

Well Name: POKER LAKE UNIT 13-24 PC	Well Location: T24S / R29E / SEC 13 / SWNE /	County or Parish/State: /
Well Number: 125Y	Type of Well: CONVENTIONAL GAS WELL	Allottee or Tribe Name:
Lease Number: NMNM005912, NMNM05912	Unit or CA Name:	Unit or CA Number: NMNM71016X
US Well Number: 3001553555	Well Status: Plugged and Abandoned	Operator: XTO PERMIAN OPERATING LLC

Notice of Intent

Sundry ID: 2757429

Type of Submission: Notice of Intent	Type of Action: APD Change
Date Sundry Submitted: 10/27/2023	Time Sundry Submitted: 03:58
Date proposed operation will begin: 10/30/2023	

Procedure Description: ** Skid Original Wellbore, and Surface Hole Location Change XTO Energy, Inc requests permission to skid the original wellbore of the Poker Lake Unit 13-24 PC 125Y (plugged well) and to replace it with a new well skid original wellbore of the Poker Lake Unit 13-24 PC 125H. Original Wellbore of the Poker Lake Unit 13-24 PC 125Y, from 2459'FNL & 2310'FEL, LAT 32.21805663, LONG -103.9369702 to New Wellbore: Poker Lake Unit 13-24 PC 125H 2367'FSL & 1986'FEL, LAT 32.218054, LONG -103.936485. No Additional Surface Disturbance Attachments: From 3160-3 C102 Drilling Program Directional Plan Well Site Layout Casing Specs Sheet

NOI Attachments

Procedure Description

PLU_13_24_PC_NEW_125H_Sundry_Attachments_v2_20231102221832.pdf

Received by OCD: 11/9/2023 4:45:59 PM

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Well Name: POKER LAKE UNIT 13-24 PC		Well Location: T24S / R29E / SEC 13 / SWNE /	County or Parish/State: /
Well Number: 125Y	Type of Well: CONVENTIONAL GAS WELL		Allottee or Tribe Name:
Lease Number: NMNM005912, NMNM05912	Unit or CA Name:	Unit or CA Number: NMNM71016X	
US Well Number: 3001553555	Well Status: Plugged and Abandoned	Operator: XTO PERMIAN OPERATING LLC	

Conditions of Approval

Specialist Review
PLU_13_24_PC_Batch_Wells_Sundries_COA_20231105120944.pdf

Authorized
PLU_13_24_PC_NEW_125H_3160_3_signed_20231106142047.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: CASSIE EVANS

Signed on: NOV 02, 2023 02:04 PM

Name: XTO PERMIAN OPERATING LLC

Title: Regulatory Analyst

Street Address: 6401 Holiday Hill Road, Bldg 5

City: MidlandState: TX

Phone: (432) 218-3671

Email address: CASSIE.EVANS@EXXONMOBIL.COM

Field

Representative Name:

Street Address:

City:State:Zip:

Phone:

Email address:

BLM Point of Contact

BLM POC Name: CHRISTOPHER WALLS

BLM POC Title: Petroleum Engineer

BLM POC Phone: 5752342234

BLM POC Email Address: cwalls@blm.gov

Disposition: Approved

Disposition Date: 11/06/2023

Signature: Chris Walls

Form 3160-3
(August 2007)UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

APPLICATION FOR PERMIT TO DRILL OR REENTER

FORM APPROVED
OMB No. 1004-0137
Expires July 31, 20105. Lease Serial No.
NMNM05912

6. If Indian, Allottee or Tribe Name

7. If Unit or CA Agreement, Name and No.

8. Lease Name and Well No.
Poker Lake Unit 13-24 PC 125H

9. API Well No.

1a. Type of work: ☒ DRILL ☐ REENTER1b. Type of Well: ☒ Oil Well ☐ Gas Well ☐ Other ☒ Single Zone ☐ Multiple Zone

2. Name of Operator XTO Energy, Inc.

3a. Address 6401 Holiday Hill Road, Bldg 5
Midland, Texas 797013b. Phone No. (include area code)
432-214-788710. Field and Pool, or Exploratory
Purple Sage; Wolfcamp4. Location of Well (Report location clearly and in accordance with any State requirements. *)
At surface SWNE / 2459 FNL / 2220 FEL / LAT 32.218055 / LONG -103.936678 SWNE /
At proposed prod. zone 1959 FNL / 2316 FEL / LAT 32.219431 / LONG -103.93698811. Sec., T. R. M. or Blk. and Survey or Area
SEC 13 / T24S / R29E / NMP

14. Distance in miles and direction from nearest town or post office*

12. County or Parish
Eddy13. State
NM15. Distance from proposed* 2459 feet
location to nearest
property or lease line, ft.
(Also to nearest drig. unit line, if any)

16. No. of acres in lease

17. Spacing Unit dedicated to this well
64018. Distance from proposed location* 30 feet
to nearest well, drilling, completed,
applied for, on this lease, ft.19. Proposed Depth
10586 feet / 20627 feet20. BLM/BIA Bond No. on file
FED: COB00005021. Elevations (Show whether DF, KDB, RT, GL, etc.)
3094 feet22. Approximate date work will start*
10/27/2323. Estimated duration
90 Days

24. Attachments

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, must be attached to this form:

- | | |
|---|---|
| 1. Well plat certified by a registered surveyor.
2. A Drilling Plan.
3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office). | 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above).
5. Operator certification
6. Such other site specific information and/or plans as may be required by the BLM. |
|---|---|

25. Signature *Cassie Evans*Name (Printed/Typed)
Cassie EvansDate
10/17/23Title
Regulatory Coordinator

Approved by (Signature)

Name (Printed/Typed)

Date 11/6/2023

Title Sup PE

Office CFO

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

*(Instructions on page 2)

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(August 2007)UNITED STATES
DEPARTMENT OF THE INTERIOR
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APPLICATION FOR PERMIT TO DRILL OR REENTER

FORM APPROVED
OMB No. 1004-0137
Expires July 31, 20105. Lease Serial No.
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6. If Indian, Allottee or Tribe Name

7. If Unit or CA Agreement, Name and No.

8. Lease Name and Well No.
Poker Lake Unit 13-24 PC 125H9. API Well No.
300155355510. Field and Pool, or Exploratory
Purple Sage; Wolfcamp11. Sec., T. R. M. or Blk. and Survey or Area
SEC 13 / T24S / R29E / NMP12. County or Parish
Eddy13. State
NM1a. Type of work: ☒ DRILL ☐ REENTER1b. Type of Well: ☒ Oil Well ☐ Gas Well ☐ Other ☒ Single Zone ☐ Multiple Zone

2. Name of Operator XTO Energy, Inc.

3a. Address 6401 Holiday Hill Road, Bldg 5
Midland, Texas 797013b. Phone No. (include area code)
432-214-78874. Location of Well (Report location clearly and in accordance with any State requirements. *)
At surface SWNE / 2459 FNL / 2220 FEL / LAT 32.218055 / LONG -103.936678 SWNE /
At proposed prod. zone 1959 FNL / 2316 FEL / LAT 32.219431 / LONG -103.936988

14. Distance in miles and direction from nearest town or post office*

15. Distance from proposed* 2459 feet
location to nearest
property or lease line, ft.
(Also to nearest drig. unit line, if any)

16. No. of acres in lease

17. Spacing Unit dedicated to this well
64018. Distance from proposed location* 30 feet
to nearest well, drilling, completed,
applied for, on this lease, ft.19. Proposed Depth
10586 feet / 20627 feet20. BLM/BIA Bond No. on file
FED: COB00005021. Elevations (Show whether DF, KDB, RT, GL, etc.)
3094 feet22. Approximate date work will start*
10/27/2323. Estimated duration
90 Days

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5. Operator certification
6. Such other site specific information and/or plans as may be required by the BLM. |
|---|---|

25. Signature *Cassie Evans*Name (Printed/Typed)
Cassie EvansDate
10/17/23

Title

Regulatory Coordinator

Approved by (Signature)

Name (Printed/Typed)

Date

Title

Office

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Conditions of approval, if any, are attached.

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(Continued on page 2)

*(Instructions on page 2)

INSTRUCTIONS

GENERAL: This form is designed for submitting proposals to perform certain well operations, as indicated on Federal and Indian lands and leases for action by appropriate Federal agencies, pursuant to applicable Federal laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from local Federal offices.

ITEM 1: If the proposal is to redrill to the same reservoir at a different subsurface location or to a new reservoir, use this form with appropriate notations. Consult applicable Federal regulations concerning subsequent work proposals or reports on the well.

ITEM 4: Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local Federal offices for specific instructions.

ITEM 14: Needed only when location of well cannot readily be found by road from the land or lease description. A plat, or plats, separate or on the reverse side, showing the roads to, and the surveyed location of, the well, and any other required information, should be furnished when required by Federal agency offices.

ITEMS 15 AND 18: If well is to be, or has been directionally drilled, give distances for subsurface location of hole in any present or objective productive zone.

ITEM 22: Consult applicable Federal regulations, or appropriate officials, concerning approval of the proposal before operations are started.

NOTICES

The Privacy Act of 1974 and regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 25 U.S.C. 396; 43 CFR 3160

PRINCIPAL PURPOSES: The information will be used to: (1) process and evaluate your application for a permit to drill a new oil, gas, or service well or to reenter a plugged and abandoned well; and (2) document, for administrative use, information for the management, disposal and use of National Resource Lands and resources including (a) analyzing your proposal to discover and extract the Federal or Indian resources encountered; (b) reviewing procedures and equipment and the projected impact on the land involved; and (c) evaluating the effects of the proposed operation on the surface and subsurface water and other environmental impacts.

ROUTINE USE: Information from the record and/or the record will be transferred to appropriate Federal, State, and local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecution, in connection with congressional inquiries and for regulatory responsibilities.

EFFECT OF NOT PROVIDING INFORMATION: Filing of this application and disclosure of the information is mandatory only if you elect to initiate a drilling or reentry operation on an oil and gas lease.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to allow evaluation of the technical, safety, and environmental factors involved with drilling for oil and/or gas on Federal and Indian oil and gas leases. This information will be used to analyze and approve applications. Response to this request is mandatory only if the operator elects to initiate drilling or reentry operations on an oil and gas lease. The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C Street, N.W., Mail Stop 401 LS, Washington, D.C. 20240.

District I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720
District II
811 S. First St., Artesia, NM 88210
Phone: (575) 748-1283 Fax: (575) 748-9720
District III
1000 Rio Brazos Road, Aztec, NM 87410
Phone: (505) 334-6178 Fax: (505) 334-6170
District IV
1220 S. St. Francis Dr., Santa Fe, NM 87505
Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico

Energy, Minerals & Natural Resources Department

OIL CONSERVATION DIVISION

1220 South St. Francis Dr.

Santa Fe, NM 87505

Form C-102

Revised August 1, 2011

Submit one copy to appropriate District Office

☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

¹ API Number 30-015 53555		² Pool Code 98220		³ Pool Name Purple Sage; Wolfcamp					
⁴ Property Code		⁵ Property Name POKER LAKE UNIT 13-24 PC						⁶ Well Number 125H	
⁷ OGRID No. 373075		⁸ Operator Name XTO PERMIAN OPERATING, LLC						⁹ Elevation 3,094'	

¹⁰ Surface Location									
UL or lot no. G	Section 13	Township 24 S	Range 29 E	Lot Idn	Feet from the 2,459	North/South line NORTH	Feet from the 2,220	East/West line EAST	County EDDY

¹¹ Bottom Hole Location If Different From Surface									
UL or lot no. J	Section 1	Township 24 S	Range 29 E	Lot Idn	Feet from the 2,366	North/South line SOUTH	Feet from the 2,316	East/West line EAST	County EDDY
¹² Dedicated Acres 640		¹³ Joint or Infill		¹⁴ Consolidation Code		¹⁵ Order No.			

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

16

LOT 3

LOT 2

LOT 1

SEC. 1

T24S R29E

BHL

2,366' FSL

2,316' FEL

330'

280'

A

J

GRID AZ.=359°35'51"

HORZ. DIST.=50.00'

SEC. 6

T24S R30E

NMLC 0070175A

SEC. 12

T24S R29E

330'

SEC. 7

T24S R30E

GRID AZ.=359°43'31"

HORZ. DIST.=9,578.06'

SEC. 13

T24S R29E

SHL

2,459' FNL

2,220' FEL

332'

SEC. 12

T24S R29E

FTP

1,959' FNL

2,316' FEL

F

GRID AZ.=348°58'59"

HORZ. DIST.=509.68'

SEC. 12

T24S R30E

NMNM 0005912

LEGEND

SECTION LINE

PROPOSED WELLBORE

NEW MEXICO MINERAL LEASE

330' BUFFER

SHL (NAD83 NME)

Y = 443,288.7

X = 664,004.3

LAT. = 32.218055 °N

LONG. = 103.936678 °W

FTP (NAD83 NME)

Y = 443,789.0

X = 663,906.9

LAT. = 32.219431 °N

LONG. = 103.936988 °W

SHL (NAD27 NME)

Y = 443,229.3

X = 622,820.8

LAT. = 32.217931 °N

LONG. = 103.936190 °W

FTP (NAD27 NME)

Y = 443,729.6

X = 622,723.4

LAT. = 32.219307 °N

LONG. = 103.936499 °W

LTP (NAD83 NME)

Y = 453,366.9

X = 663,861.0

LAT. = 32.245760 °N

LONG. = 103.937022 °W

BHL (NAD83 NME)

Y = 453,416.9

X = 663,860.6

LAT. = 32.245897 °N

LONG. = 103.937022 °W

LTP (NAD27 NME)

Y = 453,307.3

X = 622,677.8

LAT. = 32.245636 °N

LONG. = 103.936532 °W

BHL (NAD27 NME)

Y = 453,357.3

X = 622,677.5

LAT. = 32.245773 °N

LONG. = 103.936532 °W

CORNER COORDINATES (NAD83 NME)

A - Y = 453,696.5 N , X = 663,524.5 E

B - Y = 451,051.0 N , X = 663,547.9 E

C - Y = 448,399.9 N , X = 663,559.1 E

D - Y = 445,748.2 N , X = 663,570.2 E

E - Y = 443,093.9 N , X = 663,576.0 E

F - Y = 443,091.0 N , X = 664,900.3 E

G - Y = 445,747.4 N , X = 664,894.3 E

H - Y = 448,398.4 N , X = 664,882.2 E

I - Y = 451,048.8 N , X = 664,870.9 E

J - Y = 453,698.2 N , X = 664,849.6 E

CORNER COORDINATES (NAD27 NME)

A - Y = 453,636.9 N , X = 622,341.4 E

B - Y = 450,991.4 N , X = 622,364.7 E

C - Y = 448,340.4 N , X = 622,375.8 E

D - Y = 445,688.8 N , X = 622,386.8 E

E - Y = 443,034.6 N , X = 622,392.5 E

F - Y = 443,031.7 N , X = 623,716.8 E

G - Y = 445,687.9 N , X = 623,710.9 E

H - Y = 448,338.9 N , X = 623,698.9 E

I - Y = 450,989.3 N , X = 623,687.7 E

J - Y = 453,638.6 N , X = 623,666.4 E

17 OPERATOR CERTIFICATION

I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief, and that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of such a mineral or working interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.

Cassie Evans

10/15/23

Signature

Date

Cassie Evans

Printed Name

cassie.evans@exxonmobil.com

E-mail Address

18 SURVEYOR CERTIFICATION

I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my belief.

10-12-2023

Date of Survey

KC/LM

2023060309

Signature and Seal of Professional Surveyor:

I, TIM C. PAPPAS, NEW MEXICO PROFESSIONAL SURVEYOR NO. 21209, DO HEREBY CERTIFY THAT THIS SURVEY PLAT AND THE ACTUAL SURVEY ON THE GROUND UPON WHICH IT IS BASED WERE PERFORMED BY ME OR UNDER MY DIRECT SUPERVISION; THAT I AM RESPONSIBLE FOR THIS SURVEY, THAT THIS SURVEY MEETS THE MINIMUM STANDARDS FOR SURVEYING IN NEW MEXICO, AND THAT IS TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

18 OCT 2023

TIM C. PAPPAS

REGISTERED PROFESSIONAL LAND SURVEYOR

STATE OF NEW MEXICO NO. 21209

TIM C. PAPPAS 21209

Certificate Number

TIM C. PAPPAS

NEW MEXICO

21209

PROFESSIONAL SURVEYOR

Released to Imaging: 11/21/2023 12:53:21 PM

DRILLING PLAN: BLM COMPLIANCE
(Supplement to BLM 3160-3)

XTO Energy Inc.
Poker Lake Unit 13-24 PC 125H
Projected TD: 20627' MD / 10586' TVD
SHL: 2459' FNL & 2220' FEL , Section 13, T24S, R29E
BHL: 2366' FSL & 2316' FEL , Section 1, T24S, R29E
Eddy County, NM

1. Geologic Name of Surface Formation

A. Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	288'	Water
Top of Salt	524'	Water
Base of Salt	3098'	Water
Delaware	3304'	Water
Brushy Canyon	5763'	Water/Oil/Gas
Bone Spring	7061'	Water
1st Bone Spring	7918'	Water/Oil/Gas
2nd Bone Spring	8385'	Water/Oil/Gas
3rd Bone Spring	9178'	Water/Oil/Gas
Wolfcamp	10345'	Water/Oil/Gas
Wolfcamp X	10377'	Water/Oil/Gas
Wolfcamp Y	10441'	Water/Oil/Gas
Wolfcamp A	10486'	Water/Oil/Gas
Target/Land Curve	10586'	Water/Oil/Gas

*** Hydrocarbons @ Brushy Canyon

*** Groundwater depth 40' (per NM State Engineers Office).

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 13.375 inch casing @ 474.13' (50' above the salt) and circulating cement back to surface. The intermediate will isolate from the top of salt down to the next casing seat by setting 7.625 inch casing at 9826.4' and cemented to surface. A 6.75 inch curve and 6.75 inch lateral hole will be drilled to 20627 MD/TD and 5.5 inch production casing will be set at TD and cemented back up in the intermediate shoe (estimated TOC 9526.4 feet).

In the event of wellbore instability, XTO is submitting a secondary 4 string design to run an additional casing string

3. Casing Design

Hole Size	Depth	OD Csg	Weight	Grade	Collar	New/Used	SF Burst	SF Collapse	SF Tension
17.5	0' – 474.13'	13.375	54.5	J-55	BTC	New	18.62	5.46	35.18
12.25	0' – 4000'	7.625	29.7	RY P-110	Flush Joint	New	2.54	2.52	1.91
12.25	4000' – 9826.4'	7.625	29.7	HC L-80	Flush Joint	New	1.85	1.87	2.35
6.75	0' – 9726.4'	5.5	23	RY P-110	Semi-Premium	New	1.45	2.61	2.03
6.75	9726.4' - 20627'	5.5	23	RY P-110	Semi-Flush	New	1.45	2.40	2.15

- XTO requests the option to utilize a spudder rig (Atlas Copco RD20 or Equivalent) to set and cement surface casing per this Sundry
- XTO requests to not utilize centralizers in the curve and lateral
- 7.625 Collapse analyzed using 50% evacuation based on regional experience.
- 5.5 Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35
- Test on Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less
- XTO requests the option to use 5" BTC Float equipment for the the production casing

Wellhead:

Permanent Wellhead – Multibowl System

A. Starting Head: 13-5/8" 10M top flange x 13-3/8" bottom

B. Tubing Head: 13-5/8" 10M bottom flange x 7-1/16" 15M top flange

- Wellhead will be installed by manufacturer's representatives.
- Manufacturer will monitor welding process to ensure appropriate temperature of seal.
- Operator will test the 7-5/8" casing per BLM Onshore Order 2
- Wellhead Manufacturer representative will not be present for BOP test plug installation

4. Cement Program

Surface Casing: 13.375, 54.5 New BTC, J-55 casing to be set at +/- 474.13'

Tail: 480 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Top of Cement: Surface

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Intermediate Casing: 7.625, 29.7 New casing to be set at +/- 9826.4'

1st Stage

Optional Lead: 1560 sxs Class C (mixed at 10.5 ppg, 2.77 ft3/sx, 15.59 gal/sx water)

TOC: Surface

Tail: 1880 sxs Class C (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

TOC: Brushy Canyon @ 5762.52

Compressives: 12-hr = 900 psi 24 hr = 1150 psi

2nd Stage

Lead: 0 sxs Class C (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water)

Tail: 3250 sxs Class C (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Top of Cement: 0

Compressives: 12-hr = 900 psi 24 hr = 1150 psi

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brush Canyon (5762.52') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top verification.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement inside the first intermediate casing. If cement reaches the desired height, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure the first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

Production Casing: 5.5, 23 New Semi-Flush, RY P-110 casing to be set at +/- 20627'

Lead: 20 sxs NeoCem (mixed at 11.5 ppg, 2.69 ft3/sx, 15.00 gal/sx water) Top of Cement: 9526.4 feet

Tail: 760 sxs VersaCem (mixed at 13.2 ppg, 1.51 ft3/sx, 8.38 gal/sx water) Top of Cement: 10026.4 feet

Compressives: 12-hr = 800 psi 24 hr = 1500 psi

XTO requests the option to offline cement and remediate (if needed) surface and intermediate casing strings where batch drilling is approved and if unplanned remediation is needed. XTO will ensure well is static with no pressure on the csg annulus, as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed when applicable per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops. Offline cement operations will then be conducted after the rig is moved off the current well to the next well in the batch sequence.

5. Pressure Control Equipment

Once the permanent WH is installed on the 13.375 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 3726 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nipping up on the 13.375, 5M bradenhead and flange, the BOP test will be limited to 5000 psi. When nipping up on the 7.625, the BOP will be tested to a minimum of 5000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production

hole on each of the wells.

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. Based on discussions with the BLM on February 27th 2020, we will request permission to **ONLY** retest broken pressure seals if the following conditions are met: 1. After a full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW (ppg)	Viscosity (sec/qt)	Fluid Loss (cc)
0' - 474.13'	17.5	FW/Native	8.4-8.9	35-40	NC
474.13' - 9826.4'	12.25	FW / Cut Brine / Direct Emulsion / WBM	10.2-10.7	30-32	NC
9826.4' - 20627'	6.75	OBM	11-11.5	50-60	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 9-5/8" surface casing with brine solution. A 9.7 ppg - 10.2 ppg cut brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 13.375 casing.

8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 170 to 190 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 6055 psi.

10. Anticipated Starting Date and Duration of Operations

Anticipated spud date will be after BLM approval. Move in operations and drilling is expected to take 40 days.

DRILLING PLAN: BLM COMPLIANCE
(Supplement to BLM 3160-3)

XTO Energy Inc.
Poker Lake Unit 13-24 PC 125H (Secondary Design)
Projected TD: 20627' MD / 10586' TVD
SHL: 2459' FNL & 2220' FEL , Section 13, T24S, R29E
BHL: 2366' FSL & 2316' FEL , Section 1, T24S, R29E
Eddy County, NM

1. Geologic Name of Surface Formation

A. Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	288'	Water
Top of Salt	524'	Water
Base of Salt	3098'	Water
Delaware	3304'	Water
Brushy Canyon	5763'	Water/Oil/Gas
Bone Spring	7061'	Water
1st Bone Spring Ss	7918'	Water/Oil/Gas
2nd Bone Spring Ss	8385'	Water/Oil/Gas
3rd Bone Spring Sh	9178'	Water/Oil/Gas
Wolfcamp	10345'	Water/Oil/Gas
Wolfcamp X	10377'	Water/Oil/Gas
Wolfcamp Y	10441'	Water/Oil/Gas
Wolfcamp A	10486'	Water/Oil/Gas
Target/Land Curve	10586'	Water/Oil/Gas

Rows hidden for unused formations

*** Hydrocarbons @ Brushy Canyon

*** Groundwater depth 40' (per NM State Engineers Office).

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 13.375 inch casing @ 474' (50' above the salt) and circulating cement back to surface. The salt will be isolated by setting 9.625 inch casing at 4257' and circulating cement to surface. The second intermediate will be 7.625 inch casing at 9860' and cementing to surface. A 6.75 inch curve and 6.75 inch lateral hole will be drilled to 20627 MD/TD and 5.5 inch production casing will be set at TD and cemented back up to 2nd intermediate (estimated TOC 9360 feet).

This secondary 4 string design is being submitted as a contingency to Poker Lake Unit 13-24 PC 125H primary design

3. Casing Design

Hole Size	MD	OD Csg	Weight	Grade	Collar	New/Used	SF Burst	SF Collapse	SF Tension
17.5	0' – 474'	13.375	54.5	J-55	BTC	New	2.07	5.46	35.19
12.25	0' – 4257'	9.625	40	J-55	BTC	New	1.46	2.05	3.70
8.75	0' – 4357'	7.625	29.7	RY P-110	Flush Joint	New	1.96	2.49	1.91
8.75	4357' – 9860'	7.625	29.7	HC L-80	Flush Joint	New	1.43	2.84	2.48
6.75	0' – 9760'	5.5	23	RY P-110	Semi-Premium	New	1.45	2.20	2.21
6.75	9760' - 20627'	5.5	23	RY P-110	Semi-Flush	New	1.45	2.03	6.74

• Production casing meets the clearance requirements as tapered string crosses over before encountering the intermediate shoe, per Onshore Order 2.3.B.1

• XTO requests the option to utilize a spudder rig (Atlas Copco RD20 or Equivalent) to set and cement surface and intermediate 1 casing per this Sundry

• XTO requests to not utilize centralizers in the curve and lateral

• 9.625 Collapse analyzed using 50% evacuation based on regional experience.

• 7.625 Collapse analyzed using 50% evacuation based on regional experience.

• 5.5 Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35

• Test on 2M annular & Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less

• XTO requests the option to use 5" BTC Float equipment for the the production casing

Wellhead:

Permanent Wellhead – Multibowl System

A. Starting Head: 13-5/8" 10M top flange x 13-3/8" bottom

B. Tubing Head: 13-5/8" 10M bottom flange x 7-1/16" 15M top flange

• Wellhead will be installed by manufacturer's representatives.

• Manufacturer will monitor welding process to ensure appropriate temperature of seal.

• Operator will test the 7-5/8" casing per BLM Onshore Order 2

• Wellhead Manufacturer representative will not be present for BOP test plug installation

Check casing size here

4. Cement Program

Surface Casing: 13.375, 54.5 New BTC, J-55 casing to be set at +/- 474'

Tail: 480 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)
Top of Cement: Surface
Compressives: 12-hr = 250 psi 24 hr = 500 psi

1st Intermediate Casing: 9.625, 40 New BTC, J-55 casing to be set at +/- 4257'

Lead: 1780 sxs Class C (mixed at 12.9 ppg, 1.39 ft3/sx, 10.13 gal/sx water)
Tail: 130 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)
Top of Cement: Surface
Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Intermediate Casing: 7.625, 29.7 New casing to be set at +/- 9860'

1st Stage
Optional Lead: 90 sxs Class C (mixed at 10.5 ppg, 2.77 ft3/sx, 15.59 gal/sx water)
TOC: 4057
Tail: 380 sxs Class C (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)
TOC: Brushy Canyon @ 5763
Compressives: 12-hr = 900 psi 24 hr = 1150 psi

2nd Stage
Lead: 0 sxs Class C (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water)
Tail: 450 sxs Class C (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)
Top of Cement: 0
Compressives: 12-hr = 900 psi 24 hr = 1150 psi

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brush Canyon (5763') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top verification.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement to surface. If cement reaches the desired height, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure the first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

Production Casing: 5.5, 23 New Semi-Flush, RY P-110 casing to be set at +/- 20627'

Lead: 20 sxs NeoCem (mixed at 11.5 ppg, 2.69 ft3/sx, 15.00 gal/sx water) Top of Cement: 9360 feet
Tail: 760 sxs VersaCem (mixed at 13.2 ppg, 1.51 ft3/sx, 8.38 gal/sx water) Top of Cement: 10026.4 feet
Compressives: 12-hr = 1375 psi 24 hr = 2285 psi

XTO requests the option to offline cement and remediate (if needed) surface and intermediate casing strings where batch drilling is approved and if unplanned remediation is needed. XTO will ensure well is static with no pressure on the csg annulus, as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed when applicable per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops. Offline cement operations will then be conducted after the rig is moved off the current well to the next well in the batch sequence.

DV Tool can be hidden

Bradenhead squeeze hidden if not applicable

5. Pressure Control Equipment

Temporary wellhead/diverter hidden if not needed

Once the permanent WH is installed on the 13.375 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 4827 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

Check casing sizes here

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nipping up on the 13.375, 5M bradenhead and flange, the BOP test will be limited to 5000 psi. When nipping up on the 7.625, the BOP will be tested to a minimum of 5000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells.

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. Based on discussions with the BLM on February 27th 2020, we will request permission to **ONLY** retest broken pressure seals if the following conditions are met: 1. After a full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW (ppg)	Viscosity (sec/qt)	Fluid Loss (cc)
0' - 474'	17.5	FW/Native	8.4-8.9	35-40	NC
474' - 4257'	12.25	Brine	10.2-10.7	30-32	NC
4257' to 9860'	8.75	BDE/OBM or FW/Brine/WBM	9.5-10	30-32	NC
9860' to 20627'	6.75	OBM	13-13.5	50-60	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 13-3/8" surface casing with brine solution. A 10.0 ppg -10.5 ppg brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

Check properties

Double check casing sizes in this statement

7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 13.375 casing.

8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 170 to 190 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 7156 psi.

10. Anticipated Starting Date and Duration of Operations

Anticipated spud date will be after BLM approval. Move in operations and drilling is expected to take 40 days.

ROC

**HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)
(HP552) - Poker Lake Unit 13-24 Pierce Canyon
New SHL for 125H**

OH

Plan: Plan 1

Standard Planning Report

11 October, 2023

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Project	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)		
Map System:	US State Plane 1927 (Exact solution)	System Datum:	Mean Sea Level
Geo Datum:	NAD 1927 (NADCON CONUS)		
Map Zone:	New Mexico East 3001		

Site	(HP552) - Poker Lake Unit 13-24 Pierce Canyon		
Site Position:		Northing:	443,229.66 usft
From:	Map	Easting:	622,670.59 usft
Position Uncertainty:	0.0 usft	Slot Radius:	13-3/16 "
		Latitude:	32° 13' 4.559 N
		Longitude:	103° 56' 12.031 W

Well	New SHL for 125H					
Well Position	+N/-S	0.0 usft	Northing:	443,229.81 usft	Latitude:	32° 13' 4.555 N
	+E/-W	0.0 usft	Easting:	622,820.36 usft	Longitude:	103° 56' 10.288 W
Position Uncertainty		0.0 usft	Wellhead Elevation:	usft	Ground Level:	3,094.0 usft
Grid Convergence:		0.21 °				

Wellbore	OH				
Magnetics	Model Name	Sample Date	Declination (°)	Dip Angle (°)	Field Strength (nT)
	IGRF2020	10/10/2023	6.44	59.76	47,214.18348015

Design	Plan 1			
Audit Notes:				
Version:	Phase:	PLAN	Tie On Depth:	0.0
Vertical Section:	Depth From (TVD) (usft)	+N/-S (usft)	+E/-W (usft)	Direction (°)
	0.0	0.0	0.0	359.73

Plan Survey Tool Program	Date	10/11/2023		
Depth From (usft)	Depth To (usft)	Survey (Wellbore)	Tool Name	Remarks
1	0.0	20,626.4 Plan 1 (OH)	XOMR2_OWSG MWD+IFR1+	
			OWSG MWD + IFR1 + Multi-St	

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
700.0	0.00	0.00	700.0	0.0	0.0	0.00	0.00	0.00	0.00	
850.0	3.00	220.00	849.9	-3.0	-2.5	2.00	2.00	0.00	220.00	
1,900.0	3.00	220.00	1,898.5	-45.1	-37.8	0.00	0.00	0.00	0.00	
2,123.2	7.00	245.00	2,120.8	-55.3	-53.9	2.00	1.79	11.20	41.43	
3,523.2	7.00	245.00	3,510.4	-127.4	-208.6	0.00	0.00	0.00	0.00	
3,873.2	0.00	0.00	3,859.5	-136.5	-227.9	2.00	-2.00	0.00	180.00	
10,026.4	0.00	0.00	10,012.7	-136.5	-227.9	0.00	0.00	0.00	0.00	
10,926.4	90.00	9.20	10,585.7	429.1	-136.3	10.00	10.00	0.00	9.20	
11,399.8	90.00	359.73	10,585.7	900.6	-99.5	2.00	0.00	-2.00	-90.00	
20,576.8	90.00	359.73	10,585.7	10,077.5	-142.5	0.00	0.00	0.00	0.00	LTP 13-24 PC 125H
20,626.8	90.00	359.73	10,585.7	10,127.5	-142.8	0.00	0.00	0.00	0.00	BHL 13-24 PC 125H

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	2.00	220.00	800.0	-1.3	-1.1	-1.3	2.00	2.00	0.00
850.0	3.00	220.00	849.9	-3.0	-2.5	-3.0	2.00	2.00	0.00
900.0	3.00	220.00	899.9	-5.0	-4.2	-5.0	0.00	0.00	0.00
1,000.0	3.00	220.00	999.7	-9.0	-7.6	-9.0	0.00	0.00	0.00
1,100.0	3.00	220.00	1,099.6	-13.0	-10.9	-13.0	0.00	0.00	0.00
1,200.0	3.00	220.00	1,199.5	-17.0	-14.3	-17.0	0.00	0.00	0.00
1,300.0	3.00	220.00	1,299.3	-21.0	-17.7	-21.0	0.00	0.00	0.00
1,400.0	3.00	220.00	1,399.2	-25.1	-21.0	-25.0	0.00	0.00	0.00
1,500.0	3.00	220.00	1,499.0	-29.1	-24.4	-29.0	0.00	0.00	0.00
1,600.0	3.00	220.00	1,598.9	-33.1	-27.8	-32.9	0.00	0.00	0.00
1,700.0	3.00	220.00	1,698.8	-37.1	-31.1	-36.9	0.00	0.00	0.00
1,800.0	3.00	220.00	1,798.6	-41.1	-34.5	-40.9	0.00	0.00	0.00
1,900.0	3.00	220.00	1,898.5	-45.1	-37.8	-44.9	0.00	0.00	0.00
2,000.0	4.69	236.41	1,998.3	-49.4	-42.9	-49.2	2.00	1.69	16.41
2,100.0	6.56	243.85	2,097.8	-54.1	-51.5	-53.9	2.00	1.87	7.44
2,123.2	7.00	245.00	2,120.8	-55.3	-53.9	-55.1	2.00	1.91	4.98
2,200.0	7.00	245.00	2,197.0	-59.3	-62.4	-59.0	0.00	0.00	0.00
2,300.0	7.00	245.00	2,296.3	-64.4	-73.5	-64.1	0.00	0.00	0.00
2,400.0	7.00	245.00	2,395.6	-69.6	-84.5	-69.2	0.00	0.00	0.00
2,500.0	7.00	245.00	2,494.8	-74.7	-95.6	-74.3	0.00	0.00	0.00
2,600.0	7.00	245.00	2,594.1	-79.9	-106.6	-79.4	0.00	0.00	0.00
2,700.0	7.00	245.00	2,693.3	-85.0	-117.6	-84.5	0.00	0.00	0.00
2,800.0	7.00	245.00	2,792.6	-90.2	-128.7	-89.6	0.00	0.00	0.00
2,900.0	7.00	245.00	2,891.8	-95.3	-139.7	-94.7	0.00	0.00	0.00
3,000.0	7.00	245.00	2,991.1	-100.5	-150.8	-99.8	0.00	0.00	0.00
3,100.0	7.00	245.00	3,090.3	-105.6	-161.8	-104.9	0.00	0.00	0.00
3,200.0	7.00	245.00	3,189.6	-110.8	-172.9	-110.0	0.00	0.00	0.00
3,300.0	7.00	245.00	3,288.8	-115.9	-183.9	-115.1	0.00	0.00	0.00
3,400.0	7.00	245.00	3,388.1	-121.1	-195.0	-120.2	0.00	0.00	0.00
3,500.0	7.00	245.00	3,487.4	-126.2	-206.0	-125.3	0.00	0.00	0.00
3,523.2	7.00	245.00	3,510.4	-127.4	-208.6	-126.5	0.00	0.00	0.00
3,600.0	5.46	245.00	3,586.7	-131.0	-216.1	-129.9	2.00	-2.00	0.00
3,700.0	3.46	245.00	3,686.4	-134.2	-223.2	-133.2	2.00	-2.00	0.00
3,800.0	1.46	245.00	3,786.3	-136.1	-227.1	-135.0	2.00	-2.00	0.00
3,873.2	0.00	0.00	3,859.5	-136.5	-227.9	-135.4	2.00	-2.00	0.00
3,900.0	0.00	0.00	3,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,000.0	0.00	0.00	3,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,100.0	0.00	0.00	4,086.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,200.0	0.00	0.00	4,186.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,300.0	0.00	0.00	4,286.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,400.0	0.00	0.00	4,386.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,500.0	0.00	0.00	4,486.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,600.0	0.00	0.00	4,586.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,700.0	0.00	0.00	4,686.3	-136.5	-227.9	-135.4	0.00	0.00	0.00

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
4,800.0	0.00	0.00	4,786.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
4,900.0	0.00	0.00	4,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,000.0	0.00	0.00	4,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,100.0	0.00	0.00	5,086.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,200.0	0.00	0.00	5,186.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,300.0	0.00	0.00	5,286.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,400.0	0.00	0.00	5,386.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,500.0	0.00	0.00	5,486.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,600.0	0.00	0.00	5,586.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,700.0	0.00	0.00	5,686.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,800.0	0.00	0.00	5,786.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
5,900.0	0.00	0.00	5,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,000.0	0.00	0.00	5,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,100.0	0.00	0.00	6,086.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,200.0	0.00	0.00	6,186.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,300.0	0.00	0.00	6,286.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,400.0	0.00	0.00	6,386.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,500.0	0.00	0.00	6,486.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,600.0	0.00	0.00	6,586.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,700.0	0.00	0.00	6,686.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,800.0	0.00	0.00	6,786.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
6,900.0	0.00	0.00	6,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,000.0	0.00	0.00	6,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,100.0	0.00	0.00	7,086.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,200.0	0.00	0.00	7,186.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,300.0	0.00	0.00	7,286.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,400.0	0.00	0.00	7,386.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,500.0	0.00	0.00	7,486.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,600.0	0.00	0.00	7,586.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,700.0	0.00	0.00	7,686.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,800.0	0.00	0.00	7,786.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
7,900.0	0.00	0.00	7,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,000.0	0.00	0.00	7,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,100.0	0.00	0.00	8,086.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,200.0	0.00	0.00	8,186.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,300.0	0.00	0.00	8,286.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,400.0	0.00	0.00	8,386.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,500.0	0.00	0.00	8,486.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,600.0	0.00	0.00	8,586.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,700.0	0.00	0.00	8,686.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,800.0	0.00	0.00	8,786.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
8,900.0	0.00	0.00	8,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,000.0	0.00	0.00	8,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,100.0	0.00	0.00	9,086.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,200.0	0.00	0.00	9,186.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,300.0	0.00	0.00	9,286.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,400.0	0.00	0.00	9,386.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,500.0	0.00	0.00	9,486.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,600.0	0.00	0.00	9,586.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,700.0	0.00	0.00	9,686.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,800.0	0.00	0.00	9,786.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
9,900.0	0.00	0.00	9,886.3	-136.5	-227.9	-135.4	0.00	0.00	0.00

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
10,000.0	0.00	0.00	9,986.3	-136.5	-227.9	-135.4	0.00	0.00	0.00
10,026.4	0.00	0.00	10,012.7	-136.5	-227.9	-135.4	0.00	0.00	0.00
10,100.0	7.36	9.20	10,086.1	-131.8	-227.2	-130.7	10.00	10.00	0.00
10,200.0	17.36	9.20	10,183.7	-110.7	-223.7	-109.6	10.00	10.00	0.00
10,300.0	27.36	9.20	10,276.0	-73.2	-217.7	-72.2	10.00	10.00	0.00
10,400.0	37.36	9.20	10,360.4	-20.4	-209.1	-19.4	10.00	10.00	0.00
10,500.0	47.36	9.20	10,434.2	46.0	-198.4	46.9	10.00	10.00	0.00
10,600.0	57.36	9.20	10,495.2	124.1	-185.7	125.0	10.00	10.00	0.00
10,700.0	67.36	9.20	10,541.5	211.4	-171.6	212.2	10.00	10.00	0.00
10,800.0	77.36	9.20	10,571.8	305.4	-156.4	306.1	10.00	10.00	0.00
10,900.0	87.36	9.20	10,585.1	403.1	-140.5	403.7	10.00	10.00	0.00
10,926.4	90.00	9.20	10,585.7	429.1	-136.3	429.8	10.00	10.00	0.00
11,000.0	90.00	7.73	10,585.7	501.9	-125.5	502.5	2.00	0.00	-2.00
11,100.0	90.00	5.73	10,585.7	601.2	-113.8	601.8	2.00	0.00	-2.00
11,200.0	90.00	3.73	10,585.7	700.9	-105.5	701.4	2.00	0.00	-2.00
11,300.0	90.00	1.73	10,585.7	800.8	-100.8	801.2	2.00	0.00	-2.00
11,399.8	90.00	359.73	10,585.7	900.6	-99.5	901.0	2.00	0.00	-2.00
11,400.0	90.00	359.73	10,585.7	900.8	-99.5	901.2	0.00	0.00	0.00
11,500.0	90.00	359.73	10,585.7	1,000.8	-100.0	1,001.2	0.00	0.00	0.00
11,600.0	90.00	359.73	10,585.7	1,100.8	-100.4	1,101.2	0.00	0.00	0.00
11,700.0	90.00	359.73	10,585.7	1,200.8	-100.9	1,201.2	0.00	0.00	0.00
11,800.0	90.00	359.73	10,585.7	1,300.8	-101.4	1,301.2	0.00	0.00	0.00
11,900.0	90.00	359.73	10,585.7	1,400.8	-101.8	1,401.2	0.00	0.00	0.00
12,000.0	90.00	359.73	10,585.7	1,500.8	-102.3	1,501.2	0.00	0.00	0.00
12,100.0	90.00	359.73	10,585.7	1,600.8	-102.8	1,601.2	0.00	0.00	0.00
12,200.0	90.00	359.73	10,585.7	1,700.8	-103.2	1,701.2	0.00	0.00	0.00
12,300.0	90.00	359.73	10,585.7	1,800.8	-103.7	1,801.2	0.00	0.00	0.00
12,400.0	90.00	359.73	10,585.7	1,900.8	-104.2	1,901.2	0.00	0.00	0.00
12,500.0	90.00	359.73	10,585.7	2,000.8	-104.7	2,001.2	0.00	0.00	0.00
12,600.0	90.00	359.73	10,585.7	2,100.8	-105.1	2,101.2	0.00	0.00	0.00
12,700.0	90.00	359.73	10,585.7	2,200.8	-105.6	2,201.2	0.00	0.00	0.00
12,800.0	90.00	359.73	10,585.7	2,300.8	-106.1	2,301.2	0.00	0.00	0.00
12,900.0	90.00	359.73	10,585.7	2,400.8	-106.5	2,401.2	0.00	0.00	0.00
13,000.0	90.00	359.73	10,585.7	2,500.7	-107.0	2,501.2	0.00	0.00	0.00
13,100.0	90.00	359.73	10,585.7	2,600.7	-107.5	2,601.2	0.00	0.00	0.00
13,200.0	90.00	359.73	10,585.7	2,700.7	-107.9	2,701.2	0.00	0.00	0.00
13,300.0	90.00	359.73	10,585.7	2,800.7	-108.4	2,801.2	0.00	0.00	0.00
13,400.0	90.00	359.73	10,585.7	2,900.7	-108.9	2,901.2	0.00	0.00	0.00
13,500.0	90.00	359.73	10,585.7	3,000.7	-109.3	3,001.2	0.00	0.00	0.00
13,600.0	90.00	359.73	10,585.7	3,100.7	-109.8	3,101.2	0.00	0.00	0.00
13,700.0	90.00	359.73	10,585.7	3,200.7	-110.3	3,201.2	0.00	0.00	0.00
13,800.0	90.00	359.73	10,585.7	3,300.7	-110.8	3,301.2	0.00	0.00	0.00
13,900.0	90.00	359.73	10,585.7	3,400.7	-111.2	3,401.2	0.00	0.00	0.00
14,000.0	90.00	359.73	10,585.7	3,500.7	-111.7	3,501.2	0.00	0.00	0.00
14,100.0	90.00	359.73	10,585.7	3,600.7	-112.2	3,601.2	0.00	0.00	0.00
14,200.0	90.00	359.73	10,585.7	3,700.7	-112.6	3,701.2	0.00	0.00	0.00
14,300.0	90.00	359.73	10,585.7	3,800.7	-113.1	3,801.2	0.00	0.00	0.00
14,400.0	90.00	359.73	10,585.7	3,900.7	-113.6	3,901.2	0.00	0.00	0.00
14,500.0	90.00	359.73	10,585.7	4,000.7	-114.0	4,001.2	0.00	0.00	0.00
14,600.0	90.00	359.73	10,585.7	4,100.7	-114.5	4,101.2	0.00	0.00	0.00
14,700.0	90.00	359.73	10,585.7	4,200.7	-115.0	4,201.2	0.00	0.00	0.00
14,800.0	90.00	359.73	10,585.7	4,300.7	-115.4	4,301.2	0.00	0.00	0.00

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
14,900.0	90.00	359.73	10,585.7	4,400.7	-115.9	4,401.2	0.00	0.00	0.00
15,000.0	90.00	359.73	10,585.7	4,500.7	-116.4	4,501.2	0.00	0.00	0.00
15,100.0	90.00	359.73	10,585.7	4,600.7	-116.8	4,601.2	0.00	0.00	0.00
15,200.0	90.00	359.73	10,585.7	4,700.7	-117.3	4,701.2	0.00	0.00	0.00
15,300.0	90.00	359.73	10,585.7	4,800.7	-117.8	4,801.2	0.00	0.00	0.00
15,400.0	90.00	359.73	10,585.7	4,900.7	-118.3	4,901.2	0.00	0.00	0.00
15,500.0	90.00	359.73	10,585.7	5,000.7	-118.7	5,001.2	0.00	0.00	0.00
15,600.0	90.00	359.73	10,585.7	5,100.7	-119.2	5,101.2	0.00	0.00	0.00
15,700.0	90.00	359.73	10,585.7	5,200.7	-119.7	5,201.2	0.00	0.00	0.00
15,800.0	90.00	359.73	10,585.7	5,300.7	-120.1	5,301.2	0.00	0.00	0.00
15,900.0	90.00	359.73	10,585.7	5,400.7	-120.6	5,401.2	0.00	0.00	0.00
16,000.0	90.00	359.73	10,585.7	5,500.7	-121.1	5,501.2	0.00	0.00	0.00
16,100.0	90.00	359.73	10,585.7	5,600.7	-121.5	5,601.2	0.00	0.00	0.00
16,200.0	90.00	359.73	10,585.7	5,700.7	-122.0	5,701.2	0.00	0.00	0.00
16,300.0	90.00	359.73	10,585.7	5,800.7	-122.5	5,801.2	0.00	0.00	0.00
16,400.0	90.00	359.73	10,585.7	5,900.7	-122.9	5,901.2	0.00	0.00	0.00
16,500.0	90.00	359.73	10,585.7	6,000.7	-123.4	6,001.2	0.00	0.00	0.00
16,600.0	90.00	359.73	10,585.7	6,100.7	-123.9	6,101.2	0.00	0.00	0.00
16,700.0	90.00	359.73	10,585.7	6,200.7	-124.3	6,201.2	0.00	0.00	0.00
16,800.0	90.00	359.73	10,585.7	6,300.7	-124.8	6,301.2	0.00	0.00	0.00
16,900.0	90.00	359.73	10,585.7	6,400.7	-125.3	6,401.2	0.00	0.00	0.00
17,000.0	90.00	359.73	10,585.7	6,500.7	-125.8	6,501.2	0.00	0.00	0.00
17,100.0	90.00	359.73	10,585.7	6,600.7	-126.2	6,601.2	0.00	0.00	0.00
17,200.0	90.00	359.73	10,585.7	6,700.7	-126.7	6,701.2	0.00	0.00	0.00
17,300.0	90.00	359.73	10,585.7	6,800.7	-127.2	6,801.2	0.00	0.00	0.00
17,400.0	90.00	359.73	10,585.7	6,900.7	-127.6	6,901.2	0.00	0.00	0.00
17,500.0	90.00	359.73	10,585.7	7,000.7	-128.1	7,001.2	0.00	0.00	0.00
17,600.0	90.00	359.73	10,585.7	7,100.7	-128.6	7,101.2	0.00	0.00	0.00
17,700.0	90.00	359.73	10,585.7	7,200.7	-129.0	7,201.2	0.00	0.00	0.00
17,800.0	90.00	359.73	10,585.7	7,300.7	-129.5	7,301.2	0.00	0.00	0.00
17,900.0	90.00	359.73	10,585.7	7,400.7	-130.0	7,401.2	0.00	0.00	0.00
18,000.0	90.00	359.73	10,585.7	7,500.7	-130.4	7,501.2	0.00	0.00	0.00
18,100.0	90.00	359.73	10,585.7	7,600.7	-130.9	7,601.2	0.00	0.00	0.00
18,200.0	90.00	359.73	10,585.7	7,700.7	-131.4	7,701.2	0.00	0.00	0.00
18,300.0	90.00	359.73	10,585.7	7,800.7	-131.9	7,801.2	0.00	0.00	0.00
18,400.0	90.00	359.73	10,585.7	7,900.7	-132.3	7,901.2	0.00	0.00	0.00
18,500.0	90.00	359.73	10,585.7	8,000.7	-132.8	8,001.2	0.00	0.00	0.00
18,600.0	90.00	359.73	10,585.7	8,100.7	-133.3	8,101.2	0.00	0.00	0.00
18,700.0	90.00	359.73	10,585.7	8,200.7	-133.7	8,201.2	0.00	0.00	0.00
18,800.0	90.00	359.73	10,585.7	8,300.7	-134.2	8,301.2	0.00	0.00	0.00
18,900.0	90.00	359.73	10,585.7	8,400.7	-134.7	8,401.2	0.00	0.00	0.00
19,000.0	90.00	359.73	10,585.7	8,500.7	-135.1	8,501.2	0.00	0.00	0.00
19,100.0	90.00	359.73	10,585.7	8,600.7	-135.6	8,601.2	0.00	0.00	0.00
19,200.0	90.00	359.73	10,585.7	8,700.7	-136.1	8,701.2	0.00	0.00	0.00
19,300.0	90.00	359.73	10,585.7	8,800.7	-136.5	8,801.2	0.00	0.00	0.00
19,400.0	90.00	359.73	10,585.7	8,900.7	-137.0	8,901.2	0.00	0.00	0.00
19,500.0	90.00	359.73	10,585.7	9,000.7	-137.5	9,001.2	0.00	0.00	0.00
19,600.0	90.00	359.73	10,585.7	9,100.7	-137.9	9,101.2	0.00	0.00	0.00
19,700.0	90.00	359.73	10,585.7	9,200.7	-138.4	9,201.2	0.00	0.00	0.00
19,800.0	90.00	359.73	10,585.7	9,300.7	-138.9	9,301.2	0.00	0.00	0.00
19,900.0	90.00	359.73	10,585.7	9,400.7	-139.4	9,401.2	0.00	0.00	0.00
20,000.0	90.00	359.73	10,585.7	9,500.7	-139.8	9,501.2	0.00	0.00	0.00

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	
20,100.0	90.00	359.73	10,585.7	9,600.7	-140.3	9,601.2	0.00	0.00	0.00	
20,200.0	90.00	359.73	10,585.7	9,700.7	-140.8	9,701.2	0.00	0.00	0.00	
20,300.0	90.00	359.73	10,585.7	9,800.7	-141.2	9,801.2	0.00	0.00	0.00	
20,400.0	90.00	359.73	10,585.7	9,900.7	-141.7	9,901.2	0.00	0.00	0.00	
20,500.0	90.00	359.73	10,585.7	10,000.7	-142.2	10,001.2	0.00	0.00	0.00	
20,576.8	90.00	359.73	10,585.7	10,077.5	-142.5	10,078.1	0.00	0.00	0.00	
20,600.0	90.00	359.73	10,585.7	10,100.7	-142.6	10,101.2	0.00	0.00	0.00	
20,626.8	90.00	359.73	10,585.7	10,127.5	-142.8	10,128.1	0.00	0.00	0.00	

Design Targets										
Target Name										
- hit/miss target	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude		Longitude
- Shape										
New SHL for 125H	0.00	0.01	0.0	0.0	0.0	443,229.81	622,820.36	32° 13' 4.555 N		103° 56' 10.288 W
- plan hits target center										
- Rectangle (sides W20.0 H20.0 D0.0)										
BHL 13-24 PC 125H	0.00	0.01	10,585.7	10,127.5	-142.9	453,357.32	622,677.46	32° 14' 44.784 N		103° 56' 11.516 W
- plan misses target center by 0.1usft at 20626.8usft MD (10585.7 TVD, 10127.5 N, -142.8 E)										
- Point										
FTP 13-24 PC 125H	0.00	0.01	10,585.7	499.8	-96.9	443,729.61	622,723.43	32° 13' 9.505 N		103° 56' 11.394 W
- plan misses target center by 28.6usft at 11001.2usft MD (10585.7 TVD, 503.1 N, -125.3 E)										
- Point										
LTP 13-24 PC 125H	0.00	0.01	10,585.7	10,077.5	-142.5	453,307.32	622,677.83	32° 14' 44.289 N		103° 56' 11.513 W
- plan hits target center										
- Rectangle (sides W100.0 H9,578.5 D0.0)										

ExxonMobil

Planning Report

Database:	LMRKPROD3	Local Co-ordinate Reference:	Well New SHL for 125H
Company:	ROC	TVD Reference:	RKB30' @ 3124.0usft (HP552)
Project:	HP 532/547/549/552 - Eddy County, NM (NAD 27 NME)	MD Reference:	RKB30' @ 3124.0usft (HP552)
Site:	(HP552) - Poker Lake Unit 13-24 Pierce Canyon	North Reference:	Grid
Well:	New SHL for 125H	Survey Calculation Method:	Minimum Curvature
Wellbore:	OH		
Design:	Plan 1		

Formations						
Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)	
289.2	289.2	Rustler				
525.1	525.1	Salado				
3,108.7	3,099.0	Base of Salt				
3,133.9	3,124.0	Formation 26				
3,315.9	3,304.7	Delaware				
4,222.1	4,208.4	Cherry Canyon				
5,777.2	5,763.5	Brushy Canyon				
6,832.8	6,819.1	Basal Brushy Canyon				
7,075.6	7,061.9	Bone Spring				
7,200.5	7,186.8	Avalon Upper				
7,771.0	7,757.3	Avalon Lower				
7,933.0	7,919.3	1st Bone Spring Lime				
8,086.5	8,072.8	1st Bone Spring Sand				
8,399.4	8,385.8	2nd Bone Spring Lime				
8,925.0	8,911.3	2nd Bone Spring Sand				
9,192.9	9,179.2	3rd Bone Spring Lime				
9,570.2	9,556.5	Harkey Sand				
9,601.6	9,587.9	3rd Bone Spring Shale				
10,001.8	9,988.1	3rd Bone Spring Sand				
10,381.6	10,345.6	Wolfcamp				
10,422.8	10,378.2	Wolfcamp X				
10,512.1	10,442.3	Wolfcamp Y				
10,584.6	10,486.7	Wolfcamp A				

Plan Annotations					
Measured Depth (usft)	Vertical Depth (usft)	Local Coordinates			
		+N/-S (usft)	+E/-W (usft)	Comment	
700.0	700.0	0.0	0.0	Start Build 2.00	
850.0	849.9	-3.0	-2.5	Start 1050.0 hold at 850.0 MD	
1,900.0	1,898.5	-45.1	-37.8	Start DLS 2.00 TFO 41.43	
2,123.2	2,120.8	-55.3	-53.9	Start 1400.0 hold at 2123.2 MD	
3,523.2	3,510.4	-127.4	-208.6	Start Drop -2.00	
3,873.2	3,859.5	-136.5	-227.9	Start 6153.2 hold at 3873.2 MD	
10,026.4	10,012.7	-136.5	-227.9	Start Build 10.00	
10,926.4	10,585.7	429.1	-136.3	Start DLS 2.00 TFO -90.00	
11,399.8	10,585.7	900.6	-99.5	Start 9177.0 hold at 11399.8 MD	
20,576.8	10,585.7	10,077.5	-142.5	Start 50.0 hold at 20576.8 MD	
20,626.8	10,585.7	10,127.5	-142.8	TD at 20626.8	



U. S. Steel Tubular Products

10/10/2022 1:42:03 PM

13.375" 54.50lb/ft (0.380" Wall) J55 USS-CDC®



MECHANICAL PROPERTIES	Pipe	USS-CDC®		--
Minimum Yield Strength	55,000	--	psi	--
Maximum Yield Strength	80,000	--	psi	--
Minimum Tensile Strength	75,000	--	psi	--
DIMENSIONS	Pipe	USS-CDC®		--
Outside Diameter	13.375	14.375	in.	--
Wall Thickness	0.380	--	in.	--
Inside Diameter	12.615	12.615	in.	--
Standard Drift	12.459	12.459	in.	--
Alternate Drift	12.500	12.500	in.	--
Nominal Linear Weight, T&C	54.50	--	lb/ft	--
Plain End Weight	52.79	--	lb/ft	--
SECTION AREA	Pipe	USS-CDC®		--
Critical Area	15.513	15.513	sq. in.	--
Joint Efficiency	--	100.0	%	--
PERFORMANCE	Pipe	USS-CDC®		--
Minimum Collapse Pressure	1,130	1,130	psi	--
External Pressure Leak Resistance	--	900	psi	--
Minimum Internal Yield Pressure	2,740	2,740	psi	--
Minimum Pipe Body Yield Strength	853,000	--	lb	--
Joint Strength	--	909,000	lb	--
Compression Rating	--	545,400	lb	--
Reference Length	--	11,119	ft	--
Maximum Uniaxial Bend Rating	--	12.1	deg/100 ft	--
MAKE-UP DATA	Pipe	USS-CDC®		--
Make-Up Loss	--	5.31	in.	--
Minimum Make-Up Torque	--	17,000	ft-lb	--
Maximum Make-Up Torque	--	21,000	ft-lb	--
Connection Yield Torque	--	35,200	ft-lb	--

UNCONTROLLED

Notes

- Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness and Specified Minimum Yield Strength (SMYS).
- Uniaxial bending rating shown is structural only, and equal to compression efficiency.
- Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- Reference length is calculated by joint strength divided by nominal threaded and coupled weight with 1.5 safety factor.
- Connection external pressure leak resistance has been verified to 80% API pipe body collapse pressure following the guidelines of API 5C5 Call II.

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U. S. Steel Tubular Products

10/10/2022 1:43:14 PM

9.625" 40.00lb/ft (0.395" Wall) J55 USS-CDC®



MECHANICAL PROPERTIES	Pipe	USS-CDC®		--
Minimum Yield Strength	55,000	--	psi	--
Maximum Yield Strength	80,000	--	psi	--
Minimum Tensile Strength	75,000	--	psi	--
DIMENSIONS	Pipe	USS-CDC®		--
Outside Diameter	9.625	10.625	in.	--
Wall Thickness	0.395	--	in.	--
Inside Diameter	8.835	8.835	in.	--
Standard Drift	8.679	8.679	in.	--
Alternate Drift	8.750	8.750	in.	--
Nominal Linear Weight, T&C	40.00	--	lb/ft	--
Plain End Weight	38.97	--	lb/ft	--
SECTION AREA	Pipe	USS-CDC®		--
Critical Area	11.454	11.454	sq. in.	--
Joint Efficiency	--	100.0	%	--
PERFORMANCE	Pipe	USS-CDC®		--
Minimum Collapse Pressure	2,570	2,570	psi	--
External Pressure Leak Resistance	--	2,060	psi	--
Minimum Internal Yield Pressure	3,950	3,950	psi	--
Minimum Pipe Body Yield Strength	630,000	--	lb	--
Joint Strength	--	714,000	lb	--
Compression Rating	--	428,000	lb	--
Reference Length	--	11,900	ft	--
Maximum Uniaxial Bend Rating	--	17.8	deg/100 ft	--
MAKE-UP DATA	Pipe	USS-CDC®		--
Make-Up Loss	--	5.31	in.	--
Minimum Make-Up Torque	--	15,000	ft-lb	--
Maximum Make-Up Torque	--	18,500	ft-lb	--
Connection Yield Torque	--	23,100	ft-lb	--

UNCONTROLLED

Notes

- Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness and Specified Minimum Yield Strength (SMYS).
- Uniaxial bending rating shown is structural only, and equal to compression efficiency.
- Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- Reference length is calculated by joint strength divided by nominal threaded and coupled weight with 1.5 safety factor.
- Connection external pressure leak resistance has been verified to 80% API pipe body collapse pressure following the guidelines of API 5C5 Call II.

Legal Notice

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U. S. Steel Tubular Products

7/30/2020 3:27:27 PM

7.625" 29.70lbs/ft (0.375" Wall) P110 RY USS-LIBERTY FJM®



MECHANICAL PROPERTIES	Pipe	USS-LIBERTY FJM®	
Minimum Yield Strength	110,000	--	psi
Maximum Yield Strength	125,000	--	psi
Minimum Tensile Strength	125,000	--	psi
DIMENSIONS	Pipe	USS-LIBERTY FJM®	
Outside Diameter	7.625	7.625	in.
Wall Thickness	0.375	--	in.
Inside Diameter	6.875	6.789	in.
Standard Drift	6.750	6.750	in.
Alternate Drift	--	--	in.
Nominal Linear Weight, T&C	29.70	--	lbs/ft
Plain End Weight	29.06	--	lbs/ft
SECTION AREA	Pipe	USS-LIBERTY FJM®	
Critical Area	8.541	5.074	sq. in.
Joint Efficiency	--	59.4	%
PERFORMANCE	Pipe	USS-LIBERTY FJM®	
Minimum Collapse Pressure	5,350	5,350	psi
Minimum Internal Yield Pressure	9,460	9,460	psi
Minimum Pipe Body Yield Strength	940,000	--	lbs
Joint Strength	--	558,000	lbs
Compression Rating	--	558,000	lbs
Reference Length	--	12,810	ft
Maximum Uniaxial Bend Rating	--	39.3	deg/100 ft
MAKE-UP DATA	Pipe	USS-LIBERTY FJM®	
Make-Up Loss	--	3.92	in.
Minimum Make-Up Torque	--	10,800	ft-lbs
Maximum Make-Up Torque	--	15,250	ft-lbs

1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness and Specified Minimum Yield Strength (SMYS).
2. Compressive & Tensile Connection Efficiencies are calculated by dividing the connection critical area by the pipe body area.
3. Uniaxial bending rating shown is structural only, and equal to compression efficiency.
4. USS-LIBERTY FJM™ connections are optimized for each combination of OD and wall thickness and cannot be interchanged.
5. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
6. Reference length is calculated by joint strength divided by nominal plain end weight with 1.5 safety factor.
7. Connection external pressure leak resistance has been verified to 100% API pipe body collapse pressure following the guidelines of API 5C5 Cal III.

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U. S. Steel Tubular Products

DRAFT

5.500 20.00 LB (0.361)

P110 RY

USS-TALON HTQ™RD5.900

PIPE

CONNECTION

MECHANICAL PROPERTIES

[6]

Minimum Yield Strength	110,000	psi
Maximum Yield Strength	125,000	psi
Minimum Tensile Strength	125,000	psi

DIMENSIONS

Outside Diameter	5.500	5.900	in.
Wall Thickness	0.361		in.
Inside Diameter	4.778	4.778	in.
Drift - API	4.653		in.
Nominal Linear Weight, T&C	20.00		lbs/ft
Plain End Weight	19.83	19.83	lbs/ft

SECTION AREA

Cross Sectional Area Critical Area	5.828	5.828	sq. in.
Joint Efficiency		100%	% [2]

PERFORMANCE

Minimum Collapse Pressure	11,100	11,100	psi
Minimum Internal Yield Pressure	12,640	12,640	psi
Minimum Pipe Body Yield Strength	641,000		lbs
Joint Strength		641,000	lbs
Compression Rating		641,000	lbs
Reference Length		21,548	ft [5]
Maximum Uniaxial Bend Rating		91.7	deg/100 ft [3]

MAKE-UP DATA

Minimum Make-Up Torque	24,700	ft-lbs [4]
Maximum Make-Up Torque	27,700	ft-lbs [4]
Maximum Operating Torque	39,500	ft-lbs [4]
Make-Up Loss	5.58	in.

Notes:

- 1) Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2) Compressive & Tensile Connection Efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3) Uniaxial bending rating shown is structural only.
- 4) Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5) Reference length is calculated by joint strength divided by plain end weight with 1.5 safety factor.
- 6) Coupling must meet minimum mechanical properties of the pipe

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Manual USS Product Data Sheet 2019 rev28

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CONDITIONS

Action 284464

CONDITIONS

Operator: XTO PERMIAN OPERATING LLC. 6401 HOLIDAY HILL ROAD MIDLAND, TX 79707	OGRID: 373075
	Action Number: 284464
	Action Type: [C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

CONDITIONS

Created By	Condition	Condition Date
ward.rikala	Original COA's still apply. Additionally, if cement does not circulate during cementing of a string, then a CBL is required for that string.	11/21/2023