Tail Cmt	does not	circ to sfc.	Totals:	375				35,25			
omnarison o		imum Required Cem					rotaioi	0.0				,			
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis			
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp			
26	1.5053	800	1152	565	104	9.00	338	2M				2.50			
20	1.5055	000	1152	505	104	9.00	330	2141				2.50			
Proposed						·—·—·			-						
13 3/8		g inside the	20			Design I				Int 1					
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh			
"A"	48.00		h 40	stc	6.46	1.36	1.24	1,038	3	2.34	2.28	49,824			
"B"								0				0			
	w/8.4#/g	mud, 30min Sfc Csg Test	t psig:				Totals:	1,038				49,824			
		The cement	volume(s) are inter	ded to achieve a top of	0	ft from su	rface or a	375				overlap.			
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis			
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp			
							700					1.56			
17 1/2	0.6946	802	1433	843	70	10.50	739	2M							
17 1/2	0.6946 nt yld > 1.35	802	1433 13 3/8	843	70			2M		Int 2					
17 1/2 Class 'C' tail cm 9 5/8	0.6946 nt yld > 1.35			843	70	10.50 Design Fac			B@s	Int 2 a-B	a-C				
17 1/2 Class 'C' tail cm 9 5/8	0.6946 ht yld > 1.35 casing	g inside the				Design Fac	<u>ctors</u>	Length	B@s 3		a-C 3.48	Weigh			
17 1/2 Class 'C' tail cm 9 5/8 Segment	0.6946 ht yld > 1.35 casing #/ft	g inside the	13 3/8	Coupling	Body	<u>Design Fac</u> Collapse	<u>ctors</u> Burst	Length 2,987	<u> </u>	a-B		Weigh 119,48			
17 1/2 Class 'C' tail cm 9 5/8 Segment "A"	0.6946 ht yld > 1.35 casing #/ft 40.00	g inside the Grade	13 3/8 j 55	Coupling	Body	<u>Design Fac</u> Collapse	ctors Burst 0.79	Length 2,987 0	<u> </u>	a-B		Weigh 119,48 0			
17 1/2 Class 'C' tail cm 9 5/8 Segment "A"	0.6946 ht yld > 1.35 casing #/ft 40.00	g inside the Grade mud, 30min Sfc Csg Test	13 3/8 j 55 t psig: 1,462	Coupling btc	Body 5.27	Design Fac Collapse 1.84	ctors Burst 0.79 Totals:	Length 2,987 0 2,987	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B"	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g	3 inside the Grade mud, 30min Sfc Csg Test The cement	13 3/8 j 55 t psig: 1,462 volume(s) are inter	Coupling btc	Body 5.27 838	Design Fac Collapse 1.84	Ctors Burst 0.79 Totals: rface or a	Length 2,987 0 2,987 200	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap.			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage	Coupling btc Ided to achieve a top of Min	Body 5.27 838 1 Stage	Design Far Collapse 1.84 ft from su Drilling	Ctors Burst 0.79 Totals: rface or a Calc	Length 2,987 0 2,987 200 Req'd	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap. Min Dis			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt	Coupling btc Ided to achieve a top of Min Cu Ft	Body 5.27 838 1 Stage % Excess	Design Far Collapse 1.84 ft from su Drilling Mud Wt	Ctors Burst 0.79 Totals: rface or a Calc MASP	Length 2,987 0 2,987 200 Req'd BOPE	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage	Coupling btc Ided to achieve a top of Min	Body 5.27 838 1 Stage	Design Far Collapse 1.84 ft from su Drilling	Ctors Burst 0.79 Totals: rface or a Calc	Length 2,987 0 2,987 200 Req'd	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap. Min Dis			
17 1/2 class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 class 'C' tail or	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985	Coupling btc Ided to achieve a top of Min Cu Ft	Body 5.27 838 1 Stage % Excess	Design Far Collapse 1.84 ft from su Drilling Mud Wt	Ctors Burst 0.79 Totals: rface or a Calc MASP	Length 2,987 0 2,987 200 Req'd BOPE	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail or	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985	Coupling btc Ided to achieve a top of Min Cu Ft	Body 5.27 838 1 Stage % Excess	Design Far Collapse 1.84 ft from su Drilling Mud Wt	Ctors Burst 0.79 Totals: rface or a Calc MASP	Length 2,987 0 2,987 200 Req'd BOPE	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail or	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985	Coupling btc Ided to achieve a top of Min Cu Ft	Body 5.27 838 1 Stage % Excess	Design Far Collapse 1.84 ft from su Drilling Mud Wt	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971	Length 2,987 0 2,987 200 Req'd BOPE	<u> </u>	a-B	3.48	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail or Barst Frac Grav 5 1/2	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 nt(s): A, B, C, D = 1.32	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70,	Coupling btc Ided to achieve a top of Min Cu Ft 686	Body 5.27 838 1 Stage % Excess	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971	Length 2,987 0 2,987 200 Req'd BOPE 3M	3	a-B 1.33	3.48	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail or Burst Frac Grad 5 1/2 Segment	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer casing #/ft	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 mt(s): A, B, C, D = 1.32 g inside the	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8	Coupling btc Ided to achieve a top of Min Cu Ft 686 Coupling	Body 5.27 838 1 Stage % Excess 44 Body	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst	Length 2,987 0 2,987 200 Req'd BOPE 3M	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh			
17 1/2 Class 'C' tail on 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail on Surst Frac Grav 5 1/2 Segment "A"	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 mt(s): A, B, C, D = 1.32 g inside the	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70,	Coupling btc Ided to achieve a top of Min Cu Ft 686	Body 5.27 838 1 Stage % Excess 44	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Sactors	Length 2,987 0 2,987 200 Req'd BOPE 3M	3	a-B 1.33 Prod 1	3.48 a-C	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh 377,09			
17 1/2 class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 class 'C' tail or burst Frac Grav 5 1/2 Segment	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer casing #/ft 17.00	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 at(s): A, B, C, D = 1.32 g inside the Grade	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8 p 110	Coupling btc Ided to achieve a top of Min Cu Ft 686 Coupling	Body 5.27 838 1 Stage % Excess 44 Body	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst 2.14	Length 2,987 0 2,987 200 Req'd BOPE 3M	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh 377,09 0			
17 1/2 Class 'C' tail on 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail on Surst Frac Grav 5 1/2 Segment "A"	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer casing #/ft 17.00	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 tt(s): A, B, C, D = 1.32 g inside the Grade mud, 30min Sfc Csg Test	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8 p 110 t psig: 2,008	Coupling btc Ided to achieve a top of Min Cu Ft 686 Coupling btc	Body 5.27 838 1 Stage % Excess 44 Body 3.52	Design Fax Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse 1.5	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst 2.14 Totals:	Length 2,987 0 2,987 200 Req'd BOPE 3M 2,182 0 22,182	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C 2.52	Weigh 119,48 0 119,48 0 verlap. Min Dis Hole-Cp 0.81 Weigh 377,09 0 377,09			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail or Size 12 1/4 Class 'C' tail or Surst Frac Grav 5 1/2 Segment "A" "B"	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmer casing #/ft 17.00 w/8.4#/g	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 nt(s): A, B, C, D = 1.32 g inside the Grade mud, 30min Sfc Csg Test The cement	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8 p 110 t psig: 2,008 volume(s) are inter	Coupling btc ded to achieve a top of Min Cu Ft 686 Coupling btc	Body 5.27 838 1 Stage % Excess 44 Body 3.52 2787	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse 1.5 ft from su	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst 2.14 Totals: rface or a	Length 2,987 0 2,987 200 Req'd BOPE 3M 2,182 0 22,182 0 22,182 200	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C 2.52	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh 377,09 0 377,09 overlap.			
17 1/2 Class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 Class 'C' tail or Surst Frac Grad 5 1/2 Segment "A" "B" Hole	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 ht yld > 1.35 dient(s) for Segmen casing #/ft 17.00 w/8.4#/g Annular	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 ht(s): A, B, C, D = 1.32 g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8 p 110 t psig: 2,008 volume(s) are inter 1 Stage	Coupling btc ded to achieve a top of Min Cu Ft 686 Coupling btc	Body 5.27 838 1 Stage % Excess 44 Body 3.52 2787 1 Stage	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse 1.5 ft from su Drilling	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst 2.14 Totals: rface or a Calc	Length 2,987 0 2,987 200 Req'd BOPE 3M Length 22,182 0 22,182 200 Req'd	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C 2.52	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh 377,09 0 377,09 overlap. Min Dis			
17 1/2 class 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 class 'C' tail or Surst Frac Grav 5 1/2 Segment "A" "B" Hole Size	0.6946 ht yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 dient(s) for Segmen casing #/ft 17.00 w/8.4#/g Annular Volume	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 at(s): A, B, C, D = 1.32 g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8 p 110 t psig: 2,008 volume(s) are inter 1 Stage CuFt Cmt	Coupling btc ded to achieve a top of Min Cu Ft 686 Coupling btc ded to achieve a top of Min Cu Ft	Body 5.27 838 1 Stage % Excess 44 Body 3.52 2787 1 Stage % Excess	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse 1.5 ft from su Drilling Mud Wt	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst 2.14 Totals: rface or a	Length 2,987 0 2,987 200 Req'd BOPE 3M 2,182 0 22,182 0 22,182 200	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C 2.52	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh 377,09 0 377,09 0 377,09 0 377,09 0 377,09			
17 1/2 lass 'C' tail or 9 5/8 Segment "A" "B" Hole Size 12 1/4 lass 'C' tail or urst Frac Grad 5 1/2 Segment "A" "B" Hole	0.6946 nt yld > 1.35 casing #/ft 40.00 w/8.4#/g Annular Volume 0.3132 nt yld > 1.35 dient(s) for Segmer casing #/ft 17.00 w/8.4#/g Annular Volume 0.2526	g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 491 ht(s): A, B, C, D = 1.32 g inside the Grade mud, 30min Sfc Csg Test The cement 1 Stage	13 3/8 j 55 t psig: 1,462 volume(s) are inter 1 Stage CuFt Cmt 985 t, b, c, d All > 0.70, 9 5/8 p 110 t psig: 2,008 volume(s) are inter 1 Stage	Coupling btc ded to achieve a top of Min Cu Ft 686 Coupling btc ded to achieve a top of Min Cu Ft 4901	Body 5.27 838 1 Stage % Excess 44 Body 3.52 2787 1 Stage	Design Fac Collapse 1.84 ft from su Drilling Mud Wt 9.00 Design I Collapse 1.5 ft from su Drilling	Ctors Burst 0.79 Totals: rface or a Calc MASP 2971 Factors Burst 2.14 Totals: rface or a Calc	Length 2,987 0 2,987 200 Req'd BOPE 3M Length 22,182 0 22,182 200 Req'd	3 B@s	a-B 1.33 Prod 1 a-B	3.48 a-C 2.52	Weigh 119,48 0 119,48 overlap. Min Dis Hole-Cp 0.81 Weigh 377,09 0 377,09 0 verlap. Min Dis			

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1. Geologic Formations

TVD of target	9128	Pilot hole depth	N/A
MD at TD:	22182	Deepest expected fresh water	

Basin

	Donth	Water/Mineral	
	Depth		
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	85		
Salt	241		
Base of Salt	500		
Lamar	616		
Capitan Reef Top	1088		
Delaware	3012		
Cherry Canyon	3202		
Brushy Canyon	3849		
1st Bone Spring Lime	5399		
Bone Spring 1st	6583		
Bone Spring 2nd	7263		
3rd Bone Spring Lime	7615		
Bone Spring 3rd	8544		
Wolfcamp	8949		

*H2S, water flows, loss of circulation, abnormal pressures, etc.

Hole Size	Csg. Size	Wt (PPF)	Grade	Conn	Top (MD)	Bottom (MD)	Top (TVD)	Bottom (TVD)
26	20	94.0	J-55	STC	0.0	375 MD	0	375 TVD
13 1/2	10 3/4	40.5	H40	STC	0.0	1038 MD	0	1038 TVD
9 7/8	8 5/8	8.6	P110	TLW	0	8544 MD	0	8544 TVD
7 7/8	5 1/2	17.0	P110	BTC	0	22182 MD	0	9128 TVD

2. Casing Program (Primary Design)

• All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

• The Rustler top will be validated via drilling parameters (i.e. reduction in ROP), and the surface casing setting depth will be revised accordingly. In addition, surface casing will be set a minimum of 25' above the top of the salt.

Hole Size	Csg. Size	Wt (PPF)	Grade	Conn	Top (MD)	Bottom (MD)	Top (TVD)	Bottom (TVD)
26	20	94.0	J-55	STC	0.0	375 MD	0	375 TVD
17 1/2	13 3/8	48.0	H40	STC	0.0	1038 MD	0	1038 TVD
12 1/4	9 5/8	40	J-55	BTC	0	2987 MD	0	2987 TVD
8 3/4	5 1/2	17.0	P110	BTC	0	22182 MD	0	9128 TVD

2. Casing Program (Contingency Design)

• This contingency design will be used IF full returns thru the Delaware are experienced on the initial well on the pad

Casing	# Sks	тос	Wt. (lb/gal)	Yld (ft3/sack)	Slurry Description
Surface	800	Surf	13.2	1.44	Lead: Class C Cement + additives
Int	200	Surf	9	3.27	Lead: Class C Cement + additives
Int	175	500' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1	350	Surf	9	3.27	Lead: Class C Cement + additives
Int I	410	5000'	13.2	1.44	Tail: Class H / C + additives
Int 1	200	Surf	9	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	350	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	410	5000'	13.2	1.44	Tail: Class H / C + additives
Production	117	6639	9	3.27	Lead: Class H /C + additives
Production	1792	8639	13.2	1.44	Tail: Class H / C + additives

3. Cementing Program (Primary Design)

Casing	# Sks	ТОС	Wt. (lb/gal)	Yld (ft3/sack)	Slurry Description
Surface	800	Surf	13.2	1.44	Lead: Class C Cement + additives
Test	152	Surf	9	3.27	Lead: Class C Cement + additives
Int	650	500' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1	242	Surf	9	3.27	Lead: Class C Cement + additives
Int I	154	2000' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1	235	Surf	9	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	152	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	339	2000' above shoe	13.2	1.44	Tail: Class H / C + additives
Production	669	50' above	9	3.27	Lead: Class H /C + additives
Froduction	2611	Capitan 8639	13.2	1.44	Tail: Class H / C + additives

3. Cementing Program (Contingency Design)

Casing String	% Excess
Surface	50%
Intermediate and Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

3. Cementing Program (Primary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the 8-5/8'' intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Capitan Reef (1088') and the second stage performed as a bradenhead squeeze with planned cement from the Capitan Reef to surface. If necessary, a top out consisting of 175 sacks of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

BOP installed and tested before drilling which hole?	Size?	Min. Require d WP	Ţ	уре	✓	Tested to:												
			An	nular		N/A												
Int			Bline	d Ram														
IIIt			Pipe Ram			500psi												
			Doub	le Ram		500psi												
			Other*	Diverter	Х													
			Annul	ar (5M)	Х	100% of rated working pressure												
Int 1	13-5/8"	5M	Bline	d Ram	Х													
Int 1			Pipe Ram			5M												
																	Double	le Ram
			Other*															
			Annular (5M)		Х	100% of rated working pressure												
Production	13-5/8"	5M	Bline	d Ram	Х													
			Pipe Ram			5M												
			Doub	le Ram	Х	5111												
			Other*															

4. Pressure Control Equipment (Four String Design)

By definition, the diverter will only be used to divert flow from the well and not to shut in the well. Prior to drilling out, the diverter will be tested to 250 PSI to ensure functionality.

5. Mud Program (Four String Design)

Section	Туре	Weight (ppg)
Surface	WBM	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Intermediate 1	WBM	8.5-9
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, C	Coring and Testing
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the
Х	Completion Rpeort and sbumitted to the BLM.
	No logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain.
	Coring? If yes, explain.

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	4984
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren S	Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations
greater than	100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is
encountered	measured values and formations will be provided to the BLM.
Ν	H2S is present
Y	H2S plan attached.

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

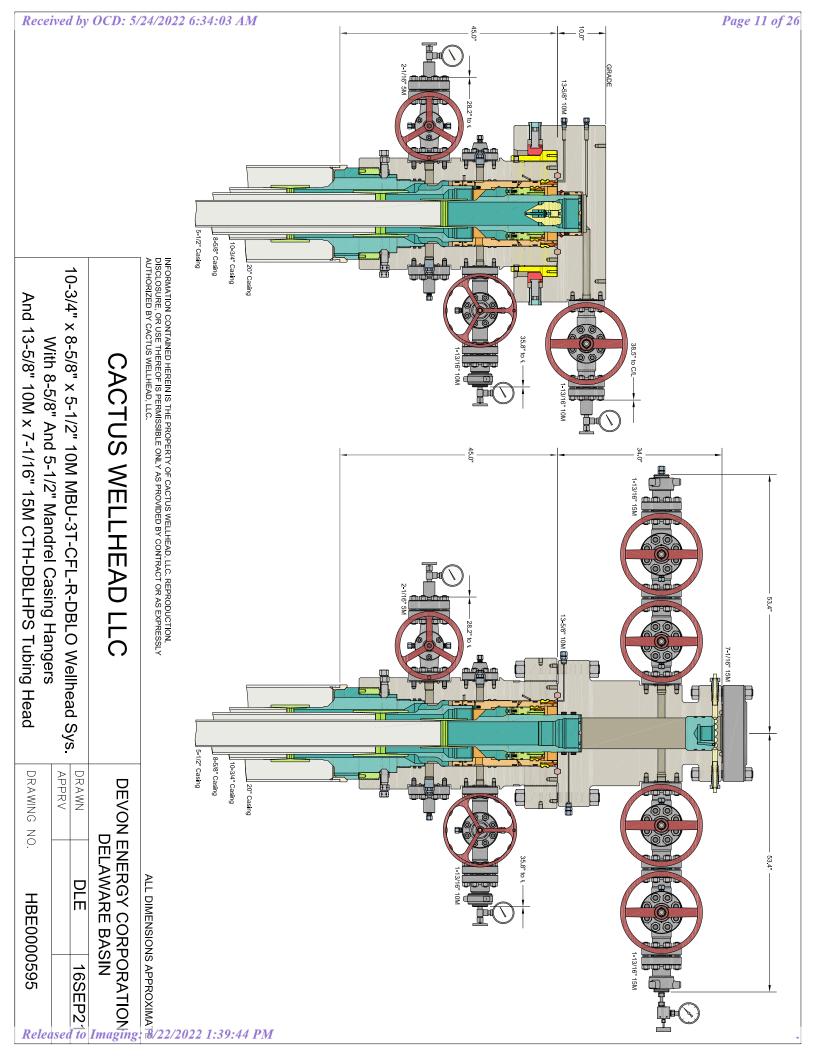
- 1 Spudder rig will move in and batch drill surface hole.
 - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).

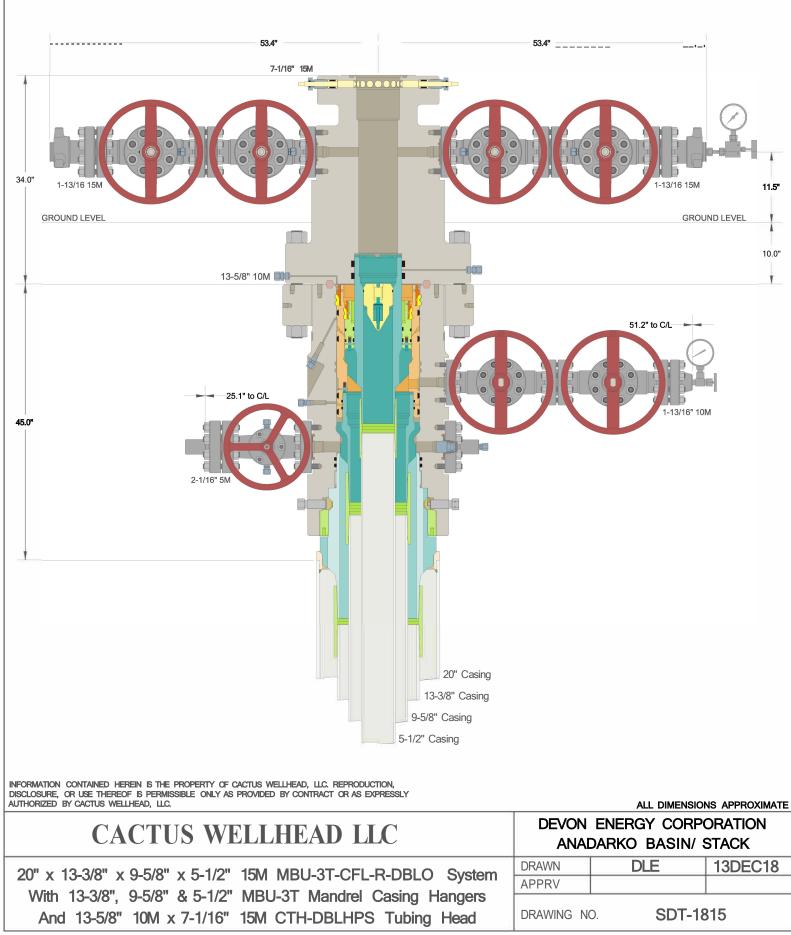
 3 The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan Other, describe





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PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	Devon Energy Production Company LP
LEASE NO.:	NMNM108513
LOCATION:	Section 26, T.20 S., R.28 E., NMPM
COUNTY:	Eddy County, New Mexico
Sundry ID:	2663401

WELL NAME & NO.:	Burton Flat 26-28 Fed State Com 623H
SURFACE HOLE FOOTAGE:	866'/S & 2438'/W
BOTTOM HOLE FOOTAGE	1870'/S & 20'/W

COA

H2S	🖸 Yes	C No	
Potash	🖸 None	C Secretary	C R-111-P
Cave/Karst Potential	🖸 Low	C Medium	🖸 High
Cave/Karst Potential	Critical		
Variance	🖸 None	🖸 Flex Hose	C Other
Wellhead	Conventional	C Multibowl	🖸 Both
Wellhead Variance	Diverter		
Other	✓ 4 String	🗹 Capitan Reef	□ WIPP
Other	Fluid Filled	🗖 Pilot Hole	Open Annulus
Cementing	Cement Squeeze	EchoMeter	
Special Requirements	□ Water Disposal	COM	🗖 Unit
Special Requirements	Break Testing	🗆 Offline	
Variance		Cementing	

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware and Wolfcamp** formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING

Primary Casing Design:

1. The 20 inch surface casing shall be set at approximately 375 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface.

- a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **10-3/4** inch intermediate casing shall be set at approximately **1038 feet** is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

3. The minimum required fill of cement behind the 8-5/8 inch intermediate casing is:

Option 1 (Single Stage):

Cement should tie-back at least 50 feet on top of Capitan Reef top or 200 feet into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.

Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the Capitan Reef.
- b. Second stage:

 Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified.
 Wait on coment (WOC) time for a primery coment job is to include

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.

- In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

Operator has proposed to pump down 10-3/4" X 8-5/8" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 8-5/8" casing to surface after the second stage BH to verify TOC.</u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 4. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Alternate Casing Design:

- 1. The 20 inch surface casing shall be set at approximately 375 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of $\underline{\mathbf{8}}$ <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)

- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **13-3/8** inch intermediate casing shall be set at approximately **1038 feet** is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.
- 3. The minimum required fill of cement behind the **9-5/8** inch intermediate casing shall be set at approximately **2987 feet** is:
 - Cement should tie-back at least 50 feet on top of Capitan Reef top or 200 feet into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef. Cement excess is less than 25%, more cement might be required.
 - In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
 - In <u>Capitan Reef Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

Operator has proposed to pump down 13-3/8" X 9-5/8" annulus after primary cementing stage. <u>Operator must run a CBL from TD of the 9-5/8" casing to surface.</u> <u>Submit results to the BLM.</u>

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

- 4. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
 Cement excess is less than 25%, more cement might be required.

C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

Primary Design:

Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be tested to 500 psi. A Diverter system is approved as a variance to drill the 10-3/4 inch intermediate casing in a 13-1/2 inch hole.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **10-3/4** inch intermediate casing shoe shall be **3000 (3M)** psi.
- c. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **8-5/8** inch intermediate casing shoe shall be **5000 (5M)** psi.

Option 2:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be tested to 500 psi. A Diverter system is approved as a variance to drill the 10-3/4 inch intermediate casing in a 13-1/2 inch hole.
- b. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 10-3/4 inch intermediate casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the intermediate casing shoe shall be 5000 (5M) psi.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.

- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

Alternate Design:

Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be tested to 500 psi. A Diverter system is approved as a variance to drill the 13-3/8 inch intermediate casing in a 17-1/2 inch hole.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **13-3/8** inch intermediate casing shoe shall be **2000 (2M)** psi.
- c. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **9-5/8** inch intermediate casing shoe shall be **5000 (5M)** psi.

Option 2:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be tested to **500** psi. A Diverter system is approved as a variance to drill the **13-3/8** inch intermediate casing in a **17-1/2** inch hole.
- b. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 13-3/8 inch intermediate casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the intermediate casing shoe shall be 5000 (5M) psi.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

D. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be on the sign.</u>

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Eddy County Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
 - Lea County
 Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)
 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24</u> <u>hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not

hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time, except the casing pressure test can be initiated immediately after bumping the plug (only applies to single stage cement jobs).
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.
- C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

District IV 1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462 State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

COMMENTS

Operator: 0	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	109667
	Action Type:
	[C-103] NOI Change of Plans (C-103A)
CONVENTS	

COMMENTS

 Created By
 Comment
 Comment

 jagarcia
 Approved, John Garcia, Petroleum Engineer
 8/22/2022

COMMENTS

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Action 109667

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

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Phone:(505) 334-6178 Fax:(505) 334-6170 District IV

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State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	109667
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

CONDITIONS

Created By Condition Condition Date 8/22/2022 jagarcia None

Action 109667