

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Sundry Print Reports
09/18/2023

Well Name: POKER LAKE UNIT 15 Well Location: T24S / R31E / SEC 22 / County or Parish/State:

TWR NWNE /

Well Number: 303H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMNM0506A Unit or CA Name: Unit or CA Number:

NMNM71016X

US Well Number: 3001554186 Well Status: Approved Application for Operator: XTO PERMIAN

Permit to Drill OPERATING LLC

#### **Notice of Intent**

**Sundry ID: 2745228** 

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 08/09/2023 Time Sundry Submitted: 06:57

Date proposed operation will begin: 08/09/2023

Procedure Description: \*\* Pool Change, First and Last Take Point Changes, Bottomhole Location Change, Drilling Plan Change, Casing/Cement Change, and Change Well Pad Names XTO Permian Operating, LCC. requests permission to make the following changes to the original APD: Change Pool from 96403 Wildcat; Bone Spring to 96546 Cotton Draw; Bone Spring South No Additional Surface Disturbance Change FTP: fr/330' FNL & 1650' FEL to 100' FNL & 1210' FEL, NMNM0506A PPP1 to 2640' FSL & 1210' FEL, NMNM0506 PPP2 to 0' FSL & 1210' FEL, NMNM0522A PPP3 to 2639' FSL & 1211' FEL, NMNM0543 Change LTP: fr/330' FSL & 1650' FEL to 100' FSL & 1210' FEL, NMNM081181 Change BHL: fr/200'FSL & 1650'FEL to 50'FSL & 1210'FEL, Section 27-T24S-R31E NMNM081181 Change Name: Well Pad A to Well Pad F Change Name: Well Pad B/C to Well Pad G Change Name: Well Pad D to Well Pad H Casing/Cement design per the attached drilling program. Attachments: C102 Drilling Program Directional Plan Well Pad F WSL Well Pad G WSL Well Pad H WSL

#### **NOI Attachments**

#### **Procedure Description**

 $Poker\_Lake\_Unit\_15\_TWR\_303H\_Attachments\_20230809065707.pdf$ 

Page 1 of 2

well Name: POKER LAKE UNIT 15

**TWR** 

Well Location: T24S / R31E / SEC 22 /

NWNE /

Well Number: 303H

Type of Well: OIL WELL

Allottee or Tribe Name:

County or Parish/State:

Page 2 of

Lease Number: NMNM0506A

Unit or CA Name:

Permit to Drill

**Unit or CA Number:** 

NMNM71016X

**US Well Number: 3001554186** 

Well Status: Approved Application for

ation for Operator: XTO PERMIAN

OPERATING LLC

#### **Conditions of Approval**

#### Additional

Sec 22 24S 31E NMP Sundry 2745228 Poker Lake Unit 15 TWR 303H COAs 20230914164426.pdf

#### **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CASSIE EVANS Signed on: AUG 09, 2023 06:57 AM

Name: XTO PERMIAN OPERATING LLC

Title: Regulatory Analyst

Street Address: 6401 Holiday Hill Road, Bldg 5

City: Midland State: TX

Phone: (432) 218-3671

Email address: CASSIE.EVANS@EXXONMOBIL.COM

#### **Field**

**Representative Name:** 

**Street Address:** 

City:

State:

Zip:

Phone:

Email address:

#### **BLM Point of Contact**

BLM POC Name: CHRISTOPHER WALLS

BLM POC Title: Petroleum Engineer

BLM POC Phone: 5752342234 BLM POC Email Address: cwalls@blm.gov

**Disposition:** Approved **Disposition Date:** 09/18/2023

Signature: Chris Walls

Page 2 of 2

<u>District I</u> 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720

District III 1000 Rio B 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170

District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

C-102.dwg

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15

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Unit\.14

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Poker

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Energy

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State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

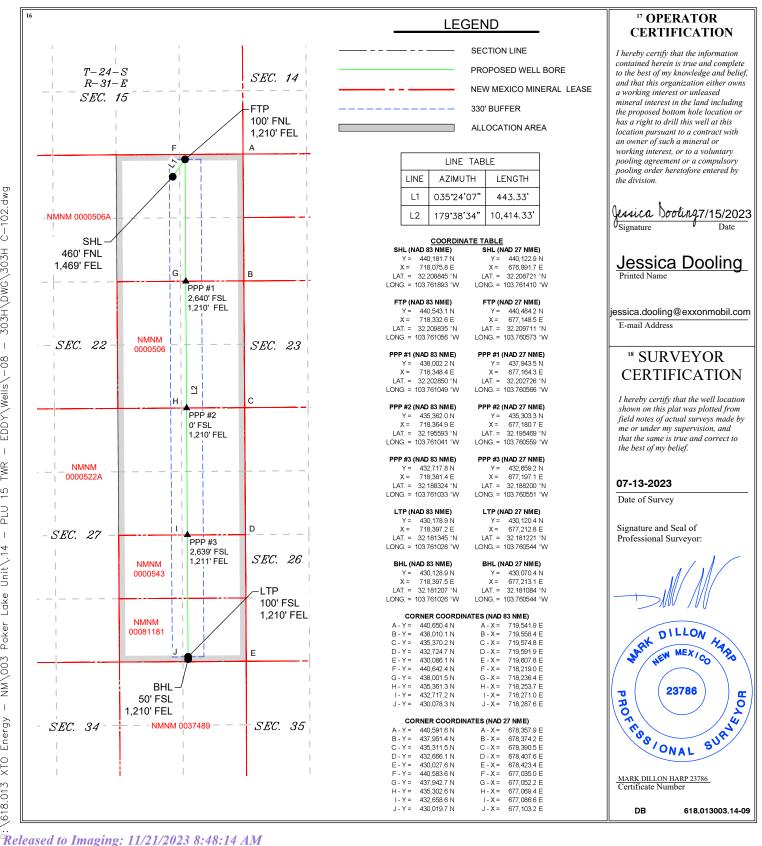
☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

<sup>1</sup> API Number <b>30-015-</b>	<sup>1</sup> API Number		Cotton Draw; Bone Spring South				
<sup>4</sup> Property Code		<sup>5</sup> Property Name POKER LAKE UNIT 15 TWR					
<sup>7</sup> OGRID No. <b>373075</b>		<sup>8</sup> Operator Name  XTO PERMIAN OPERATING, LLC.					

<sup>10</sup> Surface Location UL or lot no. Section Township Range North/South line Feet from the East/West line В 22 24 S 31 E **NORTH** 1,469 **EAST EDDY** 460 "Bottom Hole Location If Different From Surface UL or lot no. East/West line Section Feet from the County Township Range Lot Idn Feet from the North/South line 27 24 S 31 E 50 SOUTH 1,210 **EAST EDDY** <sup>3</sup> Joint or Infill Dedicated Acres Consolidation Code <sup>5</sup>Order No. 640

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



### DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. PLU 15 TWR 303H

Projected TD: 21884.9' MD / 10950' TVD
SHL: 460' FNL & 1469' FEL , Section 22, T24S, R31E
BHL: 50' FSL & 1210' FEL , Section 27, T24S, R31E
Eddy County, NM

#### 1. Geologic Name of Surface Formation

A. Quaternary

#### 2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	664'	Water
Salado	1003'	Water
Base of Salt	4258'	Water
Delaware	4466'	Water
Brushy Canyon	7021'	Water/Oil/Gas
Bone Spring	8324'	Water
1st Bone Spring	9394'	Water/Oil/Gas
2nd Bone Spring	10089'	Water/Oil/Gas
3rd Bone Spring	10777'	Water/Oil/Gas
Wolfcamp	-	Water/Oil/Gas
Wolfcamp X	-	Water/Oil/Gas
Wolfcamp Y	-	Water/Oil/Gas
Wolfcamp A	-	Water/Oil/Gas
Wolfcamp B	-	Water/Oil/Gas
Wolfcamp D	-	Water/Oil/Gas
Wolfcamp E	-	Water/Oil/Gas
Target/Land Curve	10950'	Water/Oil/Gas

<sup>\*\*\*</sup> Hydrocarbons @ Brushy Canyon

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 9.625 inch casing @ 764' (239' above the salt) and circulating cement back to surface. The intermediate will isolate from the top of salt down to the next casing seat by setting 7.625 inch casing at 10145.9' and cemented to surface. A 6.75 inch curve and 6.75 inch lateral hole will be drilled to 21884.9 MD/TD and 5.5 inch production casing will be set at TD and cemented back up in the intermediate shoe (estimated TOC 9845.9 feet).

#### 3. Casing Design

Hole Size	Depth	OD Csg	Weight	Grade	Collar	New/Used	SF Burst	SF Collapse	SF Tension
12.25	0' – 764'	9.625	40	J-55	втс	New	1.25	8.24	20.62
8.75	0' – 4000'	7.625	29.7	RY P-110	Flush Joint	New	2.01	2.52	1.85
8.75	4000' – 10145.9'	7.625	29.7	HC L-80	Flush Joint	New	1.46	1.81	2.22
6.75	0' - 10045.9'	5.5	20	RY P-110	Semi-Premium	New	1.26	1.70	2.12
6.75	10045.9' - 21884.9'	5.5	20	RY P-110	Semi-Flush	New	1.26	1.56	2.12

<sup>·</sup> XTO requests the option to utilize a spudder rig (Atlas Copco RD20 or Equivalent) to set and cement surface casing per this Sundry

<sup>\*\*\*</sup> Groundwater depth 40' (per NM State Engineers Office).

<sup>·</sup> XTO requests to not utilize centralizers in the curve and lateral

 $<sup>\</sup>cdot$  7.625 Collapse analyzed using 50% evacuation based on regional experience.

<sup>5.5</sup> Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35

- $\cdot$  Test on Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less
- · XTO requests the option to use 5" BTC Float equipment for the the production casing

#### Wellhead:

- Permanent Wellhead Multibowl System

  A. Starting Head: 11" 10M top flange x 9-5/8" bottom

  B. Tubing Head: 11" 10M bottom flange x 7-1/16" 15M top flange

  · Wellhead will be installed by manufacturer's representatives.

  - · Manufacturer will monitor welding process to ensure appropriate temperature of seal.
  - · Operator will test the 7-5/8" casing per BLM Onshore Order 2
  - $\cdot \ \text{Wellhead Manufacturer representative will not be present for BOP test plug installation}$

#### 4. Cement Program

#### Surface Casing: 9.625, 40 New BTC, J-55 casing to be set at +/- 764'

Lead: 150 sxs EconoCem-HLTRRC (mixed at 10.5 ppg, 1.87 ft3/sx, 10.13 gal/sx water) Tail: 130 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Top of Cement: Surface

Compressives: 900 psi 24 hr = 1500 psi

#### 2nd Intermediate Casing: 7.625, 29.7 New casing to be set at +/- 10145.9'

Optional Lead: 380 sxs Class C (mixed at 10.5 ppg, 2.77 ft3/sx, 15.59 gal/sx water)

TOC: Surface

Tail: 290 sxs Class C (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

TOC: Brushy Canyon @ 7021

Compressives: 12-hr = 900 psi 24 hr = 1150 psi

2nd Stage

Lead: 0 sxs Class C (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water) Tail: 790 sxs Class C (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Top of Cement: 0

900 psi Compressives: 12-hr = 24 hr = 1150 psi

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brush Canyon (7021') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top verification.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement inside the first intermediate casing. If cement reaches the desired height, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure the first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

#### Production Casing: 5.5, 20 New Semi-Flush, RY P-110 casing to be set at +/- 21884.9'

Lead: 20 sxs NeoCem (mixed at 11.5 ppg, 2.69 ft3/sx, 15.00 gal/sx water) Top of Cement: 9845.9 feet Tail: 820 sxs VersaCem (mixed at 13.2 ppg, 1.51 ft3/sx, 8.38 gal/sx water) Top of Cement: 10345.9 feet

Compressives: 12-hr = 800 psi 24 hr = 1500 psi

XTO requests the option to offline cement and remediate (if needed) surface and intermediate casing strings where batch drilling is approved and if unplanned remediation is needed. XTO will ensure well is static with no pressure on the csg annulus, as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed when applicable per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops. Offline cement operations will then be conducted after the rig is moved off the current well to the next well in the batch sequence.

#### 5. Pressure Control Equipment

Once the permanent WH is installed on the 9.625 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 4709 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nippling up on the 9.625, 5M bradenhead and flange, the BOP test will be limited to 5000 psi. When nippling up on the 7.625, the BOP will be tested to a minimum of 5000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production

hole on each of the wells.

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. Based on discussions with the BLM on February 27th 2020, we will request permission to **ONLY** retest broken pressure seals if the following conditions are met: 1. After a full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

#### 6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW	Viscosity	Fluid Loss
INTERVAL	Tible Size	Mud Type	(ppg)	(sec/qt)	(cc)
0' - 764'	12.25	FW/Native	8.4-8.9	35-40	NC
764' - 10145.9'	8.75	FW / Cut Brine / Direct Emulsion	10.2-10.7	30-32	NC
10145.9' - 21884.9'	6.75	ОВМ	12.5-13	50-60	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 9-5/8" surface casing with brine solution. A 9.7 ppg -10.2 ppg cut brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

#### 7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 9.625 casing.

#### 8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

#### 9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 175 to 195 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 7118 psi.

#### 10. Anticipated Starting Date and Duration of Operations

Anticipated spud date will be after BLM approval. Move in operations and drilling is expected to take 40 days.

## Long Lead\_Well Planning

EDDY PLU 15TWR 303H

OH

Plan: Plan 1

## **Standard Planning Report**

20 July, 2023

#### Planning Report

LMRKPROD3 Database:

Company:

Project: Site:

Long Lead\_Well Planning **EDDY** 

PLU 15TWR Well: 303H Wellbore: OH Plan 1 Design:

**Local Co-ordinate Reference:** 

**TVD Reference:** MD Reference: North Reference:

**Survey Calculation Method:** 

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid

Minimum Curvature

Project EDDY

Map System: Geo Datum:

Map Zone:

**Well Position** 

US State Plane 1927 (Exact solution) NAD 1927 (NADCON CONUS)

New Mexico East 3001

System Datum:

Mean Sea Level

PLU 15TWR Site

Site Position: From:

Мар

Northing: Easting: Slot Radius:

440,144.40 usft 674,837.30 usft

Latitude: Longitude:

32° 12' 31.717 N 103° 46' 4.986 W

**Position Uncertainty:** 3.0 usft 13-3/16 "

Well 303H

+N/-S +E/-W **Position Uncertainty** 

0.0 usft 0.0 usft 0.0 usft

Easting: Wellhead Elevation:

Northing:

440,122.90 usft 676,891.70 usft usft Latitude: Longitude: **Ground Level:** 

32° 12' 31.397 N 103° 45' 41.076 W

3,559.0 usft

0.30 **Grid Convergence:** 

ОН Wellbore

Declination Magnetics **Model Name** Sample Date Dip Angle Field Strength (°) (°) (nT) IGRF2020 47,246.41073065 7/20/2023 6.39 59.79

Design Plan 1

Audit Notes:

Version:

Vertical Section: Depth From (TVD) (usft)

Phase: **PROTOTYPE** 

+N/-S (usft)

Tie On Depth: +E/-W (usft)

0.0

0.0 Direction

(°) 179.64

**Plan Survey Tool Program** 

Date 7/20/2023

0.0

**Depth From** (usft) 0.0 1

Depth To (usft) 21,884.9

Survey (Wellbore) Plan 1 (OH)

**Tool Name** 

0.0

Remarks

XOM\_R2OWSG MWD+IFR1+ OWSG MWD + IFR1 + Multi-St

#### Planning Report

Database: LMRKPROD3

Company: Long Lead\_Well Planning

 Project:
 EDDY

 Site:
 PLU 15TWR

 Well:
 303H

 Wellbore:
 OH

 Design:
 Plan 1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,801.1	12.02	13.18	1,796.7	61.2	14.3	2.00	2.00	0.00	13.18	
6,511.0	12.02	13.18	6,403.3	1,016.3	238.0	0.00	0.00	0.00	0.00	
7,112.1	0.00	0.00	7,000.0	1,077.5	252.3	2.00	-2.00	0.00	180.00	
10,345.9	0.00	0.00	10,233.8	1,077.5	252.3	0.00	0.00	0.00	0.00	
11,470.9	90.00	179.64	10,950.0	361.3	256.8	8.00	0.00	0.00	179.64	303H_FTP
14,011.6	90.00	179.64	10,950.0	-2,179.4	272.6	0.00	0.00	0.00	0.00	303H_PP1
16,651.9	90.00	179.64	10,950.0	-4,819.6	289.0	0.00	0.00	0.00	0.00	303H_PP2
19,296.0	90.00	179.64	10,950.0	-7,463.7	305.5	0.00	0.00	0.00	0.00	303H_PP3
21,834.9	90.00	179.64	10,950.0	-10,002.5	321.2	0.00	0.00	0.00	0.00	303H_LTP
21,884.9	90.00	179.64	10,950.0	-10,052.5	321.6	0.00	0.00	0.00	0.00	303H_BHL

#### Planning Report

Database: LMRKPROD3

Company: Long Lead\_Well Planning

 Project:
 EDDY

 Site:
 PLU 15TWR

 Well:
 303H

 Wellbore:
 OH

 Design:
 Plan 1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid

Design:	Plan 1								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	2.00	13.18	1,300.0	1.7	0.4	-1.7	2.00	2.00	0.00
1,400.0	4.00	13.18	1,399.8	6.8	1.6	-6.8	2.00	2.00	0.00
1,500.0	6.00	13.18	1,499.5	15.3	3.6	-15.3	2.00	2.00	0.00
1,600.0	8.00	13.18	1,598.7	27.1	6.4	-27.1	2.00	2.00	0.00
1,700.0	10.00	13.18	1,697.5	42.4	9.9	-42.3	2.00	2.00	0.00
1,800.0	12.00	13.18	1,795.6	61.0	14.3	-60.9	2.00	2.00	0.00
1,801.1	12.02	13.18	1,796.7	61.2	14.3	-61.1	2.00	2.00	0.00
1,900.0	12.02	13.18	1,893.4	81.2	19.0	-81.1	0.00	0.00	0.00
2,000.0	12.02	13.18	1,991.2	101.5	23.8	-101.4	0.00	0.00	0.00
2,100.0	12.02	13.18	2,089.0	121.8	28.5	-121.6	0.00	0.00	0.00
2,100.0	12.02	13.18	2,186.9	142.1	33.3	-141.9	0.00	0.00	0.00
2,300.0	12.02			162.3	38.0	-141.9			
2,300.0	12.02	13.18 13.18	2,284.7 2,382.5	182.6	38.0 42.8	-162.1 -182.4	0.00 0.00	0.00 0.00	0.00 0.00
2,500.0	12.02	13.18	2,480.3	202.9	47.5	-202.6	0.00	0.00	0.00
2,600.0	12.02	13.18	2,578.1	223.2	52.3	-222.9	0.00	0.00	0.00
2,700.0	12.02	13.18	2,675.9	243.5	57.0	-243.1	0.00	0.00	0.00
2,800.0	12.02	13.18	2,773.7	263.7	61.8	-263.4	0.00	0.00	0.00
2,900.0	12.02	13.18	2,871.5	284.0	66.5	-283.6	0.00	0.00	0.00
3,000.0	12.02	13.18	2,969.3	304.3	71.3	-303.9	0.00	0.00	0.00
3,100.0	12.02	13.18	3,067.1	324.6	76.0	-324.1	0.00	0.00	0.00
3,200.0	12.02	13.18	3,164.9	344.9	80.8	-344.3	0.00	0.00	0.00
3,300.0	12.02	13.18	3,262.7	365.1	85.5	-364.6	0.00	0.00	0.00
3,400.0	12.02	13.18	3,360.5	385.4	90.3	-384.8	0.00	0.00	0.00
3,500.0	12.02	13.18	3,458.3	405.7	95.0	-405.1	0.00	0.00	0.00
3,600.0	12.02	13.18	3,556.1	426.0	99.8	-425.3	0.00	0.00	0.00
3,700.0	12.02	13.18	3,654.0	446.3	104.5	-445.6	0.00	0.00	0.00
3,800.0	12.02	13.18	3,751.8	466.5	109.3	-465.8	0.00	0.00	0.00
3,900.0	12.02	13.18	3,849.6	486.8	114.0	-486.1	0.00	0.00	0.00
4,000.0	12.02	13.18	3,947.4	507.1	118.8	-506.3	0.00	0.00	0.00
4,100.0	12.02	13.18	4,045.2	527.4	123.5	-526.6	0.00	0.00	0.00
4,200.0	12.02	13.18	4,143.0	547.7	128.3	-546.8	0.00	0.00	0.00
4,300.0	12.02	13.18	4,240.8	567.9	133.0	-567.1	0.00	0.00	0.00
4,400.0	12.02	13.18	4,338.6	588.2	137.8	-587.3	0.00	0.00	0.00
4,500.0	12.02		4,436.4	608.5	142.5	-607.6	0.00	0.00	0.00
4,600.0	12.02	13.18 13.18	4,436.4 4,534.2	628.8	142.5	-607.8	0.00	0.00	0.00
4,700.0	12.02	13.16	4,534.2	649.1	152.0	-627.6 -648.1	0.00	0.00	0.00
			4,632.0						
4,800.0 4,900.0	12.02	13.18 13.18		669.3	156.8 161.5	-668.3 -688.6	0.00	0.00	0.00 0.00
-	12.02	13.18	4,827.6	689.6	161.5	-688.6	0.00	0.00	
5,000.0	12.02	13.18	4,925.4	709.9	166.3	-708.8	0.00	0.00	0.00
5,100.0	12.02	13.18	5,023.3	730.2	171.0	-729.1	0.00	0.00	0.00
5,200.0	12.02	13.18	5,121.1	750.4	175.8	-749.3	0.00	0.00	0.00
5,300.0	12.02	13.18	5,218.9	770.7	180.5	-769.6	0.00	0.00	0.00
5,400.0	12.02	13.18	5,316.7	791.0	185.3	-789.8	0.00	0.00	0.00
5,500.0	12.02	13.18	5,414.5	811.3	190.0	-810.1	0.00	0.00	0.00
5,600.0	12.02	13.18	5,512.3	831.6	194.8	-830.3	0.00	0.00	0.00
5,700.0	12.02	13.18	5,610.1	851.8	199.5	-850.6	0.00	0.00	0.00
5,800.0	12.02	13.18	5,707.9	872.1	204.3	-870.8	0.00	0.00	0.00
5,900.0	12.02	13.18	5,805.7	892.4	209.0	-891.1	0.00	0.00	0.00
6,000.0	12.02	13.18	5,903.5	912.7	213.7	-911.3	0.00	0.00	0.00
6,100.0	12.02	13.18	6,001.3	933.0	218.5	-931.6	0.00	0.00	0.00
6,200.0	12.02	13.18	6,099.1	953.2	223.2	-951.8	0.00	0.00	0.00
6,300.0	12.02	13.18	6,196.9	973.5	228.0	-972.1	0.00	0.00	0.00
			-,			J. =. /	0.00	0.00	2.00

#### Planning Report

Database: LMRKPROD3

Company: Long Lead\_Well Planning

 Project:
 EDDY

 Site:
 PLU 15TWR

 Well:
 303H

 Wellbore:
 OH

 Design:
 Plan 1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid

esign:	Plan 1								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
6,400.0	12.02	13.18	6,294.7	993.8	232.7	-992.3	0.00	0.00	0.00
6,500.0	12.02	13.18	6,392.5	1,014.1	237.5	-1,012.6	0.00	0.00	0.00
6,511.0	12.02	13.18	6,403.3	1,016.3	238.0	-1,014.8	0.00	0.00	0.00
6,600.0	10.24	13.18	6,490.6	1,033.0	241.9	-1,031.5	2.00	-2.00	0.00
6,700.0	8.24	13.18	6,589.3	1,048.7	245.6	-1,047.1	2.00	-2.00	0.00
6,800.0	6.24	13.18	6,688.5	1,060.9	248.5	-1,059.4	2.00	-2.00	0.00
6,900.0	4.24	13.18	6,788.1	1,069.8	250.6	-1,068.2	2.00	-2.00	0.00
7,000.0	2.24	13.18	6,887.9	1,075.3	251.8	-1,073.7	2.00	-2.00	0.00
7,100.0	0.24	13.18	6,987.9	1,077.5	252.3	-1,075.9	2.00	-2.00	0.00
7,112.1	0.00	0.00	7,000.0	1,077.5	252.3	-1,075.9	2.00	-2.00	0.00
10,345.9	0.00	0.00	10,233.8	1,077.5	252.3	-1,075.9	0.00	0.00	0.00
10,400.0	4.33	179.64	10,287.9	1,075.4	252.4	-1,073.8	8.00	8.00	0.00
10,500.0	12.33	179.64	10,386.7	1,061.0	252.4	-1,059.4	8.00	8.00	0.00
10,600.0	20.33	179.64	10,482.6	1,032.9	252.6	-1,031.3	8.00	8.00	0.00
10,700.0	28.33	179.64	10,573.7	991.7	252.9	-990.1	8.00	8.00	0.00
10,800.0	36.33	179.64	10,658.1	938.3	253.2	-936.7	8.00	8.00	0.00
10,900.0	44.33	179.64	10,734.3	873.6	253.6	-872.0	8.00	8.00	0.00
11,000.0	52.33	179.64	10,800.7	799.0	254.1	-797.4	8.00	8.00	0.00
11,100.0	60.33	179.64	10,856.1	715.8	254.6	-714.2	8.00	8.00	0.00
11,200.0	68.33	179.64	10,899.4	625.8	255.2	-624.2	8.00	8.00	0.00
11,300.0	76.33	179.64	10,929.7	530.6	255.7	-529.0	8.00	8.00	0.00
11,400.0	84.33	179.64	10,946.5	432.1	256.4	-430.5	8.00	8.00	0.00
11,470.9	90.00	179.64	10,950.0	361.3	256.8	-359.7	8.00	8.00	0.00
11,500.0	90.00	179.64	10,950.0	332.2	257.0	-330.6	0.00	0.00	0.00
11,600.0	90.00	179.64	10,950.0	232.2	257.6	-230.6	0.00	0.00	0.00
11,700.0	90.00	179.64	10,950.0	132.2	258.2	-130.6	0.00	0.00	0.00
11,800.0	90.00	179.64	10,950.0	32.2	258.8	-30.6	0.00	0.00	0.00
11,900.0	90.00	179.64	10,950.0	-67.8	259.5	69.4	0.00	0.00	0.00
12,000.0	90.00	179.64	10,950.0	-167.8	260.1	169.4	0.00	0.00	0.00
12,100.0	90.00	179.64	10,950.0	-267.8	260.7	269.4	0.00	0.00	0.00
12,200.0	90.00	179.64	10,950.0	-367.8	261.3	369.4	0.00	0.00	0.00
12,300.0	90.00	179.64	10,950.0	-467.8	262.0	469.4	0.00	0.00	0.00
12,400.0	90.00	179.64	10,950.0	-567.8	262.6	569.4	0.00	0.00	0.00
12,500.0	90.00	179.64	10,950.0	-667.8	263.2	669.4	0.00	0.00	0.00
12,600.0	90.00	179.64	10,950.0	-767.8	263.8	769.4	0.00	0.00	0.00
12,700.0	90.00	179.64	10,950.0	-867.8	264.4	869.4	0.00	0.00	0.00
12,800.0	90.00	179.64	10,950.0	-967.8	265.1	969.4	0.00	0.00	0.00
12,900.0	90.00	179.64	10,950.0	-1,067.8	265.7	1,069.4	0.00	0.00	0.00
13,000.0	90.00	179.64	10,950.0	-1,167.8	266.3	1,169.4	0.00	0.00	0.00
13,100.0	90.00	179.64	10,950.0	-1,267.8	266.9	1,269.4	0.00	0.00	0.00
13,200.0	90.00	179.64	10,950.0	-1,367.8	267.6	1,369.4	0.00	0.00	0.00
13,300.0	90.00	179.64	10,950.0	-1,467.8	268.2	1,469.4	0.00	0.00	0.00
13,400.0	90.00	179.64	10,950.0	-1,567.8	268.8	1,569.4	0.00	0.00	0.00
13,500.0	90.00	179.64	10,950.0	-1,667.8	269.4	1,669.4	0.00	0.00	0.00
13,600.0	90.00	179.64	10,950.0	-1,767.8	270.0	1,769.4	0.00	0.00	0.00
13,700.0	90.00	179.64	10,950.0	-1,867.8	270.7	1,869.4	0.00	0.00	0.00
13,800.0	90.00	179.64	10,950.0	-1,967.8	271.3	1,969.4	0.00	0.00	0.00
13,900.0	90.00	179.64	10,950.0	-2,067.8	271.9	2,069.4	0.00	0.00	0.00
14,000.0	90.00	179.64	10,950.0	-2,167.8	272.5	2,169.4	0.00	0.00	0.00
14,011.6	90.00	179.64	10,950.0	-2,179.4	272.6	2,181.1	0.00	0.00	0.00
14,100.0	90.00	179.64	10,950.0	-2,267.8	273.1	2,269.4	0.00	0.00	0.00
14,200.0	90.00	179.64	10,950.0	-2,367.8	273.8	2,369.4	0.00	0.00	0.00
14,300.0	90.00	179.64	10,950.0	-2,467.7	274.4	2,469.4	0.00	0.00	0.00
14,400.0	90.00	179.64	10,950.0	-2,567.7	275.0	2,569.4	0.00	0.00	0.00

#### Planning Report

Database: LMRKPROD3

Company: Long Lead\_Well Planning

 Project:
 EDDY

 Site:
 PLU 15TWR

 Well:
 303H

 Wellbore:
 OH

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:
Survey Calculation Method:

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid

velibore: )esign:	Plan 1								
lanned Survey									
Measured			Vertical			Vertical	Dogleg	Build	Turn
Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Section (usft)	Rate (°/100usft)	Rate (°/100usft)	Rate (°/100usft)
14,500.0 14,600.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-2,667.7 -2,767.7	275.6 276.3	2,669.4 2,769.4	0.00 0.00	0.00 0.00	0.00 0.00
14,700.0	90.00	179.64	10,950.0	-2,867.7	276.9	2,869.4	0.00	0.00	0.00
14,800.0	90.00	179.64	10,950.0	-2,967.7	277.5	2,969.4	0.00	0.00	0.00
14,900.0	90.00	179.64	10,950.0	-3,067.7	278.1	3,069.4	0.00	0.00	0.00
15,000.0	90.00	179.64	10,950.0	-3,167.7	278.7	3,169.4	0.00	0.00	0.00
15,100.0	90.00	179.64	10,950.0	-3,267.7	279.4	3,269.4	0.00	0.00	0.00
15,200.0	90.00	179.64	10,950.0	-3,367.7	280.0	3,369.4	0.00	0.00	0.00
15,300.0	90.00	179.64	10,950.0	-3,467.7	280.6	3,469.4	0.00	0.00	0.00
15,400.0	90.00	179.64	10,950.0	-3,567.7	281.2	3,569.4	0.00	0.00	0.00
15,500.0	90.00	179.64	10,950.0	-3,667.7	281.9	3,669.4	0.00	0.00	0.00
15,600.0	90.00	179.64	10,950.0	-3,767.7	282.5	3,769.4	0.00	0.00	0.00
15,700.0	90.00	179.64	10,950.0	-3,867.7	283.1	3,869.4	0.00	0.00	0.00
15,800.0	90.00	179.64	10,950.0	-3,967.7	283.7	3,969.4	0.00	0.00	0.00
15,900.0	90.00	179.64	10,950.0	-4,067.7	284.3	4,069.4	0.00	0.00	0.00
16,000.0 16,100.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-4,167.7 -4,267.7	285.0 285.6	4,169.4 4,269.4	0.00 0.00	0.00 0.00	0.00 0.00
			,			,			
16,200.0	90.00	179.64	10,950.0	-4,367.7	286.2	4,369.4	0.00	0.00	0.00
16,300.0	90.00	179.64	10,950.0	-4,467.7	286.8	4,469.4	0.00	0.00	0.00
16,400.0	90.00	179.64	10,950.0	-4,567.7	287.5	4,569.4 4,669.4	0.00 0.00	0.00	0.00
16,500.0 16,600.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-4,667.7 -4,767.7	288.1 288.7	4,669.4 4,769.4	0.00	0.00 0.00	0.00 0.00
16,651.9 16,700.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-4,819.6 -4,867.7	289.0 289.3	4,821.3 4,869.4	0.00 0.00	0.00 0.00	0.00 0.00
16,800.0	90.00	179.64	10,950.0	-4,867.7 -4,967.7	289.9	4,869.4	0.00	0.00	0.00
16,900.0	90.00	179.64	10,950.0	-5,067.7	290.6	5,069.4	0.00	0.00	0.00
17,000.0	90.00	179.64	10,950.0	-5,167.7	291.2	5,169.4	0.00	0.00	0.00
17,100.0	90.00	179.64	10,950.0	-5,267.7	291.8	5,269.4	0.00	0.00	0.00
17,200.0	90.00	179.64	10,950.0	-5,367.7	292.4	5,369.4	0.00	0.00	0.00
17,300.0	90.00	179.64	10,950.0	-5,467.7	293.0	5,469.4	0.00	0.00	0.00
17,400.0	90.00	179.64	10,950.0	-5,567.7	293.7	5,569.4	0.00	0.00	0.00
17,500.0	90.00	179.64	10,950.0	-5,667.7	294.3	5,669.4	0.00	0.00	0.00
17,600.0	90.00	179.64	10,950.0	-5,767.7	294.9	5,769.4	0.00	0.00	0.00
17,700.0	90.00	179.64	10,950.0	-5,867.7	295.5	5,869.4	0.00	0.00	0.00
17,800.0	90.00	179.64	10,950.0	-5,967.7	296.2	5,969.4	0.00	0.00	0.00
17,900.0	90.00	179.64	10,950.0	-6,067.7	296.8	6,069.4	0.00	0.00	0.00
18,000.0	90.00	179.64	10,950.0	-6,167.7	297.4	6,169.4	0.00	0.00	0.00
18,100.0	90.00	179.64	10,950.0	-6,267.7	298.0	6,269.4	0.00	0.00	0.00
18,200.0	90.00	179.64	10,950.0	-6,367.7	298.6	6,369.4	0.00	0.00	0.00
18,300.0	90.00	179.64	10,950.0	-6,467.7	299.3	6,469.4	0.00	0.00	0.00
18,400.0	90.00	179.64	10,950.0	-6,567.7	299.9	6,569.4	0.00	0.00	0.00
18,500.0	90.00	179.64	10,950.0	-6,667.7	300.5	6,669.4	0.00	0.00	0.00
18,600.0	90.00	179.64	10,950.0	-6,767.7	301.1	6,769.4	0.00	0.00	0.00
18,700.0	90.00	179.64	10,950.0	-6,867.7	301.8	6,869.4	0.00	0.00	0.00
18,800.0	90.00	179.64	10,950.0	-6,967.7	302.4	6,969.4	0.00	0.00	0.00
18,900.0	90.00	179.64	10,950.0	-7,067.7	303.0	7,069.4	0.00	0.00	0.00
19,000.0	90.00	179.64	10,950.0	-7,167.7	303.6	7,169.4	0.00	0.00	0.00
19,100.0	90.00	179.64	10,950.0	-7,267.7	304.2	7,269.4	0.00	0.00	0.00
19,200.0	90.00	179.64	10,950.0	-7,367.7	304.9	7,369.4	0.00	0.00	0.00
19,296.0	90.00	179.64	10,950.0	-7,463.7	305.5	7,465.5	0.00	0.00	0.00
19,300.0	90.00	179.64	10,950.0	-7,467.7	305.5	7,469.4	0.00	0.00	0.00
19,400.0	90.00	179.64	10,950.0	-7,567.7	306.1	7,569.4	0.00	0.00	0.00
19,500.0	90.00	179.64	10,950.0	-7,667.6	306.7	7,669.4	0.00	0.00	0.00
19,600.0	90.00	179.64	10,950.0	-7,767.6	307.4	7,769.4	0.00	0.00	0.00

#### **Planning Report**

Database: LMRKPROD3

Company: Long Lead\_Well Planning

 Project:
 EDDY

 Site:
 PLU 15TWR

 Well:
 303H

 Wellbore:
 OH

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

**Survey Calculation Method:** 

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid

esign:	Plan 1								
lanned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
19,700.0 19,800.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-7,867.6 -7,967.6	308.0 308.6	7,869.4 7,969.4	0.00 0.00	0.00 0.00	0.00 0.00
19,900.0	90.00	179.64	10,950.0	-8,067.6	309.2	8,069.4	0.00	0.00	0.00
20,000.0 20,100.0	90.00 90.00	179.64 179.64	10,950.0 10.950.0	-8,167.6 -8.267.6	309.8 310.5	8,169.4 8.269.4	0.00 0.00	0.00 0.00	0.00 0.00
20,200.0	90.00	179.64	10,950.0	-8,367.6	310.5	8,369.4	0.00	0.00	0.00
20,300.0 20,400.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-8,467.6 -8,567.6	311.7 312.3	8,469.4 8,569.4	0.00 0.00	0.00 0.00	0.00 0.00
•			,	,		•			
20,500.0 20,600.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-8,667.6 -8.767.6	312.9 313.6	8,669.4 8.769.4	0.00 0.00	0.00 0.00	0.00 0.00
20,700.0	90.00	179.64	10,950.0	-8,867.6	314.2	8,869.4	0.00	0.00	0.00
20,800.0 20,900.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-8,967.6 -9,067.6	314.8 315.4	8,969.4 9,069.4	0.00 0.00	0.00 0.00	0.00 0.00
21,000.0	90.00	179.64	10,950.0	-9,167.6	316.1	9,169.4	0.00	0.00	0.00
21,100.0	90.00	179.64	10,950.0	-9,267.6	316.7	9,269.4	0.00	0.00	0.00
21,200.0 21,300.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-9,367.6 -9,467.6	317.3 317.9	9,369.4 9,469.4	0.00 0.00	0.00 0.00	0.00 0.00
21,400.0	90.00	179.64	10,950.0	-9,567.6	318.5	9,569.4	0.00	0.00	0.00
21,500.0	90.00	179.64	10,950.0	-9,667.6	319.2	9,669.4	0.00	0.00	0.00
21,600.0	90.00	179.64	10,950.0	-9,767.6 0.867.6	319.8	9,769.4	0.00	0.00	0.00
21,700.0 21,800.0	90.00 90.00	179.64 179.64	10,950.0 10,950.0	-9,867.6 -9,967.6	320.4 321.0	9,869.4 9,969.4	0.00 0.00	0.00 0.00	0.00 0.00
21,834.9	90.00	179.64	10,950.0	-10,002.5	321.2	10,004.3	0.00	0.00	0.00
21,884.9	90.00	179.64	10,950.0	-10,052.5	321.6	10,054.3	0.00	0.00	0.00
, -			,	,		•			

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
303H_SHL - plan hits target ce - Rectangle (sides		0.00	0.0	0.0	0.0	440,122.90	676,891.70	32° 12' 31.397 N	103° 45' 41.076 W
303H_BHL - plan misses targe - Point	0.00 et center by 0.2u	0.00 usft at 21884	10,950.0 .9usft MD (1	-10,052.5 0950.0 TVD, -	321.4 -10052.5 N, 32	430,070.40 21.6 E)	677,213.10	32° 10′ 51.901 N	103° 45' 37.958 W
303H_PP2 - plan hits target ce - Point	0.00 enter	0.00	10,950.0	-4,819.6	289.0	435,303.30	677,180.70	32° 11' 43.687 N	103° 45' 38.011 W
303H_FTP - plan hits target ce - Point	0.00 enter	0.00	10,950.0	361.3	256.8	440,484.20	677,148.50	32° 12' 34.959 N	103° 45' 38.065 W
303H_PP1 - plan hits target ce - Point	0.00 enter	0.00	10,950.0	-2,179.4	272.6	437,943.50	677,164.30	32° 12' 9.815 N	103° 45' 38.038 W
303H_PP3 - plan misses targe - Point	0.00 et center by 0.1u	0.00 usft at 19296	10,950.0 .0usft MD (1	-7,463.7 0950.0 TVD, -	305.4 -7463.7 N, 305	432,659.20 5.5 E)	677,197.10	32° 11' 17.520 N	103° 45' 37.984 W
303H_LTP - plan misses targe - Point	0.00 et center by 0.2u	0.00 usft at 21834	10,950.0 .9usft MD (1	-10,002.5 0950.0 TVD, -	321.1 -10002.5 N, 32	430,120.40 21.2 E)	677,212.80	32° 10′ 52.396 N	103° 45' 37.959 W

#### Planning Report

Database: LMRKPROD3

Company: Long Lead\_Well Planning

 Project:
 EDDY

 Site:
 PLU 15TWR

 Well:
 303H

 Wellbore:
 OH

 Design:
 Plan 1

Local Co-ordinate Reference:

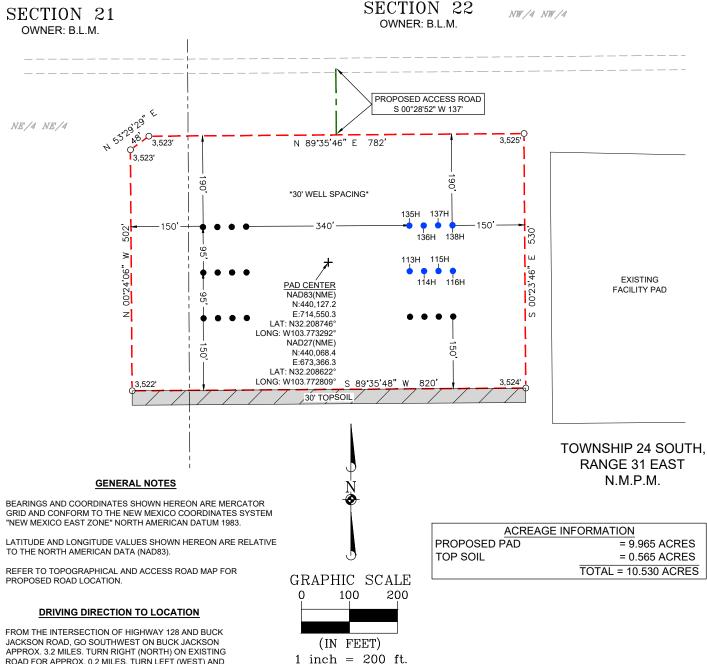
TVD Reference:
MD Reference:
North Reference:

**Survey Calculation Method:** 

Well 303H

RKB(3559+33) @ 3592.0usft RKB(3559+33) @ 3592.0usft

Grid



MARK DILLON TARE

MEN MEXICO

ROAD FOR APPROX. 0.2 MILES. TURN LEFT (WEST) AND GO APPROX, 0.7 MILES ARRIVING AT PROPOSED ROAD AND LOCATION IS TO THE SOUTH.

I.MARK DILLON HARP, NEW MEXICO PROFESSIONAL SURVEYOR NO. 23786, DO HEREBY CERTIFY THAT THIS SURVEY PLAT AND THE ACTUAL SURVEY ON THE GROUND UPON WHICH IT IS BASED WERE PREFORMED BY ME OR UNDER MY DIRECT SUPERVISION; THAT I AM RESPONSIBLE FOR THIS SURVEY, THAT THIS SURVEY MEETS THE MINIMUM STANDARDS FOR SURVEYING IN NEW MEXICO, AND THAT IS TRUE AND CORRECT TO THE



MARK DILLON HARP REGISTERED PROFESSIONAL LAND SURVEYOR STATE OF NEW MEXICO NO. 23786



505 Pecan Street, Suite 201, Fort Worth, TX 76102 ph:817.865.5344 manhard.com Texas Board of Professional Engineers & Land Surveyors Reg. No. F-10194754 (Surv), F-21732 (Eng)

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#### A WELL SITE PLAN FOR XTO PERMIAN OPERATING, LLC. POKER LAKE UNIT 15 TWR PROPOSED PAD "F"

**LEGEND** 

SECTION LINE

PROPOSED PAD

**EXISTING ROAD** TOP SOIL

**EXISTING PAD** 

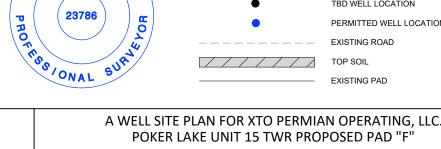
PROPOSED ACCESS ROAD

PERMITTED WELL LOCATION

TBD WELL LOCATION

PAD CENTER IS LOCATED 491 FEET FROM THE NORTH LINE AND 411 FEET FROM THE WEST LINE OF SECTION 22, TOWNSHIP 24 SOUTH, RANGE 31 EAST, N.M.P.M. EDDY COUNTY, NEW MEXICO

CHECKED BY: AR	DATE: 07/21/2023	SCALE: 1" = 200'	PROJECT NO.: 618.013003.14
DRAWN BY:	FIELD CREW:	REVISION NO.: NO	SHEET: 1 OF 3



#### OWNER: B.L.M. SE/4 SW/4 | SW/4 SE/4 NE/4 NW/4 NW/4 NE/4 SECTION 22 PROPOSED ACCESS ROAD S 00°17'53" W 151' OWNER: B.L.M. 3,543' O<sub>3,532</sub>' N 89°40'12" E 880' \*30' WELL SPACING\* 216H 202H 400 201H ≥ PAD CENTER NAD83(NME) N:440,129.7 E:716.311.6 LAT: N32.208728 LONG: W103.767598° NAD27(NME) 5 N:440,070.9 E:675,127.6 LAT: N32.208604 LONG: W103.767114° S 89°40'12" W 880' /30' TOPSOIL TOWNSHIP 24 SOUTH.

SECTION 15

BEARINGS AND COORDINATES SHOWN HEREON ARE MERCATOR
GRID AND CONFORM TO THE NEW MEXICO COORDINATES SYSTEM
"NEW MEXICO EAST ZONE" NORTH AMERICAN DATUM 1983.

**GENERAL NOTES** 

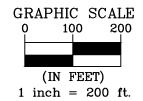
- 2. LATITUDE AND LONGITUDE VALUES SHOWN HEREON ARE RELATIVE TO THE NORTH AMERICAN DATA (NAD83).
- REFER TO TOPOGRAPHICAL AND ACCESS ROAD MAP FOR PROPOSED ROAD LOCATION.

#### **DRIVING DIRECTION TO LOCATION**

FROM THE INTERSECTION OF HIGHWAY 128 AND BUCK JACKSON ROAD, GO SOUTHWEST ON BUCK JACKSON APPROX. 3.2 MILES. TURN RIGHT (NORTH) ON EXISTING ROAD FOR APPROX. 0.2 MILES. TURN LEFT (WEST) AND GO APPROX. 0.4 MILES ARRIVING AT PROPOSED ROAD AND LOCATION IS TO THE SOUTH.

I,MARK DILLON HARP, NEW MEXICO PROFESSIONAL SURVEYOR NO. 23786, DO HEREBY CERTIFY THAT THIS SURVEY PLAT AND THE ACTUAL SURVEY ON THE GROUND UPON WHICH IT IS BASED WERE PREFORMED BY ME OR UNDER MY DIRECT SUPERVISION; THAT I AM RESPONSIBLE FOR THIS SURVEY, THAT THIS SURVEY MEETS THE MINIMUM STANDARDS FOR SURVEYING IN NEW MEXICO, AND THAT IS TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

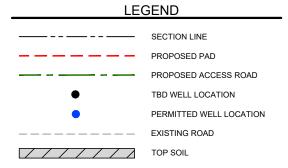
MARK DILLON HARP REGISTERED PROFESSIONAL LAND SURVEYOR STATE OF NEW MEXICO NO. 23786



RANGE 31 EAST N.M.P.M.

ACREAGE INFORMATION
PROPOSED PAD = 10.707 ACRES
TOP SOIL = 0.606 ACRES
TOTAL = 11.313 ACRES





## Manhard

505 Pecan Street, Suite 201, Fort Worth, TX 76102 ph:817.865.5344 manhard.com Texas Board of Professional Engineers & Land Surveyors Reg. No. F-10194754 (Surv), F-21732 (Eng)

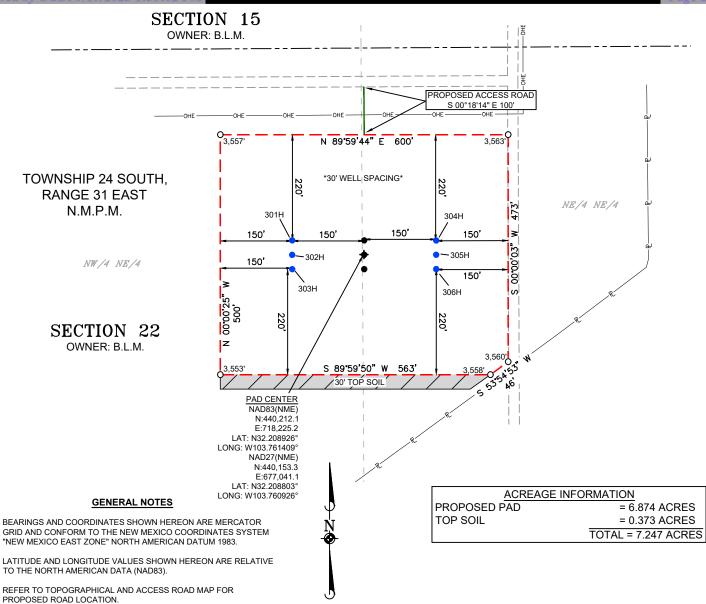
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## A WELL SITE PLAN FOR XTO PERMIAN OPERATING, LLC. POKER LAKE UNIT 15 TWR PROPOSED PAD "G"

PAD CENTER IS LOCATED 500 FEET FROM THE NORTH LINE AND 2,052 FEET FROM THE WEST LINE OF SECTION 22, TOWNSHIP 24 SOUTH, RANGE 31 EAST, N.M.P.M. EDDY COUNTY, NEW MEXICO

CHECKED BY:  AR	DATE: 07/21/2023	SCALE: 1" = 200'	PROJECT NO.: 618.013003.14
DRAWN BY:	FIELD CREW:	REVISION NO.: NO	SHEET: 1 OF 3

Released to Imaging: 11/21/2023 8.48.14 AM



#### **DRIVING DIRECTION TO LOCATION**

FROM THE INTERSECTION OF HIGHWAY 128 AND BUCK JACKSON RD. GO SOUTHWEST ON BUCK JACKSON RD. FOR APPROX. 3.2 MILES. TURN RIGHT (NORTH) ON EXISTING LEASE ROAD AND GO APPROX. 0.2 MILES. TURN LEFT (WEST) ON EXISTING LEASE ROAD AND GO 0.1 MILES ARRIVING AT PROPOSED ROAD AND THE LOCATION IS TO THE SOUTH.

I,MARK DILLON HARP, NEW MEXICO PROFESSIONAL SURVEYOR NO. 23786, DO HEREBY CERTIFY THAT THIS SURVEY PLAT AND THE ACTUAL SURVEY ON THE GROUND UPON WHICH IT IS BASED WERE PREFORMED BY ME OR UNDER MY DIRECT SUPERVISION; THAT I AM RESPONSIBLE FOR THIS SURVEY, THAT THIS SURVEY MEETS THE MINIMUM STANDARDS FOR SURVEYING IN NEW MEXICO, AND THAT IS TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND FELIFF.

MARK DILLON HARP REGISTERED PROFESSIONAL LAND SURVEYOR STATE OF NEW MEXICO NO. 23786



GRAPHIC SCALE

100

(IN FEET)

1 inch = 200 ft.

# LEGEND SECTION LINE PROPOSED PAD PROPOSED ACCESS ROAD TBD WELL LOCATION PERMITTED WELL LOCATION EXISTING ROAD OHE OHE EXISTING OVERHEAD ELECTRIC EXISTING PIPELINE TOP SOIL



505 Pecan Street, Suite 201, Fort Worth, TX 76102 ph: 8 1 7 . 8 6 5 . 5 3 4 4 manhard.com Texas Board of Professional Engineers & Land Surveyors Reg. No. F-10194754 (Surv), F-21732 (Eng)

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## A WELL SITE PLAN FOR XTO PERMIAN OPERATING, LLC. POKER LAKE UNIT 15 TWR PROPOSED PAD "H"

PAD CENTER IS LOCATED 431 FEET FROM THE NORTH LINE AND 1,316 FEET FROM THE EAST LINE OF SECTION 22, TOWNSHIP 24 SOUTH, RANGE 31 EAST, N.M.P.M. EDDY COUNTY, NEW MEXICO

AR	07/21/2023	1" = 200'	618.013003.14
DRAWN BY:	FIELD CREW:	REVISION NO.: NO	SHEET: 1 OF 3

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: XTO Permian Operating LLC
WELL NAME & NO.: Poker Lake Unit 15 TWR 303H
LOCATION: Sec 22-24S-31E-NMP
COUNTY: Eddy County, New Mexico

Changes approved through engineering via **Sundry 2745228** on 09/14/2023. Any previous COAs not addressed within the updated COAs still apply.

COA

H <sub>2</sub> S	• No	C Yes					
Potash / WIPP	None	Secretary	C R-111-P	□ WIPP			
Cave / Karst	C Low	• Medium	C High	Critical			
Wellhead	Conventional	<ul><li>Multibowl</li></ul>	O Both	<ul><li>Diverter</li></ul>			
Cementing	☐ Primary Squeeze	Cont. Squeeze	EchoMeter	□ DV Tool			
Special Req	Break Testing	☐ Water Disposal	$\square$ COM	Unit			
Variance	▼ Flex Hose	☐ Casing Clearance	☐ Pilot Hole	☐ Capitan Reef			
Variance	☐ Four-String	Offline Cementing	☐ Fluid-Filled	☐ Open Annulus			
☐ Batch APD / Sundry							

#### A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

#### **B. CASING**

- 1. The **9-5/8** inch surface casing shall be set at approximately 764 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. *Set depth checked and approved by BLM geologist*.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of

- six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 7022'
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, Capitan Reef, or potash.
- ❖ In Medium Cave/Karst Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus OR operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least **300 feet** into previous casing string. Operator shall provide method of verification. *Extra 100' of tieback due to not meeting 0.422" clearance requirement.*

#### C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2. Operator has proposed a multi-bowl wellhead assembly. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000** (**5M**) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172 must be followed.

#### D. SPECIAL REQUIREMENT (S)

#### **Unit Wells**

The well sign for a unit well shall include the unit number in addition to the surface and bottom hole lease numbers. This also applies to participating area numbers. If a participating area has not been established, the operator can use the general unit designation, but will replace the unit number with the participating area number when the sign is replaced.

#### **Commercial Well Determination**

A commercial well determination shall be submitted after production has been established for at least six months.

#### **BOPE Break Testing Variance**

• BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)

- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

#### **Offline Cementing**

Contact the BLM prior to the commencement of any offline cementing procedure.

#### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - Eddy County
    Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV (575) 361-2822
  - ✓ Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after

installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).

- b. When the operator proposes to set surface casing with Spudder Rig
  - Notify the BLM when moving in and removing the Spudder Rig.
  - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
  - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for

- details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

#### B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR part 3170 Subpart 3172 must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
  - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR part 3170 Subpart 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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1625 N. French Dr., Hobbs, NM 88240
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**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. **Santa Fe, NM 87505** 

CONDITIONS

Action 267099

#### **CONDITIONS**

Operator:	OGRID:
XTO PERMIAN OPERATING LLC.	373075
6401 HOLIDAY HILL ROAD	Action Number:
MIDLAND, TX 79707	267099
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rikala	All original COA's still apply. Additionally if cement is not circulated during cementing of a string, then a CBL is required for that string. Also a NSP must be obtained for this well.	11/21/2023