Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
PAINT 4-33 FED	621H	3002551952	NMLC061863A	NMLC061863A	DEVON
PAINT 4-33 FED	711H	3002551954	NMLC061863A	NMLC061863A	DEVON

### **Notice of Intent**

Sundry ID: 2749313

Type of Submission: Notice of Intent

Date Sundry Submitted: 09/05/2023

Date proposed operation will begin: 09/04/2023

Type of Action: APD Change

Time Sundry Submitted: 08:26

Sundry Print Repor

09/13/2023

**Procedure Description:** ENGINEERING ONLY Devon Energy Production Company, L.P. respectfully requests approval for optional surface casing/drilling plan of 10-3/4" surface casing inside of 14-3/4" surface hole at previously permitted set depths. Devon Energy Production Company, L.P. will circulate class C cement to surface behind the 10-3/4" casing. Pipe connections and bradenhead information have also been updated. Devon also request a break test variance for the subject wells. Please see attached documentation.

#### **NOI Attachments**

#### **Procedure Description**

break\_test\_variance\_BOP\_20230905081935.pdf 10.750\_45.5\_J55\_SEAH\_20230905081823.pdf PAINT\_4\_33\_FED\_COM\_621H\_14.75in\_20230905081739.pdf PAINT\_4\_33\_FED\_COM\_711H\_14.75in\_20230905081739.pdf 5.5in\_x\_20.00lb\_P110EC\_DWC\_C\_IS\_PLUS\_\_\_5\_23\_2023\_20230904063426.pdf 8.625in\_32lb\_P110EC\_SPRINT\_FJ\_09.16.2022\_20230904063304.pdf

#### Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CHELSEY GREEN Name: DEVON ENERGY PRODUCTION COMPANY LP Title: Regulatory Compliance Professional Street Address: 333 West Sheridan Avenue City: Oklahoma City State: OK Phone: (405) 228-8595 Email address: Chelsey.Green@dvn.com

State:

#### Field

**Representative Name:** 

Street Address:

City:

Phone:

Email address:

Zip:

Signed on: SEP 05, 2023 08:44 AM

.

### PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

LEASE NO.:NMLC061863ALOCATION:Section 4, T.25 S., R.32 E., NMPMCOUNTY:Lea County, New MexicoWELL NAME & NO.:Paint 4-33 Fed Com 711HSURFACE HOLE FOOTAGE:200'/S & 450'/WPOTTOM HOLE FOOTAGE:200'/S & 450'/W	
COUNTY:Lea County, New MexicoWELL NAME & NO.:Paint 4-33 Fed Com 711HSURFACE HOLE FOOTAGE:200'/S & 450'/W	
WELL NAME & NO.:Paint 4-33 Fed Com 711HSURFACE HOLE FOOTAGE:200'/S & 450'/W	
SURFACE HOLE FOOTAGE: 200'/S & 450'/W	
SURFACE HOLE FOOTAGE: 200'/S & 450'/W	
<b>DOTTOM HOLE FOOTACE</b> 202/NL $(220)/W$	
BOTTOM HOLE FOOTAGE   20'/N & 330'/W	
ATS/API ID: 3002551954	
APD ID:	
Sundry ID: 2749313	
WELL NAME & NO.: Paint 4-33 Fed Com 621H	
SURFACE HOLE FOOTAGE: 200'/S & 510'/W	
BOTTOM HOLE FOOTAGE 20'/N & 890'/W	
ATS/API ID: 3002551952	
APD ID:	
Sundry ID: 2749313	

COA

<b>XX2</b> G			1
H2S	Yes 💻		
Potash	None 🔻		
Cave/Karst	Low 🔫		
Potential			
Cave/Karst	Critical		
Potential			
Variance	C None	🖸 Flex Hose	C Other
Wellhead	Conventional and Multibov	vl 🔽	
Other	□4 String	Capitan Reef	□ WIPP
		None -	
		·	
Other	Pilot Hole	Open Annulus	
	None 🔽		
Cementing	Contingency Squeeze	Echo-Meter	Primary Cement
	None	Int 1 🔻	Squeeze
			None 🝷
Special	□ Water	COM	Unit Unit
Requirements	Disposal/Injection		
Special	Batch Sundry		
Requirements	-		
Special	Break Testing	□ Offline	Casing
Requirements	_	Cementing	Clearance
Variance			

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. As a result, the Hydrogen Sulfide area must meet **43 CFR part 3170 Subpart 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

#### **B.** CASING

- 1. The 10-3/4 inch surface casing shall be set at approximately 875 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. The surface hole shall be 14 3/4 inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of

six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.

# Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

2. The minimum required fill of cement behind the **8-5/8** inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

#### **Option 2:**

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6980' (521 sxs Class H/C+ additives).
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 493 sxs Class C)

Operator has proposed to pump down 10-3/4" X 8-5/8" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 8-5/8" casing to surface after the second stage BH to verify TOC.</u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad.

If cement does not reach surface, the next casing string must come to surface.

## Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **C. PRESSURE CONTROL**

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

#### 2.

#### **Option 1:**

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi. Annular which shall be tested to **5000 (5M)** psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 8-5/8 inch intermediate casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

#### **Option 2:**

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **10-3/4** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **10,000** (**10M**) psi. Variance is approved to use a **5000** (**5M**) Annular which shall be tested to **5000** (**5M**) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

#### **D. SPECIAL REQUIREMENT (S)**

#### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be on the sign.</u>

#### **BOPE Break Testing Variance (Approved)**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at **21**-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

### **Batch Sundry:**

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes above the deepest well shoes set depth.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)
- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

#### $\boxtimes$ Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV (575) 361-2822

# Lea County Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a

digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24 hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

#### B. PRESSURE CONTROL

- All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after

installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

- b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170
  Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR**

#### part 3170 Subpart 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

LVO 9/13/2023

#### Received by

eceived by OCD: 9/18	8/2023 9:	41:55 AM				Page 14 of 51		
Form 3160-5 (June 2019)					FORM APPROVED OMB No. 1004-0137 Expires: October 31, 2021			
SU		EAU OF LAND MANA			6. If Indian, Allottee or Tribe Name			
Do not u	se this f	orm for proposals to	o drill or to re-enter an PD) for such proposals		MULTIPLE			
S	UBMIT IN 1	RIPLICATE - Other instru	ctions on page 2		7. If Unit of CA/Agreement, Name and/or No.			
1. Type of Well					- MULTIPLE			
Oil Well	Gas W	Vell Other			8. Well Name and No. MULTIPLE			
2. Name of Operator DEVC	ON ENERG		NY LP		9. API Well No. MULTIPLE			
3a. Address 333 WEST S	HERIDAN	AVE, OKLAHOMA CITY,	3b. Phone No. <i>(include area cod</i> (405) 235-3611	le)	10. Field and Pool or Exploratory Area MULTIPLE			
4. Location of Well (Footag	ge, Sec., T.,R	.,M., or Survey Description)			11. Country or Parish, State			
MULTIPLE					MULTIPLE			
	12. CHE	CK THE APPROPRIATE BO	X(ES) TO INDICATE NATUR	E OF NOT	TCE, REPORT OR OTHER DATA			
TYPE OF SUBMISS	SION		ТҮ	PE OF AC	CTION			
✓ Notice of Intent		Acidize	Deepen Hydraulic Fracturing		duction (Start/Resume) Water Shut-Off lamation Well Integrity			
Subsequent Report		Casing Repair Change Plans	New Construction Plug and Abandon		omplete Other			
Final Abandonment	Notice	Convert to Injection	Plug Back	Wat	ter Disposal			

13. Describe Proposed or Completed Operation: Clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be perfonned or provide the Bond No. on file with BLM/BIA. Required subsequent reports must be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed and the operator has detennined that the site is ready for final inspection.)

#### ENGINEERING ONLY

Devon Energy Production Company, L.P. respectfully requests approval for optional surface casing/drilling plan of 10-3/4" surface casing inside of 14-3/4" surface hole at previously permitted set depths. Devon Energy Production Company, L.P. will circulate class C cement to surface behind the 10-3/4 casing. Pipe connections and bradenhead information have also been updated. Devon also request a break test variance for the subject wells. Please see attached documentation.

14. I hereby certify that the foregoing is true and correct. Name ( <i>Printed/Typed</i> ) CHELSEY GREEN / Ph: (405) 228-8595	Regulatory C	Compliance Professional	
Signature	Date	09/05/2	2023
THE SPACE FOR FED	ERAL OR STA	TE OFICE USE	
Approved by			
	Title		Date
Conditions of approval, if any, are attached. Approval of this notice does not warran certify that the applicant holds legal or equitable title to those rights in the subject le which would entitle the applicant to conduct operations thereon.			
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for ar any false, fictitious or fraudulent statements or representations as to any matter with		and willfully to make to any d	lepartment or agency of the United States

#### Released to Imaging: 10/2/2023 3:00:48 PM

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

#### SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13:* Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

#### NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

#### **Additional Information**

#### **Batch Well Data**

PAINT 4-33 FED COM 711H, US Well Number: 3002551954, Case Number: NMLC061863A, Lease Number: NMLC061863A, Operator:DEVON ENERGY PRODUCTION COMPANY LP

PAINT 4-33 FED COM 621H, US Well Number: 3002551952, Case Number: NMLC061863A, Lease Number: NMLC061863A, Operator:DEVON ENERGY PRODUCTION COMPANY LP

#### Section 2 - Blowout Preventer Testing Procedure

#### Variance Request

Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow OOGO2.III.A.2.i, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed OOGO2.III.A.2.i per the following: Devon Energy will perform a full BOP test per OOGO2.III.A.2.i before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third





### <u>10-3/4"</u> <u>45.50#</u> <u>0.400"</u> <u>J-55</u>

### **Dimensions (Nominal)**

Outside Diameter Wall Inside Diameter	10.750 0.400 9.950	in. in. in.
Drift	9.875	in.
Weight, T&C	45.500	lbs/ft
Weight, PE	44.260	lbs/ft
Internal Yield Pressure at Minimum Yield		
Collapse	2090	psi
Internal Yields Pressure		
PE	3580	psi
STC	3580	psi
BTC	3580	psi
Yield Strength, Pipe Body	715	1000 lbs
Joint Strength, STC		
STC	493	1000 lbs
ВТС	796	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

#### 1. Geologic Formations

TVD of target	12075	Pilot hole depth	N/A
MD at TD:	22292	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	770		
Salt	1075		
Base of Salt	4420		
Delaware	4690		
Cherry Canyon	5570		
Brushy Canyon	6980		
1st Bone Spring Lime	8530		
Bone Spring 1st	9630		
Bone Spring 2nd	10230		
3rd Bone Spring Lime	10760		
Bone Spring 3rd	11480		
Wolfcamp	11950		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45.5	J55	BTC	0	795	0	795
9 7/8	8 5/8	32	P110	Sprint FJ	0	11480	0	11480
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22292	0	12075

#### 2. Casing Program

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	485	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	493	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	519	7012	13.2	1.44	Tail: Class H / C + additives
Production	117	9464	9	3.27	Lead: Class H /C + additives
Production	1433	11464	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:		
			Annular		Annular		X	50% of rated working pressure
Int 1	13-5/8"	5M		d Ram	X			
int i	15 5/0	5101	<b>1</b>	e Ram		- 5M		
			Doub	le Ram	Х	5101		
			Other*					
	13-5/8"		Annular (5M)		X	100% of rated working pressure		
			Blind Ram		X	1014		
Production		10M	Pipe Ram Double Ram					
					Х	10M		
			Other*					
			Annular (5M)					
			Blind Ram					
			Pipe Ram			]		
			Double Ram			]		
			Other*					
N A variance is requested for	the use of a	a diverter on	the surface	casing. See	attached for s	schematic.		
Y A variance is requested to a	run a 5 M ai	nnular on a	10M system	1				

#### 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)		
Surface	FW Gel	8.5-9		
Intermediate	DBE / Cut Brine	10-10.5		
Production	OBM	10-10.5		

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
---	-----------------------------

#### **6.** Logging and Testing Procedures

Logging,	Logging, Coring and Testing						
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the						
Х	Completion Rpeort and sbumitted to the BLM.						
	No logs are planned based on well control or offset log information.						
	Drill stem test? If yes, explain.						
	Coring? If yes, explain.						

Addition	al logs planned	Interval
	Resistivity	Int. shoe to KOP
Density		Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6593
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren S	Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations						
greater than	greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered						
measured va	measured values and formations will be provided to the BLM.						
Ν	H2S is present						

Y H2S plan attached.

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe

#### 1. Geologic Formations

TVD of target	12182	Pilot hole depth	N/A	Τ
MD at TD:	22374	Deepest expected fresh water		

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	770		
Salt	1075		
Base of Salt	4420		
Delaware	4690		
Cherry Canyon	5570		
Brushy Canyon	6980		
1st Bone Spring Lime	8530		
Bone Spring 1st	9630		
Bone Spring 2nd	10230		
3rd Bone Spring Lime	10760		
Bone Spring 3rd	11480		
Wolfcamp	11950		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45.5	J55	BTC	0	795	0	795
9 7/8	8 5/8	32	P110	Sprint FJ	0	11480	0	11480
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22374	0	12182

#### 2. Casing Program

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	485	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	492	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	521	6993	13.2	1.44	Tail: Class H / C + additives
Production	117	9553	9	3.27	Lead: Class H /C + additives
Production	1432	11553	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:			
			Anı	nular	X	50% of rated working pressure			
Int 1	13-5/8"	5M		d Ram	Х				
int i	15 5/0	5101	-	e Ram		5M			
			Doub	le Ram	X	5101			
			Other*						
	13-5/8"		Annular (5M)		Х	100% of rated working pressure			
Production		10M	Blind Ram		Х				
Troduction		10101	Pipe Ram			10M			
				le Ram	X	10111			
			Other*						
			Annular (5M)						
			Blind Ram						
	Pipe Ram								
	Double Ram		le Ram						
			Other*						
N A variance is requested for	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.								
Y A variance is requested to a	A variance is requested to run a 5 M annular on a 10M system								

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	Drill stem test? If yes, explain.				
	Coring? If yes, explain.				

Additiona	al logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?			
BH pressure at deepest TVD	6652			
Abnormal temperature	No			

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren S	Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations					
greater than	greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered					
measured va	measured values and formations will be provided to the BLM.					
Ν	H2S is present					

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  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe



### **Connection Data Sheet**

OD (in.)	WEIGHT (Ibs./ft.)	WALL (in.)	GRADE	DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 20.00 Plain End: 19.83	0.361	VST P110 EC	4.653	87.5	DWC/C-IS PLUS

#### PIPE PROPERTIES

Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Area	5.828	sq.in.
Grade Type	API 5CT; Vallourec Sourced Material Only	
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	729	klb
Ultimate Strength	787	klb
Min. Internal Yield	14,360	psi
*High Collapse*	12,090	psi

#### **CONNECTION PROPERTIES**

Connection Type	Semi-Premium T&C	
Connection OD (nom)	6.300	in.
Connection ID (nom)	4.778	in.
Make-Up Loss	4.125	in.
Coupling Length	9.250	in.
Critical Cross Section	5.828	sq.in.
Tension Efficiency	100.0%	of pipe
Compression Efficiency	100.0%	of pipe
Internal Pressure Efficiency	100.0%	of pipe
External Pressure Efficiency	100.0%	of pipe

#### **CONNECTION PERFORMANCES** 729 klb Yield Strength Parting Load 787 klb **Compression Rating** 729 klb Min. Internal Yield 14,360 psi \*High Collapse\* 12,090 psi Maximum Uniaxial Bend Rating 104.2 °/100 ft Ref String Length w 1.4 Design Factor 26,040 ft

FIELD TORQUE VALUES		
Min. Make-up Torque	16,600	ft.lbs
Opti. Make-up Torque	17,850	ft.lbs
Max. Make-up Torque	19,100	ft.lbs
Min. Shoulder Torque	1,660	ft.lbs
Max. Shoulder Torque	13,280	ft.lbs
Max. Delta Turn	0.200	Turns
+Max Operational Torque	24,300	ft.lbs
+Maximum Torsional Value (MTV)	26,730	ft.lbs

#### +Maximum Operational Torque and Maximum Torsional Value Only Valid with Vallourec P110EC Material

#### For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

All information is provided by VAM USA or its affiliates at user's sole risk, without liability for loss, damage or injury resulting from the use thereof; and on an "AS IS" basis without warranty or representation of any kind, whether express or implied, including without limitation any warranty of merchantability, fitness for purpose or completeness. This document and its contents are subject to change without notice. In no event shall VAM USA or its affiliates be responsible for any indirect, special, incidental, punitive, exemplary or consequential loss or damage (including without limitation, loss of use, loss of bargain, loss of revenue, profit or anticipated profit) however caused or arising, and whether such losses or damages were foreseeable or VAM USA or its affiliates was advised of the possibility of such damages.

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VAM USA 2107 CityWest Boulevard Suite 1300 Houston, TX 77042 Phone: 713-479-3200 Fax: 713-479-3234 VAM USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support E-mail: tech.support@vam-usa.com

#### DWC Connection Data Notes:

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

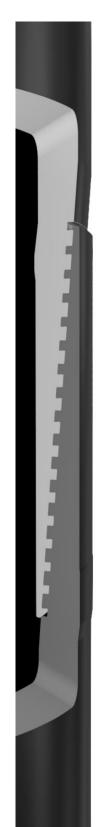
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Issued on: 16	Sep. 2022	by Logan Va	n Gorp



#### t

VAM<sup>®</sup> SPRINT-FJ

HI	GH	ER	то	RQ	UE	VEF	SIC	DN

OD

8 5/8 in.

		<b>Connection Data Sheet</b>
Grade	Alt. Drift:	Connection

7.875 in.

PIPE PROPERTIES		
Nominal OD	8.625	in.
Nominal ID	7.921	in.
Nominal Cross Section Area	9.149	sqin.
Grade Type	Hig	jh Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi
Max. Yield Strength		ks

Weight (lb/ft)

Nominal: 32.00 Plain End: 31.13 Wall Th.

0.352 in.

P110EC

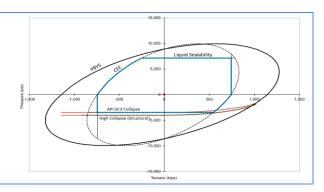
CONNECTION	PROPERTIES	
Connection Type	Semi-Premium Integ	gral Flush
Connection OD (nom):	8.665	in.
Connection ID (nom):	7.954	in.
Make-Up Loss	2.614	in.
Critical Cross Section	5.978	sqin.
Tension Efficiency	65.0	% of pipe
Compression Efficiency	65.0	% of pipe
Internal Pressure Efficiency	80.0	% of pipe
External Pressure Efficiency	100 0	% of pipe

CONNECTION PERFORMANCES		
Tensile Yield Strength	744	klb
Compression Resistance	744	klb
Max. Internal Pressure	7,150	psi
Structural Collapse Resistance	4,000	psi
Max. Structural Bending	41	°/100ft
Max. Bending with Sealability	10	°/100ft

TORQUE VALUE	S	
Min. Make-up torque	23,000	ft.lb
Opt. Make-up torque	25,500	ft.lb
Max. Make-up torque	28,000	ft.lb
Max. Torque with Sealability (MTS)	48,000	ft.lb

\* 87.5% RBW

VAM® SPRINT-FJ is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



#### Do you need help on this product? - Remember no one knows VAM<sup>®</sup> like VAM<sup>®</sup>

canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com

uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com

Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance

china@vamfieldservice.com baku@vamfieldservice.com singapore@vamfieldservice.com australia@vamfieldservice.com



#### Paint 4-33 Fed Com 711H

10 3/4	sur	face csg in a	14 3/4	inch hole.		Design	Factors			Surface	9	
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	45.50		j 55	btc	17.97	5.11	0.57	875	9	0.96	9.65	39,813
"B"			,	btc				0				0
_	w/8.4#/	g mud, 30min Sfc Csg Test	psig: 1.500	Tail Cmt	does not	circ to sfc.	Totals:	875				39,813
omparison o		nimum Required Cem					rotuis.	010				00,010
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
14 3/4	0.5563	485	698	487	43	9.00	3736	5M				1.50
14 3/4	0.3303	405	090	407	40	9.00	5750	JIW				1.50
urst Frac Grac	dient(s) for Segme	ent(s) A, B = , b All > (	D.70, OK.									
8 5/8	casir	ng inside the	10 3/4			Design	Factors			Int 1		
Segment	#/ft	Grade	10 3/4	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	32.00	Glaue	p 110	vam sprint fj	2.03	0.64	1.08	11,480	1 1	а-в 1.80	a-C 1.07	•
A "B"	52.00		pilo	vani spinit ij	2.03	0.04	1.00	,		1.00	1.07	307,30 <b>0</b>
В	10 ····						T-t-1	0				
	w/8.4#/	g mud, 30min Sfc Csg Test		ala dan sabita sa d	•	6 from 10	Totals:	11,480				367,36
				ided to achieve a top of		ft from su		875				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
9 7/8	0.1261	521	750	1455	-48	10.50	3965	5M				0.61
							sum of sx	Σ CuFt				Σ%exces
			6980				Sum OF SA					
<b>O V Tool(s):</b> by stage % :	nt yld > 1.35	32	<b>6980</b> 28				1013	1882				29
D V Tool(s): by stage % : Class 'C' tail cm Tail cmt			28				1013		a a	5 14		29
D V Tool(s): by stage % : class 'C' tail cm Tail cmt 5 1/2	casir	g inside the				Design Fa	1013	1882		Prod 1		
D V Tool(s): by stage % : class 'C' tail cm Tail cmt 5 1/2 Segment	casir #/ft		28 8 5/8	Coupling	Joint	Collapse	1013 <u>ctors</u> Burst	1882	B@s	a-B	a-C	Weigh
V Tool(s): by stage % : lass 'C' tail cm Tail cmt 5 1/2 Segment "A"	casir	g inside the	28	Coupling dwc/c is+	<b>Joint</b> 2.99		1013	1882 Length 22,374	<b>B@s</b> 2		a-C	Weigh 447,48
D V Tool(s): by stage % : class 'C' tail cm Tail cmt 5 1/2 Segment	casir #/ft 20.00	ng inside the Grade	28 <b>8 5/8</b> p 110			Collapse	1013 <u>ctors</u> Burst 2.16	1882 Length 22,374 0	<u> </u>	a-B	a-C	Weigh 447,48 0
D V Tool(s): by stage % : class 'C' tail cm Tail cmt 5 1/2 Segment "A"	casir #/ft 20.00	ng inside the Grade g mud, 30min Sfc Csg Test	28 <b>8 5/8</b> p 110 psig: 2,680	dwc/c is+	2.99	Collapse 1.82	1013 ctors Burst 2.16 Totals:	1882 Length 22,374 0 22,374	<u> </u>	a-B	a-C	Weigh 447,48 0 447,48
D V Tool(s): by stage % : class 'C' tail cmt 5 1/2 Segment "A" "B"	casir #/ft 20.00 w/8.4#/	ng inside the Grade g mud, 30min Sfc Csg Test	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter	dwc/c is+	2.99 11280	Collapse 1.82 ft from su	1013 ctors Burst 2.16 Totals: Inface or a	1882 Length 22,374 0	<u> </u>	a-B	a-C	Weigh 447,48 0 447,48 overlap.
D V Tool(s): by stage % : class 'C' tail cmt 5 1/2 Segment "A" "B" Hole	casir #/ft 20.00	ng inside the Grade g mud, 30min Sfc Csg Test	28 <b>8 5/8</b> p 110 psig: 2,680	dwc/c is+	2.99	Collapse 1.82	1013 ctors Burst 2.16 Totals: urface or a Calc	1882 Length 22,374 0 22,374 200 Req'd	<u> </u>	a-B	a-C	Weigh 447,48 0 447,48 overlap.
D V Tool(s): by stage % : Class 'C' tail cmt 51/2 Segment "A" "B"	casir #/ft 20.00 w/8.4#/	g inside the Grade g mud, 30min Sfc Csg Test The cement	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter	dwc/c is+	2.99 11280	Collapse 1.82 ft from su	1013 ctors Burst 2.16 Totals: Inface or a	1882 Length 22,374 0 22,374 200	<u> </u>	a-B	a-C	Weigh 447,480 0 447,480 overlap. Min Dist
D V Tool(s): by stage % : Class 'C' tail cm Tail cmt 5 1/2 Segment "A" "B" Hole	casir #/ft 20.00 w/8.4#/j Annular	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter 1 Stage	dwc/c is+ nded to achieve a top of Min	2.99 11280 1 Stage	Collapse 1.82 ft from su Drilling	1013 ctors Burst 2.16 Totals: urface or a Calc	1882 Length 22,374 0 22,374 200 Req'd	<u> </u>	a-B	a-C	Weigh 447,48 0 447,48
D V Tool(s): by stage % : Class 'C' tail cm Tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	28 8 5/8 p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+ nded to achieve a top of Min Cu Ft	2.99 11280 1 Stage % Excess	Collapse 1.82 ft from su Drilling Mud Wt	1013 ctors Burst 2.16 Totals: urface or a Calc	1882 Length 22,374 0 22,374 200 Req'd	<u> </u>	a-B	a-C	Weigh 447,480 0 447,480 overlap. Min Dis Hole-Cpl
D V Tool(s): by stage % : Class 'C' tail cm 5 1/2 Segment "A" "B" Hole Size 7 7/8 Class 'C' tail cm #IV/A	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	28 8 5/8 p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445	dwc/c is+ nded to achieve a top of Min Cu Ft	2.99 11280 1 Stage % Excess	Collapse 1.82 ft from su Drilling Mud Wt 10.50	1013 ctors Burst 2.16 Totals: urface or a Calc MASP	1882 Length 22,374 0 22,374 200 Req'd	2	<b>a-B</b> 3.62	<b>a-C</b> 3.05	Weigh 447,480 0 447,480 overlap. Min Dis Hole-Cpl
D V Tool(s): by stage % : Class 'C' tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 Class 'C' tail cm #N/A 0	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733 att yld > 1.35	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549	28 8 5/8 p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+ Ided to achieve a top of Min Cu Ft 1923	2.99 11280 1 Stage % Excess 27	Collapse 1.82 ft from su Drilling Mud Wt 10.50 Design	1013 ctors Burst 2.16 Totals: Irface or a Calc MASP Factors	1882 Length 22,374 0 22,374 200 Req'd BOPE	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19
D V Tool(s): by stage % : class 'C' tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	28 8 5/8 p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445	dwc/c is+	2.99 11280 1 Stage % Excess	Collapse 1.82 ft from su Drilling Mud Wt 10.50	1013 ctors Burst 2.16 Totals: urface or a Calc MASP	1882 Length 22,374 0 22,374 200 Req'd BOPE	2	<b>a-B</b> 3.62	<b>a-C</b> 3.05	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19 Weigh
D V Tool(s): by stage % : ilass 'C' tail cm 5 1/2 Segment "A" "B" Hole Size 7 7/8 ilass 'C' tail cm #N/A 0 Segment "A"	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733 att yld > 1.35	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549	28 8 5/8 p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445	dwc/c is+	2.99 11280 1 Stage % Excess 27	Collapse 1.82 ft from su Drilling Mud Wt 10.50 Design	1013 ctors Burst 2.16 Totals: Irface or a Calc MASP Factors	1882 Length 22,374 0 22,374 200 Req'd BOPE Length 0	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19 Weigh 0
D V Tool(s): by stage % : 'lass 'C' tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment	casir #/ft 20.00 w/8.4#/j Annular Volume 0.1733 nt yld > 1.35 #/ft	ng inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter 1 Stage CuFIC mt 2445 5 1/2	dwc/c is+	2.99 11280 1 Stage % Excess 27	Collapse 1.82 ft from su Drilling Mud Wt 10.50 Design	1013 ctors Burst 2.16 Totals: urface or a Calc MASP Factors Burst	1882 Length 22,374 0 22,374 200 Req'd BOPE	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19 1.19 Weigh 0 0
D V Tool(s): by stage % : ilass 'C' tail cm 5 1/2 Segment "A" "B" Hole Size 7 7/8 ilass 'C' tail cm #N/A 0 Segment "A"	casir #/ft 20.00 w/8.4#/j Annular Volume 0.1733 nt yld > 1.35 #/ft	ng inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade g mud, 30min Sfc Csg Test	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2	dwc/c is+	2.99 11280 1 Stage % Excess 27 #N/A	Collapse 1.82 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	1013 ctors Burst 2.16 Totals: urface or a Calc MASP Factors Burst Totals:	1882 Length 22,374 200 Req'd BOPE Length 0 0	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 0 447,48 0 447,48 0 447,48 0 447,48 0 1.19
D V Tool(s): by stage % : ilass 'C' tail cm 5 1/2 Segment "A" "B" Hole Size 7 7/8 ilass 'C' tail cm #N/A 0 Segment "A" "B"	casir #/ft 20.00 w/8.4#/r Annular Volume 0.1733 tt yld > 1.35 #/ft w/8.4#/r	ng inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade g mud, 30min Sfc Csg Test Cmt vol c	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445 5 1/2 psig: alc below includes	dwc/c is+	2.99 11280 1 Stage % Excess 27 #N/A	Collapse 1.82 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	1013 ctors Burst 2.16 Totals: urface or a Calc MASP Factors Burst Totals: urface or a	1882 Length 22,374 0 22,374 200 Req'd BOPE Length 0 0 0 #N/A	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0 0 0 0 0
D V Tool(s): by stage % : class 'C' tail cm 5 1/2 Segment "A" "B" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment "A" "B" Hole	casir #/ft 20.00 w/8.4#/r Annular Volume 0.1733 ut yld > 1.35 #/ft w/8.4#/r Annular	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445 <b>5 1/2</b> psig: alc below includes 1 Stage	dwc/c is+	2.99 11280 1 Stage % Excess 27 #N/A #N/A 1 Stage	Collapse 1.82 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	1013 ctors Burst 2.16 Totals: urface or a Calc MASP Factors Burst Totals: urface or a Calc	1882 Length 22,374 0 22,374 200 Req'd BOPE Length 0 0 0 0 #N/A Req'd	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0 overlap. Min Dis
D V Tool(s): by stage % : lass 'C' tail cmt 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	casir #/ft 20.00 w/8.4#/r Annular Volume 0.1733 tt yld > 1.35 #/ft w/8.4#/r	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade g mud, 30min Sfc Csg Test Cmt vol c 1 Stage Cmt Sx	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inten 1 Stage CuFt Cmt 2445 5 1/2 psig: alc below includes 1 Stage CuFt Cmt	dwc/c is+	2.99 11280 1 Stage % Excess 27 #N/A #N/A 1 Stage % Excess	Collapse 1.82 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	1013 ctors Burst 2.16 Totals: urface or a Calc MASP Factors Burst Totals: urface or a	1882 Length 22,374 0 22,374 200 Req'd BOPE Length 0 0 0 #N/A	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0 overlap. Min Dis
D V Tool(s): by stage % : lass 'C' tail cm 5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail cm #N/A 0 Segment "A" "B" Hole	casir #/ft 20.00 w/8.4#/r Annular Volume 0.1733 ut yld > 1.35 #/ft w/8.4#/r Annular	g inside the Grade g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1549 Grade g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	28 <b>8 5/8</b> p 110 psig: 2,680 volume(s) are inter 1 Stage CuFt Cmt 2445 <b>5 1/2</b> psig: alc below includes 1 Stage	dwc/c is+	2.99 11280 1 Stage % Excess 27 #N/A #N/A 1 Stage	Collapse 1.82 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	1013 ctors Burst 2.16 Totals: urface or a Calc MASP Factors Burst Totals: urface or a Calc	1882 Length 22,374 0 22,374 200 Req'd BOPE Length 0 0 0 0 #N/A Req'd	2	a-B 3.62	a-C 3.05 sing>	Weigh 447,48 0 447,48 0 447,48 0 447,48 0 447,48 0 447,48 0 1.19

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#### Paint 4-33 Fed Com 621H

	surfa	ace csg in a	14 3/4	inch hole.		Design	Factors			Surface	9	
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	45.50		j 55	btc	17.97	5.11	0.57	875	9	0.96	9.65	39,813
"B"			,	btc				0				0
	w/8.4#/g	mud, 30min Sfc Csg Test	psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	875				39,813
omparison o	f Proposed to Min	imum Required Cem	ent Volumes									
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
14 3/4	0.5563	485	698	487	43	9.00	3736	5M				1.50
urst Frac Grad	dient(s) for Segmer	nt(s) A, B = , b All > 0	).70, ОК.									
0 5 /0			10.2/4			Decima	E a a ta un		-	Int 1		
8 5/8		g inside the	10 3/4	Counting	laint	Design		l a marth	D@a		- 0	Mainh
Segment "A"	#/ft	Grade	p 110	Coupling	Joint	Collapse 0.64	Burst	Length	B@s	a-B	a-C	Weigh
"B"	32.00		p 110	vam sprint fj	2.03	0.04	1.09	11,480	1	1.82	1.07	
D	10 4111	mud 20min Cfr Crr T					Totals:	<b>0</b> 11,480				<b>0</b> 367,36
	w/8.4#/g	mud, 30min Sfc Csg Test		dad to achieve a ten of	0	ft from su		,				,
Ilala	Ammulan			ided to achieve a top of				875 Decid				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling Mud W/	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
9 7/8	0.1261	519	747	1455	-49	10.50	3930	5M				0.61
) V Tool(s):			6980				sum of sx	<u>Σ CuFt</u>				Σ%exces
by stage % : Class 'C' tail cm	1 11 4 25	32	28				1012	1881				29
Tail cmt												
		a incida tha	<u>ог/о</u>			Decign Fo	otoro		-	Dred 1		••=•=•
5 1/2		g inside the	8 5/8	Coupling	loint	Design Fa		Longth	Rea	Prod 1		
5 1/2 Segment	#/ft	g inside the Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
5 1/2 Segment "A"		0	<b>8 5/8</b> p 110	Coupling dwc/c is+	<b>Joint</b> 3.02			22,292	<b>B@s</b> 2		a-C	<b>Weigh</b> 445,84
5 1/2 Segment	<b>#/ft</b> 20.00	Grade	p 110			Collapse	<b>Burst</b> 2.18	22,292 0	-	a-B	a-C	Weigh 445,84 0
5 1/2 Segment "A"	<b>#/ft</b> 20.00	Grade mud, 30min Sfc Csg Test	p 110 psig: 2,657	dwc/c is+	3.02	Collapse 1.84	Burst 2.18 Totals:	22,292 <b>0</b> 22,292	-	a-B	a-C	Weigh 445,84 0 445,84
5 1/2 Segment "A" "B"	<b>#/ft</b> 20.00 w/8.4#/g	Grade mud, 30min Sfc Csg Test The cement	p 110 <sub>psig:</sub> 2,657 volume(s) are inter	dwc/c is+	3.02 11280	Collapse 1.84 ft from su	Burst 2.18 Totals: Irface or a	22,292 0 22,292 200	-	a-B	a-C	Weigh 445,84 0 445,84 overlap.
5 1/2 Segment "A" "B" Hole	#/ft 20.00 w/8.4#/g Annular	Grade mud, 30min Sfc Csg Test The cement 1 Stage	p 110 <sup>psig:</sup> 2,657 volume(s) are inter 1 Stage	dwc/c is+ nded to achieve a top of Min	3.02 11280 1 Stage	Collapse 1.84 ft from su Drilling	Burst 2.18 Totals: Irface or a Calc	22,292 0 22,292 200 Req'd	-	a-B	a-C	Weigh 445,84 0 445,84 overlap. Min Dis
5 1/2 Segment "A" "B" Hole Size	#/ft 20.00 w/8.4#/g Annular Volume	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+ Ided to achieve a top of Min Cu Ft	3.02 11280 1 Stage % Excess	Collapse 1.84 ft from su Drilling Mud Wt	Burst 2.18 Totals: Irface or a	22,292 0 22,292 200	-	a-B	a-C	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp
5 1/2 Segment "A" "B" Hole	#/ft 20.00 w/8.4#/g Annular Volume 0.1733	Grade mud, 30min Sfc Csg Test The cement 1 Stage	p 110 <sup>psig:</sup> 2,657 volume(s) are inter 1 Stage	dwc/c is+ nded to achieve a top of Min	3.02 11280 1 Stage	Collapse 1.84 ft from su Drilling	Burst 2.18 Totals: Irface or a Calc	22,292 0 22,292 200 Req'd	-	a-B	a-C	445,84
5 1/2 Segment "A" "B" Hole Size 7 7/8	#/ft 20.00 w/8.4#/g Annular Volume 0.1733	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+ Ided to achieve a top of Min Cu Ft	3.02 11280 1 Stage % Excess	Collapse 1.84 ft from su Drilling Mud Wt	Burst 2.18 Totals: Irface or a Calc	22,292 0 22,292 200 Req'd	-	a-B	a-C	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp
5 1/2 Segment "A" "B" Hole Size 7 7/8 Class 'C' tail or	#/ft 20.00 w/8.4#/g Annular Volume 0.1733	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt	dwc/c is+ Ided to achieve a top of Min Cu Ft	3.02 11280 1 Stage % Excess	Collapse 1.84 ft from su Drilling Mud Wt	Burst 2.18 Totals: Inface or a Calc MASP	22,292 0 22,292 200 Req'd	2	a-B	<b>a-C</b> 3.08	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp
5 1/2 Segment "A" "B" Hole Size 7 7/8 Class 'C' tail cm #N/A	#/ft 20.00 w/8.4#/g Annular Volume 0.1733	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt 2446	dwc/c is+ Ided to achieve a top of Min Cu Ft	3.02 11280 1 Stage % Excess	Collapse 1.84 ft from su Drilling Mud Wt 10.50	Burst 2.18 Totals: Inface or a Calc MASP	22,292 0 22,292 200 Req'd	2	a-B 3.65	<b>a-C</b> 3.08	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp
5 1/2 Segment "A" "B" Hole Size 7 7/8 Jass 'C' tail cm #N/A 0	#/ft 20.00 w/8.4#/g Annular Volume 0.1733 ht yld > 1.35	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1550	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt 2446	dwc/c is+	3.02 11280 1 Stage % Excess 28	Collapse 1.84 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: urface or a Calc MASP Factors	22,292 0 22,292 200 Req'd BOPE	2	a-B 3.65	a-C 3.08 sing>	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp 1.19
5 1/2 Segment "A" "B" Hole Size 7 7/8 iJass 'C' tail cm #N/A 0 Segment	#/ft 20.00 w/8.4#/g Annular Volume 0.1733 ht yld > 1.35	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1550	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt 2446	dwc/c is+	3.02 11280 1 Stage % Excess 28	Collapse 1.84 ft from su Drilling Mud Wt 10.50 Design	Burst 2.18 Totals: urface or a Calc MASP Factors	22,292 0 22,292 200 Req'd BOPE	2	a-B 3.65	a-C 3.08 sing>	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp 1.19 Weigh
5 1/2 Segment "A" "B" Hole Size 7 7/8 Jass 'C' tail cm #N/A 0 Segment "A"	#/ft 20.00 w/8.4#/g Annular Volume 0.1733 nt yld > 1.35 #/ft	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1550 Grade mud, 30min Sfc Csg Test	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt 2446 5 1/2 psig:	dwc/c is+	3.02 11280 1 Stage % Excess 28 #N/A	Collapse 1.84 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.18 Totals: urface or a Calc MASP Factors Burst Totals:	22,292 0 22,292 200 Req'd BOPE	2	a-B 3.65	a-C 3.08 sing>	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp 1.19 Weigh 0 0 0
5 1/2 Segment "A" "B" Hole Size 7 7/8 lass 'C' tail on #N/A 0 Segment "A" "B"	#/ft 20.00 w/8.4#/g Annular Volume 0.1733 ht yld > 1.35 #/ft w/8.4#/g	Grade mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1550 Grade mud, 30min Sfc Csg Test Cmt vol c	p 110 psig: 2,657 volume(s) are inter 1 Stage CuFt Cmt 2446 5 1/2 psig: alc below includes	dwc/c is+	3.02 11280 1 Stage % Excess 28 #N/A #N/A	Collapse 1.84 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.18 Totals: urface or a Calc MASP Factors Burst	22,292 0 22,292 200 Req'd BOPE Length 0 0 0 #N/A	2	a-B 3.65	a-C 3.08 sing>	Weigh 445,84 0 445,84 overlap. Min Dis Hole-Cp 1.19 
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.



### <u>10-3/4"</u> <u>45.50#</u> <u>0.400"</u> <u>J-55</u>

### **Dimensions (Nominal)**

Outside Diameter Wall Inside Diameter Drift	10.750 0.400 9.950 9.875	in. in. in. in.
Weight, T&C Weight, PE	45.500 44.260	lbs/ft lbs/ft
Internal Yield Pressure at Minimum Yield		
Collapse	2090	psi
Internal Yields Pressure		
PE	3580	psi
STC	3580	psi
BTC	3580	psi
Yield Strength, Pipe Body	715	1000 lbs
Joint Strength, STC		
STC	493	1000 lbs
ВТС	796	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.



### **Connection Data Sheet**

OD (in.)	WEIGHT (Ibs./ft.)	WALL (in.)	GRADE	DRIFT (in.)	RBW%	CONNECTION
5.500	Nominal: 20.00 Plain End: 19.83	0.361	VST P110 EC	4.653	87.5	DWC/C-IS PLUS

#### PIPE PROPERTIES

Nominal OD	5.500	in.
Nominal ID	4.778	in.
Nominal Area	5.828	sq.in.
Grade Type	API 5CT; Vallourec Sourced Material Only	
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Tensile Strength	135	ksi
Yield Strength	729	klb
Ultimate Strength	787	klb
Min. Internal Yield	14,360	psi
*High Collapse*	12,090	psi

#### **CONNECTION PROPERTIES**

Connection Type	Semi-Premium T&C	
Connection OD (nom)	6.300	in.
Connection ID (nom)	4.778	in.
Make-Up Loss	4.125	in.
Coupling Length	9.250	in.
Critical Cross Section	5.828	sq.in.
Tension Efficiency	100.0%	of pipe
Compression Efficiency	100.0%	of pipe
Internal Pressure Efficiency	100.0%	of pipe
External Pressure Efficiency	100.0%	of pipe

#### **CONNECTION PERFORMANCES** 729 klb Yield Strength Parting Load 787 klb **Compression Rating** 729 klb Min. Internal Yield 14,360 psi \*High Collapse\* 12,090 psi Maximum Uniaxial Bend Rating 104.2 °/100 ft Ref String Length w 1.4 Design Factor 26,040 ft

FIELD TORQUE VALUES		
Min. Make-up Torque	16,600	ft.lbs
Opti. Make-up Torque	17,850	ft.lbs
Max. Make-up Torque	19,100	ft.lbs
Min. Shoulder Torque	1,660	ft.lbs
Max. Shoulder Torque	13,280	ft.lbs
Max. Delta Turn	0.200	Turns
+Max Operational Torque	24,300	ft.lbs
+Maximum Torsional Value (MTV)	26,730	ft.lbs

#### +Maximum Operational Torque and Maximum Torsional Value Only Valid with Vallourec P110EC Material

#### For detailed information on performance properties, refer to DWC Connection Data Notes on following page(s).

Connection specifications within the control of VAM USA were correct as of the date printed. Specifications are subject to change without notice. Certain connection specifications are dependent on the mechanical properties of the pipe. Mechanical properties of mill proprietary pipe grades were obtained from mill publications and are subject to change. Properties of mill proprietary grades should be confirmed with the mill. Users are advised to obtain current connection specifications and verify pipe mechanical properties for each application.

All information is provided by VAM USA or its affiliates at user's sole risk, without liability for loss, damage or injury resulting from the use thereof; and on an "AS IS" basis without warranty or representation of any kind, whether express or implied, including without limitation any warranty of merchantability, fitness for purpose or completeness. This document and its contents are subject to change without notice. In no event shall VAM USA or its affiliates be responsible for any indirect, special, incidental, punitive, exemplary or consequential loss or damage (including without limitation, loss of use, loss of bargain, loss of revenue, profit or anticipated profit) however caused or arising, and whether such losses or damages were foreseeable or VAM USA or its affiliates was advised of the possibility of such damages.

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VAM USA 2107 CityWest Boulevard Suite 1300 Houston, TX 77042 Phone: 713-479-3200 Fax: 713-479-3234 VAM USA Sales E-mail: <u>VAMUSAsales@vam-usa.com</u> Tech Support E-mail: tech.support@vam-usa.com

#### DWC Connection Data Notes:

- 1. DWC connections are available with a seal ring (SR) option.
- 2. All standard DWC/C connections are interchangeable for a given pipe OD. DWC connections are interchangeable with DWC/C-SR connections of the same OD and wall.
- 3. Connection performance properties are based on nominal pipe body and connection dimensions.
- DWC connection internal and external pressure resistance is calculated using the API rating for buttress connections. API Internal pressure resistance is calculated from formulas 31, 32, and 35 in the API Bulletin 5C3.
- 5. DWC joint strength is the minimum pipe body yield strength multiplied by the connection critical area.
- 6. API joint strength is for reference only. It is calculated from formulas 42 and 43 in the API Bulletin 5C3.
- 7. Bending efficiency is equal to the compression efficiency.
- 8. The torque values listed are recommended. The actual torque required may be affected by field conditions such as temperature, thread compound, speed of make-up, weather conditions, etc.
- 9. Connection yield torque is not to be exceeded.
- Reference string length is calculated by dividing the joint strength by both the nominal weight in air and a design factor (DF) of 1.4. These values are offered for reference only and do not include load factors such as bending, buoyancy, temperature, load dynamics, etc.
- 11. DWC connections will accommodate API standard drift diameters.
- 12. DWC/C family of connections are compatible with API Buttress BTC connections. Please contact tech.support@vam-usa.com for details on connection ratings and make-up.

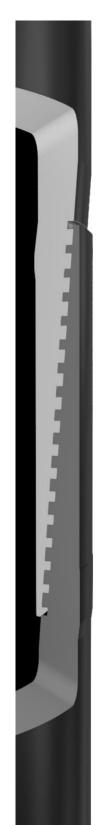
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All information is provided by VAM USA or its affiliates at user's sole risk, without liability for loss, damage or injury resulting from the use thereof; and on an "AS IS" basis without warranty or representation of any kind, whether express or implied, including without limitation any warranty of merchantability, fitness for purpose or completeness. This document and its contents are subject to change without notice. In no event shall VAM USA or its affiliates be responsible for any indirect, special, incidental, punitive, exemplary or consequential loss or damage (including without limitation, loss of use, loss of bargain, loss of revenue, profit or anticipated profit) however caused or arising, and whether such losses or damages were foreseeable or VAM USA or its affiliates was advised of the possibility of such damages.

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Issued on: 16	Sep. 2022	by Logan Va	n Gorp



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VAM<sup>®</sup> SPRINT-FJ

H	IGH	IER	то	RQ	UE	VEF	RSI	ON	

OD

8 5/8 in.

		<b>Connection Data Sheet</b>
Grade	Alt. Drift:	Connection

7.875 in.

PIPE PROPERTIES		
Nominal OD	8.625	in.
Nominal ID	7.921	in.
Nominal Cross Section Area	9.149	sqin.
Grade Type	Hig	jh Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi

Weight (lb/ft)

Nominal: 32.00 Plain End: 31.13 Wall Th.

0.352 in.

P110EC

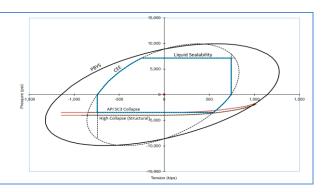
CONNECTION	N PROPERTIES	
Connection Type	Semi-Premium Integ	ral Flush
Connection OD (nom):	8.665	in.
Connection ID (nom):	7.954	in.
Make-Up Loss	2.614	in.
Critical Cross Section	5.978	sqin.
Tension Efficiency	65.0 %	6 of pipe
Compression Efficiency	65.0 %	6 of pipe
Internal Pressure Efficiency	80.0 %	6 of pipe
External Pressure Efficiency	100 %	6 of pipe

CONNECTION PERFORMANCES		
Tensile Yield Strength	744	klb
Compression Resistance	744	klb
Max. Internal Pressure	7,150	psi
Structural Collapse Resistance	4,000	psi
Max. Structural Bending	41	°/100ft
Max. Bending with Sealability	10	°/100ft

TORQUE VALUE	S	
Min. Make-up torque	23,000	ft.lb
Opt. Make-up torque	25,500	ft.lb
Max. Make-up torque	28,000	ft.lb
Max. Torque with Sealability (MTS)	48,000	ft.lb

\* 87.5% RBW

VAM® SPRINT-FJ is a semi-premium flush connection designed for shale applications, where maximum clearance and high tension capacity are required for intermediate casing strings.



#### Do you need help on this product? - Remember no one knows VAM<sup>®</sup> like VAM<sup>®</sup>

canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com

uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com

Over 140 VAM® Specialists available worldwide 24/7 for Rig Site Assistance

china@vamfieldservice.com baku@vamfieldservice.com singapore@vamfieldservice.com australia@vamfieldservice.com



# Section 2 - Blowout Preventer Testing Procedure

# Variance Request

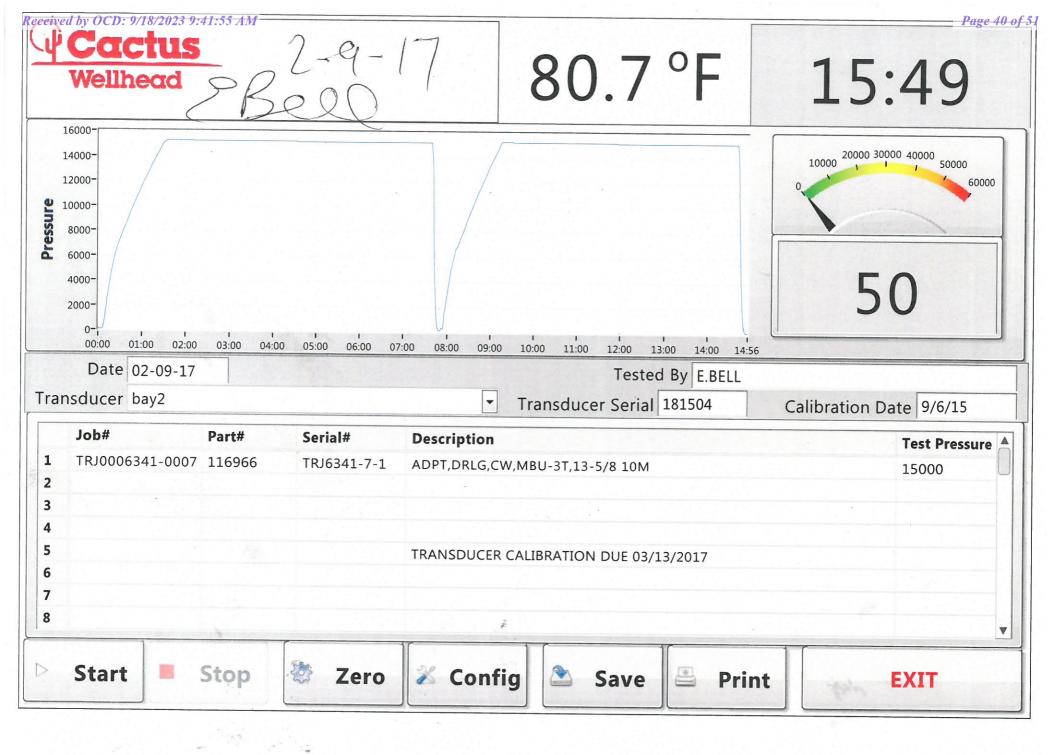
Devon Energy requests to only test BOP connection breaks after drilling out of surface casing and while skidding between wells which conforms to API Standard 53 and industry standards. This test will include the Top Pipe Rams, HCR, Kill Line Check Valve, QDC (quick disconnect to wellhead) and Shell of the 10M BOPE to 5M for 10 minutes. If a break to the flex hose that runs to the choke manifold is required due to repositioning from a skid, the HCR will remain open during the shell test to include that additional break. The variance only pertains to intermediate hole-sections and no deeper than the Bone Springs Formation where 5M BOP tests are required. The initial BOP test will follow OOGO2.III.A.2.i, and subsequent tests following a skid will only test connections that are broken. The annular preventer will be tested to 100% working pressure. This variance will meet or exceed OOGO2.III.A.2.i per the following: Devon Energy will perform a full BOP test per OOGO2.III.A.2.i before drilling out of the intermediate casing string(s) and starting the production hole, before starting any hole section that requires a 10M test, before the expiration of the allotted 14-days for 5M intermediate batch drilling or when the drilling rig is fully mobilized to a new well pad, whichever is sooner. We will utilize a 200' TVD tolerance between intermediate shoes as the cutoff for a full BOP test. The BLM will be contacted 4hrs prior to a BOPE test. The BLM will be notified if and when a well control event is encountered. Break test will be a 14 day interval and not a 30 day full BOPE test interval. If in the event break testing is not utilized, then a full BOPE test would be conducted.

1. Well Control Response:

1. Primary barrier remains fluid

2. In the event of an influx due to being underbalanced and after a realized gain or flow, the order of closing BOPE is as follows:

- a) Annular first
- b) If annular were to not hold, Upper pipe rams second (which were tested on the skid BOP test)
- c) If the Upper Pipe Rams were to not hold, Lower Pipe Rams would be third



## 1. Geologic Formations

TVD of target	12075	Pilot hole depth	N/A
MD at TD:	22292	Deepest expected fresh water	

Basin

Dasm			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	770		
Salt	1075		
Base of Salt	4420		
Delaware	4690		
Cherry Canyon	5570		
Brushy Canyon	6980		
1st Bone Spring Lime	8530		
Bone Spring 1st	9630		
Bone Spring 2nd	10230		
3rd Bone Spring Lime	10760		
Bone Spring 3rd	11480		
Wolfcamp	11950		

\*H2S, water flows, loss of circulation, abnormal pressures, etc.

		Wt (PPF)				Interval	Casing	Interval
Hole Size	Csg. Size		Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45.5	J55	BTC	0	795	0	795
9 7/8	8 5/8	32	P110	Sprint FJ	0	11480	0	11480
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22292	0	12075

#### 2. Casing Program

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	485	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	493	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	519	7012	13.2	1.44	Tail: Class H / C + additives
Production	117	9464	9	3.27	Lead: Class H /C + additives
Froduction	1433	11464	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

.

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:			
			Anı	nular	X	50% of rated working pressure			
Int 1	13-5/8"	5M		d Ram	X				
int i	15 5/0	5101	<b>1</b>	e Ram		- 5M			
				le Ram	Х	5101			
			Other*						
	13-5/8"		Annular (5M)		Х	100% of rated working pressure			
Production		10M	Blind Ram		Х				
Tioduction		10101	Pipe Ram			10M			
			Double Ram		Х	10101			
			Other*						
			Annul	ar (5M)					
			Blind Ram Pipe Ram Double Ram						
			Other*						
N A variance is requested for	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.								
Y A variance is requested to r	A variance is requested to run a 5 M annular on a 10M system								

## 4. Pressure Control Equipment (Three String Design)

#### 5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)		
Surface	FW Gel	8.5-9		
Intermediate	DBE / Cut Brine	10-10.5		
Production	OBM	10-10.5		

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
---	-----------------------------

#### 6. Logging and Testing Procedures

Logging,	Logging, Coring and Testing						
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the						
Х	Completion Report and sbumitted to the BLM.						
	No logs are planned based on well control or offset log information.						
	Drill stem test? If yes, explain.						
	Coring? If yes, explain.						

Addition	al logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6593
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations<br/>greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered<br/>measured values and formations will be provided to the BLM.NH2S is present

Y H2S plan attached.

# 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe

## 1. Geologic Formations

TVD of target	12075	Pilot hole depth	N/A
MD at TD:	22292	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
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	from KB	Zone?	
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	w a a Wt a				Casing	Interval	Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
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9 7/8	8 5/8	32	P110	Sprint FJ	0	11480	0	11480
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	22292	0	12075

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			Other*						
	13-5/8"		Annular (5M)		Х	100% of rated working pressure			
Production		10M	Blind Ram		Х				
Tioduction		10101	Pipe Ram			10M			
			Double Ram		Х	10101			
			Other*						
			Annul	ar (5M)					
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## 5. Mud Program (Three String Design)

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What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
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	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the	
X Completion Rpeort and sbumitted to the BLM.		
	No logs are planned based on well control or offset log information.	
	Drill stem test? If yes, explain.	
	Coring? If yes, explain.	

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

#### 7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6593
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations		
greater than	ter than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered	
measured values and formations will be provided to the BLM.		
Ν	H2S is present	

Y H2S plan attached.

# 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).

 $^{3}$  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

#### Attachments

X Directional Plan Other, describe

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

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# **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	266239
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
pkautz	IF ON ANY STRING CEMENT DOES NOT CIRCULATE, A RCBL MUST BE RUN ON THAT STRING OF CASING.	10/2/2023

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