U.S. Department of the Interior BUREAU OF LAND MANAGEMENT



	Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
	STRAY CAT 8-5	734H	3002551260	NMNM98826	NMNM98826	DEVON
	STRAY CAT 8-5	714H	3002551258	NMNM98826	NMNM138944	DEVON
	STRAY CAT 8-5	614H	3002551256	NMNM98826	NMNM98826	DEVON

#### **Notice of Intent**

Sundry ID: 2726179

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 04/18/2023 Time Sundry Submitted: 09:17

Date proposed operation will begin: 04/18/2023

**Procedure Description:** Engineer Review only - DRILLING CHANGE: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and cement loss plan. Please see attachments. Requested to batch drill by Long to only include attachments by pad for the drilling plan for the deepest well (TVD). Verbal given for approved design 4-5-23

#### **NOI Attachments**

#### **Procedure Description**

9.625\_40\_\_J55\_20230418091020.pdf

7.625in\_29.7ppf\_P110EC\_SPRINT\_FJ\_12.9.2020\_20230418091021.pdf

5.500in\_20.00\_\_\_0.361in\_Wall\_\_VST\_P110EC\_DWC\_C\_IS\_CDS\_AB\_20230418091020.pdf

5.5in\_20lbf\_P110EC\_VAM\_SPRINT\_SF\_20230418091021.pdf

Stray\_Cat\_8\_5\_Fed\_Com\_303H\_\_20230418090936.pdf

Slim\_Hole\_verbal\_20230418090937.pdf

## **Conditions of Approval**

#### **Specialist Review**

Gato\_Grande\_9\_4\_Fed\_Com\_301H\_Stray\_Cat\_8\_5\_Fed\_Com\_734H\_Sundry\_ID\_2726179\_20230418131558.pdf

#### **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: SHAYDA OMOUMI Signed on: APR 18, 2023 09:13 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Compliance Associate 3 Street Address: 333 W SHERIDAN AVE

City: OKLAHOMA CITY State: OK

Phone: (405) 235-3611

Email address: SHAYDA.OMOUMI@DVN.COM

**Field** 

**Representative Name:** 

**Street Address:** 

State: City: Zip:

Phone:

**Email address:** 

#### **BLM Point of Contact**

Signature: Long Vo

**BLM POC Name: LONG VO BLM POC Title:** Petroleum Engineer

**BLM POC Phone:** 5752345972 BLM POC Email Address: LVO@BLM.GOV

**Disposition:** Approved **Disposition Date:** 04/18/2023





#### **Connection Data Sheet**

OD (in.) WEIGHT (lbs./ft.) 5.500 Nominal: 20.00

**GRADE** 

API DRIFT (in.)

RBW%

CONNECTION DWC/C-IS

WALL (in.) 0.361 VST P110EC 4.653 87.5 Plain End: 19.83

F	PIPE PROPERTIES			CONNECTION PRO	OPERTIES	
Outside Diameter		5.500	in.	Connection Type	Semi-Prem	ium T&C
Inside Diameter		4.778	in.	Connection O.D. (nom)	6.050	in.
Nominal Area		5.828	sq.in.	Connection I.D. (nom)	4.778	in.
Grade Type		API 5CT		Make-Up Loss	4.125	in.
Min. Yield Strength		125	ksi	Coupling Length	9.250	in.
Max. Yield Strength		140	ksi	Critical Cross Section	5.828	sq.in.
Min. Tensile Strength		135	ksi	Tension Efficiency	100.0%	of pipe
Yield Strength		729	klb	Compression Efficiency	100.0%	of pipe
Ultimate Strength		787	klb	Internal Pressure Efficiency	97.8%	of pipe
Min. Internal Yield		14,360	psi	External Pressure Efficiency	100.0%	of pipe
Collapse		12,090	psi			

CONNECTION PERFORMANCES						
Yield Strength	729	klb				
Parting Load	787	klb				
Compression Rating	729	klb				
Min. Internal Yield	14,050	psi				
External Pressure	12,090	psi				
Maximum Uniaxial Bend Rating	104.2	°/100 ft				
Reference String Length w 1.4 Design Factor	26,040	ft				

FIELD END TORQUE VALUES							
Min. Make-up torque	15,800	ft.lb					
Opti. Make-up torque	17,050	ft.lb					
Max. Make-up torque	18,300	ft.lb					
Min. Shoulder Torque	1,580	ft.lb					
Max. Shoulder Torque	12,640	ft.lb					
Min. Delta Turn	-	Turns					
Max. Delta Turn	0.200	Turns					
Maximum Operational Torque	20,800	ft.lb					
Maximum Torsional Value (MTV)	22,880	ft.lb					
	Min. Make-up torque Opti. Make-up torque Max. Make-up torque Min. Shoulder Torque Max. Shoulder Torque Min. Delta Turn Max. Delta Turn Maximum Operational Torque	Min. Make-up torque 15,800 Opti. Make-up torque 17,050 Max. Make-up torque 18,300 Min. Shoulder Torque 1,580 Max. Shoulder Torque 12,640 Min. Delta Turn - Max. Delta Turn 0.200 Maximum Operational Torque 20,800					

Need Help? Contact: tech.support@vam-usa.com Reference Drawing: 8087PP Rev.05 & 8087BP Rev.04

Date: 01/06/2020 Time: 10:56:21 AM

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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VAM® USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support Email: <u>tech.support@vam-usa.com</u>

#### **DWC Connection Data Sheet Notes:**

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- 4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- 10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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Issued on: 08 Jul. 2020 by Wesley Ott



**Connection Data Sheet** 

OD	Weight	Wall Th.	Grade	API Drift:	Connection
5 1/2 in.	20.00 lb/ft	0.361 in.	P110EC	4.653 in.	VAM® SPRINT-SF
				ı	

PIPE PROPERTIES						
Nominal OD	5.500	in.				
Nominal ID	4.778	in.				
Nominal Cross Section Area	5.828	sqin.				
Grade Type	Hig	h Yield				
Min. Yield Strength	125	ksi				
Max. Yield Strength	140	ksi				
Min. Ultimate Tensile Strength	135	ksi				

CONNECTION P	ROPERTIES	
Connection Type	Semi-Premium Integral !	Semi-Flush
Connection OD (nom):	5.783	in.
Connection ID (nom):	4.717	in.
Make-Up Loss	5.965	in.
Critical Cross Section	5.244	sqin.
Tension Efficiency	90.0	% of pipe
Compression Efficiency	90.0	% of pipe
Internal Pressure Efficiency	100	% of pipe
External Pressure Efficiency	100	% of pipe

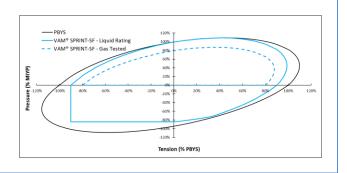
CONNECTION PERFORMANCES						
Tensile Yield Strength	656	klb				
Compression Resistance	656	klb				
Internal Yield Pressure	14,360	psi				
Collapse Resistance	12,080	psi				
Max. Structural Bending	89	°/100ft				
Max. Bending with ISO/API Sealability	30	°/100ft				

TORQUE VALUES		
Min. Make-up torque	20,000	ft.lb
Opt. Make-up torque	22,500	ft.lb
Max. Make-up torque	25,000	ft.lb
Max. Torque with Sealability (MTS)	40,000	ft.lb

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.

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Do you need help on this product? - Remember no one knows VAM® like VAM®

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Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance



<sup>\* 87.5%</sup> RBW

Page 6 of 38

Issued on: 09 Dec. 2020 by Logan Van Gorp



# **Connection Data Sheet**

OD	Weight	Wall Th.	Grade	API Drift:	Connection
7 5/8 in.	Nominal: 29.70 lb/ft	0.375 in.	P110EC	6.750 in.	VAM® SPRINT-FJ
	Plain End: 29.06 ft/lb				

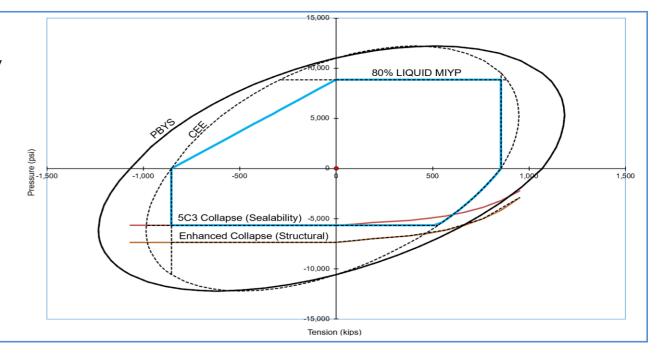
PIPE PROPERTIES						
Nominal OD	7.625	in.				
Nominal ID	6.875	in.				
Nominal Cross Section Area	8.541	sqin.				
Grade Type	Enhanced	Collapse				
Min. Yield Strength	125	ksi				
Max. Yield Strength	140	ksi				
Min. Ultimate Tensile Strength	135	ksi				

CONNECTION PROP	ERTIES	
Connection Type	Semi-Premium Into	egral Flush
Connection OD (nom):	7.654	in.
Connection ID (nom):	6.827	in.
Make-Up Loss	4.055	in.
Critical Cross Section	6.979	sqin.
Tension Efficiency	80.0	% of pipe
Compression Efficiency	80.0	% of pipe
Internal Pressure Efficiency	80.0	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMANCES		
Tensile Yield Strength	854	klb
Compression Resistance	854	klb
Max. Internal Pressure	8,610	psi
Structural Collapse Resistance	7,360	psi
Max. Structural Bending	57	°/100ft
Max. Bending with Sealability	10	°/100ft

TORQUE VALUES	5	
Min. Make-up torque	15,000	ft.lb
Opt. Make-up torque	16,500	ft.lb
Max. Make-up torque	18,000	ft.lb
Max. Torque with Sealability (MTS)	32,000	ft.lb

**VAM® SPRINT-FJ** is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com

# Do you need help on this product? - Remember no one knows $VAM^{\circledR}$ like $VAM^{\circledR}$

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9.625" 40# .395" J-55

# **Dimensions (Nominal)**

**BTC** 

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
	40.000	11 /6
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.
Daufaumanaa Duamantiaa		
Performance Properties		
Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
	2072	
PE	3950	psi
LTC	3950	psi
ВТС	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
ricia strength, ripe body	030	1000 103.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

714

1000 lbs.

#### 1. Geologic Formations

TVD of target	11250	Pilot hole depth	N/A
MD at TD:	21589	Deepest expected fresh water	

#### Basin

	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	1023		
Salt	1351		
Base of Salt	4483		
Delaware	4668		
Cherry Canyon	5586		
Brushy Canyon	6858		
1st Bone Spring Lime	8525		
Avalon B	8950		
Bone Spring 1st	9684		
2nd Bone Spring Silt	9950		
Bone Spring 2nd	10260		
3rd Bone Spring Lime	10780		

<sup>\*</sup>H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

		Wt	Grade		Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)		Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
13-1/2	9-5/8	40	J-55	ВТС	0	1048	0	1048
8-3/4	7-5/8	29.7	P110	Sprint FJ	0	10597	0	10597
6-3/4	5 1/2	20	P110	DWC/C IS & SPRINT FJ	0	21589	0	11250

- All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.
- Variance Approval
  - o 5-1/2" Production Casing will include Sprint Flush Joint connection (5.783") from base of curve and 500ft into 7-5/8" casing shoe
  - o All other 5-1/2" Production Casing will run DWC/C IS (6.05")

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	533	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	295	Surf	9	3.27	Lead: Class C Cement + additives
Int 1	363	4000' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1	As Needed	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	265	Surf	9	3.27	2nd Stage Bradenhead Squeeze Lead: Class C Cement + additives
Squeeze	330	BRUSHY 6858	13.2	1.44	Tail: Class H / C + additives
Production	62	9320	9	3.27	Lead: Class H /C + additives
Froduction	675	11320	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy canyon to surface.

If necessary, a top out consisting of 500 sacks of Class C cement will be executed as a contingency.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

4. Pressure Control Equipment (Three String Design)

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Ty	ype	<b>√</b>	Tested to:	
			Anı	nular	X	50% of rated working pressure	
Int 1	13-58"	5M	Blind	l Ram	X		
IIIL I	15-38	JIVI	Pipe	Ram		5M	
			Doub	le Ram	X	3101	
			Other*				
			Annular (5M)		X	50% of rated working pressure	
Don't sellen	10.5/01	10.5/01	53.6	Blind Ram		X	
Production	13-5/8"	5M	Pipe Ram			5M	
			Doub	le Ram	X	5M	
			Other*				
			Annul	ar (5M)			
			Blind Ram				
			Pipe Ram				
			Doub	le Ram			
			Other*				
N A variance is requested for	the use of a	a diverter or	the surface	casing. See	attached for s	chematic.	
Y A variance is requested to 1	un a 5 M a	nnular on a	10M system				

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	8.5-9

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

<u> </u>	6					
Logging, C	Logging, Coring and Testing					
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the					
X	Completion Report and sbumitted to the BLM.					
	No logs are planned based on well control or offset log information.					
	Drill stem test? If yes, explain.					
	Coring? If yes, explain.					

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5265
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

cheountered	casarea values and formations will be provided to the BEW.				
N	H2S is present				
Y	H2S plan attached.				

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

#### Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachment	ts
X	Directional Plan
	Other, describe

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT



Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
STRAY CAT 8-5	734H	3002551260	NMNM98826	NMNM98826	DEVON
STRAY CAT 8-5	714H	3002551258	NMNM98826	NMNM138944	DEVON
STRAY CAT 8-5	614H	3002551256	NMNM98826	NMNM98826	DEVON

#### **Notice of Intent**

Sundry ID: 2726179

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 04/18/2023 Time Sundry Submitted: 09:17

Date proposed operation will begin: 04/18/2023

**Procedure Description:** Engineer Review only - DRILLING CHANGE: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and cement loss plan. Please see attachments. Requested to batch drill by Long to only include attachments by pad for the drilling plan for the deepest well (TVD). Verbal given for approved design 4-5-23

#### **NOI Attachments**

#### **Procedure Description**

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Stray\_Cat\_8\_5\_Fed\_Com\_303H\_\_20230418090936.pdf

Slim\_Hole\_verbal\_20230418090937.pdf

#### **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: SHAYDA OMOUMI Signed on: APR 18, 2023 09:13 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

**Title:** Regulatory Compliance Associate 3 **Street Address:** 333 W SHERIDAN AVE

City: OKLAHOMA CITY State: OK

Phone: (405) 235-3611

Email address: SHAYDA.OMOUMI@DVN.COM

Re	presen	tative	Name:
----	--------	--------	-------

**Street Address:** 

City: State: Zip:

Phone:

**Email address:** 

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME:** Devon Energy Production Company LP

LEASE NO.: NMNM98826

LOCATION: Section 17, T.23 S., R.32 E., NMPM

**COUNTY:** Lea County, New Mexico

**Batch Sundry ID:** | **2726179** 

WELL NAME & NO.: | Gato Grande 9-4 Fed Com 301H

ATS/API ID: 3002551260 APD ID: 10400082349 Sundry ID: 2723597

WELL NAME & NO.: | Stray Cat 8-5 Fed Com 303H

ATS/API ID: 3002551258 APD ID: 10400082341 Sundry ID: 2723588

WELL NAME & NO.: Stray Cat 8-5 Fed Com 304H

ATS/API ID: 3002551256 APD ID: 10400082302 Sundry ID: 2723583

COA

H2S	Yes ▼		
Potash	None		
Cave/Karst Potential	Low		
Cave/Karst	Critical		
Potential Variance	□ None	<b>☑</b> Flex Hose	C Other
Wellhead	Conventional and Multibow	/  -	
Other	□4 String	Capitan Reef	□WIPP
		None	
Other	Pilot Hole	☐ Open Annulus	
	None 🔻		
Cementing	Contingency Squeeze	Echo-Meter	Primary Cement
	None 🔻	Int 1	Squeeze
			None -
Special	□ Water	<b>™</b> COM	□ Unit
Requirements	Disposal/Injection		
Special	☑ Batch Sundry		
Requirements			
Special	✓ Break Testing	☐ Offline	Casing
Requirements		Cementing	Clearance
Variance			

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

#### **B. CASING**

- 1. The 9-5/8 inch surface casing shall be set at approximately 1135 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. The surface hole shall be 13 1/2 inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of

- six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

#### Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the Brushy Canyon at 6858' (330 sxs Class H/C+ additives).
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 265 sxs Class C)

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### C. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

#### Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi. Annular which shall be tested to 3500 (70% Working Pressure) psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 7-5/8 inch intermediate casing shoe shall be 5000 (5M) psi.

#### **Option 2:**

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 9-5/8 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

#### D. SPECIAL REQUIREMENT (S)

#### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in Onshore Order 1 and 2.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

#### **BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 14-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

#### **Batch Sundry:**

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes above the deepest well shoes set depth.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)

- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

## **Casing Clearance:**

Operator casing variance is approved for the utilization of 5-1/2 inch **Vam Sprint SF from** base of curve and a minimum of 500 feet or the minimum tie-back back requirement above whichever is greater into the 7-5/8 inch casing shoe. **All** other 5-1/2 inch casing will run **DWC/C IS**.

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

## **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - ☑ Eddy CountyCall the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
  - ✓ Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

#### B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin

- after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

LVO 4/18/2023

#### 1. Geologic Formations

TVD of target	11250	Pilot hole depth	N/A
MD at TD:	21589	Deepest expected fresh water	

#### Basin

Dasin		TTT : /2.54	
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	1023		
Salt	1351		
Base of Salt	4483		
Delaware	4668		
Cherry Canyon	5586		
Brushy Canyon	6858		
1st Bone Spring Lime	8525		
Avalon B	8950		
Bone Spring 1st	9684		
2nd Bone Spring Silt	9950		
Bone Spring 2nd	10260		
3rd Bone Spring Lime	10780		
			·

<sup>\*</sup>H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

	,	Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
13-1/2	9-5/8	40	J-55	ВТС	0	1048	0	1048
8-3/4	7-5/8	29.7	P110	Sprint FJ	0	10597	0	10597
6-3/4	5 1/2	20	P110	DWC/C IS & SPRINT FJ	0	21589	0	11250

<sup>•</sup> All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

o All other 5-1/2" Production Casing will run DWC/C IS (6.05")

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	533	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	295	Surf	9	3.27	Lead: Class C Cement + additives
Int 1	363	4000' above shoe	13.2	1.44	Tail: Class H / C + additives
Int 1 Intermediate	As Needed	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
	265	Surf	9	3.27	2nd Stage Bradenhead Squeeze Lead: Class C Cement + additives
Squeeze	330	BRUSHY 6858	13.2	1.44	Tail: Class H / C + additives
Dua du 44	62	9320	9	3.27	Lead: Class H /C + additives
Production	675	11320	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy canyon to surface.

If necessary, a top out consisting of 500 sacks of Class C cement will be executed as a contingency.

Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

<sup>•</sup> Variance Approval -

o 5-1/2" Production Casing will include Sprint Flush Joint connection (5.783") from base of curve and 500ft into 7-5/8" casing shoe

4. Pressure Control Equipment (Three String Design)

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		<b>√</b>	Tested to:
			Annular		X	50% of rated working pressure
Int 1	13-58"	5M	Blind	l Ram	X	
IIIL I	15-38	JIVI	Pipe	Ram		5M
			Doub	le Ram	X	3101
			Other*			
			Annular (5M)		5M)   X	50% of rated working pressure
Don't sellen	10.5/01	514	Blind Ram		X	
Production	13-5/8"	5M	Pipe Ram			73.4
			Doub	le Ram	X	5M
			Other*			
			Annul	ar (5M)		
			Blind Ram			
			Pipe Ram			
			Doub	le Ram		
			Other*			
N A variance is requested for	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.					
Y A variance is requested to 1	A variance is requested to run a 5 M annular on a 10M system					

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	8.5-9

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

	00 2086mg was 1000mg 11000mg				
Logging,	Logging, Coring and Testing				
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the				
X	Completion Report and sbumitted to the BLM.				
	No logs are planned based on well control or offset log information.				
	Drill stem test? If yes, explain.				
	Coring? If yes, explain.				

Additional logs planned		Interval	
	Resistivity	Int. shoe to KOP	
Density		Int. shoe to KOP	
X	CBL	Production casing	
X	Mud log	Intermediate shoe to TD	
	PEX		

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5265
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

cheountered	incastred values and formations will be provided to the BEN.
N	H2S is present
Y	H2S plan attached.

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

#### Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachment	ts
X	Directional Plan
	Other, describe

#### Omoumi, Shayda

From: Moos, Sheldon

Sent: Wednesday, April 5, 2023 9:07 PM

**To:** Omoumi, Shayda

**Cc:** Green, Chelsey; Perez-Jimenez, Jose

Subject: Slim Hole Sundry - Stray Cat & Gato Grande

**Attachments:** Stray Cat 8-5 Fed Com 303H\_.pdf

#### Shayda and Chelsey-

We are finally comfortable calling the following wells slim hole candidates for N7503. Therefore, can we please request a batch sundry. This will be a similar request as what we did with the Bora Bora pad. Long seemed to turn around the approval quick.

His ask, batch request with the deepest well on the pad. Thankfully, all of these are the same target, 3rdBone. So I am attaching the 303H.

- Stray Cat 8-5 Fed Com 303H
- Stray Cat 8-5 Fed Com 304H
- Gato Grande 9-4 Fed Com 301H

Please let me know if you have questions. I believe the spudder rig (that is coming soon, and new to Delaware) will be catching these wells. Might need to double check that is approved, I believe it is.

Thanks.

Sheldon Moos

Drilling Engineer, Delaware Basin C: 210-323-7512

Devon Energy Corporation



9.625" 40# .395" J-55

# **Dimensions (Nominal)**

**BTC** 

Outside Diam	eter	9.625	in.
Wall		0.395	in.
Inside Diamet	er	8.835	in.
Drift		8.750	in.
Weight, T&C		40.000	lbs./ft.
Weight, PE		38.970	lbs./ft.
5 (			
Performa	nce Properties		
Collapse, PE		2570	psi
Internal Viola	Dungarung at Minimanus Viola		
internal Yield	Pressure at Minimum Yield	2050	
	PE	3950	psi
	LTC	3950	psi
	ВТС	3950	psi
Yield Strength	. Pine Body	630	1000 lbs.
ricia oti ciigai	,		1000 1001
Joint Strength			
	STC	452	1000 lbs.
	LTC	520	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

714

1000 lbs.

Issued on: 08 Jul. 2020 by Wesley Ott



**Connection Data Sheet** 

	1				
OD	Weight	Wall Th.	Grade	API Drift:	Connection
5 1/2 in.	20.00 lb/ft	0.361 in.	P110EC	4.653 in.	VAM® SPRINT-SF

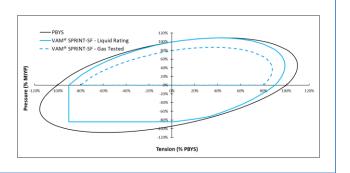
PIPE PROPERTIES		
Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Cross Section Area	5.828	sqin.
Grade Type	Hig	h Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi

CONNECTION P	ROPERTIES	
Connection Type	Semi-Premium Integral :	Semi-Flush
Connection OD (nom):	5.783	in.
Connection ID (nom):	4.717	in.
Make-Up Loss	5.965	in.
Critical Cross Section	5.244	sqin.
Tension Efficiency	90.0	% of pipe
Compression Efficiency	90.0	% of pipe
Internal Pressure Efficiency	100	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMAN	ICES	
Tensile Yield Strength	656	klb
Compression Resistance	656	klb
Internal Yield Pressure	14,360	psi
Collapse Resistance	12,080	psi
Max. Structural Bending	89	°/100ft
Max. Bending with ISO/API Sealability	30	°/100ft

TORQUE VALUES		
Min. Make-up torque	20,000	ft.lb
Opt. Make-up torque	22,500	ft.lb
Max. Make-up torque	25,000	ft.lb
Max. Torque with Sealability (MTS)	40,000	ft.lb

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.



Do you need help on this product? - Remember no one knows  $\mathrm{VAM}^{\circledR}$  like  $\mathrm{VAM}^{\circledR}$ 

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<sup>\* 87.5%</sup> RBW





#### **Connection Data Sheet**

OD (in.) 5.500 Nominal: 20.00

WEIGHT (lbs./ft.) WALL (in.) **GRADE** API DRIFT (in.) RBW% CONNECTION 0.361 VST P110EC 4.653 87.5 DWC/C-IS Plain End: 19.83

	PIPE PROPERTIES			CONNECTION PROPE	RTIES	
Outside Diameter		5.500	in.	Connection Type	Semi-Prem	ium T&C
Inside Diameter		4.778	in.	Connection O.D. (nom)	6.050	in.
Nominal Area		5.828	sq.in.	Connection I.D. (nom)	4.778	in.
Grade Type		API 5CT		Make-Up Loss	4.125	in.
Min. Yield Strength		125	ksi	Coupling Length	9.250	in.
Max. Yield Strength		140	ksi	Critical Cross Section	5.828	sq.in.
Min. Tensile Strength		135	ksi	Tension Efficiency	100.0%	of pipe
Yield Strength		729	klb	Compression Efficiency	100.0%	of pipe
Ultimate Strength		787	klb	Internal Pressure Efficiency	97.8%	of pipe
Min. Internal Yield		14,360	psi	External Pressure Efficiency	100.0%	of pipe
Collapse		12,090	psi			

CONNECTION PERFORMA	NCES	
Yield Strength	729	klb
Parting Load	787	klb
Compression Rating	729	klb
Min. Internal Yield	14,050	psi
External Pressure	12,090	psi
Maximum Uniaxial Bend Rating	104.2	°/100 ft
Reference String Length w 1.4 Design Factor	26,040	ft

	FIELD END TORQUE VA	LUES	
)	Min. Make-up torque	15,800	ft.lb
2	Opti. Make-up torque	17,050	ft.lb
o	Max. Make-up torque	18,300	ft.lb
i	Min. Shoulder Torque	1,580	ft.lb
i	Max. Shoulder Torque	12,640	ft.lb
t	Min. Delta Turn	-	Turns
t	Max. Delta Turn	0.200	Turns
	Maximum Operational Torque	20,800	ft.lb
	Maximum Torsional Value (MTV)	22,880	ft.lb

Need Help? Contact: tech.support@vam-usa.com Reference Drawing: 8087PP Rev.05 & 8087BP Rev.04

Date: 01/06/2020 Time: 10:56:21 AM

For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

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VAM® USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support Email: <u>tech.support@vam-usa.com</u>

#### **DWC Connection Data Sheet Notes:**

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- 4. DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- 10. Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

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Issued on: 09 Dec. 2020 by Logan Van Gorp



# **Connection Data Sheet**

OD	Weight	Wall Th.	Grade	API Drift:	Connection
7 5/8 in.	Nominal: 29.70 lb/ft	0.375 in.	P110EC	6.750 in.	VAM® SPRINT-FJ
	Plain End: 29.06 ft/lb				

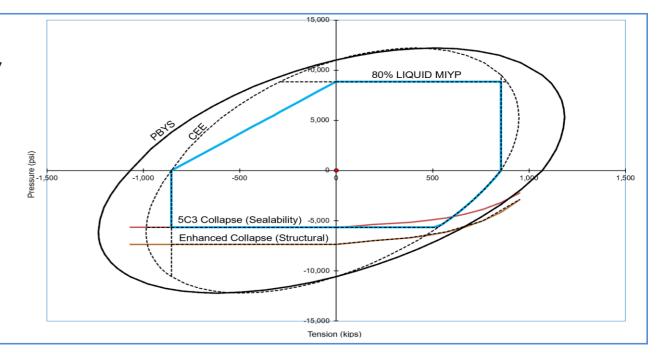
PIPE PROPERTIES		
Nominal OD	7.625	in.
Nominal ID	6.875	in.
Nominal Cross Section Area	8.541	sqin.
Grade Type	Enhanced	Collapse
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi

CONNECTION PRO	PERTIES	
Connection Type	Semi-Premium Into	egral Flush
Connection OD (nom):	7.654	in.
Connection ID (nom):	6.827	in.
Make-Up Loss	4.055	in.
Critical Cross Section	6.979	sqin.
Tension Efficiency	80.0	% of pipe
Compression Efficiency	80.0	% of pipe
Internal Pressure Efficiency	80.0	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMANCES		
Tensile Yield Strength	854	klb
Compression Resistance	854	klb
Max. Internal Pressure	8,610	psi
Structural Collapse Resistance	7,360	psi
Max. Structural Bending	57	°/100ft
Max. Bending with Sealability	10	°/100ft

TORQUE VALUES		
Min. Make-up torque	15,000	ft.lb
Opt. Make-up torque	16,500	ft.lb
Max. Make-up torque	18,000	ft.lb
Max. Torque with Sealability (MTS)	32,000	ft.lb

**VAM® SPRINT-FJ** is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



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17-23-32-A Sundry ID 2726179 Stray Cat 8-5 Fed Com 714H, 614H, 734H Lea NM98826 DEVON ENERGY PRODUCTION COMPANY LP 13-22fa 4-18-2023 LV.xlsm

#### Stray Cat 8-5 Fed Com 714H, 614H, 734H

9 5/8	S	urface csg in a	13 1/2	inch hole.		Design I	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A" <b>"B"</b>	40.00		j 55	btc btc	13.88	4.84	0.68	1,135 <b>0</b>	8	1.15	9.15	45,40 <b>0</b>
		.4#/g mud, 30min Sfc Csg Test		Tail Cmt	does not	circ to sfc.	Totals:	1,135				45,40
		Minimum Required Ceme										
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Di
Size 13 1/2	Volume 0.4887	Cmt Sx 533	CuFt Cmt 768	Cu Ft 555	% Excess 38	Mud Wt 9.00	<b>MASP</b> 3449	BOPE 5M				Hole-Cp 1.44
urst Frac Grad	lient(s) for Seg	ment(s) A, B = , b All > 0.7	70, OK.									
7 5/8		sing inside the	9 5/8			<u>Design I</u>				Int 1		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	29.70		p 110	vam sprint fj	2.71	1.27	1.64	10,597	1	3.09	2.13	314,73
"B"								0				0
	w/8	.4#/g mud, 30min Sfc Csg Test	psig: 1,403				Totals:	10,597				314,73
		The cement v	olume(s) are intend	led to achieve a top of	0	ft from su	rface or a	1135				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Di
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-C
8 3/4	0.1005	330	475	1074	-56	10.50	2785	3M				0.55
D M T = = 1/= ) .			6858				sum of sx	Σ CuFt				Σ%exce
U V I OOI(S):												
oy stage % :	t yld > 1.35	26	24				595	1342				25
by stage % : Class 'C' tail cm Tail cmt								1342		Dual 4		25
by stage % : Class 'C' tail cm Tail cmt 5 1/2	ca	ising inside the	7 5/8	Coupling	loint	Design Fac	ctors		P.O.	Prod 1		
Class 'C' tail cm  Tail cmt  5 1/2  Segment	ca #/ft		7 5/8	Coupling	Joint	Collapse	ctors Burst	Length	B@s	а-В	a-C	Weigh
Tail cmt 5 1/2 Segment "A"	ca #/ft 20.00	ising inside the	<b>75/8</b> p 110	dwc/c is	3.24	Collapse 2.56	ctors Burst 2.67	<b>Length</b> 10,097	3	<b>a-B</b> 5.05	4.84	<b>Weigl</b> 201,94
Tail cmt 5 1/2 Segment	ca #/ft 20.00 <b>20.00</b>	sing inside the Grade	<b>75/8</b> p 110 p 110			Collapse	ctors Burst 2.67 2.73	Length 10,097 1,153	_	а-В		Weigl 201,94 23,06
Tail cmt 5 1/2 Segment "A"	ca #/ft 20.00 <b>20.00</b>	sing inside the Grade .4#/g mud, 30min Sfc Csg Test	7 5/8  p 110 p 110 psig: 2,221	dwc/c is vam sprint sf	3.24 27.80	2.56 2.30	ctors Burst 2.67 2.73 Totals:	Length 10,097 1,153 21,589	3	<b>a-B</b> 5.05	4.84 4.34	Weigl 201,94 <b>23,06</b> 431,78
by stage %: Class 'C' tail cm  Tail cmt 51/2 Segment "A" "B"	ca #/ft 20.00 20.00 w/8	Ising inside the Grade -4#/g mud, 30min Sfc Csg Test The cement v	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intended	dwc/c is vam sprint sf	3.24 27.80 10397	Collapse 2.56 2.30 ft from su	Etors Burst 2.67 2.73 Totals:	Length 10,097 1,153 21,589 200	3	<b>a-B</b> 5.05	4.84 4.34	Weigl 201,94 23,06 431,78 overlap.
by stage %: Class 'C' tail cm  Tail cmt 5 1/2 Segment "A" "B"	ca #/ft 20.00 20.00 w/8	Ising inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intence 1 Stage	dwc/c is vam sprint sf led to achieve a top of Min	3.24 27.80 10397 1 Stage	Collapse 2.56 2.30  ft from su Drilling	Ctors Burst 2.67 2.73 Totals: rface or a Calc	Length 10,097 1,153 21,589 200 Req'd	3	<b>a-B</b> 5.05	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di
oy stage %:  Tail cmt  5 1/2  Segment  "A"  "B"  Hole  Size	ca #/ft 20.00 20.00 w/8 Annular Volume	using inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft	3.24 27.80 10397 1 Stage % Excess	2.56 2.30 ft from su Drilling Mud Wt	Etors Burst 2.67 2.73 Totals:	Length 10,097 1,153 21,589 200	3	<b>a-B</b> 5.05	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di Hole-C
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835	Ising inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intence 1 Stage	dwc/c is vam sprint sf led to achieve a top of Min	3.24 27.80 10397 1 Stage	Collapse 2.56 2.30  ft from su Drilling	Ctors Burst 2.67 2.73 Totals: rface or a Calc	Length 10,097 1,153 21,589 200 Req'd	3	<b>a-B</b> 5.05	4.84 4.34	Weigh 201,94 23,06 431,78
5 1/2 Segment "A" "B" Hole Size 6 3/4 Class 'C' tail cm	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835	using inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft	3.24 27.80 10397 1 Stage % Excess	2.56 2.30 ft from su Drilling Mud Wt	Ctors Burst 2.67 2.73 Totals: rface or a Calc	Length 10,097 1,153 21,589 200 Req'd	3	<b>a-B</b> 5.05	4.84 4.34	Weigh 201,94 23,06 431,78 overlap. Min Dis Hole-Cp
by stage %: Class 'C' tail cm  Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 Class 'C' tail cm	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835	using inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft	3.24 27.80 10397 1 Stage % Excess	Collapse 2.56 2.30 ft from su Drilling Mud Wt 9.00	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP	Length 10,097 1,153 21,589 200 Req'd	3 3	<b>a-B</b> 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di: Hole-C <sub>F</sub>
by stage %: Class 'C' tail cm  Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 class 'C' tail cm	#/ft 20.00 20.00 w/8 Annular Volume 0.0835 t yld > 1.35	using inside the Grade  Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt	dwc/c is vam sprint sf led to achieve a top of Min Cu Ft 937	3.24 27.80 10397 1 Stage % Excess 25	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP	Length 10,097 1,153 21,589 200 Req'd BOPE	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di: Hole-Cr 0.35
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 2 #N/A 0 Segment	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835	using inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937	3.24 27.80 10397 1 Stage % Excess	Collapse 2.56 2.30 ft from su Drilling Mud Wt 9.00	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP	Length 10,097 1,153 21,589 200 Req'd BOPE	3 3	<b>a-B</b> 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di: Hole-Cp 0.35
Tail cmt 5 1/2 Segment "A" Hole Size 6 3/4 Llass 'C' tail cm	#/ft 20.00 20.00 w/8 Annular Volume 0.0835 t yld > 1.35	using inside the Grade  Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937  Coupling 0.00	3.24 27.80 10397 1 Stage % Excess 25	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP	Length 10,097 1,153 21,589 200 Req'd BOPE	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di Hole-Cl 0.35
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 2 #N/A 0 Segment	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835 tyld > 1.35	using inside the Grade  Grade  .4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737	7 5/8  p 110 p 110 p 110 sig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937	3.24 27.80 10397 1 Stage % Excess 25	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP	Length 10,097 1,153 21,589 200 Req'd BOPE	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigi 201,94 23,06 431,74 overlap. Min Di Hole-Ci 0.35
Tail cmt 5 1/2 Segment "A" Hole Size 6 3/4 Llass 'C' tail cm	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835 tyld > 1.35	using inside the Grade  Grade  .4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737  Grade	7 5/8  p 110 p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175  5 1/2	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937  Coupling 0.00 0.00	3.24 27.80 10397 1 Stage % Excess 25 #N/A	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00  Design I Collapse	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP  Factors Burst	Length 10,097 1,153 21,589 200 Req'd BOPE  Length 0 0	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di Hole-C <sub>I</sub> 0.35
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 class 'C' tail cm  #N/A 0 Segment "A" "B"	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835 tyld > 1.35	using inside the Grade  4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737  Grade  4#/g mud, 30min Sfc Csg Test Cmt vol ca	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175  5 1/2  psig:	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937  Coupling 0.00 0.00 his csg, TOC intended	3.24 27.80 10397 1 Stage % Excess 25 #N/A	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00  Design I Collapse	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a	Length 10,097 1,153 21,589 200 Req'd BOPE  Length 0 0 #N/A	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,74 overlap. Min Di Hole-Ci 0.35  Weigl 0 0 overlap.
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 class 'C' tail cm  #N/A 0 Segment "A" "B"  Hole Hole Hole Hole Hole Hole Hole Hol	#/ft 20.00 20.00 20.00 w/8  Annular Volume 0.0835 tyld > 1.35  #/ft	using inside the Grade  .4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737  Grade  .4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175  5 1/2  psig: lc below includes ti 1 Stage	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937  Coupling 0.00 0.00 his csg, TOC intended Min	3.24 27.80 10397 1 Stage % Excess 25 #N/A	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00  Design I Collapse	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a Calc	Length 10,097 1,153 21,589 200 Req'd BOPE  Length 0 0 #N/A Req'd	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di: Hole-Cr 0.35  Weigl 0 0 overlap. Min Di:
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 Class 'C' tail cm  #N/A 0 Segment "A" "B"	ca #/ft 20.00 20.00 w/8 Annular Volume 0.0835 tyld > 1.35	James Inside the Grade  James Inside the Grade	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage Cuft Cmt 1175  5 1/2  psig: Ic below includes ti 1 Stage Cuft Cmt	dwc/c is vam sprint sf  ded to achieve a top of Min Cu Ft 937  Coupling 0.00 0.00  his csg, TOC intended Min Cu Ft	3.24 27.80 10397 1 Stage % Excess 25 #N/A #N/A	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00  Design I Collapse	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a	Length 10,097 1,153 21,589 200 Req'd BOPE  Length 0 0 #N/A	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigl 201,94 23,06 431,78 overlap. Min Di: Hole-Cr 0.35 Weigl 0 0 0 overlap.
Tail cmt 5 1/2 Segment "A" "B"  Hole Size 6 3/4 dlass 'C' tail cm  #N/A 0 Segment "A" "B"  Hole	#/ft 20.00 20.00 20.00 w/8  Annular Volume 0.0835 tyld > 1.35  #/ft	using inside the Grade  .4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 737  Grade  .4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	7 5/8  p 110 p 110 psig: 2,221 olume(s) are intend 1 Stage CuFt Cmt 1175  5 1/2  psig: lc below includes ti 1 Stage	dwc/c is vam sprint sf  led to achieve a top of Min Cu Ft 937  Coupling 0.00 0.00  his csg, TOC intended Min Cu Ft 0	3.24 27.80 10397 1 Stage % Excess 25 #N/A	Collapse 2.56 2.30  ft from su Drilling Mud Wt 9.00  Design I Collapse	Etors Burst 2.67 2.73 Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a Calc	Length 10,097 1,153 21,589 200 Req'd BOPE  Length 0 0 #N/A Req'd	3 3 3	a-B 5.05 <b>5.16</b>	4.84 4.34	Weigi 201,94 23,06 431,73 overlap. Min Di Hole-Ci 0.35  Weigi 0 0 overlap. Min Di

Carlsbad Field Office 4/18/2023

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**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 208798

#### **CONDITIONS**

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	208798
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By		Condition Date
pkautz	None	4/28/2023