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Form 3160-5 (June 2019)		UNITED STATES ARTMENT OF THE INTERIO				Ex	OMB N	I APPROVED No. 1004-0137 October 31, 2021
	BURI	EAU OF LAND MANAGEMEN	T			5. Lease Serial No. NMNM059060		
SUNDRY NOTICES AND REPORTS ON WELLS Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.						6. If Indian, Allottee or Tribe Name		
SOBMIT IN TRIPLICATE - Other Instructions on page 2						7. If Unit of CA/Agr	eement	t, Name and/or No.
1. Type of Well     Image: Oil Well	Gas W	/ell Other				8. Well Name and No	<sup>).</sup> ROS	SS DRAW 17 FED COM/592H
2. Name of Operator EOG R	ESOURC	CES INCORPORATED				9. API Well No. 30-0	)15-48	3498
3a. Address 1111 BAGBY S		E	,	ıde area code		10. Field and Pool or PURPLE SAGE;	Explo	oratory Area
4. Location of Well (Footage, SEC 17/T26S/R31E/NMP	Sec., T.,R	.,M., or Survey Description)				11. Country or Parish EDDY/NM	i, State	
	12. CHE	CK THE APPROPRIATE BOX(ES) TO	INDICA	TE NATURE	E OF NOTI	CE, REPORT OR OT	HER E	DATA
TYPE OF SUBMISSIC	N			TY	PE OF ACT	TION		
✓ Notice of Intent			eepen lydraulic	Fracturing		uction (Start/Resume)		Water Shut-Off Well Integrity
Subsequent Report			lew Cons lug and A		Recomplete   Other     Temporarily Abandon			
Final Abandonment No	tice	Convert to Injection	lug Back		Wate	er Disposal		
the Bond under which the completion of the involve completed. Final Abandor is ready for final inspectio	work will d operatio ment Not n.) wests an a	Ily or recomplete horizontally, give subs be perfonned or provide the Bond No. ns. If the operation results in a multiple ices must be filed only after all requiren amendment to our approved APD for	on file wi completionents, inc	th BLM/BIA on or recomp luding reclan	. Required letion in a	subsequent reports m new interval, a Form	ust be f 3160-4	filed within 30 days following must be filed once testing has be
Ripple 32 Fed Com 7 <sup>-</sup>	18H (FKA	A Ross Draw 17 Fed Com 592H) AP	l #: 30-0	15-48498				
Change name from R	oss Draw	/ 17 Fed Com 592H to Ripple 32 Fed	d Com 7	18H.				
Change BHL from T-2 to T-26-S, R-31-E, Se	ldy Co.,	NM,						
Change target formati	on to Wc	lfcamp Clastics Y.						
Continued on page 3 a	dditional	information						
14. I hereby certify that the foregoing is true and correct. Name ( <i>Printed/Typed</i> ) STAR HARRELL / Ph: (432) 848-9161				Regulatory Specialist Title				
Signature				Date 09/07/2023				
		THE SPACE FOR FE		L OR ST	ATE OF	ICE USE		
Approved by								
KEITH P IMMATTY / Ph: (	575) 988	-4722 / Approved		ENG Title	INEER		Date	09/11/2023
Conditions of approval, if any, certify that the applicant holds		Office CARLSBAD						

certify that the applicant holds legal or equitable title to those rigi which would entitle the applicant to conduct operations thereon.

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

#### **GENERAL INSTRUCTIONS**

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

#### SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13:* Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

#### NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

#### **Additional Information**

#### **Additional Remarks**

Update casing and cement program to current design.

Update HSU to 1862 acres.

Update the Pool as reflected in the C-102.

#### Location of Well

0. SHL: SWNE / 2595 FNL / 2626 FEL / TWSP: 26S / RANGE: 31E / SECTION: 17 / LAT: 32.042951 / LONG: -103.800317 ( TVD: 0 feet, MD: 0 feet ) PPP: SWNE / 2564 FNL / 1732 FEL / TWSP: 26S / RANGE: 31E / SECTION: 17 / LAT: 32.043041 / LONG: -103.797434 ( TVD: 10319 feet, MD: 10373 feet ) BHL: NWNE / 100 FNL / 1732 FEL / TWSP: 26S / RANGE: 31E / SECTION: 8 / LAT: 32.064458 / LONG: -103.797385 ( TVD: 10584 feet, MD: 18267 feet )

DISTRICT I French Dr., Hobbs, NM 88240 (575) 393-6161 Fax: (575) 393-0720 Hobbs, NM 88240 DISTRICT II 811 S. First St., Artes ia, NM 88210 -1283 Fax: (575) 748-9720 DISTRICT III Rd., Aztec, NM 87410 I-6178 Fax: (505) 334-6170 DISTRICT IV 1220 S. St. Francis Dr., Santa Fe, NM 8750 Phone: (505) 476-3460 Fax: (505) 476-346

#### State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, New Mexico 87505

Page 4 of 45 Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

□ AMENDED REPORT

#### WELL LOCATION AND ACREAGE DEDICATION PLAT API Number Pool Cod 30-015-48498 98220 Purple Sage; Wolfcamp (Gas) Well Number Property Code Property Name 332916 **RIPPLE 32 FED COM** 718H OGRID No. Operator Name Elevation 7377 EOG RESOURCES, INC. 3248' Surface Location UL or lot no Section Township Range Lot Idn Feet from the North/South line Feet from the East/West line County G 17 26 S 31 E 2595 NORTH 2626 EAST EDDY Bottom Hole Location If Different From Surface UL or lot no Section Township Lot Idr Feet from the East/West line Range Feet from the County 2 32 26 S 1850 EDDY 31 E NORTH 1871 EAST Dedicated Acres Joint or Infill Consolidated Code Order No PENDING NSP & PENDING COM AGREEMENT 1862 No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division. 718 8 9 SURFACE LOCATION 16 X = 706442 17 18 17 FED PERF. POINT Y = 382366' X = 709095' Y = 382384' = 709095 NEW MEXICO EAST = 703791 = 382349 NEW MEXICO EAST NAD 1983 NAD 1983 X=707537' Y=378378' X=706490' Y=379771' USA NMNM-59060 LAT=N32 042951° LAT=N32.039107 LONG=W103.800317° LONG=W103.796961° NAD 1927 NAD 1927 X=665304' Y=379714' X = 709116' Y = 379719' X=666351' Y=378321' SHL 2626 LAT=N32.042826° KOP LAT=N32.038982° X = 703806' Y = 379687' LONG=W103.799842° 1590 LONG=W103.796485° 2595' FNL 2626' FEL 1590 1590' FEL 330 FTP AZ = 108.23° 1093.3' 2612 **KOP LOCATION** FED PERF. POINT FFD NEW MEXICO EAST NEW MEXICO EAST NAD 1983 X=707527' Y=379659' NAD 1983 X=707548' Y=377047' USA NMNM-141527 X = 703820' Y = 377026' LAT=N32.042629° X = 709138 LAT=N32.035448° 179.53<sup>°</sup> 2382.1 AZ = Y = 377057 LONG=W103.796974° LONG=W103.796946° 16 18 17 NAD 1927 NAD 1927 X=666362' Y=376990' X=666340' Y=379602' 20 21 19 FED LAT=N32.042504° LAT=N32.035323° LONG=W103.796499 LONG=W103.796472° 2612' FSL 1590' FEL 1590' FEL LOWER MOST PERF./ FIRST TAKE POINT **BOTTOM HOLE LOCATION** NEW MEXICO EAST NEW MEXICO EAST Ĩ NAD 1983 5327 NAD 1983 X=707529' Y=379379' USA NMNM-0437880 ģ X=707355' Y=364544' LAT=N32.041859° X = 703840'AZ = 179.50° X = 709161' Y = 374392' SPAC = 374363 LAT=N32.001080° LONG=W103.796971° LONG=W103.797769° NAD 1927 X=666342' Y=379322 PH NAD 1927 X=666168' Y=364487' LAT=N32.041734° LAT=N32.000955° LONG=W103.796496° LONG=W103.797296° 2332' FSL 1590' FEL 1850' FNL 1871' FEL X = 703858' Y = 371702' = 709184 X = 709184 Y = 371729 AZ = 220.12° 433.4' 19 20 21 29 28 30 USA NMNM-138867 4995.6' = 703875' = 369040' X = 709201 Y = 369066 SURVEYORS CERTIFICATION = 179.64° **DIEXALOK CERTIFICATION** I hereby certify that the information contained herei is true and complete to the best of my knowledge an beilef, and that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of such a mineral or working interest, or to voluntary pooling agreement or a compulsory pooling order heretofore entered by the division. OPERATOR CERTIFICATION I hereby certify that the well location shown on ti plat was plotted from field notes of actual survey made by me or under my supervision, and that it same is true and correct to the best of my belief. MARCH 21, 2023 eys the Å 330 e and Seal of Professional Surveyor RHB. CHUST X = 703890 Y = 366378 X = 709218 Y = 366402 28 30 29 W MELICO 5 <u>AZ = 179.75°</u> 1849.8 32 33 31 Star L Harrell 9/6/23 26264 PROFE ST NM E-0920-2 YOR 850 Star L Harrell LMP/BHL LOT 1 LOT 2 LOT 4 LOT 3 X = 703902' Y = 364194' 1871'• X = 706566' Y = 364209' star\_harrell@eogresources.com = 709227 330 = 364224 N<u>M</u> TX

Released to Imaging: 11/20/2023 2:26:11 PM

E-mail Address

Job No.: EOG B190025 RALPH B. CHUSTZ, JR. N.M.P.L.S. Certificate Number 26264

#### PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

#### ALL PREVIOUS COAs STILL APPLY

OPERATOR'S NAME:	EOG Resources Incorporated
WELL NAME & NO.:	RIPLLE 32 FED COM 718H
SURFACE HOLE FOOTAGE:	2595'/N & 2626'/E
BOTTOM HOLE FOOTAGE	1850'/N & 1871'/E
LOCATION:	Section 17, T.26 S., R.31 E.
COUNTY:	Eddy County, New Mexico

#### COA

H2S	• Yes	O No	
Potash	None	Secretary	© R-111-P
Cave/Karst Potential	O Low	Medium	O High
Cave/Karst Potential	Critical		
Variance	O None	Flex Hose	Other
Wellhead	Conventional	Multibowl	O Both
Other	□4 String Area	Capitan Reef	WIPP
Other	Fluid Filled	Cement Squeeze	Pilot Hole
Special Requirements	□ Water Disposal	COM	🗹 Unit

#### A. CASING

#### Alternative Casing Design A:

- 1. The **9-5/8** inch surface casing shall be set at approximately **1,100** feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u>
     <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength,

whichever is greater.

- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The **7-5/8** inch intermediate casing shall be set at approximately **10,204** feet The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### **Option 2:**

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:
  - Cement to surface. If cement does not circulate, contact the appropriate BLM office.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
- In <u>Medium Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

# Operator has proposed to pump down 9-5/8" X 7-5/8" annulus. <u>Operator must run</u> a CBL OR ECHOMETER from TD of the 7-5/8" casing to surface. Submit results to BLM.

3. The **5-1**/2 inch production casing shall be set at approximately **26,365** feet The minimum required fill of cement behind the **5-1**/2 inch production casing is:

#### **Option 1 (Single Stage):**

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **Option 2:**

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:
  - Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **Alternative Casing Design B:**

- 1. The **10-3/4** inch surface casing shall be set at approximately **1,100** feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface.
  - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - f. Wait on cement (WOC) time for a primary cement job will be a minimum of  $\underline{8}$ <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - h. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The **8-3/4** inch intermediate casing shall be set at approximately **10,204** feet. **Keep** casing full during run for collapse SF. The minimum required fill of cement behind the **8-3/4** inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### **Option 2:**

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- c. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- d. Second stage above DV tool:
  - Cement to surface. If cement does not circulate, contact the appropriate BLM office.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
- In <u>Medium Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

# Operator has proposed to pump down 10-3/4" X 8-3/4" annulus. <u>Operator must run</u> a CBL OR ECHOMETER from TD of the 8-3/4" casing to surface. Submit results to BLM.

3. The **6** inch production casing shall be set at approximately **26,365** feet. **Keep casing full for collapse SF.** The minimum required fill of cement behind the **6** inch production casing is:

#### **Option 1 (Single Stage):**

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **Option 2:**

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- c. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- d. Second stage above DV tool:

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **B. SPECIAL REQUIREMENT (S)**

#### (Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system) BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (**575-706-2779**) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

#### **Offline Cementing**

Approved for surface and intermediate intervals. Notify the BLM prior to the commencement of any offline cementing procedure.

#### **Casing Clearance:**

- Overlap clearance OK for production casing
- Operator aware of risks with <1" clearance for surface interval

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

#### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Eddy County
 EMAIL or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,
 BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV (575) 361-2822

- Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or

if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24 hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.

- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in 43
     CFR part 3170 Subpart 3172 must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been

done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

**KPI** 9/11/2023



#### **Ripple 32 Fed Com Package**

Wells in package:	Tgt TVD
Ripple 32 Fed Com #703H	11,396
Ripple 32 Fed Com #705H	11,396
Ripple 32 Fed Com #707H	11,396
Ripple 32 Fed Com #716H	11,446
Ripple 32 Fed Com #717H	11,446
Ripple 32 Fed Com #718H	11,446
Ripple 32 Fed Com #730H	11,703
Ripple 32 Fed Com #732H	11,703
Ripple 32 Fed Com #734H	11,703
Ripple 32 Fed Com #736H	11,703
Ripple 32 Fed Com #737H	11,703
Ripple 32 Fed Com #738H	11,703

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## **S**eog resources

#### Ripple 32 Fed Com 718H

#### **Revised Permit Information 08/29/2023:**

Well Name: Ripple 32 Fed Com 718H

Location: SHL: 2595' FNL & 2626' FEL, Section 17, T-26-S, R-31-E, Eddy Co., N.M. BHL: 1850' FNL & 1871' FEL, Section 32, T-26-S, R-31-E, Eddy Co., N.M.

#### **Casing Program:**

Hole	Interval MD		Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
11"	0	1,100	0	1,100	9-5/8"	36#	J-55	LTC
8-3/4"	0	10,204	0	10,170	7-5/8"	29.7#	HCP-110	FXL
6-3/4"	0	9,704	0	9,670	5-1/2"	20#	P110-EC	DWC/C IS MS
6-3/4"	9,704	10,204	9,670	10,170	5-1/2"	20#	P110-EC	Vam Sprint SF
6-3/4"	10,204	26,365	10,170	11,220	5-1/2"	20#	P110-EC	DWC/C IS MS

Variance is requested to waive the centralizer requirements for the 7-5/8" casing in the 8-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 8-3/4" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive the annular clearance requirements for the 5-1/2" casing by 7-5/8" casing annulus to the proposed top of cement.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement from Onshore Order #2 under the following conditions:

- Annular clearance to meet or exceed 0.422" between intermediate casing ID and production casing coupling only on the first 500' overlap between both casing strings.
- Annular clearance less than 0.422" is acceptable for the production open hole section.

		Wt.	Yld	Slurry Description	
Depth	No. Sacks	ppg	Ft3/sk	Siurry Description	
1,100'	220	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-	
9-5/8''				Flake (TOC @ Surface)	
	50	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium	
				Metasilicate (TOC @ 900')	
10,170'	490	14.2	1.11	1st Stage (Tail): Class C + 0.6% Halad-9 + 0.45% HR-601 + 3%	
7-5/8''				Microbond (TOC @ 6,000')	
	1030	14.8	1.5	2nd Stage (Bradenhead squeeze): Class C + 3% Salt + 1% PreMag-	
				M + 6% Bentonite Gel (TOC @ surface)	
26,365'	2720	13.2	1.41	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond	
5-1/2''				(TOC @ 9,670')	

#### **Cementing Program:**



Additive	Purpose					
Bentonite Gel	Lightweight/Lost circulation prevention					
Calcium Chloride	Accelerator					
Cello-flake	Lost circulation prevention					
Sodium Metasilicate	Accelerator					
MagOx	Expansive agent					
Pre-Mag-M	Expansive agent					
Sodium Chloride	Accelerator					
FL-62	Fluid loss control					
Halad-344	Fluid loss control					
Halad-9	Fluid loss control					
HR-601	Retarder					
Microbond	Expansive Agent					

EOG requests variance from minimum standards to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon (6,204') and the second stage performed as a 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of 30 sacks of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. Top will be verified by Echo-meter.

EOG will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

EOG will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

0				
<b>Measured Depth</b>	Туре	Weight (ppg)	Viscosity	Water Loss
0 - 1,100'	Fresh - Gel	8.6-8.8	28-34	N/c
1,100' - 10,170'	Brine	10.0-10.2	28-34	N/c
10,170' - 10,776'	Oil Base	8.7-9.4	58-68	N/c - 6
10,776' - 26,365'	Oil Base	10.0-14.0	58-68	4 - 6
Lateral	On Dase	10.0-14.0	56-08	4-0

#### **Mud Program:**



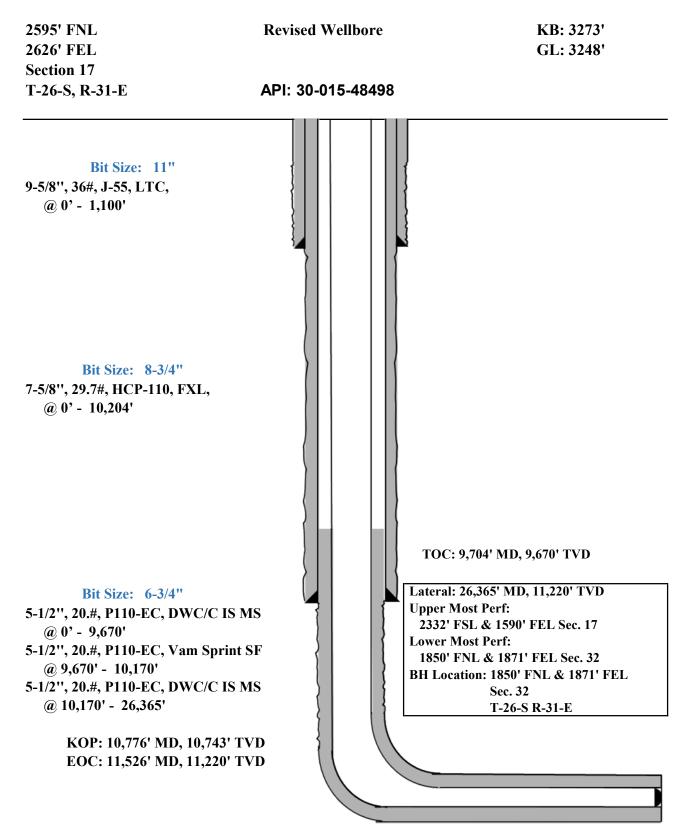
#### **TUBING REQUIREMENTS**

EOG respectively requests an exception to the following NMOCD rule:

 19.15.16.10 Casing AND TUBING RQUIREMENTS: J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.







#### **Design B** 4. CASING PROGRAM

Hole	Interval MD		Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
13"	0	1,100	0	1,100	10-3/4"	40.5#	J-55	STC
9-7/8"	0	10,204	0	10,170	8-3/4"	38.5#	P110-EC	SLIJ II NA
7-7/8"	0	26,365	0	11,220	6"	22.3#	P110-EC	DWC/C IS

Variance is requested to waive the centralizer requirements for the 8-3/4" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 6" casing in the 7-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 7-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive the annular clearance requirements for the 6" casing by 8-3/4" casing annulus to the proposed top of cement.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement from Onshore Order #2 under the following conditions:

- Annular clearance to meet or exceed 0.422" between intermediate casing ID and production casing coupling only on the first 500' overlap between both casing strings.
- Annular clearance less than 0.422" is acceptable for the production open hole section.

		Wt.	Yld	Slurry Description
Depth	No. Sacks	ppg	Ft3/sk	Sturry Description
1,100'	290	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk
10-3/4"				Cello-Flake (TOC @ Surface)
	70	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2%
				Sodium Metasilicate (TOC @ 900')
10,170'	560	14.2	1.11	1st Stage (Tail): Class C + 0.6% Halad-9 + 0.45% HR-601 + 3%
8-3/4"				Microbond (TOC @ 6,000')
	1170	14.8	1.5	2nd Stage (Bradenhead squeeze): Class C + 3% Salt + 1% PreMag-
				M + 6% Bentonite Gel (TOC @ surface)
26,365'	2150	13.2	1.31	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond
6"				(TOC @ 9,670')

#### **<u>Cementing Program</u>**:

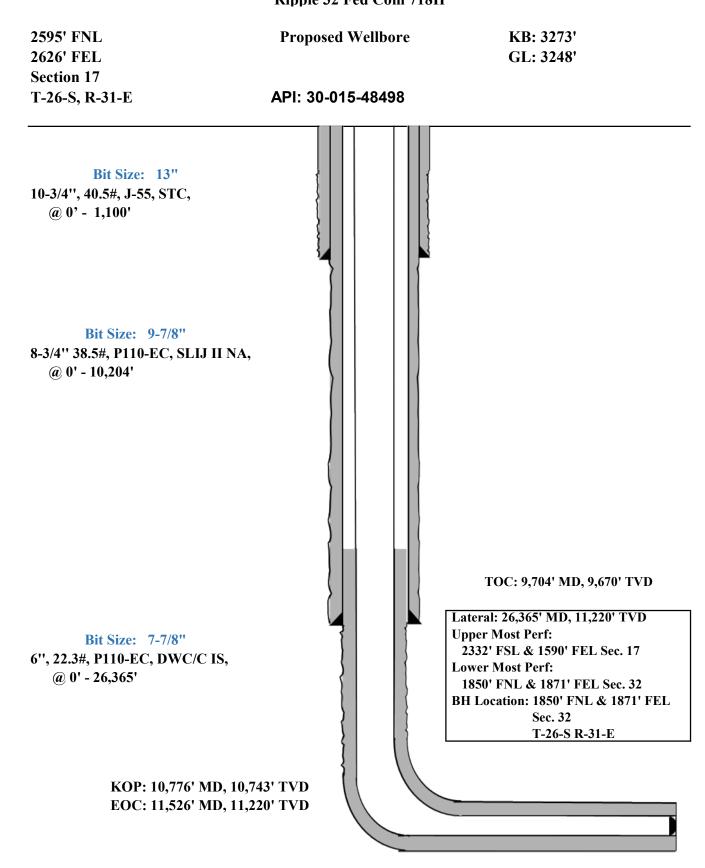


EOG requests variance from minimum standards to pump a two stage cement job on the 8-3/4" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon (6,204') and the second stage performed as a 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of 169 sacks of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. Top will be verified by Echo-meter.

EOG will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

EOG will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.





## **S**eog resources

#### Ripple 32 Fed Com 718H

#### **GEOLOGIC NAME OF SURFACE FORMATION:**

Permian

#### **ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:**

Rustler	994'
Tamarisk Anhydrite	1,078'
Top of Salt	1,340'
Base of Salt	3,807'
Lamar	4,017'
Bell Canyon	4,036'
Cherry Canyon	4,897'
Brushy Canyon	6,204'
Bone Spring Lime	7,959'
Leonard (Avalon) Shale	8,060'
1st Bone Spring Sand	8,903'
2nd Bone Spring Shale	9,170'
2nd Bone Spring Sand	9,572'
3rd Bone Spring Carb	10,072'
3rd Bone Spring Sand	10,833'
Wolfcamp	11,229'
TD	11,220'

#### ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

Upper Permian Sands	0-400'	Fresh Water
Bell Canyon	4,036'	Oil
Cherry Canyon	4,897'	Oil
Brushy Canyon	6,204'	Oil
Leonard (Avalon) Shale	8,060'	Oil
1st Bone Spring Sand	8,903'	Oil
2nd Bone Spring Shale	9,170'	Oil
2nd Bone Spring Sand	9,572'	Oil

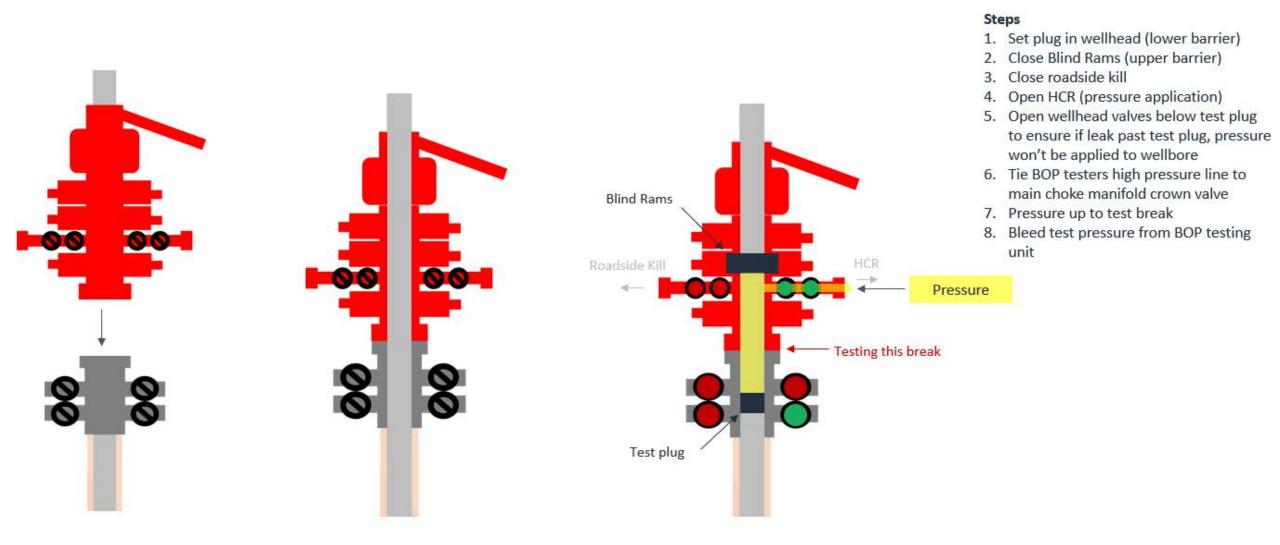


#### **Break-test BOP & Offline Cementing:**

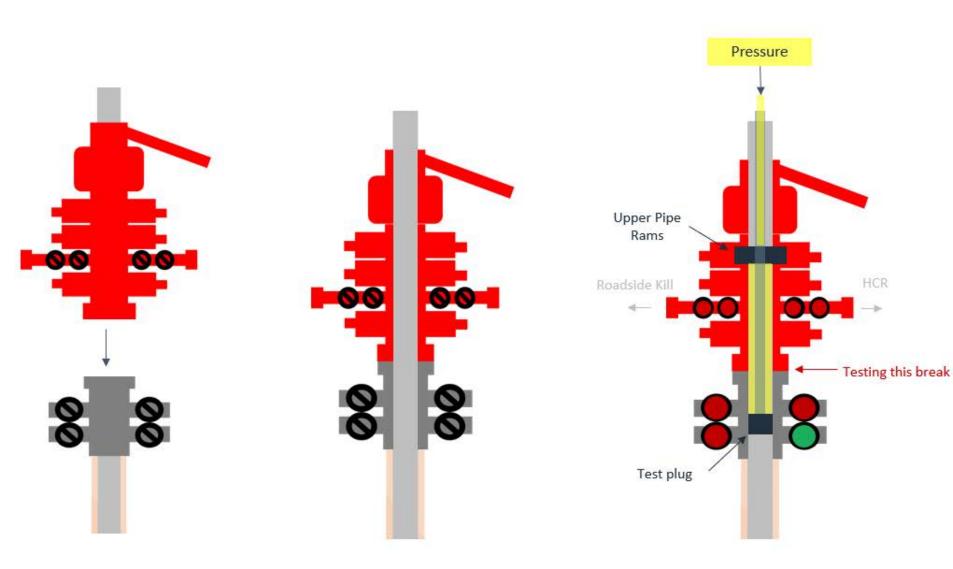
EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
  - Annular **à** during each full BOPE test
  - Upper Pipe Rams **à** On trip ins where FIT required
  - Blind Rams **à** Every trip
  - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

## **Break Test Diagram (HCR valve)**



## **Break Test Diagram (Test Joint)**



#### Steps

- 1. Set plug in with test joint wellhead (lower barrier)
- 2. Close Upper Pipe Rams (upper barrier)
- 3. Close roadside kill
- 4. Close HCR
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- 6. Tie BOP testers high pressure line to top of test joint
- 7. Pressure up to test break
- 8. Bleed test pressure from BOP testing unit

#### **Seog resources** Offline Intermediate Cementing Procedure

#### **Cement Program**

1. No changes to the cement program will take place for offline cementing.

#### Summarized Operational Procedure for Intermediate Casing

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
  - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
- 2. Land production casing on mandrel hanger through BOP.
  - a. If casing is unable to be landed with a mandrel hanger, then the **casing will be cemented online**.
- 3. Break circulation and confirm no restrictions.
  - a. Ensure no blockage of float equipment and appropriate annular returns.
  - b. Perform flow check to confirm well is static.
- 4. Set pack-off
  - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
  - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
- 5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
  - a. Minimum 4 hrs notice.
- 6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
  - a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
- 7. Skid/Walk rig off current well.
- 8. Confirm well is static before removing TA Plug.
  - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
  - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
  - c. Well control plan can be seen in Section B, Well Control Procedures.
  - d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.

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2/24/2022

### **S**eog resources

Offline Intermediate Cementing Procedure

- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
- 9. Rig up return lines to take returns from wellhead to pits and rig choke.
  - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
  - b. If either test fails, perform corrections and retest before proceeding.
  - c. Return line schematics can be seen in Figure 3.
- 10. Remove TA Plug from the casing.
- 11. Install offline cement tool.
  - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
- 12. Rig up cement head and cementing lines.
  - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
- 13. Break circulation on well to confirm no restrictions.
  - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
  - b. Max anticipated time before circulating with cement truck is 6 hrs.
- 14. Pump cement job as per plan.
  - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
  - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
- 15. Confirm well is static and floats are holding after cement job.
  - a. With floats holding and backside static:
    - i. Remove cement head.
  - b. If floats are leaking:
    - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
  - c. If there is flow on the backside:
    - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
- 16. Remove offline cement tool.
- 17. Install night cap with pressure gauge for monitoring.
- 18. Test night cap to 5,000 psi for 10 min.

#### **Example Well Control Plan Content**

#### A. Well Control Component Table

The table below, which covers the cementing of the <u>5M MASP (Maximum Allowable Surface Pressure) portion of the well</u>, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

#### **B. Well Control Procedures**

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

#### **General Procedure While Circulating**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.

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## **S**eog resources

Offline Intermediate Cementing Procedure

- 6. Read and record the following:
  - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
  - b. Pit gain
  - c. Time
  - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

#### **General Procedure While Cementing**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.
- 6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
- 7. Continue to place cement until plug bumps.
- 8. At plug bump close rig choke and cement head.
- 9. Read and record the following
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead

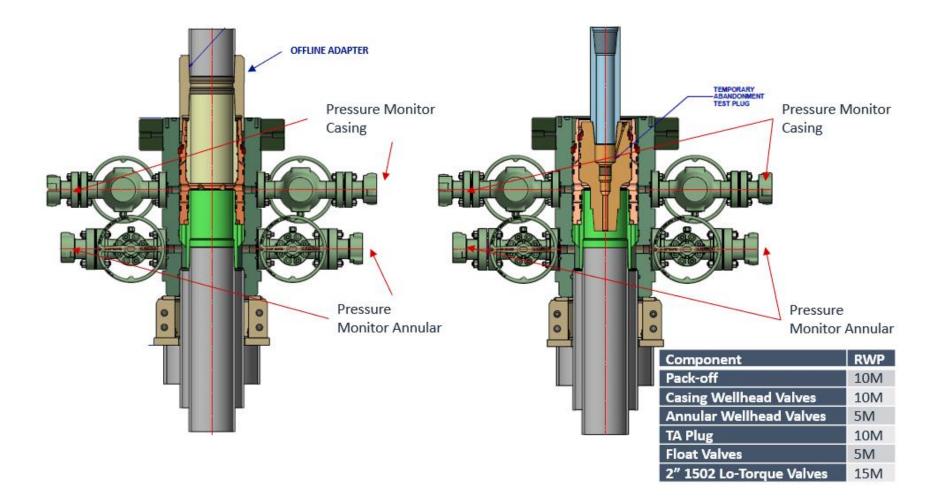
#### General Procedure After Cementing

- 1. Sound alarm (alert crew).
- 2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 3. Confirm shut-in.
- 4. Notify tool pusher/company representative.
- 5. Read and record the following:
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead

Page | 4

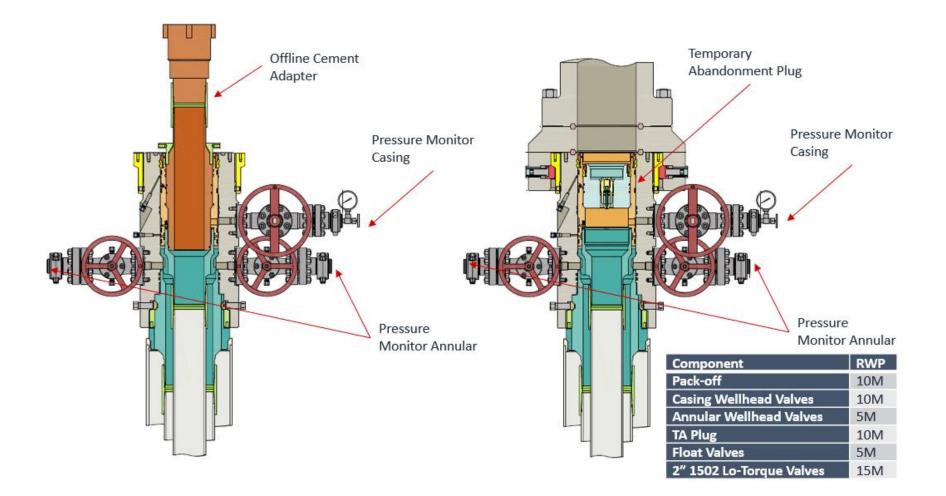
#### **Seog resources** Offline Intermediate Cementing Procedure

Figure 1: Cameron TA Plug and Offline Adapter Schematic



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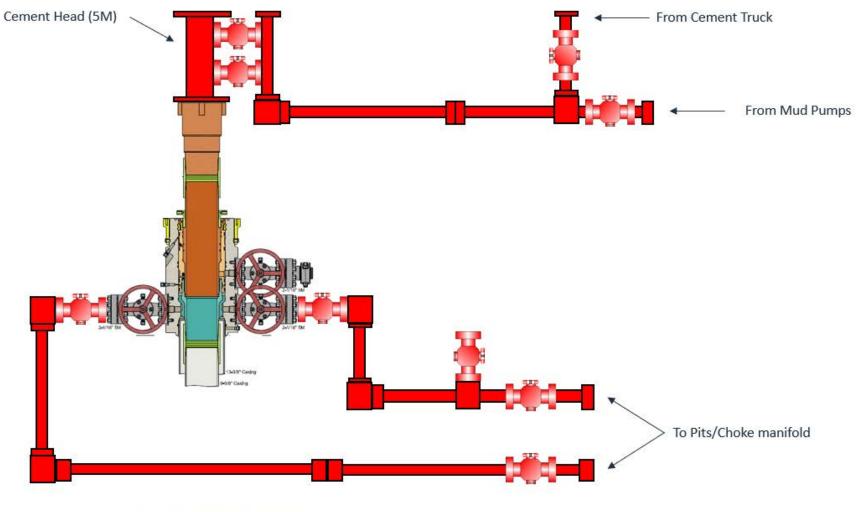
**Offline Intermediate Cementing Procedure** 



2/24/2022

#### **Seog resources** Offline Intermediate Cementing Procedure



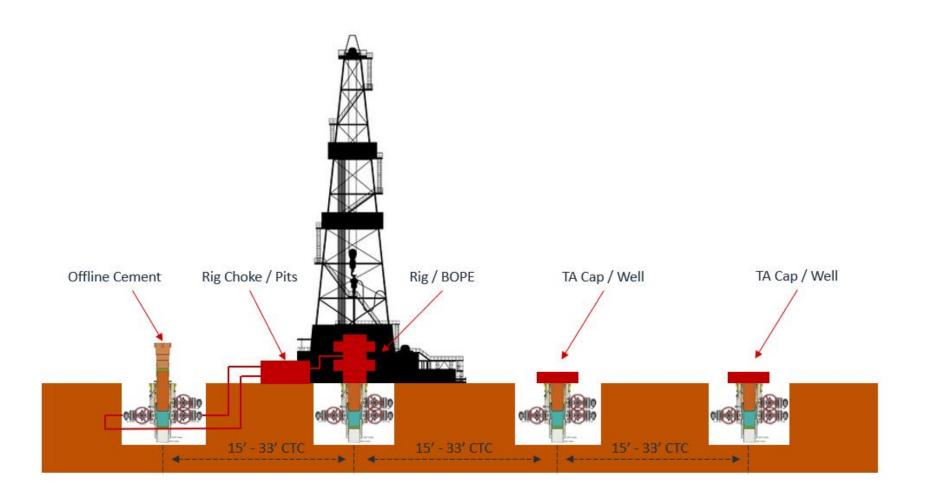


\*\*\* All Lines 10M rated working pressure

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**Offline Intermediate Cementing Procedure** 







## Midland

Eddy County, NM (NAD 83 NME) Ripple 32 Fed Com #718H

OH

Plan: Plan #0.2

## **Standard Planning Report**

06 September, 2023



Cogic								
Database: Company: Project: Site: Well: Wellbore: Design:	PEDM Midland Eddy County, N Ripple 32 Fed ( #718H OH Plan #0.2		NME)	TVD Referen MD Referen North Referen	ce:	Well #718H kb 25 @ 327 kb 25 @ 327 Grid Minimum Cu	3.0usft	
Project	Eddy County, N	/I (NAD 83 N	IME)					
Geo Datum:	US State Plane 19 North American D New Mexico Easte	atum 1983		System Datur	n:	Mean Sea Leve Using geodetic		r
Site	Ripple 32 Fed C	om						
Site Position: From: Position Uncertainty:	Мар	0.0 usft	Northing: Easting: Slot Radius:	708,89	1.00 usft <b>Latitu</b> 7.00 usft <b>Long</b> 3/16 "			32° 0' 9.625 N 103° 47' 34.029 W
Well	#718H							
Well Position Position Uncertainty	+N/-S +E/-W	0.0 usft 0.0 usft 0.0 usft	Northing: Easting: Wellhead Elev		379,771.00 usft 706,490.00 usft usft	Latitude: Longitude: Ground Level:		32° 2' 34.620 N 103° 48' 1.143 W 3,248.0 usft
Grid Convergence:		0.28 °						
Wellbore	OH							
Magnetics	Model Name	•	Sample Date	Declinatio (°)	'n	Dip Angle (°)	F	Field Strength (nT)
	IGRF	2020	8/30/2023		6.38	59.63	}	47,135.05283744
Design	Plan #0.2							
Audit Notes: Version:			Phase:	PLAN	Tie On De	epth:	0.0	
Vertical Section:		(1	rom (TVD) ısft)	+N/-S (usft)	+E/-W (usft)		Direction (°)	
			0.0	0.0	0.0		176.75	
Plan Survey Tool Pro Depth From	gram I Depth To	Date 9/6/20	023					
(usft)		ırvey (Wellb	ore)	Tool Name	Rer	narks		
1 0.0	26,365.1 PI	an #0.2 (OH	)	EOG MWD+IFR MWD + IFR1	1			



Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan #0.2		

Plan Sections

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,598.6	5.97	90.00	1,598.0	0.0	15.5	2.00	2.00	0.00	90.00	
7,547.8	5.97	90.00	7,515.0	0.0	634.5	0.00	0.00	0.00	0.00	
7,846.4	0.00	0.00	7,813.0	0.0	650.0	2.00	-2.00	0.00	180.00	
10,776.3	0.00	0.00	10,742.9	0.0	650.0	0.00	0.00	0.00	0.00	
11,526.4	90.00	156.38	11,220.5	-437.5	841.3	12.00	12.00	0.00	156.38	
12,524.2	90.00	179.51	11,220.5	-1,406.7	1,048.3	2.32	0.00	2.32	89.99	
18,134.2	90.00	179.51	11,220.5	-7,016.5	1,096.3	0.00	0.00	0.00	0.00	Interp @ 11214.5 (#7
18,578.0	90.00	188.39	11,220.5	-7,458.8	1,065.8	2.00	0.00	2.00	90.00	
19,982.3	90.00	188.39	11,220.5	-8,848.1	861.0	0.00	0.00	0.00	0.00	
20,418.3	90.00	179.67	11,220.5	-9,282.6	830.4	2.00	0.00	-2.00	-90.00	
26,365.1	90.00	179.67	11,220.5	-15,229.3	865.1	0.00	0.00	0.00	0.00	BHL (Ripple 32 Fed

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Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan #0.2		

Planned Survey

	easured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
	100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
	200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
	300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
	400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
	500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
	600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
	700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
	800.0	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
	900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
	1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
	1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
	1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
	1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
	1,400.0	2.00	90.00	1,400.0	0.0	1.7	0.1	2.00	2.00	0.00
	1,500.0	4.00	90.00	1,499.8	0.0	7.0	0.4	2.00	2.00	0.00
	1,598.6	5.97	90.00	1,598.0	0.0	15.5	0.9	2.00	2.00	0.00
	1,600.0	5.97	90.00	1,599.5	0.0	15.7	0.9	0.00	0.00	0.00
	1,700.0	5.97	90.00	1,698.9	0.0	26.1	1.5	0.00	0.00	0.00
	1,800.0	5.97	90.00	1,798.4	0.0	36.5	2.1	0.00	0.00	0.00
	1,900.0	5.97	90.00	1,897.8	0.0	46.9	2.7	0.00	0.00	0.00
	2,000.0	5.97	90.00	1,997.3	0.0	57.3	3.3	0.00	0.00	0.00
	2,100.0	5.97	90.00	2,096.7	0.0	67.7	3.8	0.00	0.00	0.00
	2,200.0	5.97 5.97	90.00 90.00	2,196.2	0.0	78.1	4.4	0.00	0.00 0.00	0.00 0.00
	2,300.0			2,295.7	0.0	88.5	5.0	0.00		
	2,400.0	5.97	90.00	2,395.1	0.0	98.9	5.6	0.00	0.00	0.00
	2,500.0	5.97	90.00	2,494.6	0.0	109.3	6.2	0.00	0.00	0.00
	2,600.0	5.97	90.00	2,594.0	0.0	119.7	6.8	0.00	0.00	0.00
	2,700.0	5.97	90.00	2,693.5	0.0	130.1	7.4	0.00	0.00	0.00
	2,800.0	5.97	90.00	2,792.9	0.0	140.5	8.0	0.00	0.00	0.00
	2,900.0	5.97	90.00	2,892.4	0.0	150.9	8.6	0.00	0.00	0.00
	3,000.0	5.97	90.00	2,991.9	0.0	161.3	9.2	0.00	0.00	0.00
	3,100.0	5.97	90.00	3,091.3	0.0	171.7	9.7	0.00	0.00	0.00
	3,200.0	5.97	90.00	3,190.8	0.0	182.1	10.3	0.00	0.00	0.00
	3,300.0	5.97	90.00	3,290.2	0.0	192.5	10.9	0.00	0.00	0.00
	3,400.0	5.97	90.00	3,389.7	0.0	203.0	11.5	0.00	0.00	0.00
	3,400.0 3,500.0	5.97	90.00 90.00	3,489.1	0.0	203.0	11.5	0.00	0.00	0.00
	3,600.0	5.97	90.00	3,588.6	0.0	213.4	12.1	0.00	0.00	0.00
	3,700.0	5.97	90.00	3,688.1	0.0	223.0	13.3	0.00	0.00	0.00
	3,800.0	5.97	90.00	3,787.5	0.0	244.6	13.9	0.00	0.00	0.00
	3,900.0	5.97	90.00	3,887.0	0.0	255.0	14.5	0.00	0.00	0.00
	4,000.0	5.97	90.00	3,986.4	0.0	265.4	15.1	0.00	0.00	0.00
	4,100.0	5.97	90.00	4,085.9	0.0	275.8	15.6	0.00	0.00	0.00
	4,200.0	5.97	90.00	4,185.3	0.0	286.2	16.2	0.00	0.00	0.00
	4,300.0	5.97	90.00	4,284.8	0.0	296.6	16.8	0.00	0.00	0.00
	4,400.0	5.97	90.00	4,384.3	0.0	307.0	17.4	0.00	0.00	0.00
	4,500.0	5.97	90.00	4,483.7	0.0	317.4	18.0	0.00	0.00	0.00
	4,600.0	5.97	90.00	4,583.2	0.0	327.8	18.6	0.00	0.00	0.00
	4,700.0	5.97	90.00	4,682.6	0.0	338.2	19.2	0.00	0.00	0.00
	4,800.0	5.97	90.00	4,782.1	0.0	348.6	19.8	0.00	0.00	0.00
	4,900.0	5.97	90.00	4,881.5	0.0	359.0	20.4	0.00	0.00	0.00
	5,000.0	5.97	90.00	4,981.0	0.0	369.4	20.4	0.00	0.00	0.00
	5,100.0	5.97	90.00	5,080.5	0.0	379.8	21.5	0.00	0.00	0.00
	5,200.0	5.97	90.00	5,179.9	0.0	390.2	22.1	0.00	0.00	0.00
L	-,	0.07	50.00	2,0.0	0.0	300.2		0.00	0.00	

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COMPASS 5000.16 Build 100



Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

5,300.0 $5.97$ $90.00$ $5,279.4$ $0.0$ $400.8$ $22.7$ $0.00$ $0.00$ $0.00$ $5,400.0$ $5.97$ $90.00$ $5,778.8$ $0.0$ $411.0$ $22.3$ $0.00$ $0.00$ $0.00$ $5,000.0$ $5.97$ $90.00$ $5,777.7$ $0.0$ $431.8$ $24.5$ $0.00$	Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	
5.500.0         5.97         90.00         5.478.3         0.0         4214         23.9         0.00         0.00         0           5.500.0         5.97         90.00         5.577.2         0.0         442.2         25.1         0.00         0.00         0           5.000.0         5.97         90.00         5.577.2         0.0         442.2         25.1         0.00         0.00         0           5.000.0         5.97         90.00         5.876.6         0.0         443.8         22.7         0.00         0.00         0	5,300.0			5,279.4	0.0	400.6	22.7	0.00	0.00	0.00	
5,500.0         5.97         90.00         5,478.3         0.0         4214         23.9         0.00         0.00         0           5,500.0         5,577         90.0         5,577.2         0.0         442.2         25.1         0.00         0.00         0           5,800.0         5,97         90.00         5,577.2         0.0         442.2         25.1         0.00         0.00         0           5,900.0         5,97         90.00         5,577.6         0.0         443.8         27.4         0.00         0.00         0	5,400.0	5.97	90.00	5,378.8	0.0	411.0	23.3	0.00	0.00	0.00	
5.800.0         5.97         90.00         5.777.7         0.0         4412         25.1         0.00         0.00           5.800.0         5.97         90.00         5.776.7         0.0         4422         25.1         0.00         0.00           5.800.0         5.97         90.00         5.375.6         0.0         473.4         26.3         0.00         0.00           6.000.0         5.97         90.00         6.375.6         0.0         473.4         26.0         0.00         0.00           6.300.0         5.97         90.00         6.373.4         0.0         594.6         28.6         0.00         0.00         0.00           6.300.0         5.97         90.00         6.373.4         0.0         575.5         28.2         0.00										0.00	
$ \left  \begin{array}{cccccccccccccccccccccccccccccccccccc$	5,600.0	5.97	90.00	5,577.7	0.0	431.8	24.5	0.00	0.00	0.00	
5.800.0         5.97         90.00         5.776.7         0.0         462.6         25.7         0.00         0.00           5.900.0         5.97         90.00         5.776.6         0.0         463.0         26.3         0.00         0.00           6.000.0         5.97         90.00         6.775.6         0.0         443.8         27.4         0.00         0.00         0.00           6.200.0         5.97         90.00         6.775.3         0.0         544.6         28.6         0.00         0.00         0.00           6.400.0         5.57         90.00         6.472.9         0.0         555.5         29.8         0.00 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.00</td><td></td></t<>										0.00	
$ \left  \begin{array}{cccccccccccccccccccccccccccccccccccc$										0.00	
$ \left( \begin{array}{cccccccccccccccccccccccccccccccccccc$	5,900.0	5.97	90.00	5,876.1	0.0	463.0	26.3	0.00	0.00	0.00	
$ \left( \begin{array}{cccccccccccccccccccccccccccccccccccc$	6,000.0	5.97	90.00	5,975.6	0.0	473.4	26.9	0.00	0.00	0.00	
$ \left( \begin{array}{cccccccccccccccccccccccccccccccccccc$	6,100.0	5.97	90.00	6,075.0	0.0	483.8	27.4	0.00	0.00	0.00	
$ \begin{bmatrix} 6,400.0 & 5.97 & 90.00 & 6,373.4 & 0.0 & 515.0 & 29.2 & 0.00 & 0.00 & 0.00 & 0.00 & 0.00 & 0.00 & 597 & 90.00 & 6,572.3 & 0.0 & 535.9 & 30.4 & 0.00 & 0$	6,200.0	5.97	90.00	6,174.5	0.0	494.2	28.0	0.00	0.00	0.00	
$ \left  \begin{array}{cccccccccccccccccccccccccccccccccccc$	6,300.0	5.97	90.00	6,273.9	0.0	504.6	28.6	0.00	0.00	0.00	
6,600.0         5.97         90.00         6,77.3         0.0         535.9         30.4         0.00         0.00           6,700.0         5.97         90.00         6,771.2         0.0         556.7         31.6         0.00         0.00           6,800.0         5.97         90.00         6,771.2         0.0         566.7         31.6         0.00         0.00           7,000.0         5.97         90.00         6,770.2         0.0         577.5         32.8         0.00         0.00         0.00           7,100.0         5.97         90.00         7,169.1         0.0         587.9         33.3         0.00         0.00         0.00           7,200.0         5.97         90.00         7,268.5         0.0         608.7         34.5         0.00         0.00         0.00           7,500.0         5.97         90.00         7,566.9         0.0         634.4         36.3         2.00         0.00         0.00         0.00         0.00         7.00.0         2.93         90.00         7,566.9         0.0         648.6         36.8         2.00         -2.00         0.0         7.80.0         9.00         7.866.6         0.0         650.0         36	6,400.0									0.00	
6,700.0         5.97         90.00         6,671.8         0.0         546.3         31.0         0.00         0.00           6,800.0         5.97         90.00         6,771.2         0.0         556.7         31.6         0.00         0.00         0.00           7,000.0         5.97         90.00         6,870.7         0.0         557.9         33.3         0.00         0.00         0.00           7,100.0         5.97         90.00         7,696.6         0.0         587.9         33.3         0.00         0.00         0.00           7,300.0         5.97         90.00         7,368.5         0.0         608.7         34.5         0.00         0.00         0.00           7,400.0         5.97         90.00         7,368.0         0.0         619.1         35.1         0.00         0.00         0.00           7,500.0         5.97         90.00         7,566.9         0.0         639.4         36.3         2.00         -2.00         00           7,800.0         0.33         90.00         7,766.6         0.0         646.3         36.7         2.00         0         0         0.00         0.00         0.00         0.00         0.00	6,500.0			6,472.9	0.0		29.8		0.00	0.00	
6,800.0         5.97         90.00         6,771.2         0.0         566.7         31.6         0.00         0.00           6,900.0         5.97         90.00         6,870.7         0.0         567.7         32.2         0.00         0.00         0.00           7,000.0         5.97         90.00         7,069.6         0.0         587.9         33.3         0.00         0.00         0.00           7,200.0         5.97         90.00         7,268.5         0.0         608.7         34.5         0.00         0.00         0.00           7,300.0         5.97         90.00         7,268.5         0.0         608.7         34.5         0.00         0.00         0.00           7,500.0         5.97         90.00         7,666.7         0.0         639.4         36.3         2.00         -2.00         0.0           7,700.0         2.93         90.00         7,666.7         0.0         646.3         36.7         2.00         -2.00         0.0           7,800.0         0.00         0.00         7,866.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00	6,600.0			6,572.3			30.4			0.00	
										0.00	
$\left \begin{array}{cccccccccccccccccccccccccccccccccccc$		5.97								0.00	
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8,100.0         0.00         8,066.6         0.0         650.0         36.9         0.00         0.00         0.00           8,200.0         0.00         0.00         8,166.6         0.0         650.0         36.9         0.00         0.00         0.00           8,300.0         0.00         0.00         8,266.6         0.0         650.0         36.9         0.00         0.00         0.00           8,400.0         0.00         0.00         8,366.6         0.0         650.0         36.9         0.00 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.00</td> <td></td>										0.00	
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8,300.0         0.00         0.00         8,266.6         0.0         650.0         36.9         0.00         0.00         0.00           8,400.0         0.00         0.00         8,366.6         0.0         650.0         36.9         0.00         0.00         0.00           8,500.0         0.00         0.00         8,466.6         0.0         650.0         36.9         0.00         0.00         0.00           8,600.0         0.00         0.00         8,566.6         0.0         650.0         36.9         0.00         0.00         0.00           8,700.0         0.00         0.00         8,666.6         0.0         650.0         36.9         0.00         0.00         0.00           8,800.0         0.00         0.00         8,766.6         0.0         650.0         36.9         0.00										0.00	
8,400.0         0.00         0.00         8,366.6         0.0         650.0         36.9         0.00         0.00         0.00           8,500.0         0.00         0.00         8,466.6         0.0         650.0         36.9         0.00         0.00         0.00           8,600.0         0.00         0.00         8,566.6         0.0         650.0         36.9         0.00         0.00         0.00           8,700.0         0.00         0.00         8,666.6         0.0         650.0         36.9         0.00         0.00         0.00           8,800.0         0.00         0.00         8,766.6         0.0         650.0         36.9         0.00         0.00         0.00           9,000.0         0.00         0.00         8,866.6         0.0         650.0         36.9         0.00										0.00	
8,500.0         0.00         0.00         8,466.6         0.0         650.0         36.9         0.00         0.00         0.00           8,600.0         0.00         0.00         8,566.6         0.0         650.0         36.9         0.00         0.00         0.00           8,700.0         0.00         0.00         8,666.6         0.0         650.0         36.9         0.00         0.00         0.00           8,800.0         0.00         0.00         8,766.6         0.0         650.0         36.9         0.00         0.00         0.00           8,900.0         0.00         0.00         8,766.6         0.0         650.0         36.9         0.00         0.00         0.00           9,000.0         0.00         0.00         8,966.6         0.0         650.0         36.9         0.00										0.00	
$\left[\begin{array}{c c c c c c c c c c c c c c c c c c c $										0.00	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$										0.00	
8,800.0         0.00         0.00         8,766.6         0.0         650.0         36.9         0.00         0.00         0.00           9,000.0         0.00         0.00         8,866.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,900.0         0.00         0.00         8,966.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,900.0         0.00         0.00         9,966.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,900.0         0.00         0.00         9,966.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,900.0         0.00         0.00         9,966.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,90.0         0.00         0.00         0.00         0.00         9,90.0         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.00</td> <td></td>										0.00	
8,900.0         0.00         0.00         8,866.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         0.00         9,000.0         0.00										0.00	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$										0.00	
9,100.0         0.00         9,066.6         0.0         650.0         36.9         0.00         0.00         0.00           9,200.0         0.00         0.00         9,166.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,300.0         0.00         0.00         9,266.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         9,366.6         0.0         650.0         36.9         0.00         0.00         0.00         9,366.6         0.0         650.0         36.9         0.00         0.00         0.00         9,366.6         0.0         650.0         36.9         0.00         0.00         0.00         9,360.0         0.00         0.00         9,366.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         0.00         9,366.6         0.0         650.0         36.9         0.00         0.00         0.00         9,360.0         0.00         0.00         9,366.6         0.0         650.0         36.9         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00										0.00	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										0.00	
9,300.0         0.00         0.00         9,266.6         0.0         650.0         36.9         0.00										0.00	
9,400.0         0.00         9,366.6         0.0         650.0         36.9         0.00										0.00	
9,500.0         0.00         0.00         9,466.6         0.0         650.0         36.9         0.00										0.00	
9,600.0         0.00         9,566.6         0.0         650.0         36.9         0.00         0.00         0.00           9,700.0         0.00         0.00         9,666.6         0.0         650.0         36.9         0.00										0.00	
9,700.0         0.00         0.00         9,666.6         0.0         650.0         36.9         0.00										0.00	
9,800.0         0.00         0.00         9,766.6         0.0         650.0         36.9         0.00	9,600.0			9,566.6						0.00	
9,900.0         0.00         0.00         9,866.6         0.0         650.0         36.9         0.00										0.00	
10,000.0         0.00         0.00         9,966.6         0.0         650.0         36.9         0.00         0.00         0.00           10,100.0         0.00         0.00         10,066.6         0.0         650.0         36.9         0.00         0.00         0.00           10,200.0         0.00         0.00         10,166.6         0.0         650.0         36.9         0.00         0.00         0.00           10,300.0         0.00         0.00         10,266.6         0.0         650.0         36.9         0.00         0.00         0.00										0.00	
10,100.0         0.00         0.00         10,066.6         0.0         650.0         36.9         0.00         0.00         0           10,200.0         0.00         0.00         10,166.6         0.0         650.0         36.9         0.00         0.00         0           10,300.0         0.00         0.00         10,266.6         0.0         650.0         36.9         0.00         0.00         0										0.00	
10,200.0         0.00         10,166.6         0.0         650.0         36.9         0.00         0.00         0           10,300.0         0.00         0.00         10,266.6         0.0         650.0         36.9         0.00         0.00         0										0.00	
10,300.0 0.00 0.00 10,266.6 0.0 650.0 36.9 0.00 0.00 0										0.00	
										0.00	
										0.00	
10,400.0 0.00 0.00 10,366.6 0.0 650.0 36.9 0.00 0.00 0	10,400.0	0.00	0.00	10,366.6	0.0	650.0	36.9	0.00	0.00	0.00	

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COMPASS 5000.16 Build 100



Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	ОН		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
10,500.0	0.00	0.00	10,466.6	0.0	650.0	36.9	0.00	0.00	0.00
10,600.0	0.00	0.00	10,566.6	0.0	650.0	36.9	0.00	0.00	0.00
			40,000,0						
10,700.0	0.00	0.00	10,666.6	0.0	650.0	36.9	0.00	0.00	0.00
10,776.3	0.00	0.00	10,742.9	0.0	650.0	36.9	0.00	0.00	0.00
10,800.0	2.85	156.38	10,766.6	-0.5	650.2	37.4	12.00	12.00	0.00
10,825.0	5.85	156.38	10,791.6	-2.3	651.0	39.2	12.00	12.00	0.00
10,850.0	8.85	156.38	10,816.3	-5.2	652.3	42.2	12.00	12.00	0.00
10,875.0	11.85	156.38	10,840.9	-9.3	654.1	46.4	12.00	12.00	0.00
10,900.0	14.85	156.38	10,865.3	-14.6	656.4	51.8	12.00	12.00	0.00
10,925.0	17.84	156.38	10,889.2	-21.1	659.2	58.4	12.00	12.00	0.00
10,950.0	20.84	156.38	10,912.8	-28.6	662.5	66.2	12.00	12.00	0.00
10,975.0	20.04	156.38	10,936.0	-20.0	666.3	75.1	12.00	12.00	0.00
10,975.0	23.04	150.50	10,930.0			75.1	12.00	12.00	
11,000.0	26.84	156.38	10,958.5	-47.1	670.6	85.1	12.00	12.00	0.00
11,025.0	29.84	156.38	10,980.5	-58.0	675.4	96.2	12.00	12.00	0.00
11,050.0	32.84	156.38	11,001.9	-69.9	680.6	108.4	12.00	12.00	0.00
11,075.0	35.84	156.38	11,022.5	-82.9	686.2	121.6	12.00	12.00	0.00
11,100.0	38.84	156.38	11,042.4	-96.7	692.3	135.9	12.00	12.00	0.00
11,125.0	41.84	156.38	11,061.5	-111.6	698.8	151.0	12.00	12.00	0.00
	41.84 44.84	156.38	11,061.5	-111.6 -127.3	698.8 705.7	167.1	12.00	12.00	0.00
11,150.0	44.84 47.84	156.38			705.7 712.9	167.1		12.00	0.00
11,175.0			11,096.9	-143.9			12.00		
11,200.0	50.84	156.38	11,113.2	-161.2	720.5	201.8	12.00	12.00	0.00
11,225.0	53.84	156.38	11,128.5	-179.4	728.4	220.4	12.00	12.00	0.00
11,250.0	56.84	156.38	11,142.7	-198.2	736.7	239.7	12.00	12.00	0.00
11,275.0	59.83	156.38	11,155.8	-217.7	745.2	259.6	12.00	12.00	0.00
11,300.0	62.83	156.38	11,167.8	-237.8	754.0	280.2	12.00	12.00	0.00
11,325.0	65.83	156.38	11,178.6	-258.4	763.0	301.3	12.00	12.00	0.00
11,350.0	68.83	156.38	11,188.3	-279.6	772.3	322.9	12.00	12.00	0.00
11,375.0	71.83	156.38	11,196.7	-301.1	781.7	345.0	12.00	12.00	0.00
11,400.0	71.83	156.38	11,203.8	-301.1	791.3	345.0	12.00	12.00	0.00
	74.83	156.38		-345.3	801.0	390.2	12.00	12.00	0.00
11,425.0			11,209.7						
11,450.0	80.83	156.38	11,214.4	-367.8	810.9	413.2	12.00	12.00	0.00
11,475.0	83.83	156.38	11,217.7	-390.5	820.8	436.5	12.00	12.00	0.00
11,500.0	86.83	156.38	11,219.7	-413.4	830.8	459.8	12.00	12.00	0.00
11,526.4	90.00	156.38	11,220.5	-437.5	841.3	484.6	12.00	12.00	0.00
11,600.0	90.00	158.09	11,220.5	-505.4	869.8	553.9	2.32	0.00	2.32
11,700.0	90.00	160.40	11,220.5	-598.9	905.3	649.3	2.32	0.00	2.32
11,800.0	90.00	162.72	11,220.5	-693.8	936.9	745.8	2.32	0.00	2.32
11,900.0	90.00	165.04	11,220.5	-789.8	964.6	843.3	2.32	0.00	2.32
12,000.0	90.00	167.36	11,220.5	-886.9	904.0 988.5	943.3 941.6	2.32	0.00	2.32
12,000.0	90.00	167.36	11,220.5	-000.9 -984.9	966.5 1,008.4	1,040.5	2.32	0.00	2.32
					1,008.4		2.32	0.00	2.32
12,200.0	90.00 90.00	171.99 174.31	11,220.5	-1,083.6	,	1,140.0	2.32	0.00	2.32
12,300.0		174.31	11,220.5	-1,182.9	1,036.2	1,239.8			
12,400.0	90.00	176.63	11,220.5	-1,282.6	1,044.1	1,339.8	2.32	0.00	2.32
12,500.0	90.00	178.95	11,220.5	-1,382.5	1,048.0	1,439.7	2.32	0.00	2.32
12,524.2	90.00	179.51	11,220.5	-1,406.7	1,048.3	1,463.9	2.32	0.00	2.32
12,600.0	90.00	179.51	11,220.5	-1,482.5	1,049.0	1,539.6	0.00	0.00	0.00
12,700.0	90.00	179.51	11,220.5	-1,582.5	1,049.8	1,639.5	0.00	0.00	0.00
12,800.0	90.00	179.51	11,220.5	-1,682.5	1.050.7	1.739.4	0.00	0.00	0.00
12,900.0	90.00	179.51	11,220.5	-1,782.5	1,050.7	1,839.3	0.00	0.00	0.00
13,000.0	90.00	179.51	11,220.5	-1,882.5	1,051.5	1,839.3	0.00	0.00	0.00
				,	1,052.4	2,039.0			
13,100.0 13,200.0	90.00 90.00	179.51 179.51	11,220.5 11,220.5	-1,982.5 -2,082.5	1,053.2	2,039.0 2,138.9	0.00 0.00	0.00 0.00	0.00 0.00
13,300.0	90.00	179.51	11,220.5	-2,182.5	1,055.0	2,238.8	0.00	0.00	0.00
13,400.0	90.00	179.51	11,220.5	-2,282.5	1.055.8	2,338.7	0.00	0.00	0.00

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COMPASS 5000.16 Build 100



Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
13,500.0	90.00	179.51	11,220.5	-2,382.5	1,056.7	2,438.6	0.00	0.00	0.00
13,600.0	90.00	179.51	11,220.5	-2,482.5	1,057.5	2,538.5	0.00	0.00	0.00
13,700.0	90.00	179.51	11,220.5	-2,582.5	1,058.4	2,638.3	0.00	0.00	0.00
13,800.0	90.00	179.51	11,220.5	-2,682.5	1,059.2	2,738.2	0.00	0.00	0.00
13,900.0	90.00	179.51	11,220.5	-2,782.5	1,060.1	2,838.1	0.00	0.00	0.00
14,000.0	90.00	179.51	11,220.5	-2,882.5	1,060.9	2,938.0	0.00	0.00	0.00
14,100.0	90.00	179.51	11,220.5	-2,982.5	1,061.8	3,037.9	0.00	0.00	0.00
14,200.0	90.00	179.51	11,220.5	-3,082.5	1,062.7	3,137.8	0.00	0.00	0.00
14,300.0	90.00	179.51	11,220.5	-3,182.4	1,063.5	3,237.6	0.00	0.00	0.00
14,400.0	90.00	179.51	11,220.5	-3,282.4	1,064.4	3,337.5	0.00	0.00	0.00
14,500.0	90.00	179.51	11,220.5	-3,382.4	1,065.2	3,437.4	0.00	0.00	0.00
14,600.0	90.00	179.51	11,220.5	-3,482.4	1,066.1	3,537.3	0.00	0.00	0.00
14,700.0	90.00	179.51	11,220.5	-3,582.4	1,066.9	3,637.2	0.00	0.00	0.00
14,800.0	90.00	179.51	11,220.5	-3,682.4	1,067.8	3,737.1	0.00	0.00	0.00
14,900.0	90.00	179.51	11,220.5	-3,782.4	1,068.6	3,836.9	0.00	0.00	0.00
15,000.0	90.00	179.51	11,220.5	-3,882.4	1,069.5	3,936.8	0.00	0.00	0.00
15,100.0	90.00	179.51	11,220.5	-3,982.4	1,070.3	4,036.7	0.00	0.00	0.00
15,200.0	90.00	179.51	11,220.5	-4,082.4	1,070.3	4,030.7	0.00	0.00	0.00
					1.072.1				
15,300.0 15,400.0	90.00 90.00	179.51 179.51	11,220.5	-4,182.4	, -	4,236.5	0.00 0.00	0.00	0.00 0.00
15,400.0		179.51 179.51	11,220.5 11,220.5	-4,282.4 -4,382.4	1,072.9	4,336.4	0.00	0.00 0.00	0.00
15,500.0	90.00				1,073.8	4,436.3			
15,600.0	90.00	179.51	11,220.5	-4,482.4	1,074.6	4,536.1	0.00	0.00	0.00
15,700.0	90.00	179.51	11,220.5	-4,582.4	1,075.5	4,636.0	0.00	0.00	0.00
15,800.0	90.00	179.51	11,220.5	-4,682.4	1,076.3	4,735.9	0.00	0.00	0.00
15,900.0	90.00	179.51	11,220.5	-4,782.4	1,077.2	4,835.8	0.00	0.00	0.00
16,000.0	90.00	179.51	11,220.5	-4,882.4	1,078.0	4,935.7	0.00	0.00	0.00
16,100.0	90.00	179.51	11,220.5	-4,982.4	1,078.9	5,035.6	0.00	0.00	0.00
16,200.0	90.00	179.51	11,220.5	-5,082.4	1,079.8	5,135.4	0.00	0.00	0.00
16,300.0	90.00	179.51	11,220.5	-5,182.4	1,080.6	5,235.3	0.00	0.00	0.00
16,400.0	90.00	179.51	11,220.5	-5,282.4	1,081.5	5,335.2	0.00	0.00	0.00
16,500.0	90.00	179.51	11,220.5	-5,382.4	1,082.3	5,435.1	0.00	0.00	0.00
16,600.0	90.00	179.51	11,220.5	-5,482.4	1,083.2	5,535.0	0.00	0.00	0.00
16,700.0	90.00	179.51	11,220.5	-5,582.4	1,084.0	5,634.9	0.00	0.00	0.00
16,800.0	90.00	179.51	11,220.5	-5,682.4	1,084.9	5,734.7	0.00	0.00	0.00
16,900.0	90.00	179.51	11,220.5	-5,782.4	1,085.7	5,834.6	0.00	0.00	0.00
17,000.0	90.00	179.51	11,220.5	-5,882.3	1,086.6	5,934.5	0.00	0.00	0.00
17,100.0	90.00	179.51	11,220.5	-5,982.3	1,087.5	6,034.4	0.00	0.00	0.00
17,200.0	90.00	179.51	11,220.5	-6,082.3	1,088.3	6,134.3	0.00	0.00	0.00
17,300.0	90.00	179.51	11,220.5	-6,182.3	1,089.2	6,234.2	0.00	0.00	0.00
17,400.0	90.00	179.51	11,220.5	-6,282.3	1,000.0	6,334.0	0.00	0.00	0.00
17,500.0	90.00	179.51	11,220.5	-6,382.3	1,090.9	6,433.9	0.00	0.00	0.00
17,600.0	90.00	179.51	11,220.5	-6,482.3	1,091.7	6,533.8	0.00	0.00	0.00
17,700.0	90.00	179.51	11,220.5	-6,582.3	1,092.6	6,633.7	0.00	0.00	0.00
17,800.0	90.00	179.51	11,220.5	-6,682.3	1,093.4	6,733.6	0.00	0.00	0.00
17,800.0	90.00 90.00	179.51	11,220.5	-0,082.3 -6,782.3	1,093.4	6,833.5	0.00	0.00	0.00
18,000.0	90.00	179.51	11,220.5	-6,882.3	1,094.3	6,933.3	0.00	0.00	0.00
18,000.0	90.00	179.51	11,220.5	-0,002.3 -6,982.3	1,095.1	0,933.3 7,033.2	0.00	0.00	0.00
18,134.2	90.00	179.51	11,220.5	-0,902.3 -7,016.5	1,096.0	7,033.2	0.00	0.00	0.00
18,200.0	90.00	180.83	11,220.5	-7,082.3	1,096.1	7,133.1	2.00	0.00	2.00
18,300.0	90.00	182.83	11,220.5	-7,182.3	1,092.9	7,232.7	2.00	0.00	2.00
18,400.0	90.00	184.83	11,220.5	-7,282.0	1,086.2	7,331.9	2.00	0.00	2.00
18,500.0	90.00	186.83	11,220.5	-7,381.5	1,076.1	7,430.7	2.00	0.00	2.00
18,578.0	90.00	188.39	11,220.5	-7,458.8	1,065.8	7,507.2	2.00	0.00	2.00
	90.00	188.39	11,220.5	-7,480.6	1,062.6	7,528.8	0.00	0.00	0.00

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Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
18,700.0	90.00	188.39	11,220.5	-7,579.5	1,048.0	7,626.7	0.00	0.00	0.00
18,800.0	90.00	188.39	11,220.5	-7,678.4	1,033.4	7,724.7	0.00	0.00	0.00
18,900.0	90.00	188.39	11,220.5	-7,777.4	1,018.8	7,822.6	0.00	0.00	0.00
19,000.0	90.00	188.39	11,220.5	-7,876.3	1,004.2	7,920.6	0.00	0.00	0.00
19,100.0	90.00	188.39	11,220.5	-7,975.2	989.6	8,018.5	0.00	0.00	0.00
19,200.0	90.00	188.39	11,220.5	-8,074.2	975.1	8,116.5	0.00	0.00	0.00
19,300.0	90.00	188.39	11,220.5	-8,173.1	960.5	8,214.4	0.00	0.00	0.00
19,400.0	90.00	188.39	11,220.5	-8,272.0	945.9	8,312.4	0.00	0.00	0.00
19,500.0	90.00	188.39	11,220.5	-8,371.0	931.3	8,410.3	0.00	0.00	0.00
	90.00	188.39			916.7	8,508.2	0.00	0.00	0.00
19,600.0 19,700.0	90.00	188.39	11,220.5 11,220.5	-8,469.9 -8,568.8	910.7 902.1	8,606.2	0.00	0.00	0.00
19,700.0	90.00	188.39	11,220.5	-8,667.7	887.6	8,704.1	0.00	0.00	0.00
19,800.0	90.00	188.39	11,220.5	-8,766.7	873.0	8,802.1	0.00	0.00	0.00
19,982.3	90.00	188.39	11,220.5	-8,848.1	861.0	8,882.7	0.00	0.00	0.00
20,000.0	90.00	188.03	11,220.5	-8,865.6	858.5	8,900.0	2.00	0.00	-2.00
20,000.0	90.00	186.03	11,220.5	-0,005.0 -8,964.9	846.2	8,900.0 8,998.4	2.00	0.00	-2.00
20,100.0	90.00	186.03	11,220.5	-0,964.9 -9,064.5	837.4	8,998.4 9,097.4	2.00	0.00	-2.00
20,200.0	90.00	182.03	11,220.5	-9,164.3	832.2	9,196.8	2.00	0.00	-2.00
20,300.0	90.00	180.03	11,220.5	-9,264.3	830.4	9,296.5	2.00	0.00	-2.00
20,418.3	90.00	179.67	11,220.5	-9,282.6	830.4	9,314.7	2.00	0.00	-2.00
20,500.0	90.00	179.67	11,220.5	-9,364.3	830.9	9,396.4	0.00	0.00	0.00
20,600.0	90.00	179.67	11,220.5	-9,464.3	831.5	9,496.2	0.00	0.00	0.00
20,700.0	90.00	179.67	11,220.5	-9,564.3	832.1	9,596.1	0.00	0.00	0.00
20,800.0	90.00	179.67	11,220.5	-9,664.3	832.6	9,696.0	0.00	0.00	0.00
20,900.0	90.00	179.67	11,220.5	-9,764.3	833.2	9,795.8	0.00	0.00	0.00
21,000.0	90.00	179.67	11,220.5	-9,864.3	833.8	9,895.7	0.00	0.00	0.00
21,100.0	90.00	179.67	11,220.5	-9,964.3	834.4	9,995.6	0.00	0.00	0.00
21,200.0	90.00	179.67	11,220.5	-10,064.3	835.0	10,095.4	0.00	0.00	0.00
21,300.0	90.00	179.67	11,220.5	-10,164.3	835.6	10,195.3	0.00	0.00	0.00
21,400.0	90.00	179.67	11,220.5	-10,264.3	836.1	10,295.2	0.00	0.00	0.00
21,500.0	90.00	179.67	11,220.5	-10,364.3	836.7	10,395.1	0.00	0.00	0.00
21,600.0	90.00	179.67	11,220.5	-10,464.3	837.3	10,494.9	0.00	0.00	0.00
21,700.0	90.00	179.67	11,220.5	-10,564.3	837.9	10,594.8	0.00	0.00	0.00
21,800.0	90.00	179.67	11,220.5	-10,664.3	838.5	10,694.7	0.00	0.00	0.00
21,900.0	90.00	179.67	11,220.5	-10,764.3	839.1	10,794.5	0.00	0.00	0.00
22,000.0	90.00	179.67	11,220.5	-10,864.3	839.6	10,894.4	0.00	0.00	0.00
22,100.0	90.00	179.67	11,220.5	-10,964.3	840.2	10,994.3	0.00	0.00	0.00
22,200.0	90.00	179.67	11,220.5	-11,064.3	840.8	11,094.2	0.00	0.00	0.00
22,300.0	90.00	179.67	11,220.5	-11,164.3	841.4	11,194.0	0.00	0.00	0.00
22,400.0	90.00	179.67	11,220.5	-11,264.3	842.0	11,293.9	0.00	0.00	0.00
22,500.0	90.00	179.67	11,220.5	-11,364.3	842.6	11,393.8	0.00	0.00	0.00
22,600.0	90.00	179.67	11,220.5	-11,464.3	843.1	11,493.6	0.00	0.00	0.00
22,700.0	90.00	179.67	11,220.5	-11,564.3	843.7	11,593.5	0.00	0.00	0.00
22,800.0	90.00	179.67	11,220.5	-11,664.3	844.3	11,693.4	0.00	0.00	0.00
22,900.0	90.00	179.67	11,220.5	-11,764.3	844.9	11,793.2	0.00	0.00	0.00
23,000.0	90.00	179.67	11,220.5	-11,864.3	845.5	11,893.1	0.00	0.00	0.00
23,100.0	90.00	179.67	11,220.5	-11,964.3	846.1	11,993.0	0.00	0.00	0.00
23,200.0	90.00	179.67	11,220.5	-12,064.3	846.6	12,092.9	0.00	0.00	0.00
23,300.0	90.00	179.67	11,220.5	-12,164.3	847.2	12,192.7	0.00	0.00	0.00
23,400.0	90.00	179.67	11,220.5	-12,264.3	847.8	12,292.6	0.00	0.00	0.00
23,500.0	90.00	179.67	11,220.5	-12,364.3	848.4	12,392.5	0.00	0.00	0.00
23,600.0	90.00	179.67	11,220.5	-12,464.3	849.0	12,492.3	0.00	0.00	0.00
23,700.0	90.00	179.67	11,220.5	-12,564.2	849.6	12,592.2	0.00	0.00	0.00
23,800.0	90.00	179.67	11,220.5	-12,664.2	850.2	12,692.1	0.00	0.00	0.00

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Page 8

COMPASS 5000.16 Build 100



Database:	PEDM	Local Co-ordinate Reference:	Well #718H
Company:	Midland	TVD Reference:	kb 25 @ 3273.0usft
Project:	Eddy County, NM (NAD 83 NME)	MD Reference:	kb 25 @ 3273.0usft
Site:	Ripple 32 Fed Com	North Reference:	Grid
Well:	#718H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan #0.2		

Planned Survey

Measu Dept (usft	Inclinatio	n Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
23,9	00.0 90	.00 179.0	67 11,220.5	-12,764.2	850.7	12,791.9	0.00	0.00	0.00
24,0	00.0 90	.00 179.0	67 11,220.5	-12,864.2	851.3	12,891.8	0.00	0.00	0.00
24,1	00.0 90	.00 179.0	67 11,220.5	-12,964.2	851.9	12,991.7	0.00	0.00	0.00
24,2	00.0 90	.00 179.0	67 11,220.5	-13,064.2	852.5	13,091.6	0.00	0.00	0.00
24,3	00.0 90	.00 179.0	67 11,220.5	-13,164.2	853.1	13,191.4	0.00	0.00	0.00
24,4	00.0 90	.00 179.0	67 11,220.5	-13,264.2	853.7	13,291.3	0.00	0.00	0.00
24,5	00.0 90	.00 179.0	67 11,220.5	-13,364.2	854.2	13,391.2	0.00	0.00	0.00
24,6	00.0 90	.00 179.0	67 11,220.5	-13,464.2	854.8	13,491.0	0.00	0.00	0.00
24,7	00.0 90	.00 179.0	67 11,220.5	-13,564.2	855.4	13,590.9	0.00	0.00	0.00
24,8	00.0 90	.00 179.0	67 11,220.5	-13,664.2	856.0	13,690.8	0.00	0.00	0.00
24,9	00.0 90	.00 179.0	67 11,220.5	-13,764.2	856.6	13,790.7	0.00	0.00	0.00
25,0	00.0 90	.00 179.0	67 11,220.5	-13,864.2	857.2	13,890.5	0.00	0.00	0.00
25,1	00.0 90	.00 179.0	67 11,220.5	-13,964.2	857.7	13,990.4	0.00	0.00	0.00
25,2	00.0 90	.00 179.0	67 11,220.5	-14,064.2	858.3	14,090.3	0.00	0.00	0.00
25,3	00.0 90	.00 179.0	67 11,220.5	-14,164.2	858.9	14,190.1	0.00	0.00	0.00
25,4	00.0 90	.00 179.0	67 11,220.5	-14,264.2	859.5	14,290.0	0.00	0.00	0.00
25,5	00.0 90	.00 179.0	67 11,220.5	-14,364.2	860.1	14,389.9	0.00	0.00	0.00
25,6	00.0 90	.00 179.0	67 11,220.5	-14,464.2	860.7	14,489.7	0.00	0.00	0.00
25,7	00.0 90	.00 179.0	67 11,220.5	-14,564.2	861.2	14,589.6	0.00	0.00	0.00
25,8	00.0 90	.00 179.0	67 11,220.5	-14,664.2	861.8	14,689.5	0.00	0.00	0.00
25,9	00.0 90	.00 179.0	67 11,220.5	-14,764.2	862.4	14,789.4	0.00	0.00	0.00
26,0	00.0 90	.00 179.0	57 11,220.5	-14,864.2	863.0	14,889.2	0.00	0.00	0.00
26,1	00.0 90	.00 179.0	57 11,220.5	-14,964.2	863.6	14,989.1	0.00	0.00	0.00
26,2	00.0 90	.00 179.0	57 11,220.5	-15,064.2	864.2	15,089.0	0.00	0.00	0.00
26,3	00.0 90	.00 179.0	67 11,220.5	-15,164.2	864.7	15,188.8	0.00	0.00	0.00
26,3	65.1 90	.00 179.0	67 11,220.5	-15,229.3	865.1	15,253.8	0.00	0.00	0.00

Des	ian	Tar	aets
500			90.0

Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
Interp @ 11214.5 (#718ł - plan hits target cente - Point	0.00 er	0.00	11,220.5	-7,016.5	1,096.3	372,755.90	707,586.07	32° 1' 25.145 N	103° 47' 48.814 W
Point 1 (Ripple 32 Fed C - plan misses target c - Point	0.00 enter by 125	0.00 6usft at 191.	11,220.5 59.6usft MD	-8,052.5 (11220.5 TVD	1,105.2 , -8034.2 N, 9	371,720.00 81.0 E)	707,595.00	32° 1' 14.894 N	103° 47' 48.770 W
BHL (Ripple 32 Fed Con - plan hits target cente - Point	0.00 er	0.00	11,220.5	-15,229.3	865.1	364,544.00	707,355.00	32° 0' 3.892 N	103° 47' 51.970 W
Point 2 (Ripple 32 Fed C - plan misses target c - Point	0.00 enter by 103	0.01 2usft at 195.	11,220.5 28.0usft MD	-8,383.6 (11220.5 TVD	825.2 , -8398.6 N, 9	371,389.00 27.2 E)	707,315.00	32° 1' 11.632 N	103° 47' 52.041 W
FTP (Ripple 32 Fed Con - plan misses target c - Point	0.00 enter by 199	0.00 8usft at 115.	11,220.5 61.1usft MD	-392.1 (11220.5 TVD	1,039.3 , -469.4 N, 85	379,379.00 5.0 E)	707,529.00	32° 2' 30.690 N	103° 47' 49.095 W

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# *leogresources*

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Eddy County, NM (NAD 83 NME)

**Ripple 32 Fed Com** #718H

# Plan #0.2

PROJECT DETAILS: Eddy County, NM (NAD 83 NME)

Geodetic System: US State Plane 1983 Datum: North American Datum 1983 Ellipsoid: GRS 1980 Zone: New Mexico Eastern Zone System Datum: Mean Sea Level

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14950

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15600

To convert a Magnetic Direction to a Grid Direction, Add 6.09° To convert a Magnetic Direction to a True Direction, Add 6.38° East To convert a True Direction to a Grid Direction, Subtract 0.28°

**Azimuths to Grid North** 

Magnetic North: 6.09°

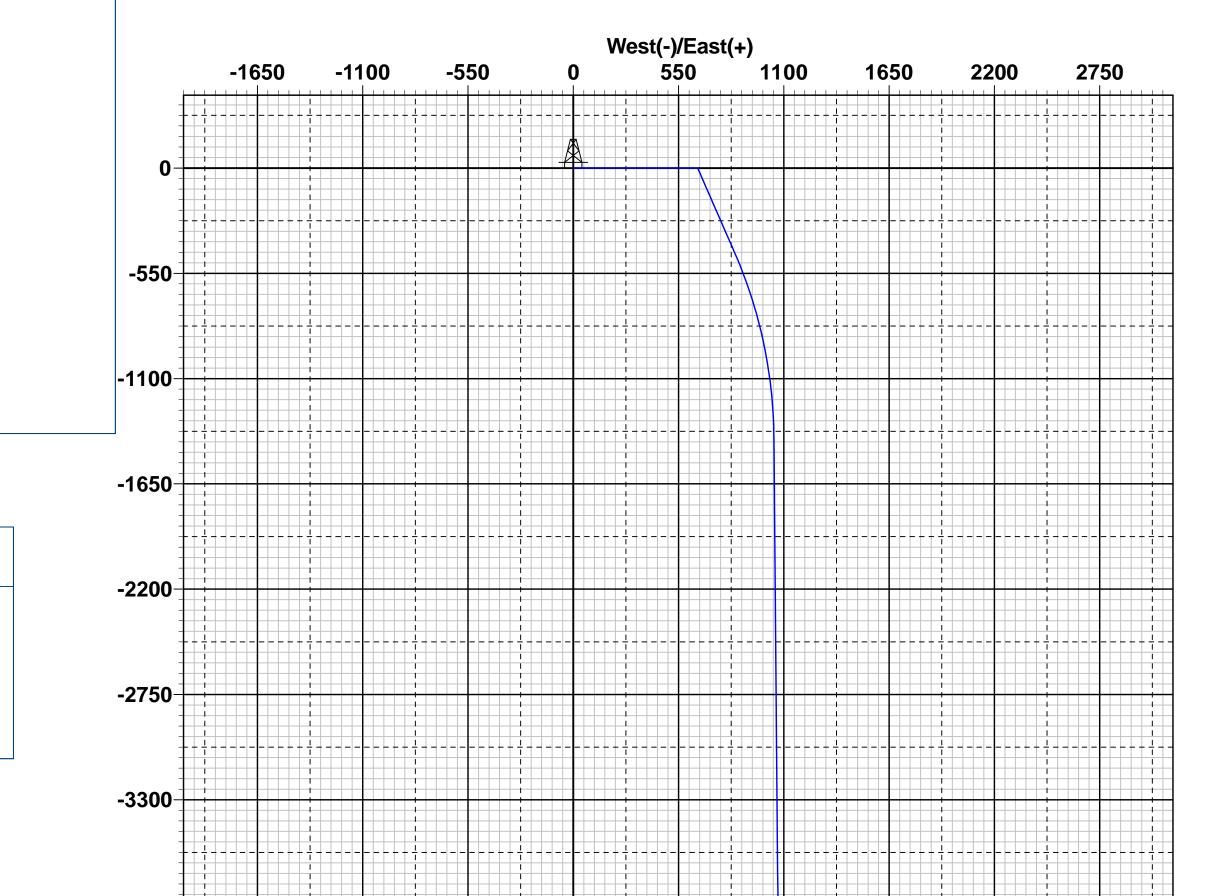
Strength: 47135.1nT

Dip Angle: 59.63° Date: 8/30/2023

Model: IGRF2020

True North: -0.28°

**Magnetic Field** 



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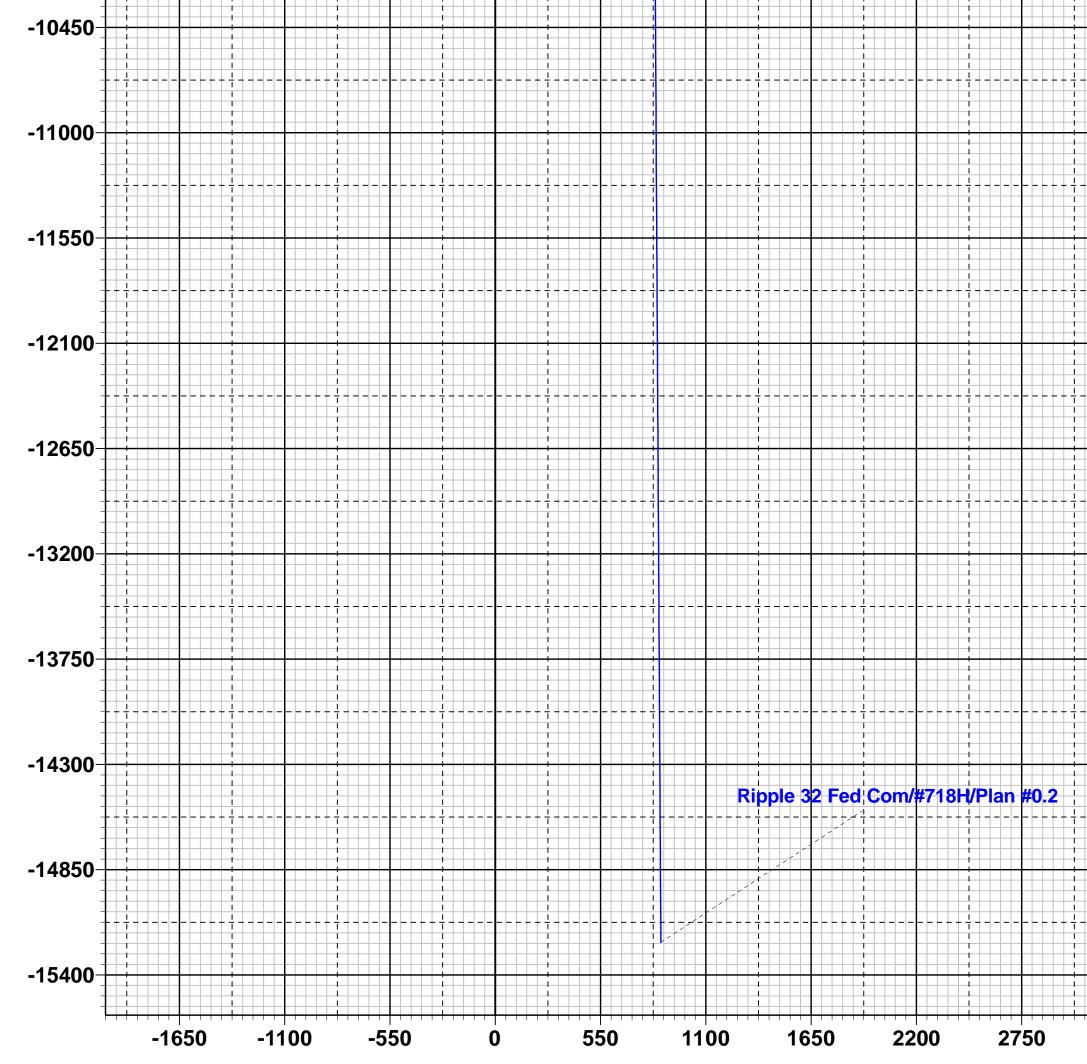
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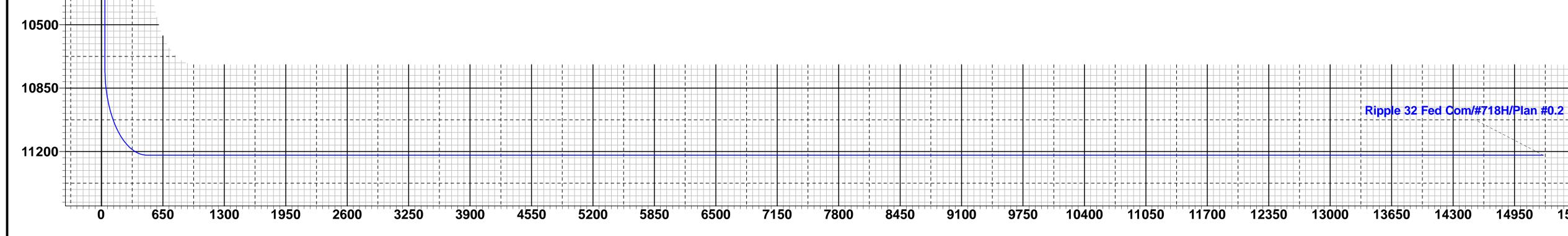
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												-3850	
												-4400	
							WELL	DETAILS: #	¢718H				
									3248.0			-4950	
						_		kb 25 @ 32					
					North 37977	•	East 70649	-	Latittude 32° 2' 34.620 N	Longitude 103° 48' 1.143 W		-5500	
												-6050	
												-6600	
						S	ECTION	DETAILS					
												-7150	
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target		<b>•</b>	
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0			+ + + + + + + + + + + + + + + + + + +	
2	1300.0	0.00	0.00	1300.0	0.0	0.0	0.00	0.00	0.0			-7700	
3	1598.6	5.97	90.00	1598.0	0.0	15.5	2.00	90.00	0.9				
4	7547.8	5.97	90.00	7515.0	0.0	634.5	0.00	0.00	36.0			onth	
5	7846.4	0.00	0.00	7813.0	0.0	650.0	2.00	180.00	36.9			ທີ -8250	
6	10776.3	0.00	0.00	10742.9	0.0	650.0	0.00	0.00	36.9				
7	11526.4	90.00	156.38	11220.5	-437.5	841.3	12.00	156.38	484.6				
8	12524.2	90.00	179.51	11220.5	-1406.7	1048.3	2.32	89.99	1463.9			-8800	
9	18134.2	90.00	179.51	11220.5	-7016.5	1096.3	0.00	0.00	7067.4	Interp @ 11214.5	(#718H OH Plan #0.2)		
10	18578.0	90.00	188.39	11220.5	-7458.8	1065.8	2.00	90.00	7507.2				
11	19982.3	90.00	188.39	11220.5	-8848.1	861.0	0.00	0.00	8882.7			-9350	
12	20418.3	90.00	179.67	11220.5	-9282.6	830.4	2.00	-90.00	9314.7				
13	26365.1	90.00	179.67	11220.5	-15229.3	865.1	0.00	0.00	15253.8	BHL (Ripple 32 F	ed Com 718H)	-9900	

TVD	+N/-S			
		+E/-W	Northing	Easting
8H OH Plan #0.2) 11220.5	-7016.5	1096.3	372755.90	707586.08
om 718H) 11220.5	-15229.3	865.1	364544.00	707355.00
	-392.1	1039.3	379379.00	707529.00
	-8052.5	1105.2	371720.00	707595.00
•	-8383.6	825.2	371389.00	707315.00
•				
	Com 718H)11220.5Com 718H)11220.5d Com 718H)11220.5	Com 718H)11220.5-15229.3Com 718H)11220.5-392.1d Com 718H)11220.5-8052.5	Com 718H)11220.5-15229.3865.1Com 718H)11220.5-392.11039.3d Com 718H)11220.5-8052.51105.2	Com 718H)11220.5-15229.3865.1364544.00Com 718H)11220.5-392.11039.3379379.00d Com 718H)11220.5-8052.51105.2371720.00



West(-)/East(+)



Eddy County, NM (NAD 83 NME) Ripple 32 Fed Com #718H OH Plan #0.2 12:59, September 06 2023

Vertical Section at 176.75°

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

District IV

1220 S. St Francis Dr., Santa Fe, NM 87505 Phone:(505) 476-3470 Fax:(505) 476-3462

#### **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
EOG RESOURCES INC	7377
P.O. Box 2267	Action Number:
Midland, TX 79702	264248
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rikala	All original COA's still apply. Additionally, if cement does not circulate during a cement job, then a CBL is required.	11/20/2023

CONDITIONS

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Action 264248