

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Sundry Print Reports
04/05/2023

Well Name: SAKER 6-7 FEDERAL Well Location: T24S / R35E / SEC 6 / County or Parish/State:

COM LOT 1 /

Well Number: 38H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMNM14164 Unit or CA Name: Unit or CA Number:

US Well Number: 3002548939 Well Status: Approved Application for Operator: OXY USA

Permit to Drill INCORPORATED

Notice of Intent

Sundry ID: 2714730

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 02/08/2023 Time Sundry Submitted: 12:34

Date proposed operation will begin: 03/31/2023

Procedure Description: OXY USA Inc. respectfully requests approved to amend the subject well AAPD BHL and drill plan casing, cementing and mud programs. See the attached well plat with the update BHL and the attached drilling files for reference. The surface hole location is not changing. OLD BHL: 20' FSL 331' FEL P-7-T24S-R35E New BHL: 20' FSL 550' FEL P-7-T24S-R35E

NOI Attachments

Procedure Description

 $Saker 6_7 Fed Com 38 H_TNS Wedge 461_5.500 in_20.00 ppf_P110 CY_20230208123402. pdf$

Saker6_7FedCom38H_TNSWedge441_5.500in_20.00ppf_P110CY_20230208123356.pdf

Saker6_7FedCom38H_TNSWedge425_5.500in_20.00ppf_P110CY_20230208123347.pdf

Saker6_7FedCom38H_StandardSL1TiebackDetails_20230208123341.pdf

Saker6_7FedCom38H_13inADAPT_10.75in_7.625in_10x10_20230208123334.pdf

Saker6_7FedCom38H_DirectPlan_20230208123325.pdf

Saker6_7FedCom38H_DirectPlot_20230208123318.pdf

Saker6_7FedCom38H_DrillPlan_20230208123304.pdf

 $Saker 6_7 Fed Com 38 H_C 102_20230208123139. pdf$

eived by OCD: 4/6/2023 2:13:24 PM Well Name: SAKER 6-7 FEDERAL

COM

Well Location: T24S / R35E / SEC 6 /

LOT 1/

County or Parish/State:

Zip:

Well Number: 38H

Type of Well: OIL WELL

Allottee or Tribe Name:

Page 2 of

Lease Number: NMNM14164

Unit or CA Name:

Unit or CA Number:

US Well Number: 3002548939

Well Status: Approved Application for Permit to Drill

Operator: OXY USA **INCORPORATED**

Conditions of Approval

Additional

SAKER_6_7_FED_COM_38H___SUNDRY_COA_20230405101520.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: LESLIE REEVES Signed on: FEB 08, 2023 12:32 PM

Name: OXY USA INCORPORATED

Title: Advisor Regulatory

Street Address: 5 GREENWAY PLAZA, SUITE 110

City: HOUSTON State: TX

Phone: (713) 497-2492

Email address: LESLIE_REEVES@OXY.COM

Field

Representative Name:

Street Address:

City:

Phone:

Email address:

BLM Point of Contact

Signature: KEITH IMMATTY

BLM POC Name: KEITH P IMMATTY BLM POC Title: ENGINEER

State:

BLM POC Phone: 5759884722 BLM POC Email Address: KIMMATTY@BLM.GOV

Disposition: Approved Disposition Date: 04/05/2023

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PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

All previous COAs still apply.

OPERATOR'S NAME: OXY USA INC.

LEASE NO.: NMNM14164

WELL NAME & NO.: SAKER 6-7 FEDERAL COM 38H

SURFACE HOLE FOOTAGE: 180'/N & 850'/E BOTTOM HOLE FOOTAGE 20'/S & 550'/E

LOCATION: Section 6, T.24 S., R.35 E. COUNTY: Lea County, New Mexico

COA

H2S	• Yes	O No	
Potash	None	Secretary	© R-111-P
Cave/Karst Potential	• Low	Medium	O High
Cave/Karst Potential	Critical		
Variance	O None	• Flex Hose	Other
Wellhead	Conventional	• Multibowl	O Both
Other	☐4 String Area	☐ Capitan Reef	□WIPP
Other	☐ Fluid Filled		☐ Pilot Hole
Special Requirements	☐ Water Disposal	☑ COM	□ Unit

A. CASING

Alternate Casing Design:

- 1. The 10-3/4 inch surface casing shall be set at approximately 836 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite and above the salt) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours

- after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The **7-5/8** inch intermediate casing shall be set at approximately **11,131** feet. **Ensure** casing is atleast half full during run for collapse safety factor. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

Option 1 (Single Stage):

Cement to surface. If cement does not circulate see B.1.a, c-d above.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Option 2:

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:
 - Cement to surface. If cement does not circulate, contact the appropriate BLM office.

Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down 10-3/4" X 7-5/8" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 7-5/8" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

3. The 5-1/2 inch production casing shall be set at approximately 22,125 feet. Operator to run production casing as liner during drilling operations and bring in workover rig to tie-in production casing to surface. The minimum required fill of cement behind the 5-1/2 inch production casing is:

Option 1 (Single Stage):

Cement should tie-back at least 100 feet into previous casing string.
 Operator shall provide method of verification.

Option 2:

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:
 - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Eddy County
 Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.

- Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
- BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.

- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
- e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time, except the casing pressure test can be initiated immediately after bumping the plug (only applies to single stage cement jobs).
 - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
 - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
 - e. The results of the test shall be reported to the appropriate BLM office.

- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

KPI - 04/05/2023

<u>District I</u> 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 District III 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

Section Township Range

Lot Idn

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

County

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WELL LOCATION AND ACREAGE DEDICATION PLAT

Г	¹ API Number	² Pool Code					
[3	80-025-48939	2220	ANTELOPE RIDGE; WOLFCAMP				
Г	4 Property Code	5 P	roperty Name	6 Well Number			
3	30848	SAKEF	38H				
Г	⁷ OGRID No.	8 O	perator Name	⁹ Elevation			
L	16696	OX	Y USA INC.	3450.8' (NAVD 88)			

¹⁰ Surface Location

1	6	24S	35Ē		180	NORTH	850	EAST	LEA
			11	Bottom H	ole Location I	f Different From	Surface		

North/South line

Т

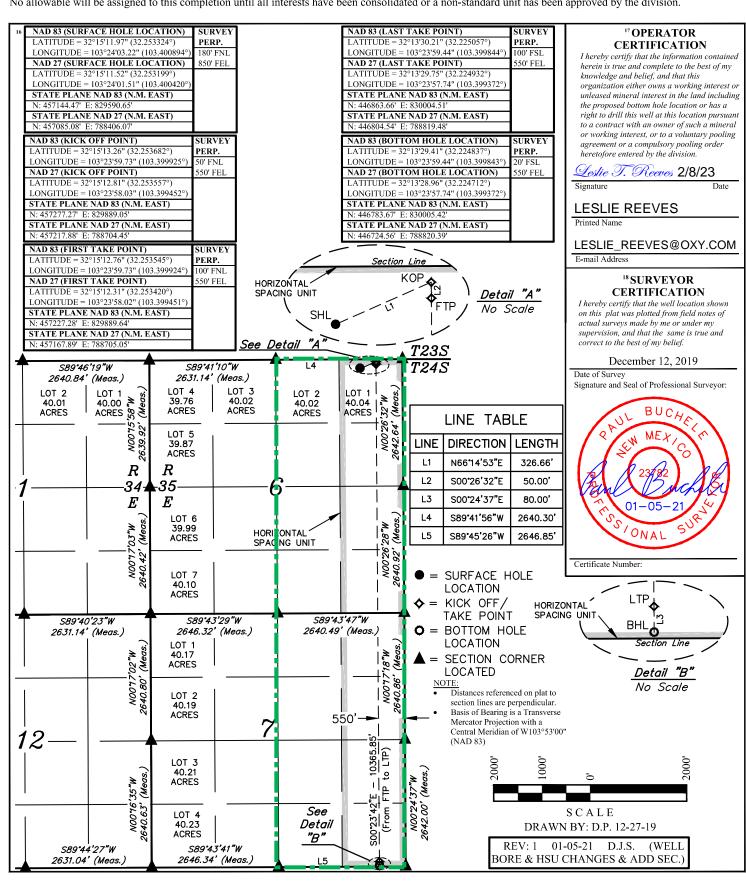
Feet from the

East/West line

UL or lot no. P	Secti 7	ion	Township 24S	Range 35E	Lot Idn	Fo	eet from the 20	North/South line SOUTH	Feet from the 550	East/West line EAST	County LEA
12 Dedicated Acr 640.06	es	¹³ Jo	oint or Infill	14 Conso	olidation Code		15 Order No.				

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

Feet from the



Oxy USA Inc. - Saker 6_7 Fed Com 38H Drill Plan

1. Geologic Formations

TVD of Target (ft):	12043	Pilot Hole Depth (ft):	
Total Measured Depth (ft):	22125	Deepest Expected Fresh Water (ft):	776

Delaware Basin

Formation	MD-RKB (ft)	TVD-RKB (ft)	Expected Fluids
Rustler	776	776	
Salado	1116	1116	Salt
Castile	3426	3426	Salt
Delaware	5288	5288	Oil/Gas/Brine
Bell Canyon	5336	5336	Oil/Gas/Brine
Cherry Canyon	6220	6220	Oil/Gas/Brine
Brushy Canyon	7596	7596	Losses
Bone Spring	8765	8765	Oil/Gas
Bone Spring 1st	9936	9935	Oil/Gas
Bone Spring 2nd	10405	10399	Oil/Gas
Bone Spring 3rd	11434	11412	Oil/Gas
Wolfcamp	11873	11758	Oil/Gas
Penn			Oil/Gas
Strawn	_	_	Oil/Gas

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program

		M	ID	T۱	/D				
	Hole	From	То	From	То	Csg.	Csg Wt.		
Section	Size (in)	(ft)	(ft)	(ft)	(ft)	OD (in)	(ppf)	Grade	Conn.
Surface	14.75	0	836	0	836	10.75	45.5	J-55	ВТС
Intermediate	9.875	0	6650	0	6631	7.625	26.4	L-80 HC	BTC
Intermediate	9.875	6650	11150	6631	11131	7.625	29.7	L-80 HC	ВТС
Production	6.75	11050	22125	11031	12043	5.5	20	P-110	Wedge 461

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h

^{*}Oxy requests the option to run production casing with DQX, TORQ DQW, Wedge 425, Wedge 461, and/or Wedge 441 connections to accommodate hole conditions or drilling operations.

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All Casing SF Values will meet or exceed									
those below									
SF	SF Body SF Joint SF								
Collapse	Burst	Tension	Tension						
1.125	1.2	1.4	1.4						

Annular Clearance Variance Request

As per the agreement reached in the Oxy/BLM face-to-face meeting on Feb 22, 2018, Oxy requests permission to allow deviation from the 0.422" annular clearance requirement from Onshore Order #2 under the following conditions:

- 1. Annular clearance to meet or exceed 0.422" between intermediate casing ID and production casing coupling only on the first 500' overlap between both casings.
- 2. Annular clearance less than 0.422" is acceptable for the curve and lateral portions of the production open hole section.

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does casing meet API specifications? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	Y
Does the above casing design meet or exceed BLM's minimum standards?	Y
If not provide justification (loading assumptions, casing design criteria).	1
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching	Y
the collapse pressure rating of the casing?	1
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back	
500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there strings cemented to surface?	

3. Cementing Program

Section	Stage	Slurry:	Sacks	Yield (ft^3/ft)	Density (lb/gal)	Excess:	тос	Placement	Description
Surface	1	Surface - Tail	699	1.33	14.8	100%	1	Circulate	Class C+Accel.
Int.	1	Intermediate 1S - Tail	452	1.65	13.2	5%	7,846	Circulate	Class H+Accel., Disper., Salt
Int.	2	Intermediate 2S - Tail BH	1215	1.71	13.3	25%	-	Bradenhead	Class C+Accel.
Prod.	1	Production - Tail	737	1.38	13.2	10%	11,050	Circulate	Class H+Ret., Disper., Salt

Cement Top and Liner Overlap

• Oxy is requesting permission to have minimum fill of cement behind the 5-1/2" production liner to be 100 ft into previous casing string

The reason for this is so that we can come back and develop shallower benches from the same 7.625" mainbore in the future

• Cement will be brought to the top of this liner hanger

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Offline Cementing

Oxy requests a variance to cement the 9.625" and/or 7.625" intermediate casing strings offline in accordance to the approved variance, EC Tran 461365.

The summarized operational sequence will be as follows:

Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe). Land casing.

Fill pipe with kill weight fluid, and confirm well is static.

If well Oxy requests a variance to cement the 9.625" and/or 7.625" intermediate casing strings offline in accordance to the approved variance, EC Tran 461365.

The summarized operational sequence will be as follows:

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe).
- 2. Land casing.
- 3. Fill pipe with kill weight fluid, and confirm well is static.
 - a. If well is not static notify BLM and kill well.
 - b. Once well is static notify BLM with intent to proceed with nipple down and offline cementing.
- 4. Set and pressure test annular packoff.
- 5. After confirmation of both annular barriers and internal barriers, nipple down BOP and install cap flange. If any barrier fails to test, the BOP stack will not be nippled down until after the cement job is completed.
- 6. Skid rig to next well on pad.
- 7. Confirm well is static before removing cap flange.
- 8. If well is not static notify BLM and kill well prior to cementing or nippling up for further remediation.
- 9. Install offline cement tool.
- 10. Rig up cement equipment.
 - a. Notify BLM prior to cement job.
- 11. Perform cement job.
- 12. Confirm well is static and floats are holding after cement job.
- 13. Remove cement equipment, offline cement tools and install night cap with pressure gauge for monitoring.

Oxy requests permission to adjust the CBL requirement after bradenhead cement jobs, on 7-5/8" intermediate casings, as per the agreement reached in the OXY/BLM meeting on September 5, 2019.

Three string wells:

- CBL will be required on one well per pad
- If the pumped volume of cement is less than permitted in the APD, BLM will be notified and a CBL may be run
- Echometer will be used after bradenhead cement job to determine TOC before pumping top-out cement

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4. Pressure Control Equipment

BOP installed and tested before drilling which hole?	Size?	Min. Required WP		Туре	1	Tested to:	Deepest TVD Depth (ft) per Section:	
		5M		Annular	✓	70% of working pressure		
9.875" Hole				Blind Ram	✓		11131	
	13-5/8"	5M		Pipe Ram		250 psi / 5000 psi		
		SIVI	Double Ram		✓	230 psi / 3000 psi		
			Other*					
		5M	Annular		\	100% of working pressure		
				Blind Ram	\			
6.75" Hole	13-5/8"	1014		Pipe Ram		250 poi / 10000 poi	12043	
		10M		Double Ram		250 psi / 10000 psi		
			Other*					

*Specify if additional ram is utilized

Per BLM's Memorandum No. NM-2017-008: *Decision and Rationale for a Variance Allowing the Use of a 5M Annular Preventer with a 10M BOP Stack,* Oxy requests to employ a 5M annular with a 10M BOPE stack in the pilot and lateral sections of the well and will ensure that two barriers to flow are maintained at all times. Please see attached Well Control Plan.

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold.

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Formation integrity test will be performed per Onshore Order #2.

On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.i.

A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart.

Y Are anchors required by manufacturer?

A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per Onshore Order #2 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015.

See attached schematics.

BOP Break Testing Request

Oxy requests permission to adjust the BOP break testing requirements as per the agreement reached in the OXY/BLM meeting on September 5, 2019.

BOP break test under the following conditions:

- After a full BOP test is conducted
- When skidding to drill an intermediate section where ICP is set into the third Bone Spring or shallower.

If the kill line is broken prior to skid, two tests will be performed.

- 1) Wellhead flange, co-flex hose, kill line connections and upper pipe rams
- 2) Wellhead flange, HCR valve, check valve, upper pipe rams

If the kill line is not broken prior to skid, only one test will be performed.

1) Wellhead flange, co-flex hose, check valve, upper pipe rams

Oxy will use Cameron ADAPT wellhead system that uses an OEC top flange connection. This connection has been fully vetted and verified by API to Spec 6A and carries an API monogram.

Page 6 of 8

Created On: 1/26/2023 at 1:22 PM

5. Mud Program

Saatian	Depth - MD		Depth -	TVD	Tymo	Weight	Viceosity	Water
Section	From (ft)	To (ft)	From (ft)	To (ft)	Туре	(ppg)	Viscosity	Loss
Surface	0	836	0	836	Water-Based Mud	8.6 - 8.8	40-60	N/C
Intermediate	836	11150	836	11131	Saturated Brine-Based or Oil-Based Mud	8.0 - 10.0	35-45	N/C
Production	11150	22125	11131	12043	Water-Based or Oil- Based Mud	9.5 - 12.5	38-50	N/C

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls, Drilling Paper, Salt Water Clay, CACL2. Oxy will use a closed mud system.

What will be used to monitor the	DVT/NAD Totas (Visual Maxitarias
loss or gain of fluid?	PVT/MD Totco/Visual Monitoring

6. Logging and Testing Procedures

	00 0
Loggi	ing, Coring and Testing.
Yes	Will run GR from TD to surface (horizontal well – vertical portion of hole).
res	Stated logs run will be in the Completion Report and submitted to the BLM.
No	Logs are planned based on well control or offset log information.
No	Drill stem test? If yes, explain
No	Coring? If yes, explain

Addit	ional logs planned	Interval
No	Resistivity	
No	Density	
Yes	CBL	Production string
Yes	Mud log	Bone Spring – TD
No	PEX	

7. Drilling Conditions

Condition	Specify what type and where?
BH Pressure at deepest TVD	7828 psi
Abnormal Temperature	No
BH Temperature at deepest TVD	177°F

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for zonal

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

DLIVI.	
N	H2S is present
Υ	H2S Plan attached

8. Other facets of operation

	Yes/No
Will the well be drilled with a walking/skidding operation? If yes, describe.	
We plan to drill the 3 well pad in batch by section: all surface sections, intermediate	Vas
sections and production sections. The wellhead will be secured with a night cap whenever	Yes
the rig is not over the well.	
Will more than one drilling rig be used for drilling operations? If yes, describe.	
Oxy requests the option to contract a Surface Rig to drill, set surface casing, and cement for	
this well. If the timing between rigs is such that Oxy would not be able to preset surface,	Yes
the Primary Rig will MIRU and drill the well in its entirety per the APD. Please see the	
attached document for information on the spudder rig.	

Total Estimated Cuttings Volume: 1640 bbls

Attachments

- _x__ Directional Plan
- _x__ H2S Contingency Plan
- _x__ Flex III Attachments
- _x__ Spudder Rig Attachment
- _x__ Premium Connection Specs

9. Company Personnel

Name	<u>Title</u>	Office Phone	Mobile Phone
Garrett Granier	Drilling Engineer	713-513-6633	832-265-0581
Derek Adam	Drilling Engineer Supervisor	713-366-5170	916-802-8873
Casey Martin	Drilling Superintendent	713-497-2530	337-764-4278
Kevin Threadgill	Drilling Manager	713-366-5958	361-815-0788

PROJECT DETAILS: NM DIRECTIONAL PLANS (NAD 1983)

OXY

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Saker 6_7

Well: Saker 6_7 Fed Com 38H

Wellbore: Wellbore #1
Design: Permitting Plan

Geodetic System: US State Plane 1983

Datum: North American Datum 1983

Ellipsoid: GRS 1980

Zone: New Mexico Eastern Zone

System Datum: Mean Sea Level

		WELL DETAI	ILS: Saker 6_7 Fed	i Com 38H				2000—		Hold	10°	Tang	ent				
+N/-S 0.00	+E/-W 0.00	Northing 457144.47	3450.80 Easting 829590.65	Latittude 32.253324		Longitude 03.400894		1000		Build 1°/10	10'	\	KOP,	Build	& Turn 1	10°/100'	
		S	ECTION DETAILS					_		Sulla 1710		X			TP		
MD 0.00 9345.00 10344.91 11250.09	Inc Az 0.00 0.00 0.00 0.00 10.00 58.00 10.00 58.00	0 0.00 0.00 0 9345.00 0.00 5 10339.84 46.05 5 11231.27 129.21	0.00 0.00 73.85 207.21	Dleg TFace 0.00 0.00 0.00 0.00 1.00 58.05 0.00 0.00	0.00 0.00 Bu -43.06 Ho -120.82 KC	nnotation uild 1°/100' old 10° Tangent DP, Build & Turn 10°/100'		0-				*				ding Dai	
12190.79 22124.79	88.88 179.36 88.88 179.36	6 11849.13 -429.28 6 12043.30 -10360.78		0.00 121.09 0.00 0.00	441.13 La 10369.08 TD	nding Point) at 22124.79' MD		-1000							Land	ding Poi	nt
0			٦	T ★ M	True	to Grid North North: -0.50° North: 6.10°		-2000— 			Line	g Area					
1000			-		Strengtl Dip	lagnetic Field h: 47831.2nT Angle: 59.87° 12/31/2019	100 ft/in)	-3000 			Lease Line	Producing					
2000—				Τ	Model	: HDGM_FILE	1(+) (20	-4000 -									
3000—							South(-)/North(+) (2000 ft/in)	-5000									
4000							Sout	-6000									
5000								-7000 									
6000								-8000 -									
5000 —								-9000 									
8000—							-	-10000 									
_			Build 1°/100'					_				РВНІ		TD at	22124.7	'9' MD -	
9000—							-	-11000 —	-2000	-1000	-	++	++	10	00	2000	
=			Hold 10° Ta	angent					2000				(+)		00 0 ft/in		
10000—			KOP, Build &	. Turn 10°/100	0'						\		` /			,	
11000			Landing Po									.464	70' '	45			
_										TD	at 22	2124.	79' N	1D	PBI	ΗL	
12000															4		

4000

5000

Vertical Section at 177.71° (2000 ft/in)

6000

7000

8000

9000

10000

11000

12000

-1000

1000

13000-

PRD NM DIRECTIONAL PLANS (NAD 1983) Saker 6_7 Saker 6_7 Fed Com 38H

Wellbore #1

Plan: Permitting Plan

Standard Planning Report

11 December, 2022

Planning Report

Database: HOPSPP

Company: ENGINEERING DESIGNS

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Saker 6_7

Well: Saker 6_7 Fed Com 38H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well Saker 6_7 Fed Com 38H

RKB=26.5' @ 3477.30ft RKB=26.5' @ 3477.30ft

Grid

Minimum Curvature

Project PRD NM DIRECTIONAL PLANS (NAD 1983)

Map System: US State Plane 1983

Geo Datum: North American Datum 1983
Map Zone: New Mexico Eastern Zone

System Datum: Mea

Mean Sea Level

Using geodetic scale factor

Site Saker 6_7

 Site Position:
 Northing:
 457,094.74 usft
 Latitude:
 32.253262

 From:
 Map
 Easting:
 826,474.44 usft
 Longitude:
 -103.410974

Position Uncertainty: 1.00 ft Slot Radius: 13.200 in

Well Saker 6_7 Fed Com 38H **Well Position** +N/-S 0.00 ft Northing: 457.144.47 usf Latitude: 32.253324 829,590.65 usf +E/-W Easting: Longitude: -103.400894 0.00 ft **Position Uncertainty** 1.00 ft Wellhead Elevation: ft **Ground Level:** 3,450.80 ft

Grid Convergence: $0.50\,^\circ$

 Wellbore
 Wellbore #1

 Magnetics
 Model Name
 Sample Date (°)
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 HDGM FILE
 12/31/2019
 6.60
 59.87
 47,831.20000000

Design Permitting Plan Audit Notes: Version: Phase: **PROTOTYPE** Tie On Depth: 0.00 Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (ft) (ft) (ft) (°) 0.00 0.00 0.00 177.71

Plan Survey Tool Program
Date 12/11/2022

Depth From (ft)
Depth To (ft)
Survey (Wellbore)
Tool Name
Remarks

1 0.00 22,124.79 Permitting Plan (Wellbore #1)
B001Mb_MWD+HRGM
OWSG MWD + HRGM

Plan Sections Measured Vertical Dogleg Build Turn Depth Depth +N/-S Inclination **Azimuth** +E/-W Rate Rate Rate **TFO** (ft) (ft) (°/100ft) (°/100ft) (°/100ft) (ft) (°) (°) (ft) (°) **Target** 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 9,345.00 0.00 0.00 9,345.00 0.00 0.00 0.00 0.00 0.00 0.00 10,344.91 10.00 58.05 10,339.84 46.05 73.85 1.00 1.00 0.00 58.05 11,250.09 10.00 58.05 11,231.27 129.21 207.21 0.00 0.00 0.00 0.00 12,190.79 88.88 179.36 11,849.13 -429.28 304.67 10.00 8.39 12.90 121 09 22,124.79 88.88 179.36 12,043.30 -10,360.78 414.77 0.00 0.00 0.00 0.00 PBHL (Saker 6_7

Planning Report

Database: Company: Project: HOPSPP

ENGINEERING DESIGNS

PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Saker 6_7

Well: Saker 6_7 Fed Com 38H

Wellbore: Wellbore #1
Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well Saker 6_7 Fed Com 38H

RKB=26.5' @ 3477.30ft RKB=26.5' @ 3477.30ft

Grid

esigii.		all							
Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00 600.00	0.00 0.00	0.00 0.00	500.00 600.00	0.00	0.00 0.00	0.00 0.00	0.00	0.00	0.00
				0.00			0.00	0.00	0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	0.00	0.00	1,100.00	0.00	0.00	0.00	0.00	0.00	0.00
1,200.00	0.00	0.00	1,200.00	0.00	0.00	0.00	0.00	0.00	0.00
1,300.00	0.00	0.00	1,300.00	0.00	0.00	0.00	0.00	0.00	0.00
1,400.00	0.00	0.00	1,400.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.00	1,500.00	0.00	0.00	0.00	0.00	0.00	0.00
1,600.00	0.00	0.00	1,600.00	0.00	0.00	0.00	0.00	0.00	0.00
1,700.00	0.00	0.00	1,700.00	0.00	0.00	0.00	0.00	0.00	0.00
1,800.00	0.00	0.00	1,800.00	0.00	0.00	0.00	0.00	0.00	0.00
1,900.00	0.00	0.00	1,900.00	0.00	0.00	0.00	0.00	0.00	0.00
2,000.00	0.00	0.00	2,000.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	0.00	0.00	2,100.00	0.00	0.00	0.00	0.00	0.00	0.00
2,200.00	0.00	0.00	2.200.00	0.00	0.00	0.00	0.00	0.00	0.00
2,300.00	0.00	0.00	2,300.00	0.00	0.00	0.00	0.00	0.00	0.00
2,400.00	0.00	0.00	2,400.00	0.00	0.00	0.00	0.00	0.00	0.00
2,500.00	0.00	0.00	2,500.00	0.00	0.00	0.00	0.00	0.00	0.00
2,600.00	0.00	0.00	2,600.00	0.00	0.00	0.00	0.00	0.00	0.00
2,700.00	0.00	0.00	2,700.00	0.00	0.00	0.00	0.00	0.00	0.00
2,800.00	0.00	0.00	2,800.00	0.00	0.00	0.00	0.00	0.00	0.00
2,900.00	0.00	0.00	2,900.00	0.00	0.00	0.00	0.00	0.00	0.00
3,000.00	0.00	0.00	3,000.00	0.00	0.00	0.00	0.00	0.00	0.00
3,100.00	0.00	0.00	3,100.00	0.00	0.00	0.00	0.00	0.00	0.00
3,200.00	0.00	0.00	3,200.00	0.00	0.00	0.00	0.00	0.00	0.00
3,300.00	0.00	0.00	3,300.00	0.00	0.00	0.00	0.00	0.00	0.00
3,400.00	0.00	0.00	3,400.00	0.00	0.00	0.00	0.00	0.00	0.00
3,500.00	0.00	0.00	3,500.00	0.00	0.00	0.00	0.00	0.00	0.00
3,600.00	0.00	0.00	3,600.00	0.00	0.00	0.00	0.00	0.00	0.00
3,700.00	0.00	0.00	3,700.00	0.00	0.00	0.00	0.00	0.00	0.00
3,800.00	0.00	0.00	3,800.00	0.00	0.00	0.00	0.00	0.00	0.00
3,900.00	0.00	0.00	3,900.00	0.00	0.00	0.00	0.00	0.00	0.00
4,000.00	0.00	0.00	4,000.00	0.00	0.00	0.00	0.00	0.00	0.00
4,100.00	0.00	0.00	4,100.00	0.00	0.00	0.00	0.00	0.00	0.00
4,200.00	0.00	0.00	4,200.00	0.00	0.00	0.00	0.00	0.00	0.00
4,300.00	0.00	0.00	4,300.00	0.00	0.00	0.00	0.00	0.00	0.00
4,400.00	0.00	0.00	4,400.00	0.00	0.00	0.00	0.00	0.00	0.00
			,						
4,500.00	0.00	0.00	4,500.00	0.00	0.00	0.00	0.00	0.00	0.00
4,600.00	0.00	0.00	4,600.00	0.00	0.00	0.00	0.00	0.00	0.00
4,700.00	0.00	0.00	4,700.00	0.00	0.00	0.00	0.00	0.00	0.00
4,800.00	0.00	0.00	4,800.00	0.00	0.00	0.00	0.00	0.00	0.00
4,900.00	0.00	0.00	4,900.00	0.00	0.00	0.00	0.00	0.00	0.00
5,000.00	0.00	0.00	5,000.00	0.00	0.00	0.00	0.00	0.00	0.00
5,100.00	0.00	0.00	5,100.00	0.00	0.00	0.00	0.00	0.00	0.00
5,200.00	0.00	0.00	5,200.00	0.00	0.00	0.00	0.00	0.00	0.00
5,300.00	0.00	0.00	5,300.00	0.00	0.00	0.00	0.00	0.00	0.00
5,400.00	0.00	0.00	5,400.00	0.00	0.00	0.00	0.00	0.00	0.00
3,400.00	0.00	0.00	5,700.00	0.00	0.00	0.00	0.00	0.00	0.00

Planning Report

Database: Company: HOPSPP

ENGINEERING DESIGNS

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Well Saker 6_7 Fed Com 38H

RKB=26.5' @ 3477.30ft RKB=26.5' @ 3477.30ft

Grid

Design:	Permitting Pla	an							
Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
5,500.00	0.00	0.00	5,500.00	0.00	0.00	0.00	0.00	0.00	0.00
5,600.00	0.00	0.00	5,600.00	0.00	0.00	0.00	0.00	0.00	0.00
5,700.00	0.00	0.00	5,700.00	0.00	0.00	0.00	0.00	0.00	0.00
5,800.00	0.00	0.00	5,800.00	0.00	0.00	0.00	0.00	0.00	0.00
5,900.00	0.00	0.00	5,900.00	0.00	0.00	0.00	0.00	0.00	0.00
6,000.00	0.00	0.00	6,000.00	0.00	0.00	0.00	0.00	0.00	0.00
6,100.00	0.00	0.00	6,100.00	0.00	0.00	0.00	0.00	0.00	0.00
6,200.00	0.00	0.00	6,200.00	0.00	0.00	0.00	0.00	0.00	0.00
6,300.00	0.00	0.00	6,300.00	0.00	0.00	0.00	0.00	0.00	0.00
6,400.00	0.00	0.00	6,400.00	0.00	0.00	0.00	0.00	0.00	0.00
6,500.00	0.00	0.00	6,500.00	0.00	0.00	0.00	0.00	0.00	0.00
6,600.00	0.00	0.00	6,600.00	0.00	0.00	0.00	0.00	0.00	0.00
6,700.00	0.00	0.00	6,700.00	0.00	0.00	0.00	0.00	0.00	0.00
6,800.00	0.00	0.00	6.800.00	0.00	0.00	0.00	0.00	0.00	0.00
6,900.00	0.00	0.00	6,900.00	0.00	0.00	0.00	0.00	0.00	0.00
7,000.00	0.00	0.00	7,000.00	0.00	0.00	0.00	0.00	0.00	0.00
7,100.00	0.00	0.00	7,100.00	0.00	0.00	0.00	0.00	0.00	0.00
7,200.00	0.00	0.00	7,200.00	0.00	0.00	0.00	0.00	0.00	0.00
7,300.00	0.00	0.00	7,300.00	0.00	0.00	0.00	0.00	0.00	0.00
7,400.00	0.00	0.00	7,400.00	0.00	0.00	0.00	0.00	0.00	0.00
7,500.00	0.00	0.00	7,500.00	0.00	0.00	0.00	0.00	0.00	0.00
7,600.00	0.00	0.00	7,600.00	0.00	0.00	0.00	0.00	0.00	0.00
7,700.00	0.00	0.00	7,700.00	0.00	0.00	0.00	0.00	0.00	0.00
7,800.00	0.00	0.00	7,800.00	0.00	0.00	0.00	0.00	0.00	0.00
7,900.00	0.00	0.00	7,900.00	0.00	0.00	0.00	0.00	0.00	0.00
8,000.00	0.00	0.00	8,000.00	0.00	0.00	0.00	0.00	0.00	0.00
8,100.00	0.00	0.00	8,100.00	0.00	0.00	0.00	0.00	0.00	0.00
8,200.00	0.00	0.00	8,200.00	0.00	0.00	0.00	0.00	0.00	0.00
8,300.00	0.00	0.00	8,300.00	0.00	0.00	0.00	0.00	0.00	0.00
8,400.00	0.00	0.00	8,400.00	0.00	0.00	0.00	0.00	0.00	0.00
8,500.00	0.00	0.00	8,500.00	0.00	0.00	0.00	0.00	0.00	0.00
8,600.00	0.00	0.00	8,600.00	0.00	0.00	0.00	0.00	0.00	0.00
8,700.00	0.00	0.00	8,700.00	0.00	0.00	0.00	0.00	0.00	0.00
8,800.00	0.00	0.00	8,800.00	0.00	0.00	0.00	0.00	0.00	0.00
8,900.00	0.00	0.00	8,900.00	0.00	0.00	0.00	0.00	0.00	0.00
9,000.00	0.00	0.00	9,000.00	0.00	0.00	0.00	0.00	0.00	0.00
9,000.00	0.00	0.00	9,000.00	0.00	0.00	0.00	0.00	0.00	0.00
9,200.00	0.00	0.00	9,200.00	0.00	0.00	0.00	0.00	0.00	0.00
9,300.00	0.00	0.00	9,300.00	0.00	0.00	0.00	0.00	0.00	0.00
9,345.00	0.00	0.00	9,345.00	0.00	0.00	0.00	0.00	0.00	0.00
9,400.00	0.55	58.05	9,400.00	0.14	0.22	-0.13	1.00	1.00	0.00
9,400.00 9,500.00	0.55 1.55	58.05 58.05	9,400.00	1.11	1.78	-0.13 -1.04	1.00	1.00	0.00
9,600.00	2.55	58.05	9,499.90	3.00	4.81	-1.0 4 -2.81	1.00	1.00	0.00
9,700.00	3.55	58.05	9,699.77	5.82	9.33	-2.61 -5.44	1.00	1.00	0.00
9,800.00	4.55	58.05	9,799.52	9.55	15.32	-8.93	1.00	1.00	0.00
9,900.00	5.55 6.55	58.05	9,899.13	14.21	22.79	-13.29	1.00	1.00	0.00
10,000.00 10,100.00	6.55 7.55	58.05 58.05	9,998.57 10,097.82	19.79 26.28	31.73 42.15	-18.50 -24.58	1.00 1.00	1.00 1.00	0.00 0.00
10,100.00	7.55 8.55	58.05 58.05	10,097.82	33.69	42.15 54.03	-24.58 -31.50	1.00	1.00	0.00
10,300.00	9.55	58.05	10,190.63	42.02	67.38	-39.29	1.00	1.00	0.00
10,344.91	10.00	58.05	10,339.84	46.05	73.85	-43.06	1.00	1.00	0.00
10,400.00	10.00	58.05	10,394.10	51.11	81.96	-47.79	0.00	0.00	0.00
10,500.00	10.00	58.05	10,492.58	60.30	96.70	-56.38	0.00	0.00	0.00
10,600.00	10.00	58.05	10,591.06	69.49 79.67	111.43	-64.97	0.00	0.00	0.00
10,700.00	10.00	58.05	10,689.54	78.67	126.17	-73.56	0.00	0.00	0.00

Planning Report

Database: Company: HOPSPP

ENGINEERING DESIGNS

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Saker 6_7

Well: Saker 6_7 Fed Com 38H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well Saker 6_7 Fed Com 38H

RKB=26.5' @ 3477.30ft RKB=26.5' @ 3477.30ft

Grid

Design:	Permitting Pla	an							
Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
10,800.00 10,900.00 11,000.00 11,100.00 11,200.00	10.00 10.00 10.00 10.00 10.00	58.05 58.05 58.05 58.05 58.05	10,788.02 10,886.50 10,984.98 11,083.46 11,181.94	87.86 97.05 106.24 115.42 124.61	140.90 155.63 170.37 185.10 199.83	-82.15 -90.75 -99.34 -107.93 -116.52	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
11,250.09 11,300.00 11,400.00 11,500.00 11,600.00	10.00 8.55 12.97 21.49 30.88	58.05 88.11 138.78 157.08 164.97	11,231.27 11,280.56 11,378.98 11,474.47 11,564.13	129.21 131.63 123.41 98.04 56.27	207.21 214.60 229.47 244.03 257.86	-120.82 -122.94 -114.13 -88.20 -45.91	0.00 10.00 10.00 10.00 10.00	0.00 -2.90 4.42 8.52 9.39	0.00 60.23 50.67 18.30 7.89
11,700.00 11,800.00 11,900.00 12,000.00 12,100.00	40.55 50.32 60.16 70.02 79.90	169.41 172.37 174.58 176.40 178.00	11,645.24 11,715.33 11,772.28 11,814.35 11,840.26	-0.61 -70.88 -152.41 -242.71 -339.05	270.52 281.63 290.86 297.92 302.60	11.43 82.09 163.92 254.43 350.88	10.00 10.00 10.00 10.00 10.00	9.66 9.78 9.83 9.86 9.88	4.44 2.96 2.22 1.81 1.60
12,190.79 12,200.00 12,300.00 12,400.00 12,500.00	88.88 88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,849.13 11,849.31 11,851.26 11,853.22 11,855.17 11,857.12	-429.28 -438.49 -538.47 -638.44 -738.42 -838.39	304.67 304.77 305.88 306.99 308.09 309.20	441.13 450.33 550.27 650.21 750.15 850.09	10.00 0.00 0.00 0.00 0.00 0.00	9.89 0.00 0.00 0.00 0.00	1.50 0.00 0.00 0.00 0.00 0.00
12,700.00 12,800.00 12,900.00 13,000.00	88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36	11,859.08 11,861.03 11,862.99 11,864.94	-938.37 -1,038.34 -1,138.32 -1,238.29	310.31 311.42 312.53 313.64	950.03 1,049.97 1,149.91 1,249.85	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
13,100.00 13,200.00 13,300.00 13,400.00 13,500.00	88.88 88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,866.90 11,868.85 11,870.81 11,872.76 11,874.72	-1,338.27 -1,438.24 -1,538.22 -1,638.19 -1,738.17	314.74 315.85 316.96 318.07 319.18	1,349.79 1,449.73 1,549.66 1,649.60 1,749.54	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
13,600.00 13,700.00 13,800.00 13,900.00 14,000.00	88.88 88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,876.67 11,878.63 11,880.58 11,882.53 11,884.49	-1,838.14 -1,938.12 -2,038.09 -2,138.07 -2,238.04	320.29 321.39 322.50 323.61 324.72	1,849.48 1,949.42 2,049.36 2,149.30 2,249.24	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
14,100.00 14,200.00 14,300.00 14,400.00 14,500.00	88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,886.44 11,888.40 11,890.35 11,892.31 11,894.26	-2,338.02 -2,437.99 -2,537.96 -2,637.94 -2,737.91	325.83 326.94 328.04 329.15 330.26	2,349.18 2,449.12 2,549.06 2,648.99 2,748.93	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
14,600.00 14,700.00 14,800.00 14,900.00 15,000.00	88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,896.22 11,898.17 11,900.13 11,902.08 11,904.04	-2,837.89 -2,937.86 -3,037.84 -3,137.81 -3,237.79	331.37 332.48 333.59 334.69 335.80	2,848.87 2,948.81 3,048.75 3,148.69 3,248.63	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
15,100.00 15,200.00 15,300.00 15,400.00 15,500.00	88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,905.99 11,907.95 11,909.90 11,911.85 11,913.81	-3,337.76 -3,437.74 -3,537.71 -3,637.69 -3,737.66	336.91 338.02 339.13 340.24 341.34	3,348.57 3,448.51 3,548.45 3,648.39 3,748.32	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00
15,600.00 15,700.00 15,800.00 15,900.00 16,000.00	88.88 88.88 88.88 88.88	179.36 179.36 179.36 179.36 179.36	11,915.76 11,917.72 11,919.67 11,921.63 11,923.58	-3,837.64 -3,937.61 -4,037.59 -4,137.56 -4,237.54	342.45 343.56 344.67 345.78 346.89	3,848.26 3,948.20 4,048.14 4,148.08 4,248.02	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00

Planning Report

Database: Company: HOPSPP

ENGINEERING DESIGNS

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Saker 6_7

Well: Saker 6_7 Fed Com 38H

Wellbore: Wellbore #1

Design: Permitting Plan

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well Saker 6_7 Fed Com 38H

RKB=26.5' @ 3477.30ft RKB=26.5' @ 3477.30ft

Grid

Design:	Permitting Pla	an							
Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
16,100.00	88.88	179.36	11,925.54	-4,337.51	347.99	4,347.96	0.00	0.00	0.00
16,200.00	88.88	179.36	11,927.49	-4,437.48	349.10	4,447.90	0.00	0.00	0.00
16,300.00	88.88	179.36	11,929.45	-4,537.46	350.21	4,547.84	0.00	0.00	0.00
16,400.00	88.88	179.36	11,931.40	-4,637.43	351.32	4,647.78	0.00	0.00	0.00
16,500.00	88.88	179.36	11,933.36	-4,737.41	352.43	4,747.71	0.00	0.00	0.00
16,600.00	88.88	179.36	11,935.31	-4,837.38	353.54	4,847.65	0.00	0.00	0.00
16,700.00	88.88	179.36	11,937.26	-4,937.36	354.64	4,947.59	0.00	0.00	0.00
16,800.00	88.88	179.36	11,939.22	-5,037.33	355.75	5,047.53	0.00	0.00	0.00
16,900.00	88.88	179.36	11,941.17	-5,137.31	356.86	5,147.47	0.00	0.00	0.00
17,000.00	88.88	179.36	11,943.13	-5,237.28	357.97	5,247.41	0.00	0.00	0.00
17,100.00	88.88	179.36	11,945.08	-5,337.26	359.08	5,347.35	0.00	0.00	0.00
17,200.00	88.88	179.36	11,947.04	-5,437.23	360.19	5,447.29	0.00	0.00	0.00
17,300.00	88.88	179.36	11,948.99	-5,537.21	361.29	5,547.23	0.00	0.00	0.00
17,400.00	88.88	179.36	11,950.95	-5,637.18	362.40	5,647.17	0.00	0.00	0.00
17,500.00	88.88	179.36	11,952.90	-5,737.16	363.51	5,747.11	0.00	0.00	0.00
17,600.00	88.88	179.36	11,954.86	-5,837.13	364.62	5,847.04	0.00	0.00	0.00
17,700.00	88.88	179.36	11,956.81	-5,937.11	365.73	5,946.98	0.00	0.00	0.00
17,800.00	88.88	179.36	11,958.77	-6,037.08	366.84	6,046.92	0.00	0.00	0.00
17,900.00	88.88	179.36	11,960.72	-6,137.06	367.94	6,146.86	0.00	0.00	0.00
18,000.00	88.88	179.36	11,962.68	-6,237.03	369.05	6,246.80	0.00	0.00	0.00
18,100.00	88.88	179.36	11,964.63	-6,337.01	370.16	6,346.74	0.00	0.00	0.00
18,200.00	88.88	179.36	11,966.58	-6,436.98	371.27	6,446.68	0.00	0.00	0.00
18,300.00	88.88	179.36	11,968.54	-6,536.95	372.38	6,546.62	0.00	0.00	0.00
18,400.00	88.88	179.36	11,970.49	-6,636.93	373.49	6,646.56	0.00	0.00	0.00
18,500.00	88.88	179.36	11,972.45	-6,736.90	374.59	6,746.50	0.00	0.00	0.00
18,600.00	88.88	179.36	11,974.40	-6,836.88	375.70	6,846.44	0.00	0.00	0.00
18,700.00	88.88	179.36	11,976.36	-6,936.85	376.81	6,946.37	0.00	0.00	0.00
18,800.00	88.88	179.36	11,978.31	-7,036.83	377.92	7,046.31	0.00	0.00	0.00
18,900.00	88.88	179.36	11,980.27	-7,136.80	379.03	7,146.25	0.00	0.00	0.00
19,000.00	88.88	179.36	11,982.22	-7,236.78	380.14	7,246.19	0.00	0.00	0.00
19,100.00	88.88	179.36	11,984.18	-7,336.75	381.24	7,346.13	0.00	0.00	0.00
19,200.00	88.88	179.36	11,986.13	-7,436.73	382.35	7,446.07	0.00	0.00	0.00
19,300.00	88.88	179.36	11,988.09	-7,536.70	383.46	7,546.01	0.00	0.00	0.00
19,400.00	88.88	179.36	11,990.04	-7,636.68	384.57	7,645.95	0.00	0.00	0.00
19,500.00	88.88	179.36	11,992.00	-7,736.65	385.68	7,745.89	0.00	0.00	0.00
19,600.00	88.88	179.36	11.993.95	-7,836.63	386.79	7,845.83	0.00	0.00	0.00
19,700.00	88.88	179.36	11,995.90	-7,936.60	387.89	7,945.77	0.00	0.00	0.00
19,800.00	88.88	179.36	11,997.86	-8,036.58	389.00	8,045.70	0.00	0.00	0.00
19,900.00	88.88	179.36	11,999.81	-8,136.55	390.11	8,145.64	0.00	0.00	0.00
20,000.00	88.88	179.36	12,001.77	-8,236.53	391.22	8,245.58	0.00	0.00	0.00
20,100.00	88.88	179.36	12.003.72	-8,336.50	392.33	8,345.52	0.00	0.00	0.00
20,200.00	88.88	179.36	12,005.68	-8,436.47	393.44	8,445.46	0.00	0.00	0.00
20,300.00	88.88	179.36	12,007.63	-8,536.45	394.54	8,545.40	0.00	0.00	0.00
20,400.00	88.88	179.36	12,009.59	-8,636.42	395.65	8,645.34	0.00	0.00	0.00
20,500.00	88.88	179.36	12,011.54	-8,736.40	396.76	8,745.28	0.00	0.00	0.00
20.600.00	88.88	179.36	12,013.50	-8,836.37	397.87	8,845.22	0.00	0.00	0.00
20,700.00	88.88	179.36	12,015.45	-8,936.35	398.98	8,945.16	0.00	0.00	0.00
20,800.00	88.88	179.36	12,017.41	-9,036.32	400.09	9,045.10	0.00	0.00	0.00
20,900.00	88.88	179.36	12,019.36	-9,136.30	401.19	9,145.03	0.00	0.00	0.00
21,000.00	88.88	179.36	12,021.31	-9,236.27	402.30	9,244.97	0.00	0.00	0.00
21,100.00	88.88	179.36	12,023.27	-9,336.25	403.41	9,344.91	0.00	0.00	0.00
21,200.00	88.88	179.36	12,025.22	-9,436.22	404.52	9,444.85	0.00	0.00	0.00
21,300.00	88.88	179.36	12,027.18	-9,536.20	405.63	9,544.79	0.00	0.00	0.00
21,400.00	88.88	179.36	12,029.13	-9,636.17	406.74	9,644.73	0.00	0.00	0.00
21,500.00	88.88	179.36	12,031.09	-9,736.15	407.84	9,744.67	0.00	0.00	0.00

Planning Report

Database: HOPSPP

Company: ENGINEERING DESIGNS

Project: PRD NM DIRECTIONAL PLANS (NAD 1983)

Site: Saker 6_7

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Wellbore: Wellbore #1
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Local Co-ordinate Reference:

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Survey Calculation Method:

Well Saker 6_7 Fed Com 38H

RKB=26.5' @ 3477.30ft RKB=26.5' @ 3477.30ft

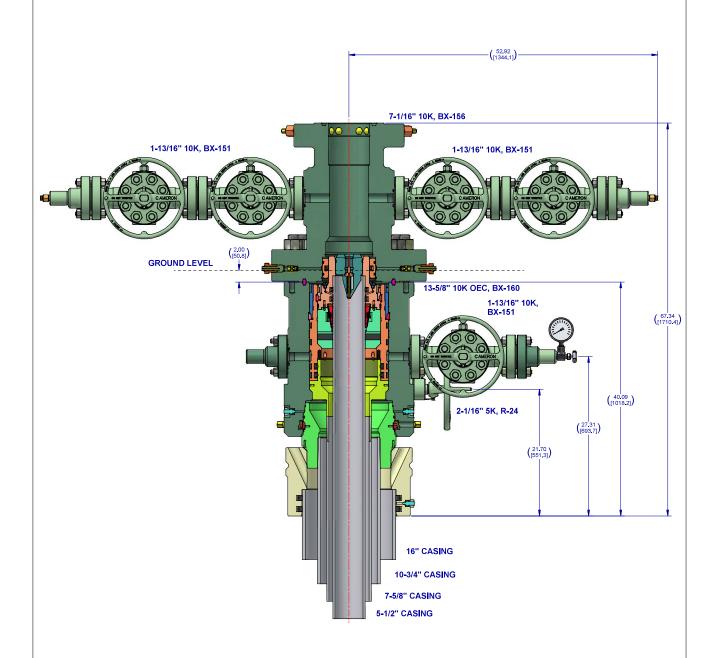
Grid

Planned Survey									
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
21,600.00	88.88	179.36	12,033.04	-9,836.12	408.95	9,844.61	0.00	0.00	0.00
21,700.00	88.88	179.36	12,035.00	-9,936.10	410.06	9,944.55	0.00	0.00	0.00
21,800.00	88.88	179.36	12,036.95	-10,036.07	411.17	10,044.49	0.00	0.00	0.00
21,900.00	88.88	179.36	12,038.91	-10,136.05	412.28	10,144.42	0.00	0.00	0.00
22,000.00	88.88	179.36	12,040.86	-10,236.02	413.39	10,244.36	0.00	0.00	0.00
22,100.00	88.88	179.36	12,042.82	-10,336.00	414.49	10,344.30	0.00	0.00	0.00
22,124.79	88.88	179.36	12,043.30	-10,360.78	414.77	10,369.08	0.00	0.00	0.00

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (ft)	+N/-S (ft)	+E/-W (ft)	Northing (usft)	Easting (usft)	Latitude	Longitude
FTP (Saker 6_7 Fed - plan misses target - Point	0.00 center by 20		11,849.30 787.80ft ME	82.81) (11707.45 T	298.99 VD, -61.66 N	457,227.28 280.37 E)	829,889.64	32.253545	-103.399925
PBHL (Saker 6_7 Fed - plan hits target cer - Point	0.00 nter	0.00	12,043.30	-10,360.78	414.77	446,783.67	830,005.42	32.224837	-103.399844

Formations						
	Measured Depth (ft)	Vertical Depth (ft)	Name	Lithology	Dip (°)	Dip Direction (°)
	776.30	776.30	RUSTLER			
	1,116.30	1,116.30	SALADO			
	3,426.30	3,426.30	CASTILE			
	5,288.30	5,288.30	DELAWARE			
	5,336.30	5,336.30	BELL CANYON			
	6,220.30	6,220.30	CHERRY CANYON			
	7,596.30	7,596.30	BRUSHY CANYON			
	8,765.30	8,765.30	BONE SPRING			
	9,936.35	9,935.30	BONE SPRING 1ST			
	10,405.29	10,399.30	BONE SPRING 2ND			
	11,434.40	11,412.30	BONE SPRING 3RD			
	11,872.99	11,758.30	WOLFCAMP			

Plan Annotatio	ons				
	Measured	Vertical	Local Coor	dinates	
	Depth (ft)	Depth (ft)	+N/-S (ft)	+E/-W (ft)	Comment
	9,345.00	9,345.00	0.00	0.00	Build 1°/100'
	10,344.91	10,339.84	46.05	73.85	Hold 10° Tangent
	11,250.09	11,231.27	129.21	207.21	KOP, Build & Turn 10°/100'
	12,190.79	11,849.13	-429.28	304.67	Landing Point
	22,124.79	12,043.30	-10,360.78	414.77	TD at 22124.79' MD



Notes:

1. THIS IS A PROPOSAL DRAWING AND DIMENSIONS SHOWN ARE SUBJECT TO CHANGE DURING THE FINAL DESIGN PROCESS.

		CONF	IDEN	ITIAL	
SURFACE TREATMENT	DO NOT SC	ALE		CAMERON	SURFACE
	DRAWN BY:	DATE	W/	A Schlumberger Company	SYSTEMS
	D. GOTTUNG	2 Dec 21		A Schlumberger Company	
MATERIAL & HEAT TREAT		DATE			
	D, GOTTUNG	2 Dec 21		OXY 13-5/8" 10K AD/	APT
	APPROVED BY:	DATE	1	16" X 10-3/4" X 7-5/8" >	C5-1/2"
	D, GOTTUNG	2 Dec 21			
	5.617 LBS INITIAL USE BM: 55.434 KG		SHEET 4 of 4	SD-053434-94-	.05 REV:

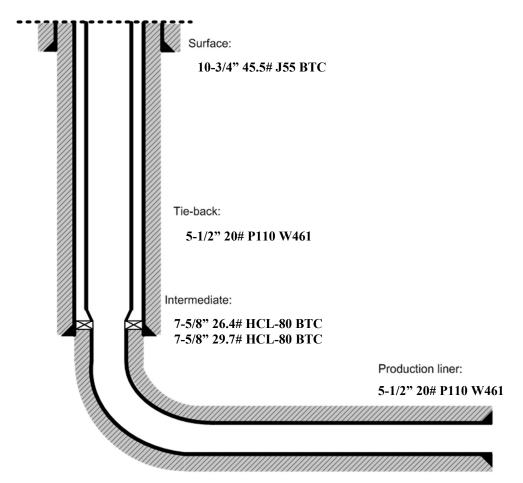
OXY USA WTP LP

Standard SL1 Tieback Details

Below is a summary that describes the general operational steps to drill and complete the well.

- Drill 14-3/4" hole x 10-3/4" casing for surface section. Cement to surface.
- Drill 9-7/8" hole x 7-5/8" casing for intermediate section. Cement to surface.
- Drill 6-3/4" hole x 5-1/2" liner for production section. Cement to top of liner, 100' inside 7-5/8" shoe.
- Release drilling rig from location.
- Move in workover rig and run a 5-1/2" 20# P110 Wedge 461 tie-back frac string and seal assembly. Tie into liner hanger Polished Bore Receptacle (PBR) with seal assembly.
- Pump hydraulic fracture job.
- Flowback and produce well.

General well schematic:





TenarisHydril Wedge 425®



Coupling	Pipe Body
Grade: P110-CY	Grade: P110-CY
Body: White	1st Band: White
1st Band: Grey	2nd Band: Grey
2nd Band: -	3rd Band: -
3rd Band: -	4th Band: -
	5th Band: -
	6th Band: -

Outside Diameter	5.500 in.	Wall Thickness	0.361 in.	Grade	P110-CY
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	REGULAR				

Pipe Body Data

Geometry			
Nominal OD	5.500 in.	Wall Thickness	0.361 in.
Nominal Weight	20 lb/ft	Plain End Weight	19.83 lb/ft
Drift	4.653 in.	OD Tolerance	API
Nominal ID	4.778 in.		

Performance	
Body Yield Strength	641 x1000 lb
Min. Internal Yield Pressure	12,640 psi
SMYS	110,000 psi
Collapse Pressure	11,100 psi

Connection Data

5.777 in.
4.734 in.
5.823 in.
3.77
Regular

Performance	
Tension Efficiency	90 %
Joint Yield Strength	577 x1000 lb
Internal Pressure Capacity	12,640 psi
Compression Efficiency	90 %
Compression Strength	577 x1000 lb
Max. Allowable Bending	82 °/100 ft
External Pressure Capacity	11,100 psi

15,700 ft-lb
19,600 ft-lb
21,600 ft-lb
29,000 ft-lb
36,000 ft-lb

Notes

This connection is fully interchangeable with: TORQ® SFW $^{\text{m}}$ - 5.5 in. - 0.361 in. Connections with Dopeless® Technology are fully compatible with the same connection in its Standard version

For the lastest performance data, always visit our website: www.tenaris.com

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TenarisHydril Wedge 441®



Coupling	Pipe Body
Grade: P110-CY	Grade: P110-CY
Body: White	1st Band: White
1st Band: Grey	2nd Band: Grey
2nd Band: -	3rd Band: -
3rd Band: -	4th Band: -
	5th Band: -
	6th Band: -

Outside Diameter	5.500 in.	Wall Thickness	0.361 in.	Grade	P110-CY
Min. Wall Thickness	87.50 %	Drift	API Standard	Туре	Casing
Connection OD Option	REGULAR				

Pipe Body Data

Geometry			
Nominal OD	5.500 in.	Wall Thickness	0.361 in.
Nominal Weight	20 lb/ft	Plain End Weight	19.83 lb/ft
Drift	4.653 in.	OD Tolerance	API
Nominal ID	4.778 in.		

Performance	
Body Yield Strength	641 x1000 lb
Min. Internal Yield Pressure	12,640 psi
SMYS	110,000 psi
Collapse Pressure	11,100 psi

Connection Data

Geometry	
Connection OD	5.852 in.
Coupling Length	8.714 in.
Connection ID	4.778 in.
Make-up Loss	3.780 in.
Threads per inch	3.40
Connection OD Option	Regular

Performance	
Tension Efficiency	81.50 %
Joint Yield Strength	522 x1000 lb
Internal Pressure Capacity	12,640 psi
Compression Efficiency	81.50 %
Compression Strength	522 x1000 lb
Max. Allowable Bending	71 °/100 ft
External Pressure Capacity	11,100 psi

Make-Up Torques	
Minimum	15,000 ft-lb
Optimum	16,000 ft-lb
Maximum	19,200 ft-lb
Operation Limit Torques	
	20,000 # 11-
Operating Torque	32,000 ft-lb
Operating Torque Yield Torque	32,000 π-Ib 38,000 ft-Ib
	<u> </u>
Yield Torque	<u> </u>

Notes

This connection is fully interchangeable with: Wedge 441% - 5.5 in. - 0.304 in. Connections with Dopeless% Technology are fully compatible with the same connection in its Standard version

For the lastest performance data, always visit our website: www.tenaris.com

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TenarisHydril

5.500" 20.00 lb/ft P110-CY TenarisHydril Wedge 461™ Matched Strength



Special Data Sheet TH DS-20.0359 12 August 2020 Rev 00

Nominal OD	5.500 in.	Wall Thickness	0.361 in.	Grade	P110-CY
Min Wall Thickness	87.5%	Туре	CASING	Connection OD Option	MATCHED STRENGTH
Pipe Body Data					
Geometry				Performance	
Nominal OD	5.500 in.	Nominal ID	4.778 in.	Body Yield Strength	641 x 1000 lbs
Nominal Weight	20.00 lbs/ft	Wall Thickness	0.361 in.	Internal Yield	12640 psi
Standard Drift Diameter	4.653 in.	Plain End Weight	19.83 lbs/ft	SMYS	110000 psi
Special Drift Diameter	N/A	OD Tolerance	API	Collapse Pressure	11110 psi
Connection Data					
Geometry		Performance		Make-up Torques	
Matched Strength OD	6.050 in.	Tension Efficiency	100%	Minimum	17000 ft-lbs
Make-up Loss	3.775 in.	Joint Yield Strength	641 x 1000 lbs	Optimum	18000 ft-lbs
Threads per in.	3.40	Internal Yield	12640 psi	Maximum	21600 ft-lbs
Connection OD Option	MATCHED STRENGTH	Compression Efficiency	100%	Operational Limit Torques	5
Coupling Length	7.714 in.	Compression Strength	641 x 1000 lbs	Operating Torque	32000 ft-lbs
		Bending	92 °/100 ft	Yield Torque	38000 ft-lbs
		Collapse	11110 psi	Buck-On Torques	
				Minimum	21600 ft-lbs
				Maximum	23100 ft-lbs

Notes

^{*}If you need to use torque values that are higher than the maximum indicated, please contact a local Tenaris technical sales representative

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State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 204904

CONDITIONS

Operator:	OGRID:
OXY USA INC	16696
P.O. Box 4294	Action Number:
Houston, TX 772104294	204904
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

CONDITIONS

Created By	Condition	Condition Date
pkautz	None	5/4/2023