U.S. Department of the Interior BUREAU OF LAND MANAGEMENT



| Well Name | Well Number | US Well Number | Lease Number | Case Number | Operator |
|----------------|-------------|----------------|--------------|-------------|----------|
| ARENA ROJA 28- | 702H | | NMNM138900 | NMNM138900 | DEVON |
| ARENA ROJA 28- | 802H | | NMNM138900 | NMNM138900 | DEVON |

Notice of Intent

Sundry ID: 2713247

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/31/2023 Time Sundry Submitted: 08:34

Date proposed operation will begin: 01/31/2023

Procedure Description: Engineer Review only - DRILLING CHANGE: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and cement loss plan. Please see attachments. Requested to batch drill by Long to only include attachments by pad for the drilling plan for the deepest well (TVD). Verbal given for approved design 1-24-23.

NOI Attachments

Procedure Description

Arena_Roja_28_33_Fed_Com_802H_Slim_Hole_Sundry_20230131083151.pdf

Verbal___Slim_Hole_Design_1.24.23_20230130213738_20230131082928.pdf

9.625_40__J55_20230131082648.pdf

 $7.625 in_29.7 ppf_P110 EC_SPRINT_FJ_12.9.2020_20230131082649.pdf$

5.5in_20lbf_P110EC_VAM_SPRINT_SF_20230131082625.pdf

5.500in_20.00___0.361in_Wall__VST_P110EC_DWC_C_IS_CDS_AB_20230131082625.pdf

Conditions of Approval

Specialist Review

Arena_Roja_28_33_Fed_Com_702H__802H_Sundry_ID_2713247_Batch_20230201142631.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: SHAYDA OMOUMI Signed on: JAN 31, 2023 08:33 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Compliance Associate 3 **Street Address:** 333 W SHERIDAN AVE

City: OKLAHOMA CITY State: OK

Phone: (405) 235-3611

Email address: SHAYDA.OMOUMI@DVN.COM

Field

Representative Name:

Street Address:

City: State: Zip

Phone:

Email address:

BLM Point of Contact

Signature: Long Vo

BLM POC Name: LONG VO BLM POC Title: Petroleum Engineer

BLM POC Phone: 5752345972 BLM POC Email Address: LVO@BLM.GOV

Disposition: Approved **Disposition Date:** 02/01/2023





Connection Data Sheet

OD (in.) WEIGHT (lbs./ft.) 5.500 Nominal: 20.00 WALL (in.) 0.361 GRADE VST P110EC API DRIFT (in.) 4.653 RBW% 87.5 CONNECTION DWC/C-IS

0 Nominal: 20.00 Plain End: 19.83

| PIPE | PROPERTIES | |
|-----------------------|------------|--------|
| | | |
| Outside Diameter | 5.500 | in. |
| Inside Diameter | 4.778 | in. |
| Nominal Area | 5.828 | sq.in. |
| Grade Type | API 5CT | |
| Min. Yield Strength | 125 | ksi |
| Max. Yield Strength | 140 | ksi |
| Min. Tensile Strength | 135 | ksi |
| Yield Strength | 729 | klb |
| Ultimate Strength | 787 | klb |
| Min. Internal Yield | 14,360 | psi |
| Callanas | 12.000 | |

| | CONNECTION PROPERT | IES | |
|-----|------------------------------|-----------|---------|
| in. | Connection Type | Semi-Prem | ium T&C |
| in. | Connection O.D. (nom) | 6.050 | in. |
| in. | Connection I.D. (nom) | 4.778 | in. |
| | Make-Up Loss | 4.125 | in. |
| ksi | Coupling Length | 9.250 | in. |
| ksi | Critical Cross Section | 5.828 | sq.in. |
| ksi | Tension Efficiency | 100.0% | of pipe |
| ιlb | Compression Efficiency | 100.0% | of pipe |
| ιlb | Internal Pressure Efficiency | 97.8% | of pipe |
| osi | External Pressure Efficiency | 100.0% | of pipe |
| osi | | | |

| CONNECTION PERFORMANCES | | | | |
|---|--------|----------|--|--|
| Yield Strength | 729 | klb | | |
| Parting Load | 787 | klb | | |
| Compression Rating | 729 | klb | | |
| Min. Internal Yield | 14,050 | psi | | |
| External Pressure | 12,090 | psi | | |
| Maximum Uniaxial Bend Rating | 104.2 | °/100 ft | | |
| Reference String Length w 1.4 Design Factor | 26,040 | ft | | |

| | FIELD END TORQUE VAL | UES | |
|---|-------------------------------|--------|-------|
| | | | |
|) | Min. Make-up torque | 15,800 | ft.lb |
| , | Opti. Make-up torque | 17,050 | ft.lb |
|) | Max. Make-up torque | 18,300 | ft.lb |
| i | Min. Shoulder Torque | 1,580 | ft.lb |
| i | Max. Shoulder Torque | 12,640 | ft.lb |
| t | Min. Delta Turn | - | Turns |
| t | Max. Delta Turn | 0.200 | Turns |
| _ | Maximum Operational Torque | 20,800 | ft.lb |
| | Maximum Torsional Value (MTV) | 22,880 | ft.lb |
| | | | |

Need Help? Contact: tech.support@vam-usa.com
Reference Drawing: 8087PP Rev.05 & 8087BP Rev.04

Date: 01/06/2020 Time: 10:56:21 AM

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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VAM USA 2107 CityWest Boulevard Suite 1300

Houston, TX 77042 Phone: 713-479-3200 Fax: 713-479-3234

VAM® USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support Email: <u>tech.support@vam-usa.com</u>

DWC Connection Data Sheet Notes:

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- 4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- 10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

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Issued on: 08 Jul. 2020 by Wesley Ott



Connection Data Sheet

| | I | | l | | |
|-----------|-------------|-----------|--------|------------|----------------|
| OD | Weight | Wall Th. | Grade | API Drift: | Connection |
| 5 1/2 in. | 20.00 lb/ft | 0.361 in. | P110EC | 4.653 in. | VAM® SPRINT-SF |
| | | • | - | | |

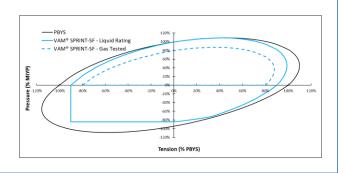
| PIPE PROPERTIES | | | | |
|--------------------------------|-------|---------|--|--|
| Nominal OD | 5.500 | in. | | |
| Nominal ID | 4.778 | in. | | |
| Nominal Cross Section Area | 5.828 | sqin. | | |
| Grade Type | Hig | h Yield | | |
| Min. Yield Strength | 125 | ksi | | |
| Max. Yield Strength | 140 | ksi | | |
| Min. Ultimate Tensile Strength | 135 | ksi | | |

| CONNECTION P | PROPERTIES | |
|------------------------------|-------------------------|------------|
| Connection Type | Semi-Premium Integral ! | Semi-Flush |
| Connection OD (nom): | 5.783 | in. |
| Connection ID (nom): | 4.717 | in. |
| Make-Up Loss | 5.965 | in. |
| Critical Cross Section | 5.244 | sqin. |
| Tension Efficiency | 90.0 | % of pipe |
| Compression Efficiency | 90.0 | % of pipe |
| Internal Pressure Efficiency | 100 | % of pipe |
| External Pressure Efficiency | 100 | % of pipe |

| CONNECTION PERFORMANCES | | | | |
|---------------------------------------|--------|---------|--|--|
| Tensile Yield Strength | 656 | klb | | |
| Compression Resistance | 656 | klb | | |
| Internal Yield Pressure | 14,360 | psi | | |
| Collapse Resistance | 12,080 | psi | | |
| Max. Structural Bending | 89 | °/100ft | | |
| Max. Bending with ISO/API Sealability | 30 | °/100ft | | |

| TORQUE VALUES | | |
|------------------------------------|--------|-------|
| Min. Make-up torque | 20,000 | ft.lb |
| Opt. Make-up torque | 22,500 | ft.lb |
| Max. Make-up torque | 25,000 | ft.lb |
| Max. Torque with Sealability (MTS) | 40,000 | ft.lb |

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.



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brazil@vamfieldservice.com

Do you need help on this product? - Remember no one knows VAM^{\circledR} like VAM^{\circledR}

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Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance



^{* 87.5%} RBW

Page 6 of 37

Issued on: 09 Dec. 2020 by Logan Van Gorp



Connection Data Sheet

| OD | Weight | Wall Th. | Grade | API Drift: | Connection |
|-----------|------------------------|-----------|--------|------------|----------------|
| 7 5/8 in. | Nominal: 29.70 lb/ft | 0.375 in. | P110EC | 6.750 in. | VAM® SPRINT-FJ |
| | Plain End: 29.06 ft/lb | | | | |

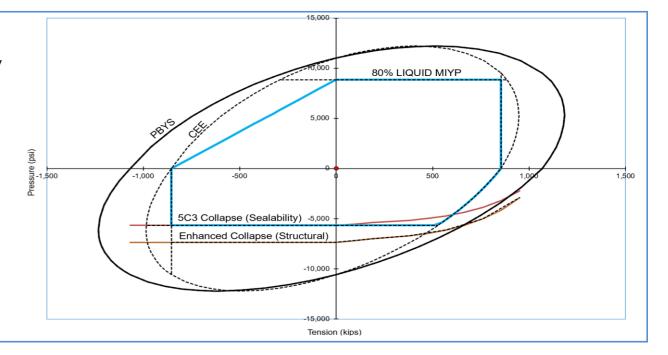
| PIPE PROPERTIES | | |
|--------------------------------|----------|----------|
| Nominal OD | 7.625 | in. |
| Nominal ID | 6.875 | in. |
| Nominal Cross Section Area | 8.541 | sqin. |
| Grade Type | Enhanced | Collapse |
| Min. Yield Strength | 125 | ksi |
| Max. Yield Strength | 140 | ksi |
| Min. Ultimate Tensile Strength | 135 | ksi |

| CONNECTION PROP | ERTIES | |
|------------------------------|------------------|-------------|
| Connection Type | Semi-Premium Int | egral Flush |
| Connection OD (nom): | 7.654 | in. |
| Connection ID (nom): | 6.827 | in. |
| Make-Up Loss | 4.055 | in. |
| Critical Cross Section | 6.979 | sqin. |
| Tension Efficiency | 80.0 | % of pipe |
| Compression Efficiency | 80.0 | % of pipe |
| Internal Pressure Efficiency | 80.0 | % of pipe |
| External Pressure Efficiency | 100 | % of pipe |

| CONNECTION PERFORMANCES | | | | | | |
|--------------------------------|-------|---------|--|--|--|--|
| Tensile Yield Strength | 854 | klb | | | | |
| Compression Resistance | 854 | klb | | | | |
| Max. Internal Pressure | 8,610 | psi | | | | |
| Structural Collapse Resistance | 7,360 | psi | | | | |
| Max. Structural Bending | 57 | °/100ft | | | | |
| Max. Bending with Sealability | 10 | °/100ft | | | | |

| TORQUE VALUES | | |
|------------------------------------|--------|-------|
| Min. Make-up torque | 15,000 | ft.lb |
| Opt. Make-up torque | 16,500 | ft.lb |
| Max. Make-up torque | 18,000 | ft.lb |
| Max. Torque with Sealability (MTS) | 32,000 | ft.lb |

VAM® SPRINT-FJ is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



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^{* 87.5%} RBW



9.625" 40# .395" J-55

Dimensions (Nominal)

BTC

| 3.023 | in. |
|--------|---|
| 0.395 | in. |
| 8.835 | in. |
| 8.750 | in. |
| 40.000 | lbs./ft. |
| 38.970 | lbs./ft. |
| | |
| 2570 | psi |
| | |
| 3950 | psi |
| 3950 | psi |
| 3950 | psi |
| 630 | 1000 lbs. |
| | |
| 452 | 1000 lbs. |
| 520 | 1000 lbs. |
| | 8.835 8.750 40.000 38.970 2570 3950 3950 3950 452 |

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

714

1000 lbs.

Arena Roja 28-33 Fed Com 802H

1. Geologic Formations

| TVD of target | 12900 | Pilot hole depth | N/A |
|---------------|-------|------------------------------|-----|
| MD at TD: | 20371 | Deepest expected fresh water | |

Basin

| Dasin | | 777 . 72.54 | |
|----------------------|---------|----------------|----------|
| | Depth | Water/Mineral | |
| Formation | (TVD) | Bearing/Target | Hazards* |
| | from KB | Zone? | |
| Rustler | 1035 | | |
| Salt | 1615 | | |
| Base of Salt | 4950 | | |
| Delaware | 5280 | | |
| Cherry Canyon | 6325 | | |
| Brushy Canyon | 7930 | | |
| 1st Bone Spring Lime | 9170 | | |
| Bone Spring 1st | 10430 | | |
| Bone Spring 2nd | 10960 | | |
| 3rd Bone Spring Lime | 11395 | | |
| Bone Spring 3rd | 12060 | | |
| Wolfcamp | 12380 | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

| | | Wt | | | Casing | Interval | Casing | Interval |
|-----------|-----------|-------|-------|-------------------------|-----------|----------|------------|----------|
| Hole Size | Csg. Size | (PPF) | Grade | Conn | From (MD) | To (MD) | From (TVD) | To (TVD) |
| 12 1/4 | 9-5/8 | 40 | J55 | ВТС | 0 | 1060 | 0 | 1060 |
| 8-3/4 | 7 5/8 | 29.7 | P110 | SPRINT FJ | 0 | 12060 | 0 | 12060 |
| 6-3/4 | 5 1/2 | 17 | P110 | SPRINT FJ & DWC/C IS | 0 | 20371 | 0 | 12900 |

- All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.
- Variance Approval
 - o 5-1/2" Production Casing will include Sprint Flush Joint connection (5.783") from base of curve and 500ft into 7-5/8" casing shoe
 - o All other 5-1/2" Production Casing will run DWC/C IS (6.05")

3. Cementing Program (Primary Design)

| Casing | # Sks | TOC | Wt. ppg | Yld (ft3/sack) | Slurry Description |
|--------------|-----------------------|----------------|--|-------------------|---|
| Surface | 345 | Surf | 13.2 1.44 Lead: Class C Cement + addit | | Lead: Class C Cement + additives |
| Int 1 | 330 | Surf | 9 | 3.27 | Lead: Class C Cement + additives |
| Int 1 | 362 | 4000' above | 13.2 1.44 Tail: Class H / C | | Tail: Class H / C + additives |
| Int 1 | 500sx or As Needed | Surf | 13.2 | 1.44 | Squeeze Lead: Class C Cement + additives |
| Intermediate | 311 | Surf | 9 | 3.27 | 2nd Stage Bradenhead - Lead: Class C Cement + additives |
| No Returns | 361 | BRUSHY 7930 | 13.2 | 1.44 | Tail: Class H / C + additives |
| Production | 58 | 10405 | 9 | 3.27 | Lead: Class H /C + additives |
| Froduction | 508 | 12405 | 13.2 | 1.44 | Tail: Class H / C + additives |

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy canyon to surface.

If necessary, a top out consisting of 500 sacks of Class C cement will be executed as a contingency.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

| Casing String | % Excess |
|----------------------------|----------|
| Surface | 50% |
| Intermediate 1 | 30% |
| Intermediate 1 (Two Stage) | 25% |
| Prod | 10% |

4. Pressure Control Equipment (Three String Design)

| BOP installed and tested before drilling which hole? | Size? | Min. Required WP | Туре | | ✓ | Tested to: |
|--|--------------|------------------------|--------------|---------------|----------------|--------------------------------|
| | | | Annular | | X | 50% of rated working pressure |
| Int 1 | 13-5/8" | 5M | Bline | l Ram | X | |
| IIIt I | 13-3/6 | JIVI | Pipe | Ram | | 5M |
| | | | Doub | le Ram | X | JIVI |
| | | | Other* | | | |
| | | | Annular (5M) | | X | 100% of rated working pressure |
| D 1 .: | 13-5/8" | Blind Ram | | X | | |
| Production | | 10M | Pipe | Ram | | 101/4 |
| | | | Doub | le Ram | X | 10M |
| | | | Other* | | | |
| | | | Annul | ar (5M) | | |
| | | | Blind | l Ram | | |
| | | | Pipe Ram | | | 1 |
| | | | Doub | le Ram | | 1 |
| | | | Other* | | | |
| N A variance is requested for | the use of a | diverter or | the surface | casing. See a | attached for s | chematic. |
| Y A variance is requested to 1 | run a 5 M aı | nnular on a | 10M system | | | |

5. Mud Program (Three String Design)

| Section | Туре | Weight (ppg) |
|--------------|-----------------|-----------------|
| Surface | FW Gel | 8.5-9 |
| Intermediate | DBE / Cut Brine | 10-10.5 |
| Production | OBM | 10-10.5 |

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

| What will be used to monitor the loss or gain of fluid? | PVT/Pason/Visual Monitoring |
|---|-----------------------------|
| E | C |

6. Logging and Testing Procedures

| <u> </u> | 6 | | | | | |
|------------|---|--|--|--|--|--|
| Logging, C | Logging, Coring and Testing | | | | | |
| | Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the | | | | | |
| X | Completion Report and sbumitted to the BLM. | | | | | |
| | No logs are planned based on well control or offset log information. | | | | | |
| | Drill stem test? If yes, explain. | | | | | |
| | Coring? If yes, explain. | | | | | |

| Additional | logs planned | Interval |
|-------------------|--------------|-------------------------|
| | Resistivity | Int. shoe to KOP |
| | Density | Int. shoe to KOP |
| X | CBL | Production casing |
| X | Mud log | Intermediate shoe to TD |
| | PEX | |

7. Drilling Conditions

| Condition | Specfiy what type and where? |
|----------------------------|------------------------------|
| BH pressure at deepest TVD | 7043 |
| Abnormal temperature | No |

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

N H2S is present
Y H2S plan attached.

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed

Arena Roja 28-33 Fed Com 802H

from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
 - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- 3 The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

| X | Directional Plan |
|---|------------------|
| | Other, describe |

Green, Chelsey

From: Moos, Sheldon

Sent: Tuesday, January 24, 2023 1:27 PM **To:** Green, Chelsey; Omoumi, Shayda

Cc: Dzurisin, Ryan; Porraz, Isac Subject: FW: Slim Hole Sundry's

Attachments: Arena Roja 28-33 Fed Com 802H Slim Hole Sundry.pdf; Cotton Draw Unit 648H Slim Hole Sundry.pdf

Follow Up Flag: Follow up Flag Status: Flagged

Chelsey and Shayda-

We need to file some batch sundries for two pads, shown below.

He has verbally approved the design, but asked that we batch sundry the deepest well on the pad. Those are attached.

We are about 1month out from spud. Please let me know if you have questions.

Sheldon Moos

C: 210-323-7512





| Well Name | Well Number | US Well Number | Lease Number | Case Number | Operator |
|----------------|-------------|----------------|--------------|-------------|----------|
| ARENA ROJA 28- | 702H | | NMNM138900 | NMNM138900 | DEVON |
| ARENA ROJA 28- | 802H | | NMNM138900 | NMNM138900 | DEVON |

Notice of Intent

Sundry ID: 2713247

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/31/2023 Time Sundry Submitted: 08:34

Date proposed operation will begin: 01/31/2023

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NOI Attachments

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Verbal___Slim_Hole_Design_1.24.23_20230130213738_20230131082928.pdf

9.625_40__J55_20230131082648.pdf

 $7.625 in_29.7 ppf_P110 EC_SPRINT_FJ_12.9.2020_20230131082649.pdf$

 $5.5 in_20 lbf_P110 EC_VAM_SPRINT_SF_20230131082625.pdf$

5.500in_20.00___0.361in_Wall__VST_P110EC_DWC_C_IS_CDS_AB_20230131082625.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: SHAYDA OMOUMI Signed on: JAN 31, 2023 08:33 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Compliance Associate 3 **Street Address:** 333 W SHERIDAN AVE

City: OKLAHOMA CITY State: OK

Phone: (405) 235-3611

Email address: SHAYDA.OMOUMI@DVN.COM

| Represent | ative Name: |
|-----------|-------------|
|-----------|-------------|

Street Address:

City: State: Zip:

Phone:

Email address:

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: Devon Energy Production Company LP

LEASE NO.: | NMNM138900

LOCATION: Section 28, T.26 S., R.35 E., NMPM

COUNTY: Lea County, New Mexico

WELL NAME & NO.: | Arena Roja 28-33 Fed Com 702H

SURFACE HOLE FOOTAGE: 250'/N & 1385'/W **BOTTOM HOLE FOOTAGE** 20'/S & 1650'/W **ATS/API ID: ATS-22-1135**

APD ID:

Sundry ID: 2713247

WELL NAME & NO.: Arena Roja 28-33 Fed Com 802H

SURFACE HOLE FOOTAGE: 250'/N & 1415'/W **BOTTOM HOLE FOOTAGE** 20'/S & 2310'/W **ATS/API ID: ATS-22-1138**

ATS/API ID: APD ID:

Sundry ID: 2713247

COA

| H2S | ☐ Yes | ○ No | |
|----------------------|------------------|---------------|------------------|
| Potash | None | ☐ Secretary | R-111-P |
| Cave/Karst Potential | O Low | ☐ Medium | ☐ High |
| Cave/Karst Potential | Critical | | |
| Variance | None | ■ Flex Hose | Other |
| Wellhead | Conventional | ☐ Multibowl | © Both |
| Wellhead Variance | ☐ Diverter | | |
| Other | □4 String | □Capitan Reef | □WIPP |
| Other | Fluid Filled | ☐ Pilot Hole | Open Annulus |
| Cementing | ☐ Contingency | ✓ EchoMeter | ☐ Primary Cement |
| | Cement Squeeze | | Squeeze |
| Special Requirements | ☐ Water Disposal | ☑ COM | ☐ Unit |
| Special Requirements | ☑ Batch Sundry | | |
| | | | |
| Special Requirements | ☑ Break Testing | ☐ Offline | ✓ Casing |
| Variance | | Cementing | Clearance |
| | | | |

A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

B. CASING

- 1. The 9-5/8 inch surface casing shall be set at approximately 1115 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

Option 1 (Single Stage):

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

a. First stage: Operator will cement with intent to reach the top of the Brushy Canyon at 7930' (361 sxs Class H/C+ additives).

b. Second stage:

 Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 311 sxs Class C)

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi. Annular which shall be tested to 5000 (5M) psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 7-5/8 inch intermediate casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

Option 2:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 9-5/8 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

D. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in Onshore Order 1 and 2.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.

- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 14-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

Batch Sundry:

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)
- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

Casing Clearance:

Operator casing variance is approved for the utilization of 5-1/2 inch P 110 Sprint SF 20# **from** base of curve and **500 feet** into the 7-5/8 inch casing shoe. **All** other 5-1/2 inch production casing will run DWC/C IS+.

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Eddy County
 Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
 - ✓ Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin

- after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

LVO 2/1/2023

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1. Geologic Formations

| TVD of target | 12900 | Pilot hole depth | N/A |
|---------------|-------|------------------------------|-----|
| MD at TD: | 20371 | Deepest expected fresh water | |

Basin

| Dasin | | 777 . 72.54 | |
|----------------------|---------|----------------|----------|
| | Depth | Water/Mineral | |
| Formation | (TVD) | Bearing/Target | Hazards* |
| | from KB | Zone? | |
| Rustler | 1035 | | |
| Salt | 1615 | | |
| Base of Salt | 4950 | | |
| Delaware | 5280 | | |
| Cherry Canyon | 6325 | | |
| Brushy Canyon | 7930 | | |
| 1st Bone Spring Lime | 9170 | | |
| Bone Spring 1st | 10430 | | |
| Bone Spring 2nd | 10960 | | |
| 3rd Bone Spring Lime | 11395 | | |
| Bone Spring 3rd | 12060 | | |
| Wolfcamp | 12380 | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

| | | Wt | | | Casing | Interval | Casing | Interval |
|-----------|-----------|-------|-------|-------------------------|-----------|----------|------------|----------|
| Hole Size | Csg. Size | (PPF) | Grade | Conn | From (MD) | To (MD) | From (TVD) | To (TVD) |
| 12 1/4 | 9-5/8 | 40 | J55 | ВТС | 0 | 1060 | 0 | 1060 |
| 8-3/4 | 7 5/8 | 29.7 | P110 | SPRINT FJ | 0 | 12060 | 0 | 12060 |
| 6-3/4 | 5 1/2 | 17 | P110 | SPRINT FJ & DWC/C IS | 0 | 20371 | 0 | 12900 |

- All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.
- Variance Approval
 - o 5-1/2" Production Casing will include Sprint Flush Joint connection (5.783") from base of curve and 500ft into 7-5/8" casing shoe
 - o All other 5-1/2" Production Casing will run DWC/C IS (6.05")

3. Cementing Program (Primary Design)

| Casing | # Sks | TOC | Wt. ppg | Yld (ft3/sack) | Slurry Description |
|--------------|-----------------------|----------------|------------|-------------------|---|
| Surface | 345 | 345 Surf | | 1.44 | Lead: Class C Cement + additives |
| Int 1 | 330 | Surf | 9 | 3.27 | Lead: Class C Cement + additives |
| Int 1 | 362 | 4000' above | 13.2 | 1.44 | Tail: Class H / C + additives |
| Int 1 | 500sx or As Needed | Surf | 13.2 | 1.44 | Squeeze Lead: Class C Cement + additives |
| Intermediate | 311 | Surf | 9 | 3.27 | 2nd Stage Bradenhead - Lead: Class C Cement + additives |
| No Returns | 361 | BRUSHY 7930 | 13.2 | 1.44 | Tail: Class H / C + additives |
| Production | 58 | 10405 | 9 | 3.27 | Lead: Class H /C + additives |
| Froduction | 508 | 12405 | 13.2 | 1.44 | Tail: Class H / C + additives |

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy canyon to surface.

If necessary, a top out consisting of 500 sacks of Class C cement will be executed as a contingency.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

| Casing String | % Excess |
|----------------------------|----------|
| Surface | 50% |
| Intermediate 1 | 30% |
| Intermediate 1 (Two Stage) | 25% |
| Prod | 10% |

4. Pressure Control Equipment (Three String Design)

| BOP installed and tested before drilling which hole? | Size? | Min. Required WP | Ty | ype | √ | Tested to: | | | | | | | |
|--|--|------------------------|--------------|-------------|----------------|--------------------------------|-----|-----|--------------|--------|--|-----|--|
| | | | Annular | | X | 50% of rated working pressure | | | | | | | |
| Int 1 | 13-5/8" | 5M | Blind Ram | | X | | | | | | | | |
| IIIL I | 13-3/6 | JIVI | Pipe | Ram | | 5M | | | | | | | |
| | | | Doub | le Ram | X | 3101 | | | | | | | |
| | | | Other* | | |] | | | | | | | |
| | 13-5/8" | | Annular (5M) | | X | 100% of rated working pressure | | | | | | | |
| Don't sellen | | 101/ | Blind Ram | | X | | | | | | | | |
| Production | | 13-5/8" | 13-5/8" | 13-5/8" 10 | 13-5/8" | 10M | 10M | 10M | 3-5/8" 10M | Pipe F | | Ram | |
| | | | | Doub | le Ram | X | 10M | | | | | | |
| | | | Other* | | | | | | | | | | |
| | | | Annul | ar (5M) | | | | | | | | | |
| | | | Blind | d Ram | | | | | | | | | |
| | | | Pipe | Ram | | 1 | | | | | | | |
| | | | Doub | le Ram | |] | | | | | | | |
| | | | Other* | | | 1 | | | | | | | |
| N A variance is requested for | the use of a | diverter or | the surface | casing. See | attached for s | schematic. | | | | | | | |
| Y A variance is requested to 1 | A variance is requested to run a 5 M annular on a 10M system | | | | | | | | | | | | |

5. Mud Program (Three String Design)

| Section | Туре | Weight (ppg) |
|--------------|-----------------|-----------------|
| Surface | FW Gel | 8.5-9 |
| Intermediate | DBE / Cut Brine | 10-10.5 |
| Production | OBM | 10-10.5 |

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

| What will be used to monitor the loss or gain of fluid? | PVT/Pason/Visual Monitoring |
|---|-----------------------------|

6. Logging and Testing Procedures

| ** — *888 *** = ******* | | | | | | |
|---|---|--|--|--|--|--|
| Logging, C | Logging, Coring and Testing | | | | | |
| | Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the | | | | | |
| X Completion Report and shumitted to the BLM. | | | | | | |
| | No logs are planned based on well control or offset log information. | | | | | |
| | Drill stem test? If yes, explain. | | | | | |
| | Coring? If yes, explain. | | | | | |

| Additional logs planned | | Interval | |
|-------------------------|-------------|-------------------------|--|
| | Resistivity | Int. shoe to KOP | |
| | Density | Int. shoe to KOP | |
| X | CBL | Production casing | |
| X | Mud log | Intermediate shoe to TD | |
| | PEX | | |

7. Drilling Conditions

| Condition | Specfiy what type and where? |
|----------------------------|------------------------------|
| BH pressure at deepest TVD | 7043 |
| Abnormal temperature | No |

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

| IN | H2S is present |
|----|--------------------|
| Y | H2S plan attached. |

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed

Arena Roja 28-33 Fed Com 802H

from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
 - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- 3 The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

| Attachments | |
|-------------|------------------|
| X | Directional Plan |
| | Other, describe |





Connection Data Sheet

OD (in.) WEIGHT (lbs./ft.) 5.500 Nominal: 20.00 WALL (in.) 0.361 GRADE VST P110EC

12,090

API DRIFT (in.) 4.653 RBW% 87.5 CONNECTION DWC/C-IS

500 | Nominal: 20.00 | Plain End: 19.83

PIPE PROPERTIES Outside Diameter 5.500 Inside Diameter 4.778 Nominal Area 5.828 sq.i Grade Type **API 5CT** Min. Yield Strength 125 Max. Yield Strength 140 Min. Tensile Strength 135 Yield Strength 729 Ultimate Strength 787 Min. Internal Yield 14,360

| | CONNECTION PROPERT | IES | |
|-----|------------------------------|------------|---------|
| in. | Connection Type | Semi-Premi | um T&C |
| in. | Connection O.D. (nom) | 6.050 | in. |
| in. | Connection I.D. (nom) | 4.778 | in. |
| | Make-Up Loss | 4.125 | in. |
| ksi | Coupling Length | 9.250 | in. |
| ksi | Critical Cross Section | 5.828 | sq.in. |
| ksi | Tension Efficiency | 100.0% | of pipe |
| ιlb | Compression Efficiency | 100.0% | of pipe |
| ιlb | Internal Pressure Efficiency | 97.8% | of pipe |
| osi | External Pressure Efficiency | 100.0% | of pipe |
| osi | | | |

| COMMISSION PERSONANCES | | | | |
|---|--------|----------|--|--|
| CONNECTION PERFORMANCES | | | | |
| | | | | |
| Yield Strength | 729 | klb | | |
| Parting Load | 787 | klb | | |
| Compression Rating | 729 | klb | | |
| Min. Internal Yield | 14,050 | psi | | |
| External Pressure | 12,090 | psi | | |
| Maximum Uniaxial Bend Rating | 104.2 | °/100 ft | | |
| Reference String Length w 1.4 Design Factor | 26,040 | ft | | |

| | FIELD END TORQUE VALUES | | | | |
|---|-------------------------------|--------|--------------|--|--|
| | | | 5. 11 | | |
|) | Min. Make-up torque | 15,800 | ft.lb | | |
|) | Opti. Make-up torque | 17,050 | ft.lb | | |
| 2 | Max. Make-up torque | 18,300 | ft.lb | | |
| i | Min. Shoulder Torque | 1,580 | ft.lb | | |
| i | Max. Shoulder Torque | 12,640 | ft.lb | | |
| t | Min. Delta Turn | - | Turns | | |
| t | Max. Delta Turn | 0.200 | Turns | | |
| | Maximum Operational Torque | 20,800 | ft.lb | | |
| | Maximum Torsional Value (MTV) | 22,880 | ft.lb | | |

Need Help? Contact: <u>tech.support@vam-usa.com</u>
Reference Drawing: 8087PP Rev.05 & 8087BP Rev.04

Date: 01/06/2020 Time: 10:56:21 AM

Collapse

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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VAM® USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support Email: <u>tech.support@vam-usa.com</u>

DWC Connection Data Sheet Notes:

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- 4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- 10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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Issued on: 09 Dec. 2020 by Logan Van Gorp



Connection Data Sheet

| OD | Weight | Wall Th. | Grade | API Drift: | Connection |
|-----------|------------------------|-----------|--------|------------|----------------|
| 7 5/8 in. | Nominal: 29.70 lb/ft | 0.375 in. | P110EC | 6.750 in. | VAM® SPRINT-FJ |
| | Plain End: 29.06 ft/lb | | | | |

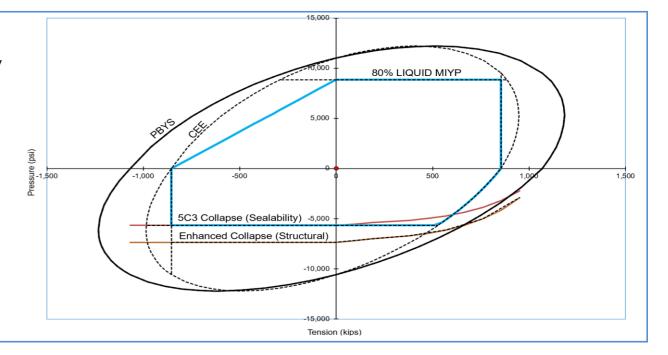
| PIPE PROPERTIES | | |
|--------------------------------|----------|----------|
| Nominal OD | 7.625 | in. |
| Nominal ID | 6.875 | in. |
| Nominal Cross Section Area | 8.541 | sqin. |
| Grade Type | Enhanced | Collapse |
| Min. Yield Strength | 125 | ksi |
| Max. Yield Strength | 140 | ksi |
| Min. Ultimate Tensile Strength | 135 | ksi |

| CONNECTION PROP | ERTIES | |
|------------------------------|------------------|-------------|
| Connection Type | Semi-Premium Int | egral Flush |
| Connection OD (nom): | 7.654 | in. |
| Connection ID (nom): | 6.827 | in. |
| Make-Up Loss | 4.055 | in. |
| Critical Cross Section | 6.979 | sqin. |
| Tension Efficiency | 80.0 | % of pipe |
| Compression Efficiency | 80.0 | % of pipe |
| Internal Pressure Efficiency | 80.0 | % of pipe |
| External Pressure Efficiency | 100 | % of pipe |

| CONNECTION PERFORMANCES | | |
|--------------------------------|-------|---------|
| Tensile Yield Strength | 854 | klb |
| Compression Resistance | 854 | klb |
| Max. Internal Pressure | 8,610 | psi |
| Structural Collapse Resistance | 7,360 | psi |
| Max. Structural Bending | 57 | °/100ft |
| Max. Bending with Sealability | 10 | °/100ft |

| TORQUE VALUES | | |
|------------------------------------|--------|-------|
| Min. Make-up torque | 15,000 | ft.lb |
| Opt. Make-up torque | 16,500 | ft.lb |
| Max. Make-up torque | 18,000 | ft.lb |
| Max. Torque with Sealability (MTS) | 32,000 | ft.lb |

VAM® SPRINT-FJ is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



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Do you need help on this product? - Remember no one knows VAM^{\circledR} like VAM^{\circledR}

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Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance



^{* 87.5%} RBW

Issued on: 08 Jul. 2020 by Wesley Ott



Connection Data Sheet

| OD | Weight | Wall Th. | Grade | API Drift: | Connection |
|-------------|--------------|-----------|--------|------------|-----------------|
| 5 1/2 in. | 20.00 lb/ft | 0.361 in. | P110EC | 4.653 in. | VAM® SPRINT-SF |
| 5 1, 1 IIII | 20.00 15, 10 | | 1 | | VAIN SI MILL SI |
| | | | | | |

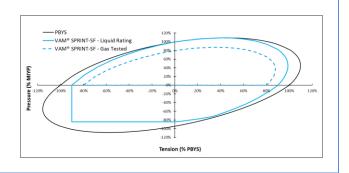
| PIPE PROPERTIES | | |
|--------------------------------|-------|---------|
| Nominal OD | 5.500 | in. |
| Nominal ID | 4.778 | in. |
| Nominal Cross Section Area | 5.828 | sqin. |
| Grade Type | Hig | h Yield |
| Min. Yield Strength | 125 | ksi |
| Max. Yield Strength | 140 | ksi |
| Min. Ultimate Tensile Strength | 135 | ksi |

| CONNECTION P | ROPERTIES | |
|------------------------------|-----------------------|------------|
| Connection Type | Semi-Premium Integral | Semi-Flush |
| Connection OD (nom): | 5.783 | in. |
| Connection ID (nom): | 4.717 | in. |
| Make-Up Loss | 5.965 | in. |
| Critical Cross Section | 5.244 | sqin. |
| Tension Efficiency | 90.0 | % of pipe |
| Compression Efficiency | 90.0 | % of pipe |
| Internal Pressure Efficiency | 100 | % of pipe |
| External Pressure Efficiency | 100 | % of pipe |

| CONNECTION PERFORMANCES | | | | | | | | |
|---------------------------------------|--------|---------|--|--|--|--|--|--|
| Tensile Yield Strength | 656 | klb | | | | | | |
| Compression Resistance | 656 | klb | | | | | | |
| Internal Yield Pressure | 14,360 | psi | | | | | | |
| Collapse Resistance | 12,080 | psi | | | | | | |
| Max. Structural Bending | 89 | °/100ft | | | | | | |
| Max. Bending with ISO/API Sealability | 30 | °/100ft | | | | | | |

| TORQUE VALUES | S | |
|------------------------------------|--------|-------|
| Min. Make-up torque | 20,000 | ft.lb |
| Opt. Make-up torque | 22,500 | ft.lb |
| Max. Make-up torque | 25,000 | ft.lb |
| Max. Torque with Sealability (MTS) | 40,000 | ft.lb |

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.



Do you need help on this product? - Remember no one knows VAM^{\circledR} like VAM^{\circledR}

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^{* 87.5%} RBW



9.625" 40# .395" J-55

Dimensions (Nominal)

BTC

| Outside Diameter | 9.625 | in. |
|--|--------|-----------|
| Wall | 0.395 | in. |
| Inside Diameter | 8.835 | in. |
| Drift | 8.750 | in. |
| Weight, T&C | 40.000 | lbs./ft. |
| Weight, PE | 38.970 | lbs./ft. |
| Performance Properties | | |
| Collapse, PE | 2570 | psi |
| Internal Yield Pressure at Minimum Yield | | |
| PE | 3950 | psi |
| LTC | 3950 | psi |
| ВТС | 3950 | psi |
| Yield Strength, Pipe Body | 630 | 1000 lbs. |
| | | |
| Joint Strength | 452 | 1000 lb- |
| STC | 452 | 1000 lbs. |
| LTC | 520 | 1000 lbs. |

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

714

1000 lbs.

Page 36 of 37 28-26-35-C Sundry ID 2713247 Arena Roja 28-33 Fed Com 802H Lea NM138900 DEVON ENERGY PRODUCTION COMPANY LP 13-22d 2-1-2023 LV.xlsm

Arena Roja 28-33 Fed Com 802H

| 9 5/8 | S | surface csg in a | 12 1/4 | inch hole. | | <u>Design l</u> | Factors | | | Surfac | e | |
|---|-----------------|---------------------------------|-------------|------------|----------|-----------------|---------|--------|-----|--------|------|-----------|
| Segment | #/ft | Grade | | Coupling | Body | Collapse | Burst | Length | B@s | a-B | a-C | Weight |
| "A" | 40.00 | | j 55 | btc | 14.12 | 4.93 | 0.6 | 1,115 | 8 | 1.01 | 9.31 | 44,600 |
| "B" | | | | btc | | | | 0 | | | | 0 |
| | w/8. | .4#/g mud, 30min Sfc Csg Test p | osig: 1,500 | Tail Cmt | does not | circ to sfc. | Totals: | 1,115 | _ | | | 44,600 |
| Comparison of Proposed to Minimum Required Cement Volumes | | | | | | | | | | | | |
| Hole | Annular | 1 Stage | 1 Stage | Min | 1 Stage | Drilling | Calc | Req'd | | | | Min Dist |
| Size | Volume | Cmt Sx | CuFt Cmt | Cu Ft | % Excess | Mud Wt | MASP | BOPE | | | | Hole-Cplg |
| 12 1/4 | 0.3132 | 426 | 613 | 349 | 76 | 9.00 | 3925 | 5M | | | | 0.81 |
| | | | | | | | | | | | | |
| Burst Frac Gra | dient(s) for Se | gment(s) A, B = , b $AII > 0$ | .70, OK. | | | | | | | | | |
| | | | | | | | | | | | | |

| 7 5/8 | cas | ing inside the | 9 5/8 | | | Design | Factors - | | - | Int 1 | | |
|-------------------|---------------|--------------------------------|--------------------|--------------------------|----------|------------|-------------|--------|-----|-------|------|-----------|
| Segment | #/ft | Grade | | Coupling | Joint | Collapse | Burst | Length | B@s | a-B | a-C | Weight |
| "A" | 29.70 | | p 110 | vam sprint fj | 2.38 | 1.12 | 1.22 | 12,060 | 1 | 2.05 | 1.88 | 358,182 |
| "B" | | | | | | | | 0 | | | | 0 |
| | w/8.4 | #/g mud, 30min Sfc Csg Test ps | sig: 764 | | | | Totals: | 12,060 | | | | 358,182 |
| İ | | The cement vo | olume(s) are inter | nded to achieve a top of | 0 | ft from su | ırface or a | 1115 | | | | overlap. |
| Hole | Annular | 1 Stage | 1 Stage | Min | 1 Stage | Drilling | Calc | Req'd | | | | Min Dist |
| Size | Volume | Cmt Sx | CuFt Cmt | Cu Ft | % Excess | Mud Wt | MASP | BOPE | | | | Hole-Cplg |
| 8 3/4 | 0.1005 | 361 | 520 | 1221 | -57 | 10.50 | 4198 | 5M | | | | 0.55 |
| D V Tool(s): | | | 7930 | | | | sum of sx | Σ CuFt | | | | Σ%excess |
| t by stage %: | | 25 | 26 | | | | 672 | 1537 | | | | 26 |
| Class 'H' tail cm | nt yld > 1.20 | | | | | | | | | | | |
| | | | | | | | | | | | | |

| 5 1/2 | casing | inside the | 7 5/8 | - | | Design Fa | ctors | | _ | Prod 1 | | |
|------------------|------------------------------|----------------------|------------------------|-------------------------|----------|------------|-------------|--------|-----|--------|------|-----------------|
| Segment | #/ft | Grade | | Coupling | Joint | Collapse | Burst | Length | B@s | a-B | a-C | Weight |
| "A" | 17.00 | | p 110 | dwc/c is+ | 2.44 | 1.19 | 1.51 | 11,560 | 2 | 2.53 | 1.99 | 196,520 |
| "B" | 20.00 | | p 110 | vam sprint sf | 2.81 | 1.60 | 2.04 | 1,340 | 2 | 3.42 | 2.88 | 26,800 |
| "C" | 17.00 | | 0 110 | dwc/c is+ | 00 | 1.06 | 1.51 | 7,471 | 2 | 2.53 | 1.78 | 127,007 |
| "D" | | | | 0 | | | | 0 | | | | 0 |
| | w/8.4#/g m | ud, 30min Sfc Csg Te | st psig: 2,543 | | | | Totals: | 20,371 | | | | 350,327 |
| | | The cemen | t volume(s) are intend | ded to achieve a top of | 11860 | ft from su | ırface or a | 200 | | | | overlap. |
| Hole | Annular | 1 Stage | 1 Stage | Min | 1 Stage | Drilling | Calc | Req'd | | | | Min Dist |
| Size | Volume | Cmt Sx | CuFt Cmt | Cu Ft | % Excess | Mud Wt | MASP | BOPE | | | | Hole-Cplg |
| 6 3/4 | 0.0835 | 1171 | 1900 | 713 | 167 | 10.50 | | | | | | 0.35 |
| | Setting | Depths for D V To | ool(s): | | | | sum of sx | Σ CuFt | | | | <u>Σ%excess</u> |
| % exces | ss cmt by stage: | #VALUE! | #VALUE! | | | | 1171 | 1900 | | | | 167 |
| lass 'C' tail cn | lass 'C' tail cmt yld > 1.35 | | | | | | | | | | | |

| #N/A | | | | | | | _ <i></i> | | - | | | |
|--|----------------|------------------------------------|-----------------|--------------|-----------------------|------------|-----------|--------|-----|-----------------------------|----------|-----------|
| 0 | 5 1/2 <u> </u> | | | | <u>Design Factors</u> | | | | | <choose casing=""></choose> | | |
| Segment | #/ft | Grade | | Coupling | #N/A | Collapse | Burst | Length | B@s | а-В | a-C | Weight |
| "A" | | | | 0.00 | | | | 0 | | | | 0 |
| "B" | | | | 0.00 | | | | 0 | | | | 0 |
| | w/8.4 | 4#/g mud, 30min Sfc Csg Test psig: | | | | | Totals: | 0 | | | | 0 |
| Cmt vol calc below includes this csg, TOC intended | | | | #N/A | ft from su | rface or a | #N/A | | | | overlap. | |
| Hole | Annular | 1 Stage | 1 Stage | Min | 1 Stage | Drilling | Calc | Reg'd | | | | Min Dist |
| Size | Volume | Cmt Sx | CuFt Cmt | Cu Ft | % Excess | Mud Wt | MASP | BOPE | | | | Hole-Cplg |
| 0 | | #N/A | #N/A | 0 | #N/A | | | | | | | |
| #N/A | | | Capitan Reef es | st top XXXX. | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |

Carlsbad Field Office 2/1/2023

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District II 811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III 1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 181802

CONDITIONS

| Operator: | OGRID: |
|-------------------------------------|--------------------------------------|
| DEVON ENERGY PRODUCTION COMPANY, LP | 6137 |
| 333 West Sheridan Ave. | Action Number: |
| Oklahoma City, OK 73102 | 181802 |
| | Action Type: |
| | [C-103] NOI Change of Plans (C-103A) |

CONDITIONS

| Created By | Condition | Condition Date |
|---------------|-----------|-------------------|
| pkautz | None | 2/2/2023 |