Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
BORA BORA 13-	713H	3001549352	NMNM0404441	NMNM0404441	DEVON
BORA BORA 13-	623H	3001549351	NMNM0404441	NMNM0404441	DEVON

## **Notice of Intent**

Sundry ID: 2717379

Type of Submission: Notice of Intent

Date Sundry Submitted: 02/23/2023

Date proposed operation will begin: 02/23/2023

Type of Action: APD Change

Time Sundry Submitted: 09:18

Sundry Print Repor

02/23/2023

**Procedure Description:** Engineer Review only - DRILLING CHANGE: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and cement loss plan. Please see attachments. Requested to batch drill by Long to only include attachments by pad for the drilling plan for the deepest well (TVD). Verbal given for approved design 2-23-23.

### **NOI Attachments**

#### **Procedure Description**

Verbal\_Slim\_Hole\_Design\_2.23.2023\_20230223091719.pdf

5.500in\_20.00\_\_\_0.361in\_Wall\_\_VST\_P110EC\_DWC\_C\_IS\_CDS\_AB\_20230223091719.pdf

BORA\_BORA\_13\_24\_FED\_COM\_713H\_Slim\_Hole\_20230223091719.pdf

5.5in\_20lbf\_P110EC\_VAM\_SPRINT\_SF\_20230223091718.pdf

7.625in\_29.7ppf\_P110EC\_SPRINT\_FJ\_12.9.2020\_20230223091719.pdf

9.625\_40\_\_J55\_20230223091719.pdf

## **Conditions of Approval**

#### Specialist Review

Bora\_Bora\_13\_24\_Fed\_Com\_623H\_\_713H\_Sundry\_ID\_2717379\_Batch\_20230223134057.pdf

## Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: SHAYDA OMOUMI Name: DEVON ENERGY PRODUCTION COMPANY LP Title: Regulatory Compliance Associate 3 Street Address: 333 W SHERIDAN AVE City: OKLAHOMA CITY State: OK Phone: (405) 235-3611 Email address: SHAYDA.OMOUMI@DVN.COM

#### Field

Representative Name: Street Address:

City:

Phone:

Email address:

State:

Zip:

## **BLM Point of Contact**

BLM POC Name: LONG VO BLM POC Phone: 5752345972 Disposition: Approved Signature: Long Vo

BLM POC Title: Petroleum Engineer BLM POC Email Address: LVO@BLM.GOV Disposition Date: 02/23/2023

Signed on: FEB 23, 2023 09:17 AM

USA			Connection		beet
OD (in.)      WEIGHT (Ibs./ft.)      WALL (in.)        5.500      Nominal: 20.00      0.361        Plain End: 19.83      19.83	-	RADE P110EC	API DRIFT (in.) RBW% 4.653 87.5	CONNECTIO DWC/C-IS	N
PIPE PROPERTIES			CONNECTION PROF	PERTIES	
Outside Diameter	5.500	in.	Connection Type	Semi-Pren	nium T&C
Inside Diameter	4.778	in.	Connection O.D. (nom)	6.050	in
Nominal Area	5.828	sq.in.	Connection I.D. (nom)	4.778	in
Grade Type	API 5CT		Make-Up Loss	4.125	in
Min. Yield Strength	125	ksi	Coupling Length	9.250	in
Max. Yield Strength	140	ksi	Critical Cross Section	5.828	sq.in
Min. Tensile Strength	135	ksi	Tension Efficiency	100.0%	of pipe
Yield Strength	729	klb	Compression Efficiency	100.0%	of pipe
Ultimate Strength	787	klb	Internal Pressure Efficiency	97.8%	of pipe
Min. Internal Yield	14,360	psi	External Pressure Efficiency	100.0%	of pipe
Collapse	12,090	psi			
CONNECTION PERFORMA	NCES		FIELD END TORQUE	VALUES	
Yield Strength	729	klb	Min. Make-up torque	15,800	ft.lb
Parting Load	787	klb	Opti. Make-up torque	17,050	ft.lk
Compression Rating	729	klb	Max. Make-up torque	18,300	ft.lk
Min. Internal Yield	14,050	psi	Min. Shoulder Torque	1,580	ft.lk
External Pressure	12,090	psi	Max. Shoulder Torque	12,640	ft.lb
Maximum Uniaxial Bend Rating	104.2	°/100 ft	Min. Delta Turn	-	Turns
Reference String Length w 1.4 Design Factor	26,040	ft	Max. Delta Turn	0.200	Turns
			Maximum Operational Torque	20,800	ft.lb
			Maximum Torsional Value (MTV)	22,880	ft.lb

Need Help? Contact: <u>tech.support@vam-usa.com</u> Reference Drawing: 8087PP Rev.05 & 8087BP Rev.04 Date: 01/06/2020 Time: 10:56:21 AM

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

All information is provided by VAM USA or its affiliates at user's sole risk, without liability for loss, damage or injury resulting from the use thereof; and on an "AS IS" basis without warranty or representation of any kind, whether express or implied, including without limitation any warranty of merchantability, fitness for purpose or completeness. This document and its contents are subject to change without notice. In no event shall VAM USA or its affiliates be responsible for any indirect, special, incidental, punitive, exemplary or consequential loss or damage (including without limitation, loss of use, loss of bargain, loss of revenue, profit or anticipated profit) however caused or arising, and whether such losses or damages.



VAM USA 2107 CityWest Boulevard Suite 1300 Houston, TX 77042 Phone: 713-479-3200 Fax: 713-479-3234 VAM<sup>®</sup> USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support Email: <u>tech.support@vam-usa.com</u>

**DWC Connection Data Sheet Notes:** 

1. DWC connections are available with a seal ring (SR) option.

2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.

Connection performance properties are based on nominal pipe body and connection dimensions.
 DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
 DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.

6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.

7. Bending efficiency is equal to the compression efficiency.

8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.

9. Connection yield torque is not to be exceeded.

10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.

11. DWC connections will accommodate API standard drift diameters.

12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

All information is provided by VAM USA or its affiliates at user's sole risk, without liability for loss, damage or injury resulting from the use thereof; and on an "AS IS" basis without warranty or representation of any kind, whether express or implied, including without limitation any warranty of merchantability, fitness for purpose or completeness. This document and its contents are subject to change without notice. In no event shall VAM USA or its affiliates be responsible for any indirect, special, incidental, punitive, exemplary or consequential loss or damage (including without limitation, loss of use, loss of bargain, loss of revenue, profit or anticipated profit) however caused or arising, and whether such losses or damages were foreseeable or VAM USA or its affiliates was advised of the possibility of such damages.



Issued on: 08 Jul. 2020 by Wesley Ott



OD	Weight	Wall Th.	Grade	API Drift:	Connection
5 1/2 in.	20.00 lb/ft	0.361 in.	P110EC	4.653 in.	VAM <sup>®</sup> SPRINT-SF

PIPE PROPERTIES		
lominal OD	5.500	in.
lominal ID	4.778	in.
Iominal Cross Section Area	5.828	sqin.
Grade Type	Н	igh Yield
lin. Yield Strength	125	ksi
lax. Yield Strength	140	ksi
lin. Ultimate Tensile Strength	135	ksi
	Iominal OD Iominal ID Iominal Cross Section Area Grade Type Iin. Yield Strength Iax. Yield Strength	Iominal OD5.500Iominal ID4.778Iominal Cross Section Area5.828Grade TypeHIin. Yield Strength125Iax. Yield Strength140

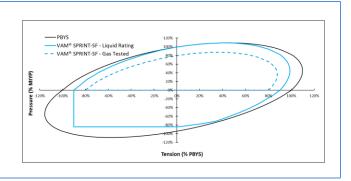
CONNECTIO	N PROPERTIES	
Connection Type	Semi-Premium Integral S	emi-Flush
Connection OD (nom):	5.783	in.
Connection ID (nom):	4.717	in.
Make-Up Loss	5.965	in.
Critical Cross Section	5.244	sqin.
Tension Efficiency	90.0	% of pipe
Compression Efficiency	90.0	% of pipe
Internal Pressure Efficiency	100	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMAN	NCES	
Tensile Yield Strength	656	klb
Compression Resistance	656	klb
Internal Yield Pressure	14,360	psi
Collapse Resistance	12,080	psi
Max. Structural Bending	89	°/100ft
Max. Bending with ISO/API Sealability	30	°/100ft

TORQUE VALUES		
Min. Make-up torque	20,000	ft.lb
Opt. Make-up torque	22,500	ft.lb
Max. Make-up torque	25,000	ft.lb
Max. Torque with Sealability (MTS)	40,000	ft.lb

\* 87.5% RBW

**VAM® SPRINT-SF** is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.



#### Do you need help on this product? - Remember no one knows $\text{VAM}^{\circledast}$ like $\text{VAM}^{\circledast}$

canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com china@vamfieldservice.com baku@vamfieldservice.com singapore@vamfieldservice.com australia@vamfieldservice.com

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Issued on: 09 Dec. 2020 by Logan Van Gorp



# **Connection Data Sheet**

100 % of pipe

OD	Weight	Wall Th.	Grade	API Drift:	Connection
7 5/8 in.	Nominal: 29.70 lb/ft	0.375 in.	P110EC	6.750 in.	VAM <sup>®</sup> SPRINT-FJ
	Plain End: 29.06 ft/lb				

PIPE PROPERTIES			CONNECTION	PROPERTIES	
Nominal OD	7.625	in.	Connection Type	Semi-Premium Int	egral Flush
Nominal ID	6.875	in.	Connection OD (nom):	7.654	in.
Nominal Cross Section Area	8.541	sqin.	Connection ID (nom):	6.827	in.
Grade Type	Enhanced C	ollapse	Make-Up Loss	4.055	in.
Min. Yield Strength	125	ksi	Critical Cross Section	6.979	sqin.
Max. Yield Strength	140	ksi	Tension Efficiency	80.0	% of pipe
Min. Ultimate Tensile Strength	135	ksi	Compression Efficiency	80.0	% of pipe
			Internal Pressure Efficiency	80.0	% of pipe

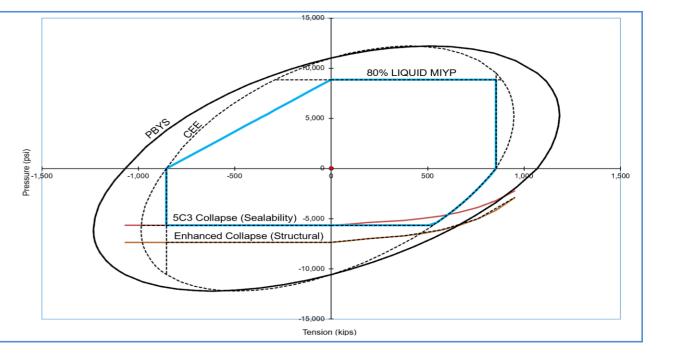
External Pressure Efficiency

CONNECTION PERFORMANCES					
Tensile Yield Strength	854	klb			
Compression Resistance	854	klb			
Max. Internal Pressure	8,610	psi			
Structural Collapse Resistance	7,360	psi			
Max. Structural Bending	57	°/100ft			
Max. Bending with Sealability	10	°/100ft			

	TORQUE VALUES		
)	Min. Make-up torque	15,000	ft.lb
)	Opt. Make-up torque	16,500	ft.lb
i	Max. Make-up torque	18,000	ft.lb
i	Max. Torque with Sealability (MTS)	32,000	ft.lb

\* 87.5% RBW

**VAM® SPRINT-FJ** is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



# Do you need help on this product? - Remember no one knows $\text{VAM}^{\textcircled{B}}$ like $\text{VAM}^{\textcircled{B}}$

- canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com
- uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com

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# **SěAH** 9.625" 40# .395" J-55

# **Dimensions (Nominal)**

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.

## **Performance Properties**

Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
BTC	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
BTC	714	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

#### 1. Geologic Formations

TVD of target	11995	Pilot hole depth	N/A
MD at TD:	22312	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	1025		
Salt	1330		
Base of Salt	4280		
Bell Canyon	4525		
Cherry Canyon	5460		
Brushy Canyon	6710		
1st Bone Spring Lime	8430		
1st Bone Spring Sand	9515		
Bone Spring 2nd	10090		
3rd Bone Spring Lime	10600		
Bone Spring 3rd	11320		
Wolfcamp	11750		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

	Wt Wt			Casing		Casing Interval		
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
12 1/4	9 5/8	40	J55	BTC	0	1050	0	1050
8 3/4	7 5/8	29.7	P110	SPRINT FJ	0	11320	0	11320
6 3/4	5 1/2	20	P110	DWC/C IS & SPRINT FJ	0	22312	0	11995

#### 2. Casing Program (Primary Design)

• All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

• Variance Approval -

o 5-1/2" Production Casing will include Sprint Flush Joint connection (5.783") from base of curve and 500ft into 7-5/8" casing shoe

o All other 5-1/2" Production Casing will run DWC/C IS (6.05")

#### 3. Cementing Program (Primary Design)

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	342	Surf	13.2	1.44	Lead: Class C Cement + additives
Let 1	295	Surf	9	3.27	Lead: Class C Cement + additives
Int 1	363	4000' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1	As Needed	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Int 1 Intermediate Squeeze	261	Surf	9	3.27	2nd Stage Bradenhead Squeeze Lead: Class C Cement + additives
	402	BRUSHY 6710	13.2	1.44	Tail: Class H / C + additives
Production	62	9320	9	3.27	Lead: Class H /C + additives
	701	11320	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy canyon to surface.

If necessary, a top out consisting of 500 sacks of Class C cement will be executed as a contingency.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	T	уре	~	Tested to:		
			Anı	nular	X	50% of rated working pressure		
Int 1	13-5/8"	5M		d Ram	Х			
	15 5/0	5101		e Ram		- 5M		
			Doub	le Ram	X	5111		
			Other*					
	13-5/8"		Annul	ar (5M)	Х	100% of rated working pressure		
Production		5M	Blind Ram		Х			
Fioduction		13-3/8	5 5101	5-5/8 5141	Pipe	e Ram		10M
					Doub	le Ram	Х	10111
			Other*			]		
			Annul	ar (5M)				
			Blind	d Ram				
			Pipe Ram		7			
			Doub	le Ram				
			Other*			]		
N A variance is requested for	the use of a	a diverter or	the surface	casing. See	attached for	schematic.		
Y A variance is requested to	A variance is requested to run a 5 M annular on a 10M system							

#### 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
what will be used to monitor the loss of gain of huid?	r v 1/r ason/ v isuai Wontoring

#### 6. Logging and Testing Procedures

Logging, C	oring and Testing
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the
Х	Completion Rpeort and sbumitted to the BLM.
	No logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain.
	Coring? If yes, explain.

Additional	logs planned	Interval	
	Resistivity	Int. shoe to KOP	
	Density	Int. shoe to KOP	
Х	CBL	Production casing	
Х	Mud log	Intermediate shoe to TD	
	PEX		

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6549
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

	H2S is present
Y	H2S plan attached.

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed

from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan Other, describe

#### Omoumi, Shayda

From:	Moos, Sheldon
Sent:	Thursday, February 23, 2023 8:32 AM
То:	Omoumi, Shayda; Green, Chelsey
Cc:	Porraz, Isac
Subject:	RE: Slim Hole Sundry's
Attachments:	BORA BORA 13-24 FED COM 713H Slim Hole.pdf

Shayda and Chelsey-Please see the attached sundry for Nabors 7503's next pad, spud in April.

This is the same style of batch sundry that Long requested and represents both Bora Bora wells.....

<mark>Bora Bora 13-24 Fed Com 713H - SUNDRY</mark> Bora Bora 13-24 Fed Com 623H

Sheldon Moos C: 210-323-7512

From: Moos, Sheldon <<u>Sheldon.Moos@dvn.com</u>> Sent: Tuesday, January 24, 2023 1:27 PM To: Green, Chelsey <<u>Chelsey.Green@dvn.com</u>>; Omoumi, Shayda <<u>Shayda.Omoumi@dvn.com</u>> Cc: Dzurisin, Ryan <<u>Ryan.Dzurisin@dvn.com</u>>; Porraz, <u>Isac <Isac.Porraz@dvn.com</u>> Subject: FW: Slim Hole Sundry's

Chelsey and Shayda-We need to file some batch sundries for two pads, shown below.

He has verbally approved the design, but asked that we batch sundry the deepest well on the pad. Those are attached.

We are about 1month out from spud. Please let me know if you have questions.

*Sheldon Moos* C: 210-323-7512

Sunar	y Prir	it Repo
		02/23/2023

Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
BORA BORA 13-	713H	3001549352	NMNM0404441	NMNM0404441	DEVON
BORA BORA 13-	623H	3001549351	NMNM0404441	NMNM0404441	DEVON

## **Notice of Intent**

Sundry ID: 2717379

Type of Submission: Notice of Intent

Date Sundry Submitted: 02/23/2023

Date proposed operation will begin: 02/23/2023

Type of Action: APD Change

Time Sundry Submitted: 09:18

**Procedure Description:** Engineer Review only - DRILLING CHANGE: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and cement loss plan. Please see attachments. Requested to batch drill by Long to only include attachments by pad for the drilling plan for the deepest well (TVD). Verbal given for approved design 2-23-23.

## **NOI Attachments**

#### **Procedure Description**

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7.625in\_29.7ppf\_P110EC\_SPRINT\_FJ\_12.9.2020\_20230223091719.pdf

9.625\_40\_\_J55\_20230223091719.pdf

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry

Operator Electronic Signature: SHAYDA OMOUMI Name: DEVON ENERGY PRODUCTION COMPANY LP Title: Regulatory Compliance Associate 3 Street Address: 333 W SHERIDAN AVE City: OKLAHOMA CITY State: OK Phone: (405) 235-3611 Email address: SHAYDA.OMOUMI@DVN.COM **Field** 

State:

Notices through this system satisfies regulations requiring a

**Representative Name:** 

**Street Address:** 

City:

Phone:

Email address:

Signed on: FEB 23, 2023 09:17 AM

Zip:

.

## PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

<b>OPERATOR'S NAME:</b>	Devon Energy Production Company LP				
LEASE NO.:	NMNM0404441				
LOCATION:	Section 12, T.23 S., R.31 E., NMPM				
COUNTY:	Eddy County, New Mexico				
WELL NAME & NO.:	Bora Bora 13-24 Fed Com 623H				
SURFACE HOLE FOOTAGE:	340'/S & 2540'/E				
<b>BOTTOM HOLE FOOTAGE</b>	20'/S & 2310'/E				
ATS/API ID:	3001549351				
APD ID:	10400088030				
Sundry ID:	2717379				
WELL NAME & NO.:	Bora Bora 13-24 Fed Com 713H				
SURFACE HOLE FOOTAGE:	340'/S & 2510'/E				
<b>BOTTOM HOLE FOOTAGE</b>	20'/S & 1850'/E				
ATS/API ID:	3001549352				
APD ID:					
Sundry ID:	2717379				

## COA

H2S	• Yes	🖸 No	
Potash	🖸 None	Secretary	🖸 R-111-P
Cave/Karst Potential	🖸 Low	🖸 Medium	🖸 High
Cave/Karst Potential	Critical		
Variance	None	Flex Hose	Other
Wellhead	Conventional	🖸 Multibowl	🖸 Both
Wellhead Variance	Diverter		
Other	4 String	Capitan Reef	WIPP
Other	Fluid Filled	🗌 Pilot Hole	Open Annulus
Cementing	Contingency	EchoMeter	Primary Cement
	Cement Squeeze		Squeeze
Special Requirements	□ Water Disposal	COM	🗆 Unit
Special Requirements	Batch Sundry		
Special Requirements	Break Testing	□ Offline	Casing
Variance		Cementing	Clearance

### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Sand Dunes, Triste Draw, Wildcat, Bone Springs** formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

### **B.** CASING

- 1. The **9-5/8** inch surface casing shall be set at approximately **1050 feet** (a minimum of **70 feet (Eddy County)** into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>24 hours in the Potash Area</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### **Option 2:**

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6710' (402 sxs Class H/C+ additives).

- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 261 sxs Class C)
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
- In Secretary Potash Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.</u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

# Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 500 feet into previous casing string. Operator shall provide method of verification.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

## **Option 1:**

a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. Annular which shall be tested to **5000 (5M)** psi.

b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **7-5/8** inch intermediate casing shoe shall be **5000 (5M)** psi.

#### **Option 2:**

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **9-5/8** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

#### **D. SPECIAL REQUIREMENT (S)**

#### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in Onshore Order 1 and 2.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be on the sign.</u>

## **BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at **14**-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

## **Batch Sundry:**

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)
- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

## **Casing Clearance:**

Operator casing variance is approved for the utilization of 5-1/2 inch Sprint FJ **from** base of curve and **500 feet** into the 7-5/8 inch casing shoe. **All** other 5-1/2 inch casing will run **DWC/C IS**.

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

## GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - Eddy County Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
  - Lea County
    Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)
    689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24</u> <u>hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

#### B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin

after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.
- C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

LVO 2/23/2023

#### 1. Geologic Formations

TVD of target	11995	Pilot hole depth	N/A
MD at TD:	22312	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	1025		
Salt	1330		
Base of Salt	4280		
Bell Canyon	4525		
Cherry Canyon	5460		
Brushy Canyon	6710		
1st Bone Spring Lime	8430		
1st Bone Spring Sand	9515		
Bone Spring 2nd	10090		
3rd Bone Spring Lime	10600		
Bone Spring 3rd	11320		
Wolfcamp	11750		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

WI CONTRACTOR WI				Casing	Interval	Casing Interval		
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
12 1/4	9 5/8	40	J55	BTC	0	1050	0	1050
8 3/4	7 5/8	29.7	P110	SPRINT FJ	0	11320	0	11320
6 3/4	5 1/2	20	P110	DWC/C IS & SPRINT FJ	0	22312	0	11995

#### 2. Casing Program (Primary Design)

• All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

• Variance Approval -

o 5-1/2" Production Casing will include Sprint Flush Joint connection (5.783") from base of curve and 500ft into 7-5/8" casing shoe

o All other 5-1/2" Production Casing will run DWC/C IS (6.05")

#### 3. Cementing Program (Primary Design)

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	342	Surf	13.2	1.44	Lead: Class C Cement + additives
	295	Surf	9	3.27	Lead: Class C Cement + additives
Int 1	363	4000' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1	As Needed	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	261	Surf	9	3.27	2nd Stage Bradenhead Squeeze Lead: Class C Cement + additives
Squeeze	402	BRUSHY 6710	13.2	1.44	Tail: Class H / C + additives
	62	9320	9	3.27	Lead: Class H /C + additives
Production	701	11320	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy canyon to surface.

If necessary, a top out consisting of 500 sacks of Class C cement will be executed as a contingency.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:															
			Anı	nular	X	50% of rated working pressure															
Int 1	13-5/8"	5M		d Ram	Х																
Int 1	15-5/0	5101		Ram		- 5M															
			Doub	le Ram	X	5111															
			Other*																		
	13-5/8"	5M	Annular (5M)		Х	100% of rated working pressure															
Production			Blind Ram		Х																
Troduction		5101	Pipe Ram			10M															
																		Doub	le Ram	Х	10111
			Other*																		
			Annul	ar (5M)																	
			Blind	l Ram																	
	Pipe Ram																				
			Doub	le Ram																	
			Other*																		
N A variance is requested for	the use of a	a diverter or	the surface	casing. See	attached for	schematic.															
Y A variance is requested to	A variance is requested to run a 5 M annular on a 10M system																				

#### 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
what will be used to monitor the loss of gain of huid?	r v 1/r ason/ v isuai Wontoring

#### 6. Logging and Testing Procedures

Logging, C	Logging, Coring and Testing					
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the					
X Completion Rpeort and sbumitted to the BLM.						
	No logs are planned based on well control or offset log information.					
	Drill stem test? If yes, explain.					
	Coring? If yes, explain.					

Additional logs planned		Interval	
Resistivity		Int. shoe to KOP	
Density		Int. shoe to KOP	
X CBL		Production casing	
X Mud log		Intermediate shoe to TD	
	PEX		

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6549
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

Y H2S plan attached.	N	H2S is present
	Y	H2S plan attached.

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed

from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan Other, describe

# **SěAH** 9.625" 40# .395" J-55

# Dimensions (Nominal)

Outside Diameter Wall Inside Diameter	9.625 0.395 8.835	in. in. in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.

## **Performance Properties**

Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
BTC	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
BTC	714	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility. Issued on: 09 Dec. 2020 by Logan Van Gorp



# **Connection Data Sheet**

100 % of pipe

OD	Weight	Wall Th.	Grade	API Drift:	Connection
7 5/8 in.	Nominal: 29.70 lb/ft	0.375 in.	P110EC	6.750 in.	VAM <sup>®</sup> SPRINT-FJ
	Plain End: 29.06 ft/lb				

PIPE PROPERTIES			CONNECTION PROPERTIES		
Nominal OD	7.625	in.	Connection Type	Semi-Premium Int	egral Flush
Nominal ID	6.875	in.	Connection OD (nom):	7.654	in.
Nominal Cross Section Area	8.541	sqin.	Connection ID (nom):	6.827	in.
Grade Type	Enhanced C	Collapse	Make-Up Loss	4.055	in.
Min. Yield Strength	125	ksi	Critical Cross Section	6.979	sqin.
Max. Yield Strength	140	ksi	Tension Efficiency	80.0	% of pipe
Min. Ultimate Tensile Strength	135	ksi	Compression Efficiency	80.0	% of pipe
			Internal Pressure Efficiency	80.0	% of pipe

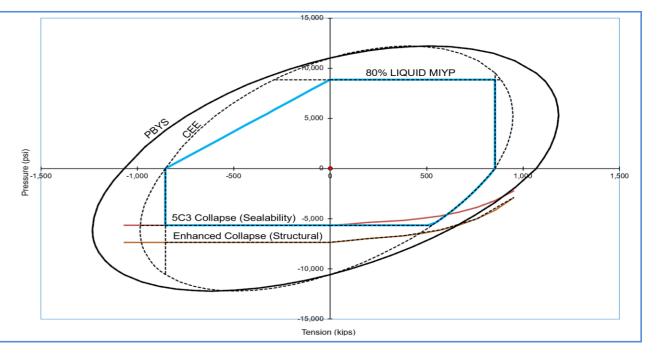
External Pressure Efficiency

CONNECTION PERFORMANCES		
Tensile Yield Strength	854	klb
Compression Resistance	854	klb
Max. Internal Pressure	8,610	psi
Structural Collapse Resistance	7,360	psi
Max. Structural Bending	57	°/100ft
Max. Bending with Sealability	10	°/100ft

	TORQUE VALUES		
)	Min. Make-up torque	15,000	ft.lb
>	Opt. Make-up torque	16,500	ft.lb
i	Max. Make-up torque	18,000	ft.lb
i	Max. Torque with Sealability (MTS)	32,000	ft.lb

\* 87.5% RBW

**VAM® SPRINT-FJ** is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



# Do you need help on this product? - Remember no one knows $\text{VAM}^{\textcircled{B}}$ like $\text{VAM}^{\textcircled{B}}$

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Issued on: 08 Jul. 2020 by Wesley Ott



OD	Weight	Wall Th.	Grade	API Drift:	Connection
5 1/2 in.	20.00 lb/ft	0.361 in.	P110EC	4.653 in.	VAM <sup>®</sup> SPRINT-SF

PIPE PROPERTIES		
Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Cross Section Area	5.828	sqin.
Grade Type	Hig	h Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi
	Nominal OD Nominal ID Nominal Cross Section Area Grade Type Min. Yield Strength Max. Yield Strength	Nominal OD5.500Nominal ID4.778Nominal Cross Section Area5.828Grade TypeHigMin. Yield Strength125Max. Yield Strength140

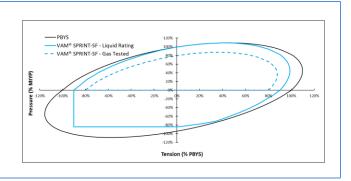
CONNECTIO	N PROPERTIES	
Connection Type	Semi-Premium Integral S	Semi-Flush
Connection OD (nom):	5.783	in.
Connection ID (nom):	4.717	in.
Make-Up Loss	5.965	in.
Critical Cross Section	5.244	sqin.
Tension Efficiency	90.0	% of pipe
Compression Efficiency	90.0	% of pipe
Internal Pressure Efficiency	100	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMANCES						
Tensile Yield Strength	656	klb				
Compression Resistance	656	klb				
Internal Yield Pressure	14,360	psi				
Collapse Resistance	12,080	psi				
Max. Structural Bending	89	°/100ft				
Max. Bending with ISO/API Sealability	30	°/100ft				

TORQUE VALUES		
Min. Make-up torque	20,000	ft.lb
Opt. Make-up torque	22,500	ft.lb
Max. Make-up torque	25,000	ft.lb
Max. Torque with Sealability (MTS)	40,000	ft.lb

\* 87.5% RBW

**VAM® SPRINT-SF** is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.

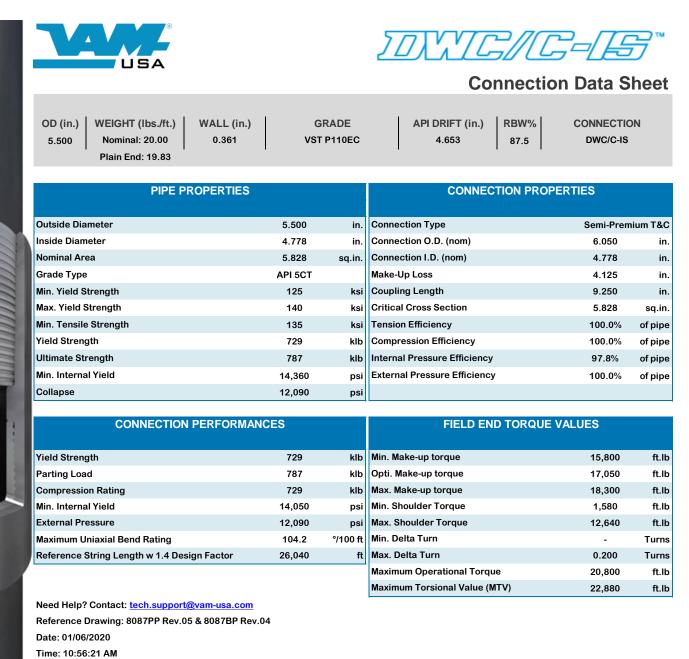


#### Do you need help on this product? - Remember no one knows $\text{VAM}^{\circledast}$ like $\text{VAM}^{\circledast}$

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For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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VAM USA 2107 CityWest Boulevard Suite 1300 Houston, TX 77042 Phone: 713-479-3200 Fax: 713-479-3234 VAM<sup>®</sup> USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support Email: <u>tech.support@vam-usa.com</u>

**DWC Connection Data Sheet Notes:** 

1. DWC connections are available with a seal ring (SR) option.

2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.

Connection performance properties are based on nominal pipe body and connection dimensions.
 DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
 DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.

6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.

7. Bending efficiency is equal to the compression efficiency.

8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.

9. Connection yield torque is not to be exceeded.

10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.

11. DWC connections will accommodate API standard drift diameters.

12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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#### Omoumi, Shayda

From:	Moos, Sheldon
Sent:	Thursday, February 23, 2023 8:32 AM
То:	Omoumi, Shayda; Green, Chelsey
Cc:	Porraz, Isac
Subject:	RE: Slim Hole Sundry's
Attachments:	BORA BORA 13-24 FED COM 713H Slim Hole.pdf

Shayda and Chelsey-Please see the attached sundry for Nabors 7503's next pad, spud in April.

This is the same style of batch sundry that Long requested and represents both Bora Bora wells.....

<mark>Bora Bora 13-24 Fed Com 713H - SUNDRY</mark> Bora Bora 13-24 Fed Com 623H

Sheldon Moos C: 210-323-7512

From: Moos, Sheldon <<u>Sheldon.Moos@dvn.com</u>> Sent: Tuesday, January 24, 2023 1:27 PM To: Green, Chelsey <<u>Chelsey.Green@dvn.com</u>>; Omoumi, Shayda <<u>Shayda.Omoumi@dvn.com</u>> Cc: Dzurisin, Ryan <<u>Ryan.Dzurisin@dvn.com</u>>; Porraz, <u>Isac <Isac.Porraz@dvn.com</u>> Subject: FW: Slim Hole Sundry's

Chelsey and Shayda-We need to file some batch sundries for two pads, shown below.

He has verbally approved the design, but asked that we batch sundry the deepest well on the pad. Those are attached.

We are about 1month out from spud. Please let me know if you have questions.

*Sheldon Moos* C: 210-323-7512

#### *Received by OCD: 2/23/2023 2:56:24 PM*

Page 37 of 38 12-23-31-P Sundry ID 2717379 Bora Bora 13-24 Fed Com 623H Eddy NMNM040441 DEVON ENERGY PRODUCTION COMPANY LP 13-22d 2-23-2023 LV.xlsm

#### Bora Bora 13-24 Fed Com 623H

•	3	urface csg in a	12 1/4	inch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	40.00		i 55	btc	15.00	5.24	0.64	1,050	9	1.07	9.89	42,000
"B"			,	btc				0				0
	w/8.	4#/g mud, 30min Sfc Csg Test	psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	1,050				42,000
omparison of	f Proposed to	Minimum Required Cem	ent Volumes					,				
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
12 1/4	0.3132	342	492	329	50	9.00	3684	5M				0.81
urst Frac Grac	lient(s) for Seg	gment(s)  A, B = , b     All > (	0.70, ОК.									
7 5 /0				· _ · _ · _ · _ · _ · _ · _ · _	· — · — · —	Desian	Factors	_ <i></i>		<b>1-4</b>		
7 5/8	ca #/ft	sing inside the	9 5/8	Coupling	loint	Design Collense		Lanath	D@-	Int 1	- 0	Moight
Segment		Grade	m 110	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	29.70		p 110	vam sprint fj	2.54	1.19	1.32	11,320	1	2.21	2.00	336,204
"B"	10	4#/a mud 20mil: 65: 6:- 7	asia: 1.027				T-+-1	11 220				<b>0</b> 336,204
	w/8.	4#/g mud, 30min Sfc Csg Test		adad to achieve a ten of	0	ft from su	Totals:	11,320 <b>1050</b>				,
Hole	Annular	1 Stage	1 Stage	nded to achieve a top of Min	0 1 Stage	Drilling	Calc					overlap. Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	Req'd BOPE				Hole-Cpl
8 3/4	0.1005	402	579	1146	-49	10.50	3904	5M				0.55
	0.1005	402	6710	1140	-49	10.50						Σ%exces
V Tool(s):		25	25				sum of sx 663	<u>Σ CuFt</u> 1432				25
by stage % : lass 'C' tail cm	111.4.25	25	20				003	1432				20
Tail cmt 5 1/2	ca	ising inside the	7 5/8			<u>Design Fa</u>			a a	Prod 1		
Tail cmt 5 1/2 Segment	ca #/ft	ising inside the Grade		Coupling	Joint	Collapse	Burst	Length		a-B	a-C	-
Tail cmt 5 1/2 Segment "A"	ca #/ft 20.00	0	p 110	dwc/c is	3.04	Collapse 2.05	Burst 2.15	10,820	2	<b>a-B</b> 3.60	<b>a-C</b> 3.43	216,40
Tail cmt 5 1/2 Segment "A" "B"	ca #/ft 20.00 <b>20.00</b>	0	p 110 <b>p 110</b>	dwc/c is vam sprint sf	3.04 27.28	Collapse 2.05 1.85	Burst 2.15 <b>2.19</b>	10,820 <b>1,175</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09	216,400 <b>23,500</b>
Tail cmt 5 1/2 Segment "A" <b>"B"</b> "C"	ca #/ft 20.00	0	p 110	dwc/c is vam sprint sf dwc/c is	3.04	Collapse 2.05	Burst 2.15	10,820 <b>1,175</b> 10,317	2	<b>a-B</b> 3.60	<b>a-C</b> 3.43	216,40 <b>23,500</b> 206,34
Tail cmt 5 1/2 Segment "A" <b>"B"</b>	ca #/ft 20.00 <b>20.00</b> 20.00	Grade	p 110 <b>p 110</b> 0 110	dwc/c is vam sprint sf	3.04 27.28	Collapse 2.05 1.85	Burst 2.15 <b>2.19</b> 2.15	10,820 <b>1,175</b> 10,317 <b>0</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09	216,40 23,500 206,34 0
Tail cmt 5 1/2 Segment "A" <b>"B"</b> "C"	ca #/ft 20.00 <b>20.00</b> 20.00	Grade 4#/g mud, 30min Sfc Csg Test	p 110 p 110 0 110 psig: 2,380	dwc/c is vam sprint sf dwc/c is 0	3.04 27.28 ∞	Collapse 2.05 1.85 1.85	Burst 2.15 2.19 2.15 Totals:	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09 3.10	216,40 23,500 206,34 0 446,24
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	ca #/ft 20.00 20.00 20.00 w/8.	Grade 4#/g mud, 30min Sfc Csg Test The cement	p 110 p 110 0 110 psig: 2,380 volume(s) are inter	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of	3.04 27.28 ∞ 10820	Collapse 2.05 1.85 1.85 ft from su	Burst 2.15 2.19 2.15 Totals: Inface or a	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole	ca #/ft 20.00 20.00 20.00 w/8. Annular	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min	3.04 27.28 ∞ 10820 1 Stage	Collapse 2.05 1.85 1.85 ft from su Drilling	Burst 2.15 2.19 2.15 Totals: Inface or a Calc	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b> <b>Req'd</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft	3.04 27.28 ∞ 10820 1 Stage % Excess	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt	Burst 2.15 2.19 2.15 Totals: Inface or a	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist Hole-Cpl
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min	3.04 27.28 ∞ 10820 1 Stage	Collapse 2.05 1.85 1.85 ft from su Drilling	Burst 2.15 2.19 2.15 Totals: Inface or a Calc	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b> <b>Req'd</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft	3.04 27.28 ∞ 10820 1 Stage % Excess	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt 10.50	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b> <b>Req'd</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b> 3.60	<b>a-C</b> 3.43 3.09 3.10	446,240 overlap. Min Dist Hole-Cpl
Tail cmt 51/2 Segment "A" "C" "D" Hole Size 6 3/4 class 'C' tail cm	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft	3.04 27.28 ∞ 10820 1 Stage % Excess	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b> <b>Req'd</b>	2 2 2	<b>a-B</b> 3.60 <b>3.68</b>	<b>a-C</b> 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist Hole-Cpl
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 diass 'C' tail cm #N/A 0 Segment	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling	3.04 27.28 ∞ 10820 1 Stage % Excess	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt 10.50	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP	10,820 <b>1,175</b> 10,317 <b>0</b> 22,312 <b>500</b> <b>Req'd</b>	2 2 2	a-B 3.60 3.68 3.60	<b>a-C</b> 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist Hole-Cpl 0.35
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 diass 'C' tail cm #N/A 0 Segment "A"	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling 0.00	3.04 27.28 ∞ 10820 1 Stage % Excess 26	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt 10.50	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP	10,820 1,175 10,317 0 22,312 500 Req'd BOPE	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist Hole-Cpl 0.35 Weight 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 diass 'C' tail cm #N/A 0 Segment	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling	3.04 27.28 ∞ 10820 1 Stage % Excess 26	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt 10.50	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP	10,820 1,175 10,317 0 22,312 500 Req'd BOPE	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10	216,400 23,500 206,340 0 446,240 overlap. Min Dist Hole-Cpl 0.35 Weight 0 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 diass 'C' tail cm #N/A 0 Segment "A"	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835 tt yld > 1.35 #/ft	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763 Grade 4#/g mud, 30min Sfc Csg Test	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212 5 1/2	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling 0.00 0.00	3.04 27.28 ∞ 10820 1 Stage % Excess 26 #N/A	Collapse 2.05 1.85 1.85 1.85 Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.15 2.19 2.15 Totals: Inface or a Calc MASP Factors Burst	10,820 1,175 10,317 0 22,312 500 Req'd BOPE	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10 sing> a-C	216,400 23,500 206,344 0 446,244 overlap. Min Dis Hole-Cpl 0.35 Weigh 0 0
Tail cmt 51/2 Segment "A" "C" "D" Hole Size 63/4 Class 'C' tail cm #N/A 0 Segment "A" "B"	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835 tt yld > 1.35 #/ft	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763 Grade 4#/g mud, 30min Sfc Csg Test	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212 5 1/2	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling 0.00	3.04 27.28 ∞ 10820 1 Stage % Excess 26	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt 10.50	Burst 2.15 2.19 2.15 Totals: Inface or a Calc MASP Factors Burst	10,820 1,175 10,317 0 22,312 500 Req'd BOPE	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10 sing> a-C	216,40 23,500 206,34 0 446,24 overlap. Min Dis Hole-Cpl 0.35
Tail cmt 5 1/2 Segment "A" "C" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B" Hole	ca #/ft 20.00 20.00 20.00 20.00 w/8. Annular Volume 0.0835 t yld > 1.35 t yld > 1.35 t yld > 1.35 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763 Grade 4#/g mud, 30min Sfc Csg Test	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212 5 1/2 5 1/2	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling 0.00 0.00 0.00 this csg, TOC intended Min	3.04 27.28 ∞ 10820 1 Stage % Excess 26 #N/A	Collapse 2.05 1.85 1.85 1.85 Drilling Mud Wt 10.50 Design Collapse	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP Factors Burst	10,820 1,175 10,317 0 22,312 500 Req'd BOPE	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10 sing> a-C	216,400 23,500 206,344 0 446,244 overlap. Min Dis Hole-Cpj 0.35 Weigh 0 0 0 0 0 0 0 0 0 0
Tail cmt 5 1/2 Segment "A" "C" "D" Hole Size 6 3/4 Cass 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	ca #/ft 20.00 20.00 20.00 w/8. Annular Volume 0.0835 tt yld > 1.35 #/ft w/8.	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763 Grade 4#/g mud, 30min Sfc Csg Test Cmt vol c	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212 5 1/2	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling 0.00 0.00 this csg, TOC intended	3.04 27.28 ∞ 10820 1 Stage % Excess 26 #N/A #N/A 1 Stage % Excess	Collapse 2.05 1.85 1.85 ft from su Drilling Mud Wt 10.50 Design Collapse	Burst 2.15 2.19 2.15 Totals: Inface or a Calc MASP Factors Burst	10,820 1,175 10,317 0 22,312 500 Req'd BOPE	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10 sing> a-C	216,400 23,500 206,340 0 446,240 overlap. Min Dist Hole-Cpl 0.35 Weight 0 0 0
Tail cmt 5 1/2 Segment "A" "C" "D" Hole Size 6 3/4 Lass 'C' tail cm #N/A 0 Segment "A" "B" Hole	ca #/ft 20.00 20.00 20.00 20.00 w/8. Annular Volume 0.0835 t yld > 1.35 t yld > 1.35 t yld > 1.35 t yld > 1.35	Grade 4#/g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 763 Grade 4#/g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	p 110 p 110 0 110 psig: 2,380 volume(s) are inter 1 Stage CuFt Cmt 1212 5 1/2 5 1/2	dwc/c is vam sprint sf dwc/c is 0 nded to achieve a top of Min Cu Ft 964 Coupling 0.00 0.00 0.00 this csg, TOC intended Min	3.04 27.28 ∞ 10820 1 Stage % Excess 26 #N/A 1 Stage	Collapse 2.05 1.85 1.85 1.85 Drilling Mud Wt 10.50 Design Collapse	Burst 2.15 2.19 2.15 Totals: urface or a Calc MASP Factors Burst	10,820 1,175 10,317 0 22,312 500 Req'd BOPE Length 0 0 0 0 #N/A Req'd	2 2 2	a-B 3.60 3.68 3.60	a-C 3.43 3.09 3.10 sing> a-C	216,400 23,500 206,344 0 446,244 overlap. Min Dis Hole-CpJ 0.35 Weigh 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

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## **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	190098
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

CONDITIONS

CONDITIONS		
Created By		Condition Date
kpickford	Adhere to previous NMOCD Conditions of Approval	3/2/2023

CONDITIONS

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Action 190098