

Form 3160-5
(June 2019)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 2021

SUNDRY NOTICES AND REPORTS ON WELLS
Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.

| | | |
|---|-----------------------------------|---|
| SUBMIT IN TRIPLICATE - Other instructions on page 2 | | 5. Lease Serial No. |
| 1. Type of Well <input type="checkbox"/> Oil Well <input type="checkbox"/> Gas Well <input type="checkbox"/> Other | | 6. If Indian, Allottee or Tribe Name |
| 2. Name of Operator | | 7. If Unit of CA/Agreement, Name and/or No. |
| 3a. Address | 3b. Phone No. (include area code) | 8. Well Name and No. |
| 4. Location of Well (Footage, Sec., T.,R.,M., or Survey Description) | | 9. API Well No. |
| | | 10. Field and Pool or Exploratory Area |
| | | 11. Country or Parish, State |

12. CHECK THE APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | | |
|---|---|---|--|---|--|
| <input type="checkbox"/> Notice of Intent | <input type="checkbox"/> Acidize | <input type="checkbox"/> Deepen | <input type="checkbox"/> Production (Start/Resume) | <input type="checkbox"/> Water Shut-Off | |
| | <input type="checkbox"/> Alter Casing | <input type="checkbox"/> Hydraulic Fracturing | <input type="checkbox"/> Reclamation | <input type="checkbox"/> Well Integrity | |
| <input type="checkbox"/> Subsequent Report | <input type="checkbox"/> Casing Repair | <input type="checkbox"/> New Construction | <input type="checkbox"/> Recomplete | <input type="checkbox"/> Other | |
| | <input type="checkbox"/> Change Plans | <input type="checkbox"/> Plug and Abandon | <input type="checkbox"/> Temporarily Abandon | | |
| <input type="checkbox"/> Final Abandonment Notice | <input type="checkbox"/> Convert to Injection | <input type="checkbox"/> Plug Back | <input type="checkbox"/> Water Disposal | | |

13. Describe Proposed or Completed Operation: Clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recompleate horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be perfonned or provide the Bond No. on file with BLM/BIA. Required subsequent reports must be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed and the operator has detennined that the site is ready for final inspection.)

| | | |
|---|-------|--|
| 14. I hereby certify that the foregoing is true and correct. Name (Printed/Typed) | | |
| | Title | |
| Signature | Date | |

THE SPACE FOR FEDERAL OR STATE OFFICE USE

| | | |
|---|--------|------|
| Approved by | | |
| | Title | Date |
| Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. | Office | |

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

DISTRICT I
1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-6161 Fax: (575) 393-0720

DISTRICT II
811 S. First St., Artesia, NM 88210
Phone: (575) 748-1283 Fax: (575) 748-9720

DISTRICT III
1000 Rio Brazos Rd., Aztec, NM 87410
Phone: (505) 334-6178 Fax: (505) 334-6170

DISTRICT IV
1220 S. St. Francis Dr., Santa Fe, NM 87505
Phone: (505) 476-3460 Fax: (505) 476-3462

State of New Mexico
Energy, Minerals & Natural Resources Department
OIL CONSERVATION DIVISION
1220 South St. Francis Dr.
Santa Fe, New Mexico 87505

Form C-102
Revised August 1, 2011
Submit one copy to appropriate
District Office
☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

| | | | |
|-----------------------------------|---|---------------------------|--|
| API Number 30-025-52152 | | Pool Code 97366 | Pool Name Billbrey Basin; Bone Spring, South |
| Property Code 333115 | Property Name AMAZING 19 FED | | Well Number 505H |
| OGRID No. 7377 | Operator Name EOG RESOURCES, INC. | | Elevation 3653' |

Surface Location

| | | | | | | | | | |
|---------------|---------|----------|-------|---------|---------------|------------------|---------------|----------------|--------|
| UL or lot no. | Section | Township | Range | Lot Idn | Feet from the | North/South line | Feet from the | East/West line | County |
| A | 19 | 22 S | 32 E | | 905 | NORTH | 1051 | EAST | LEA |

Bottom Hole Location If Different From Surface

| | | | | | | | | | |
|---------------|---------|----------|-------|---------|---------------|------------------|---------------|----------------|--------|
| UL or lot no. | Section | Township | Range | Lot Idn | Feet from the | North/South line | Feet from the | East/West line | County |
| O | 30 | 22 S | 32 E | | 100 | SOUTH | 1320 | EAST | LEA |

| | | | | |
|-----------------|-----------------|-------------------|-----------|------------|
| Dedicated Acres | Joint or Infill | Consolidated Code | Order No. | LEASE WELL |
| 640 | | | | |

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

| | | |
|--|---|---|
| <p>SURFACE LOCATION</p> <p>NEW MEXICO EAST NAD 1983 X=734149' Y=503200' LAT=N32.381820° LONG=W103.708741° NAD 1927 X=692966' Y=503140' LAT=N32.381697° LONG=W103.708253° 905' FNL 1051' FEL</p> <p>KOP LOCATION</p> <p>NEW MEXICO EAST NAD 1983 X=733874' Y=504052' LAT=N32.384165° LONG=W103.709615° NAD 1927 X=692691' Y=503992' LAT=N32.384042° LONG=W103.709127° 50' FNL 1320' FEL</p> | <p>The map displays a grid of sections (e.g., 13-18, 24-29) and lots (LOT 1-4). A proposed well path is shown in red, starting from the KOP (Kilometer Offset Point) at X=732552', Y=504087'. The path includes a turn at X=735193', Y=504118' (AZ = 342.10°, 895.0', 1051') and another at X=735211', Y=501477' (AZ = 179.61°, 5231.2'). The path ends at the BHL/LMP (Bottom Hole Location / Last Measured Point) at X=732627', Y=493534'. Other points include X=735229', Y=498836' and X=735247', Y=496194'. A green shaded area indicates the USA NMNM-00090. A dashed line marks the HZ SPACING UNIT.</p> | <p>FIRST TAKE POINT</p> <p>NEW MEXICO EAST NAD 1983 X=733874' Y=504002' LAT=N32.384028° LONG=W103.709615° NAD 1927 X=692692' Y=503942' LAT=N32.383905° LONG=W103.709127° 100' FNL 1320' FEL</p> <p>LOWER MOST PERF./ BOTTOM HOLE LOCATION</p> <p>NEW MEXICO EAST NAD 1983 X=733944' Y=493643' LAT=N32.355554° LONG=W103.709584° NAD 1927 X=692761' Y=493583' LAT=N32.355431° LONG=W103.709097° 100' FSL 1320' FEL</p> |
| <p>OPERATOR CERTIFICATION</p> <p>I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief, and that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of such a mineral or working interest, or to voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.</p> <p><i>Star L Harrell</i> 11/1/23 Signature Date</p> <p>Star L Harrell Print Name</p> <p>star_harrell@eogresources.com E-mail Address</p> | <p>SURVEYORS CERTIFICATION</p> <p>I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the same is true and correct to the best of my belief. SEPTEMBER 11, 2023</p> <p>Date of Survey _____ Signature and Seal of Professional Surveyor:</p> <div style="text-align: center;"> <p>Ralph B. Chustz, Jr. NEW MEXICO PROFESSIONAL SURVEYOR 26264 10/27/2023</p> </div> | |
| <p>Job No.: EOG B200015 RALPH B. CHUSTZ, JR. N.M.P.L.S. Certificate Number 26264</p> | | |



Amazing 19 Fed 505H

Revised Permit Information 10/24/2023:

Well Name: Amazing 19 Fed 505H

Location: SHL: 905' FNL & 1051' FEL, Section 19, T-22-S, R-32-E, Lea Co., N.M.

BHL: 100' FSL & 1320' FEL, Section 30, T-22-S, R-32-E, Lea Co., N.M.

Casing Program A:

| Hole Size | Interval MD | | Interval TVD | | Csg OD | Weight | Grade | Conn |
|-----------|-------------|---------|--------------|---------|---------|--------|---------|------|
| | From (ft) | To (ft) | From (ft) | To (ft) | | | | |
| 16" | 0 | 940 | 0 | 940 | 13-3/8" | 54.5# | J-55 | STC |
| 11" | 0 | 5,222 | 0 | 5,140 | 9-5/8" | 40# | J-55 | LTC |
| 6-3/4" | 0 | 20,916 | 0 | 10,638 | 5-1/2" | 17# | HCP-110 | LTC |

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

Cementing Program:

| Depth | No. Sacks | Wt. ppg | Yld Ft ³ /sk | Slurry Description |
|-------------------|-----------|---------|-------------------------|--|
| 940' 13-3/8" | 240 | 13.5 | 1.73 | Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl ₂ + 0.25 lb/sk Cello-Flake (TOC @ Surface) |
| | 160 | 14.8 | 1.34 | Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 740') |
| 5,140' 9-5/8" | 470 | 12.7 | 2.22 | Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface) |
| | 100 | 14.8 | 1.32 | Tail: Class C + 10% NaCl + 3% MagOx (TOC @ 4,110') |
| 20,916' 5-1/2" | 320 | 10.5 | 3.21 | Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,410') |
| | 750 | 13.2 | 1.52 | Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 10240') |


eog resources
Amazing 19 Fed 505H

| Additive | Purpose |
|---------------------|---|
| Bentonite Gel | Lightweight/Lost circulation prevention |
| Calcium Chloride | Accelerator |
| Cello-flake | Lost circulation prevention |
| Sodium Metasilicate | Accelerator |
| MagOx | Expansive agent |
| Pre-Mag-M | Expansive agent |
| Sodium Chloride | Accelerator |
| FL-62 | Fluid loss control |
| Halad-344 | Fluid loss control |
| Halad-9 | Fluid loss control |
| HR-601 | Retarder |
| Microbond | Expansive Agent |

Note: Cement volumes based on bit size plus at least 25% excess in the open hole plus 10% excess in the cased-hole overlap section.

Mud Program:

| Depth (TVD) | Type | Weight (ppg) | Viscosity | Water Loss |
|------------------|-------------|--------------|-----------|------------|
| 0 – 940' | Fresh - Gel | 8.6-8.8 | 28-34 | N/c |
| 940' – 5,140' | Brine | 8.6-8.8 | 28-34 | N/c |
| 5,140' – 20,916' | Oil Base | 8.8-9.5 | 58-68 | N/c - 6 |



TUBING REQUIREMENTS

EOG respectfully requests an exception to the following NMOCD rule:

- 19.15.16.10 Casing AND TUBING REQUIREMENTS:
J (3): “The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone.”

With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.



905' FNL
1051' FEL
Section 19
T-22-S, R-32-E

Revised Wellbore A:

KB: 3678'
GL: 3653'

API: 30-025-52152

Bit Size: 16"
13-3/8", 54.5#, J-55, STC
@ 0' - 940'

Bit Size: 11"
9-5/8", 40.#, J-55, LTC
@ 0' - 5,140'

Bit Size: 6-3/4"
5-1/2", 17.#, HCP-110, LTC
@ 0' - 20,916'

TOC: 4,410'

Lateral: 20,916' MD, 10,638' TVD
Upper Most Perf:
100' FNL & 1320' FEL Sec. 19
Lower Most Perf:
100' FSL & 1320' FEL Sec. 30
BH Location: 100' FSL & 1320' FEL
Sec. 30
T-22-S R-32-E

KOP: 10,234' MD, 10,160' TVD
EOC: 10,984' MD, 10,638' TVD



Amazing 19 Fed 505H

Revised Permit Information 10/24/2023:

Well Name: Amazing 19 Fed 505H

Location: SHL: 905' FNL & 1051' FEL, Section 19, T-22-S, R-32-E, Lea Co., N.M.

BHL: 100' FSL & 1320' FEL, Section 30, T-22-S, R-32-E, Lea Co., N.M.

Casing Program B:

| Hole Size | Interval MD | | Interval TVD | | Csg OD | Weight | Grade | Conn |
|-----------|-------------|---------|--------------|---------|---------|--------|---------|--------|
| | From (ft) | To (ft) | From (ft) | To (ft) | | | | |
| 13-1/2" | 0 | 940 | 0 | 940 | 10-3/4" | 40.5# | J-55 | STC |
| 9-7/8" | 0 | 5,222 | 0 | 5,140 | 8-5/8" | 32# | J-55 | BTC-SC |
| 6-3/4" | 0 | 20,916 | 0 | 10,638 | 5-1/2" | 17# | HCP-110 | LTC |

Cementing Program:

| Depth | No. Sacks | Wt. ppg | Yld Ft3/sk | Slurry Description |
|-------------------|-----------|---------|------------|--|
| 940' 10-3/4" | 320 | 13.5 | 1.73 | Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl ₂ + 0.25 lb/sk Cello-Flake (TOC @ Surface) |
| | 110 | 14.8 | 1.34 | Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 740') |
| 5,140' 8-5/8" | 410 | 12.7 | 2.22 | Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface) |
| | 650 | 14.8 | 1.32 | Tail: Class C + 10% NaCl + 3% MagOx (TOC @ 4,110') |
| 20,916' 5-1/2" | 520 | 10.5 | 3.21 | Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,410') |
| | 1040 | 13.2 | 1.52 | Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 10240') |



Amazing 19 Fed 505H

Variance is requested to waive the centralizer requirements for the 8-5/8" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

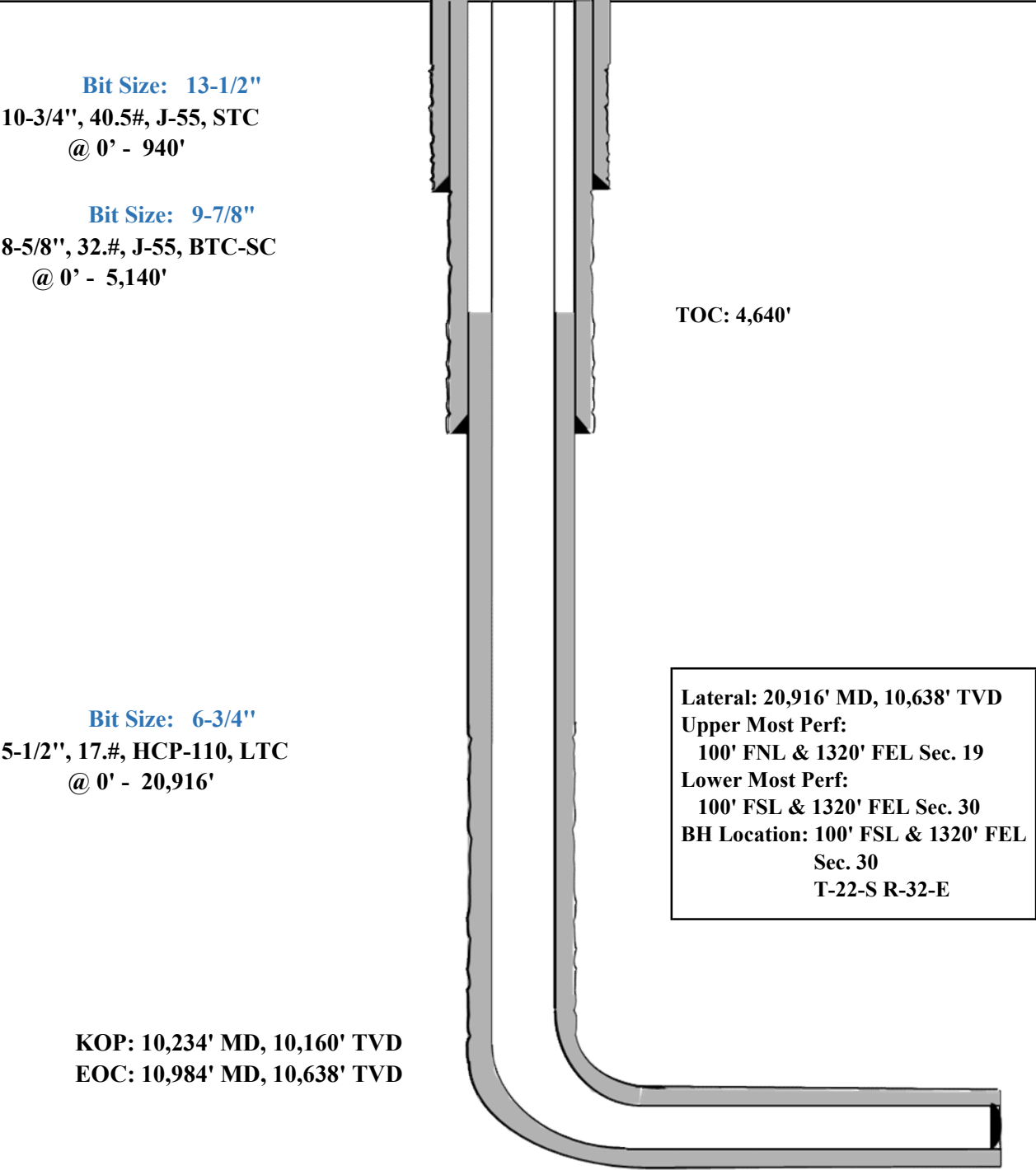


905'
1051'
Section 19
T-22-S, R-32-E

Revised Wellbore B:

API: 30-025-52152

KB: 3678'
GL: 3653'



Bit Size: 13-1/2"
10-3/4", 40.5#, J-55, STC
@ 0' - 940'

Bit Size: 9-7/8"
8-5/8", 32.#, J-55, BTC-SC
@ 0' - 5,140'

Bit Size: 6-3/4"
5-1/2", 17.#, HCP-110, LTC
@ 0' - 20,916'

Lateral: 20,916' MD, 10,638' TVD
Upper Most Perf:
100' FNL & 1320' FEL Sec. 19
Lower Most Perf:
100' FSL & 1320' FEL Sec. 30
BH Location: 100' FSL & 1320' FEL
Sec. 30
T-22-S R-32-E

KOP: 10,234' MD, 10,160' TVD
EOC: 10,984' MD, 10,638' TVD

**GEOLOGIC NAME OF SURFACE FORMATION:**

Permian

ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

| | |
|------------------------|---------|
| Rustler | 831' |
| Tamarisk Anhydrite | 912' |
| Top of Salt | 1,168' |
| Base of Salt | 4,808' |
| Lamar | 5,044' |
| Bell Canyon | 5,071' |
| Cherry Canyon | 6,102' |
| Brushy Canyon | 8,095' |
| Bone Spring Lime | 9,240' |
| Leonard (Avalon) Shale | 9,313' |
| 1st Bone Spring Sand | 10,191' |
| 2nd Bone Spring Shale | 10,355' |
| 2nd Bone Spring Sand | 10,727' |
| 3rd Bone Spring Carb | 11,164' |
| 3rd Bone Spring Sand | 11,814' |
| Wolfcamp | 12,238' |
| Penn | 14,391' |
| --- | --- |

ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

| | | |
|------------------------|---------|-------------|
| Upper Permian Sands | 0- 400' | Fresh Water |
| Bell Canyon | 5,071' | Oil |
| Cherry Canyon | 6,102' | Oil |
| Brushy Canyon | 8,095' | Oil |
| Leonard (Avalon) Shale | 9,313' | Oil |
| 1st Bone Spring Sand | 10,191' | Oil |
| 2nd Bone Spring Shale | 10,355' | Oil |
| 2nd Bone Spring Sand | 10,727' | Oil |



Midland

Lea County, NM (NAD 83 NME)

Amazing 19 Fed

#505H

OH

Plan: Plan #0.1 RT

Standard Planning Report

31 October, 2023



Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
| Company: | Midland | TVD Reference: | kb=25' @ 3678.0usft |
| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| | | | |
|--------------------|-----------------------------|----------------------|----------------|
| Project | Lea County, NM (NAD 83 NME) | | |
| Map System: | US State Plane 1983 | System Datum: | Mean Sea Level |
| Geo Datum: | North American Datum 1983 | | |
| Map Zone: | New Mexico Eastern Zone | | |

| | | | | | |
|-----------------------|----------|----------------|-----------------|------------|-------------------|
| Site | | Amazing 19 Fed | | | |
| Site Position: | | Northing: | 503,794.00 usft | Latitude: | 32° 23' 0.425 N |
| From: | Map | Easting: | 734,151.00 usft | Longitude: | 103° 42' 31.400 W |
| Position Uncertainty: | 0.0 usft | Slot Radius: | 13-3/16 " | | |

| Well | | #505H | | | | |
|----------------------|-------|----------|---------------------|-----------------|---------------|-------------------|
| Well Position | +N/-S | 0.0 usft | Northing: | 503,200.00 usft | Latitude: | 32° 22' 54.547 N |
| | +E/-W | 0.0 usft | Easting: | 734,149.00 usft | Longitude: | 103° 42' 31.464 W |
| Position Uncertainty | | 0.0 usft | Wellhead Elevation: | usft | Ground Level: | 3,653.0 usft |
| Grid Convergence: | | 0.33 ° | | | | |

| | | | | | |
|------------------|-------------------|--------------------|------------------------|----------------------|----------------------------|
| Wellbore | OH | | | | |
| Magnetics | Model Name | Sample Date | Declination (°) | Dip Angle (°) | Field Strength (nT) |
| | IGRF2020 | 10/31/2023 | 6.34 | 59.94 | 47,323.91015975 |

| | | | | | |
|--------------------------|--------------------------------|---------------------|---------------------|----------------------|-----|
| Design | Plan #0.1 RT | | | | |
| Audit Notes: | | | | | |
| Version: | | Phase: | PLAN | Tie On Depth: | 0.0 |
| Vertical Section: | Depth From (TVD) (usft) | +N/-S (usft) | +E/-W (usft) | Direction (°) | |
| | 0.0 | 0.0 | 0.0 | 181.23 | |

| | | | | | |
|---------------------------------|------------------------|--------------------------|-------------------|----------------|--|
| Plan Survey Tool Program | Date | 10/31/2023 | | | |
| Depth From (usft) | Depth To (usft) | Survey (Wellbore) | Tool Name | Remarks | |
| 1 | 0.0 | 20,915.7 | Plan #0.1 RT (OH) | EOG MWD+IFR1 | |
| | | | MWD + IFR1 | | |



Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
| Company: | Midland | TVD Reference: | kb=25' @ 3678.0usft |
| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| Plan Sections | | | | | | | | | | |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|------------------------|-----------------------|---------|--------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) | TFO (°) | Target |
| 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 1,356.0 | 0.00 | 0.00 | 1,356.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 1,839.4 | 9.67 | 342.11 | 1,837.1 | 38.7 | -12.5 | 2.00 | 2.00 | 0.00 | 342.11 | |
| 6,686.0 | 9.67 | 342.11 | 6,614.9 | 813.3 | -262.5 | 0.00 | 0.00 | 0.00 | 0.00 | |
| 7,169.4 | 0.00 | 0.00 | 7,096.0 | 852.0 | -275.0 | 2.00 | -2.00 | 0.00 | 180.00 | |
| 10,233.9 | 0.00 | 0.00 | 10,160.5 | 852.0 | -275.0 | 0.00 | 0.00 | 0.00 | 0.00 | KOP(Amazing 19 Fed |
| 10,454.4 | 26.46 | 180.00 | 10,373.2 | 802.0 | -275.0 | 12.00 | 12.00 | 81.65 | 180.00 | FTP(Amazing 19 Fed |
| 10,983.9 | 90.00 | 179.61 | 10,637.9 | 374.5 | -273.0 | 12.00 | 12.00 | -0.07 | -0.44 | |
| 20,915.7 | 90.00 | 179.61 | 10,638.0 | -9,557.0 | -205.0 | 0.00 | 0.00 | 0.00 | 0.00 | PBHL(Amazing 19 Fe |



Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
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| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| Planned Survey | | | | | | | | | |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 100.0 | 0.00 | 0.00 | 100.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 200.0 | 0.00 | 0.00 | 200.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 300.0 | 0.00 | 0.00 | 300.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 400.0 | 0.00 | 0.00 | 400.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 500.0 | 0.00 | 0.00 | 500.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 600.0 | 0.00 | 0.00 | 600.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 700.0 | 0.00 | 0.00 | 700.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 800.0 | 0.00 | 0.00 | 800.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 900.0 | 0.00 | 0.00 | 900.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,000.0 | 0.00 | 0.00 | 1,000.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,100.0 | 0.00 | 0.00 | 1,100.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,200.0 | 0.00 | 0.00 | 1,200.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,300.0 | 0.00 | 0.00 | 1,300.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,356.0 | 0.00 | 0.00 | 1,356.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 1,400.0 | 0.88 | 342.11 | 1,400.0 | 0.3 | -0.1 | -0.3 | 2.00 | 2.00 | 0.00 |
| 1,500.0 | 2.88 | 342.11 | 1,499.9 | 3.4 | -1.1 | -3.4 | 2.00 | 2.00 | 0.00 |
| 1,600.0 | 4.88 | 342.11 | 1,599.7 | 9.9 | -3.2 | -9.8 | 2.00 | 2.00 | 0.00 |
| 1,700.0 | 6.88 | 342.11 | 1,699.2 | 19.6 | -6.3 | -19.5 | 2.00 | 2.00 | 0.00 |
| 1,800.0 | 8.88 | 342.11 | 1,798.2 | 32.7 | -10.5 | -32.4 | 2.00 | 2.00 | 0.00 |
| 1,839.4 | 9.67 | 342.11 | 1,837.1 | 38.7 | -12.5 | -38.4 | 2.00 | 2.00 | 0.00 |
| 1,900.0 | 9.67 | 342.11 | 1,896.8 | 48.4 | -15.6 | -48.1 | 0.00 | 0.00 | 0.00 |
| 2,000.0 | 9.67 | 342.11 | 1,995.4 | 64.4 | -20.8 | -63.9 | 0.00 | 0.00 | 0.00 |
| 2,100.0 | 9.67 | 342.11 | 2,094.0 | 80.4 | -25.9 | -79.8 | 0.00 | 0.00 | 0.00 |
| 2,200.0 | 9.67 | 342.11 | 2,192.6 | 96.3 | -31.1 | -95.7 | 0.00 | 0.00 | 0.00 |
| 2,300.0 | 9.67 | 342.11 | 2,291.2 | 112.3 | -36.3 | -111.5 | 0.00 | 0.00 | 0.00 |
| 2,400.0 | 9.67 | 342.11 | 2,389.7 | 128.3 | -41.4 | -127.4 | 0.00 | 0.00 | 0.00 |
| 2,500.0 | 9.67 | 342.11 | 2,488.3 | 144.3 | -46.6 | -143.3 | 0.00 | 0.00 | 0.00 |
| 2,600.0 | 9.67 | 342.11 | 2,586.9 | 160.3 | -51.7 | -159.1 | 0.00 | 0.00 | 0.00 |
| 2,700.0 | 9.67 | 342.11 | 2,685.5 | 176.3 | -56.9 | -175.0 | 0.00 | 0.00 | 0.00 |
| 2,800.0 | 9.67 | 342.11 | 2,784.1 | 192.2 | -62.0 | -190.9 | 0.00 | 0.00 | 0.00 |
| 2,900.0 | 9.67 | 342.11 | 2,882.6 | 208.2 | -67.2 | -206.7 | 0.00 | 0.00 | 0.00 |
| 3,000.0 | 9.67 | 342.11 | 2,981.2 | 224.2 | -72.4 | -222.6 | 0.00 | 0.00 | 0.00 |
| 3,100.0 | 9.67 | 342.11 | 3,079.8 | 240.2 | -77.5 | -238.5 | 0.00 | 0.00 | 0.00 |
| 3,200.0 | 9.67 | 342.11 | 3,178.4 | 256.2 | -82.7 | -254.3 | 0.00 | 0.00 | 0.00 |
| 3,300.0 | 9.67 | 342.11 | 3,277.0 | 272.1 | -87.8 | -270.2 | 0.00 | 0.00 | 0.00 |
| 3,400.0 | 9.67 | 342.11 | 3,375.5 | 288.1 | -93.0 | -286.1 | 0.00 | 0.00 | 0.00 |
| 3,500.0 | 9.67 | 342.11 | 3,474.1 | 304.1 | -98.2 | -301.9 | 0.00 | 0.00 | 0.00 |
| 3,600.0 | 9.67 | 342.11 | 3,572.7 | 320.1 | -103.3 | -317.8 | 0.00 | 0.00 | 0.00 |
| 3,700.0 | 9.67 | 342.11 | 3,671.3 | 336.1 | -108.5 | -333.7 | 0.00 | 0.00 | 0.00 |
| 3,800.0 | 9.67 | 342.11 | 3,769.9 | 352.1 | -113.6 | -349.5 | 0.00 | 0.00 | 0.00 |
| 3,900.0 | 9.67 | 342.11 | 3,868.4 | 368.0 | -118.8 | -365.4 | 0.00 | 0.00 | 0.00 |
| 4,000.0 | 9.67 | 342.11 | 3,967.0 | 384.0 | -123.9 | -381.3 | 0.00 | 0.00 | 0.00 |
| 4,100.0 | 9.67 | 342.11 | 4,065.6 | 400.0 | -129.1 | -397.1 | 0.00 | 0.00 | 0.00 |
| 4,200.0 | 9.67 | 342.11 | 4,164.2 | 416.0 | -134.3 | -413.0 | 0.00 | 0.00 | 0.00 |
| 4,300.0 | 9.67 | 342.11 | 4,262.8 | 432.0 | -139.4 | -428.9 | 0.00 | 0.00 | 0.00 |
| 4,400.0 | 9.67 | 342.11 | 4,361.3 | 447.9 | -144.6 | -444.7 | 0.00 | 0.00 | 0.00 |
| 4,500.0 | 9.67 | 342.11 | 4,459.9 | 463.9 | -149.7 | -460.6 | 0.00 | 0.00 | 0.00 |
| 4,600.0 | 9.67 | 342.11 | 4,558.5 | 479.9 | -154.9 | -476.5 | 0.00 | 0.00 | 0.00 |
| 4,700.0 | 9.67 | 342.11 | 4,657.1 | 495.9 | -160.1 | -492.3 | 0.00 | 0.00 | 0.00 |
| 4,800.0 | 9.67 | 342.11 | 4,755.7 | 511.9 | -165.2 | -508.2 | 0.00 | 0.00 | 0.00 |
| 4,900.0 | 9.67 | 342.11 | 4,854.2 | 527.8 | -170.4 | -524.1 | 0.00 | 0.00 | 0.00 |
| 5,000.0 | 9.67 | 342.11 | 4,952.8 | 543.8 | -175.5 | -539.9 | 0.00 | 0.00 | 0.00 |
| 5,100.0 | 9.67 | 342.11 | 5,051.4 | 559.8 | -180.7 | -555.8 | 0.00 | 0.00 | 0.00 |



Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
| Company: | Midland | TVD Reference: | kb=25' @ 3678.0usft |
| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| Planned Survey | | | | | | | | | |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 5,200.0 | 9.67 | 342.11 | 5,150.0 | 575.8 | -185.8 | -571.7 | 0.00 | 0.00 | 0.00 |
| 5,300.0 | 9.67 | 342.11 | 5,248.6 | 591.8 | -191.0 | -587.5 | 0.00 | 0.00 | 0.00 |
| 5,400.0 | 9.67 | 342.11 | 5,347.1 | 607.8 | -196.2 | -603.4 | 0.00 | 0.00 | 0.00 |
| 5,500.0 | 9.67 | 342.11 | 5,445.7 | 623.7 | -201.3 | -619.3 | 0.00 | 0.00 | 0.00 |
| 5,600.0 | 9.67 | 342.11 | 5,544.3 | 639.7 | -206.5 | -635.1 | 0.00 | 0.00 | 0.00 |
| 5,700.0 | 9.67 | 342.11 | 5,642.9 | 655.7 | -211.6 | -651.0 | 0.00 | 0.00 | 0.00 |
| 5,800.0 | 9.67 | 342.11 | 5,741.5 | 671.7 | -216.8 | -666.9 | 0.00 | 0.00 | 0.00 |
| 5,900.0 | 9.67 | 342.11 | 5,840.0 | 687.7 | -222.0 | -682.7 | 0.00 | 0.00 | 0.00 |
| 6,000.0 | 9.67 | 342.11 | 5,938.6 | 703.6 | -227.1 | -698.6 | 0.00 | 0.00 | 0.00 |
| 6,100.0 | 9.67 | 342.11 | 6,037.2 | 719.6 | -232.3 | -714.5 | 0.00 | 0.00 | 0.00 |
| 6,200.0 | 9.67 | 342.11 | 6,135.8 | 735.6 | -237.4 | -730.3 | 0.00 | 0.00 | 0.00 |
| 6,300.0 | 9.67 | 342.11 | 6,234.4 | 751.6 | -242.6 | -746.2 | 0.00 | 0.00 | 0.00 |
| 6,400.0 | 9.67 | 342.11 | 6,332.9 | 767.6 | -247.7 | -762.1 | 0.00 | 0.00 | 0.00 |
| 6,500.0 | 9.67 | 342.11 | 6,431.5 | 783.6 | -252.9 | -777.9 | 0.00 | 0.00 | 0.00 |
| 6,600.0 | 9.67 | 342.11 | 6,530.1 | 799.5 | -258.1 | -793.8 | 0.00 | 0.00 | 0.00 |
| 6,686.0 | 9.67 | 342.11 | 6,614.9 | 813.3 | -262.5 | -807.5 | 0.00 | 0.00 | 0.00 |
| 6,700.0 | 9.39 | 342.11 | 6,628.7 | 815.5 | -263.2 | -809.7 | 2.00 | -2.00 | 0.00 |
| 6,800.0 | 7.39 | 342.11 | 6,727.6 | 829.4 | -267.7 | -823.4 | 2.00 | -2.00 | 0.00 |
| 6,900.0 | 5.39 | 342.11 | 6,827.0 | 840.0 | -271.1 | -833.9 | 2.00 | -2.00 | 0.00 |
| 7,000.0 | 3.39 | 342.11 | 6,926.7 | 847.2 | -273.5 | -841.2 | 2.00 | -2.00 | 0.00 |
| 7,100.0 | 1.39 | 342.11 | 7,026.6 | 851.2 | -274.7 | -845.1 | 2.00 | -2.00 | 0.00 |
| 7,169.4 | 0.00 | 0.00 | 7,096.0 | 852.0 | -275.0 | -845.9 | 2.00 | -2.00 | 0.00 |
| 7,200.0 | 0.00 | 0.00 | 7,126.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,300.0 | 0.00 | 0.00 | 7,226.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,400.0 | 0.00 | 0.00 | 7,326.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,500.0 | 0.00 | 0.00 | 7,426.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,600.0 | 0.00 | 0.00 | 7,526.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,700.0 | 0.00 | 0.00 | 7,626.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,800.0 | 0.00 | 0.00 | 7,726.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 7,900.0 | 0.00 | 0.00 | 7,826.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,000.0 | 0.00 | 0.00 | 7,926.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,100.0 | 0.00 | 0.00 | 8,026.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,200.0 | 0.00 | 0.00 | 8,126.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,300.0 | 0.00 | 0.00 | 8,226.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,400.0 | 0.00 | 0.00 | 8,326.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,500.0 | 0.00 | 0.00 | 8,426.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,600.0 | 0.00 | 0.00 | 8,526.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,700.0 | 0.00 | 0.00 | 8,626.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,800.0 | 0.00 | 0.00 | 8,726.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 8,900.0 | 0.00 | 0.00 | 8,826.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,000.0 | 0.00 | 0.00 | 8,926.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,100.0 | 0.00 | 0.00 | 9,026.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,200.0 | 0.00 | 0.00 | 9,126.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,300.0 | 0.00 | 0.00 | 9,226.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,400.0 | 0.00 | 0.00 | 9,326.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,500.0 | 0.00 | 0.00 | 9,426.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,600.0 | 0.00 | 0.00 | 9,526.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,700.0 | 0.00 | 0.00 | 9,626.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,800.0 | 0.00 | 0.00 | 9,726.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 9,900.0 | 0.00 | 0.00 | 9,826.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 10,000.0 | 0.00 | 0.00 | 9,926.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 10,100.0 | 0.00 | 0.00 | 10,026.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 10,200.0 | 0.00 | 0.00 | 10,126.6 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |
| 10,233.9 | 0.00 | 0.00 | 10,160.5 | 852.0 | -275.0 | -845.9 | 0.00 | 0.00 | 0.00 |



Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
| Company: | Midland | TVD Reference: | kb=25' @ 3678.0usft |
| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| Planned Survey | | | | | | | | | |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 10,250.0 | 1.93 | 180.00 | 10,176.6 | 851.7 | -275.0 | -845.6 | 12.00 | 12.00 | 0.00 |
| 10,275.0 | 4.93 | 180.00 | 10,201.5 | 850.2 | -275.0 | -844.1 | 12.00 | 12.00 | 0.00 |
| 10,300.0 | 7.93 | 180.00 | 10,226.4 | 847.4 | -275.0 | -841.3 | 12.00 | 12.00 | 0.00 |
| 10,325.0 | 10.93 | 180.00 | 10,251.0 | 843.3 | -275.0 | -837.2 | 12.00 | 12.00 | 0.00 |
| 10,350.0 | 13.93 | 180.00 | 10,275.4 | 838.0 | -275.0 | -831.9 | 12.00 | 12.00 | 0.00 |
| 10,375.0 | 16.93 | 180.00 | 10,299.5 | 831.3 | -275.0 | -825.2 | 12.00 | 12.00 | 0.00 |
| 10,400.0 | 19.93 | 180.00 | 10,323.3 | 823.4 | -275.0 | -817.3 | 12.00 | 12.00 | 0.00 |
| 10,425.0 | 22.93 | 180.00 | 10,346.5 | 814.3 | -275.0 | -808.2 | 12.00 | 12.00 | 0.00 |
| 10,450.0 | 25.93 | 180.00 | 10,369.3 | 803.9 | -275.0 | -797.8 | 12.00 | 12.00 | 0.00 |
| 10,454.4 | 26.46 | 180.00 | 10,373.2 | 802.0 | -275.0 | -795.9 | 12.00 | 12.00 | 0.00 |
| 10,475.0 | 28.93 | 179.96 | 10,391.5 | 792.4 | -275.0 | -786.3 | 12.00 | 12.00 | -0.19 |
| 10,500.0 | 31.93 | 179.92 | 10,413.0 | 779.7 | -275.0 | -773.7 | 12.00 | 12.00 | -0.16 |
| 10,525.0 | 34.93 | 179.89 | 10,433.9 | 766.0 | -275.0 | -759.9 | 12.00 | 12.00 | -0.13 |
| 10,550.0 | 37.93 | 179.86 | 10,454.0 | 751.1 | -274.9 | -745.1 | 12.00 | 12.00 | -0.12 |
| 10,575.0 | 40.93 | 179.83 | 10,473.3 | 735.3 | -274.9 | -729.2 | 12.00 | 12.00 | -0.10 |
| 10,600.0 | 43.93 | 179.81 | 10,491.8 | 718.4 | -274.8 | -712.3 | 12.00 | 12.00 | -0.09 |
| 10,625.0 | 46.93 | 179.79 | 10,509.3 | 700.6 | -274.8 | -694.5 | 12.00 | 12.00 | -0.08 |
| 10,650.0 | 49.93 | 179.77 | 10,525.9 | 681.9 | -274.7 | -675.8 | 12.00 | 12.00 | -0.07 |
| 10,675.0 | 52.93 | 179.76 | 10,541.5 | 662.3 | -274.6 | -656.3 | 12.00 | 12.00 | -0.07 |
| 10,700.0 | 55.93 | 179.74 | 10,556.0 | 642.0 | -274.5 | -636.0 | 12.00 | 12.00 | -0.06 |
| 10,725.0 | 58.93 | 179.73 | 10,569.5 | 620.9 | -274.4 | -614.9 | 12.00 | 12.00 | -0.06 |
| 10,750.0 | 61.93 | 179.71 | 10,581.8 | 599.2 | -274.3 | -593.2 | 12.00 | 12.00 | -0.05 |
| 10,775.0 | 64.93 | 179.70 | 10,593.0 | 576.8 | -274.2 | -570.8 | 12.00 | 12.00 | -0.05 |
| 10,800.0 | 67.93 | 179.69 | 10,603.0 | 553.9 | -274.1 | -547.9 | 12.00 | 12.00 | -0.05 |
| 10,825.0 | 70.93 | 179.68 | 10,611.7 | 530.5 | -274.0 | -524.5 | 12.00 | 12.00 | -0.05 |
| 10,850.0 | 73.93 | 179.66 | 10,619.3 | 506.7 | -273.8 | -500.7 | 12.00 | 12.00 | -0.04 |
| 10,875.0 | 76.93 | 179.65 | 10,625.6 | 482.5 | -273.7 | -476.5 | 12.00 | 12.00 | -0.04 |
| 10,900.0 | 79.93 | 179.64 | 10,630.6 | 458.0 | -273.5 | -452.0 | 12.00 | 12.00 | -0.04 |
| 10,925.0 | 82.93 | 179.63 | 10,634.3 | 433.3 | -273.4 | -427.3 | 12.00 | 12.00 | -0.04 |
| 10,950.0 | 85.93 | 179.62 | 10,636.7 | 408.4 | -273.2 | -402.5 | 12.00 | 12.00 | -0.04 |
| 10,975.0 | 88.93 | 179.61 | 10,637.9 | 383.4 | -273.0 | -377.5 | 12.00 | 12.00 | -0.04 |
| 10,983.9 | 90.00 | 179.61 | 10,637.9 | 374.5 | -273.0 | -368.6 | 12.00 | 12.00 | -0.04 |
| 11,000.0 | 90.00 | 179.61 | 10,637.9 | 358.4 | -272.9 | -352.5 | 0.00 | 0.00 | 0.00 |
| 11,100.0 | 90.00 | 179.61 | 10,637.9 | 258.4 | -272.2 | -252.5 | 0.00 | 0.00 | 0.00 |
| 11,200.0 | 90.00 | 179.61 | 10,637.9 | 158.4 | -271.5 | -152.6 | 0.00 | 0.00 | 0.00 |
| 11,300.0 | 90.00 | 179.61 | 10,637.9 | 58.4 | -270.8 | -52.6 | 0.00 | 0.00 | 0.00 |
| 11,400.0 | 90.00 | 179.61 | 10,637.9 | -41.6 | -270.1 | 47.3 | 0.00 | 0.00 | 0.00 |
| 11,500.0 | 90.00 | 179.61 | 10,637.9 | -141.6 | -269.4 | 147.3 | 0.00 | 0.00 | 0.00 |
| 11,600.0 | 90.00 | 179.61 | 10,637.9 | -241.6 | -268.8 | 247.3 | 0.00 | 0.00 | 0.00 |
| 11,700.0 | 90.00 | 179.61 | 10,637.9 | -341.5 | -268.1 | 347.2 | 0.00 | 0.00 | 0.00 |
| 11,800.0 | 90.00 | 179.61 | 10,637.9 | -441.5 | -267.4 | 447.2 | 0.00 | 0.00 | 0.00 |
| 11,900.0 | 90.00 | 179.61 | 10,638.0 | -541.5 | -266.7 | 547.1 | 0.00 | 0.00 | 0.00 |
| 12,000.0 | 90.00 | 179.61 | 10,638.0 | -641.5 | -266.0 | 647.1 | 0.00 | 0.00 | 0.00 |
| 12,100.0 | 90.00 | 179.61 | 10,638.0 | -741.5 | -265.3 | 747.1 | 0.00 | 0.00 | 0.00 |
| 12,200.0 | 90.00 | 179.61 | 10,638.0 | -841.5 | -264.7 | 847.0 | 0.00 | 0.00 | 0.00 |
| 12,300.0 | 90.00 | 179.61 | 10,638.0 | -941.5 | -264.0 | 947.0 | 0.00 | 0.00 | 0.00 |
| 12,400.0 | 90.00 | 179.61 | 10,638.0 | -1,041.5 | -263.3 | 1,046.9 | 0.00 | 0.00 | 0.00 |
| 12,500.0 | 90.00 | 179.61 | 10,638.0 | -1,141.5 | -262.6 | 1,146.9 | 0.00 | 0.00 | 0.00 |
| 12,600.0 | 90.00 | 179.61 | 10,638.0 | -1,241.5 | -261.9 | 1,246.9 | 0.00 | 0.00 | 0.00 |
| 12,700.0 | 90.00 | 179.61 | 10,638.0 | -1,341.5 | -261.2 | 1,346.8 | 0.00 | 0.00 | 0.00 |
| 12,800.0 | 90.00 | 179.61 | 10,638.0 | -1,441.5 | -260.5 | 1,446.8 | 0.00 | 0.00 | 0.00 |
| 12,900.0 | 90.00 | 179.61 | 10,638.0 | -1,541.5 | -259.9 | 1,546.7 | 0.00 | 0.00 | 0.00 |
| 13,000.0 | 90.00 | 179.61 | 10,638.0 | -1,641.5 | -259.2 | 1,646.7 | 0.00 | 0.00 | 0.00 |
| 13,100.0 | 90.00 | 179.61 | 10,638.0 | -1,741.5 | -258.5 | 1,746.7 | 0.00 | 0.00 | 0.00 |



Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
| Company: | Midland | TVD Reference: | kb=25' @ 3678.0usft |
| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| Planned Survey | | | | | | | | | |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 13,200.0 | 90.00 | 179.61 | 10,638.0 | -1,841.5 | -257.8 | 1,846.6 | 0.00 | 0.00 | 0.00 |
| 13,300.0 | 90.00 | 179.61 | 10,638.0 | -1,941.5 | -257.1 | 1,946.6 | 0.00 | 0.00 | 0.00 |
| 13,400.0 | 90.00 | 179.61 | 10,638.0 | -2,041.5 | -256.4 | 2,046.5 | 0.00 | 0.00 | 0.00 |
| 13,500.0 | 90.00 | 179.61 | 10,638.0 | -2,141.5 | -255.8 | 2,146.5 | 0.00 | 0.00 | 0.00 |
| 13,600.0 | 90.00 | 179.61 | 10,638.0 | -2,241.5 | -255.1 | 2,246.5 | 0.00 | 0.00 | 0.00 |
| 13,700.0 | 90.00 | 179.61 | 10,638.0 | -2,341.5 | -254.4 | 2,346.4 | 0.00 | 0.00 | 0.00 |
| 13,800.0 | 90.00 | 179.61 | 10,638.0 | -2,441.5 | -253.7 | 2,446.4 | 0.00 | 0.00 | 0.00 |
| 13,900.0 | 90.00 | 179.61 | 10,638.0 | -2,541.5 | -253.0 | 2,546.3 | 0.00 | 0.00 | 0.00 |
| 14,000.0 | 90.00 | 179.61 | 10,638.0 | -2,641.5 | -252.3 | 2,646.3 | 0.00 | 0.00 | 0.00 |
| 14,100.0 | 90.00 | 179.61 | 10,638.0 | -2,741.5 | -251.6 | 2,746.3 | 0.00 | 0.00 | 0.00 |
| 14,200.0 | 90.00 | 179.61 | 10,638.0 | -2,841.5 | -251.0 | 2,846.2 | 0.00 | 0.00 | 0.00 |
| 14,300.0 | 90.00 | 179.61 | 10,638.0 | -2,941.5 | -250.3 | 2,946.2 | 0.00 | 0.00 | 0.00 |
| 14,400.0 | 90.00 | 179.61 | 10,638.0 | -3,041.5 | -249.6 | 3,046.1 | 0.00 | 0.00 | 0.00 |
| 14,500.0 | 90.00 | 179.61 | 10,638.0 | -3,141.5 | -248.9 | 3,146.1 | 0.00 | 0.00 | 0.00 |
| 14,600.0 | 90.00 | 179.61 | 10,638.0 | -3,241.5 | -248.2 | 3,246.1 | 0.00 | 0.00 | 0.00 |
| 14,700.0 | 90.00 | 179.61 | 10,638.0 | -3,341.5 | -247.5 | 3,346.0 | 0.00 | 0.00 | 0.00 |
| 14,800.0 | 90.00 | 179.61 | 10,638.0 | -3,441.5 | -246.9 | 3,446.0 | 0.00 | 0.00 | 0.00 |
| 14,900.0 | 90.00 | 179.61 | 10,638.0 | -3,541.5 | -246.2 | 3,545.9 | 0.00 | 0.00 | 0.00 |
| 15,000.0 | 90.00 | 179.61 | 10,638.0 | -3,641.5 | -245.5 | 3,645.9 | 0.00 | 0.00 | 0.00 |
| 15,100.0 | 90.00 | 179.61 | 10,638.0 | -3,741.5 | -244.8 | 3,745.9 | 0.00 | 0.00 | 0.00 |
| 15,200.0 | 90.00 | 179.61 | 10,638.0 | -3,841.5 | -244.1 | 3,845.8 | 0.00 | 0.00 | 0.00 |
| 15,300.0 | 90.00 | 179.61 | 10,638.0 | -3,941.5 | -243.4 | 3,945.8 | 0.00 | 0.00 | 0.00 |
| 15,400.0 | 90.00 | 179.61 | 10,638.0 | -4,041.5 | -242.8 | 4,045.7 | 0.00 | 0.00 | 0.00 |
| 15,500.0 | 90.00 | 179.61 | 10,638.0 | -4,141.5 | -242.1 | 4,145.7 | 0.00 | 0.00 | 0.00 |
| 15,600.0 | 90.00 | 179.61 | 10,638.0 | -4,241.5 | -241.4 | 4,245.7 | 0.00 | 0.00 | 0.00 |
| 15,700.0 | 90.00 | 179.61 | 10,638.0 | -4,341.5 | -240.7 | 4,345.6 | 0.00 | 0.00 | 0.00 |
| 15,800.0 | 90.00 | 179.61 | 10,638.0 | -4,441.5 | -240.0 | 4,445.6 | 0.00 | 0.00 | 0.00 |
| 15,900.0 | 90.00 | 179.61 | 10,638.0 | -4,541.5 | -239.3 | 4,545.5 | 0.00 | 0.00 | 0.00 |
| 16,000.0 | 90.00 | 179.61 | 10,638.0 | -4,641.4 | -238.6 | 4,645.5 | 0.00 | 0.00 | 0.00 |
| 16,100.0 | 90.00 | 179.61 | 10,638.0 | -4,741.4 | -238.0 | 4,745.5 | 0.00 | 0.00 | 0.00 |
| 16,200.0 | 90.00 | 179.61 | 10,638.0 | -4,841.4 | -237.3 | 4,845.4 | 0.00 | 0.00 | 0.00 |
| 16,300.0 | 90.00 | 179.61 | 10,638.0 | -4,941.4 | -236.6 | 4,945.4 | 0.00 | 0.00 | 0.00 |
| 16,400.0 | 90.00 | 179.61 | 10,638.0 | -5,041.4 | -235.9 | 5,045.3 | 0.00 | 0.00 | 0.00 |
| 16,500.0 | 90.00 | 179.61 | 10,638.0 | -5,141.4 | -235.2 | 5,145.3 | 0.00 | 0.00 | 0.00 |
| 16,600.0 | 90.00 | 179.61 | 10,638.0 | -5,241.4 | -234.5 | 5,245.3 | 0.00 | 0.00 | 0.00 |
| 16,700.0 | 90.00 | 179.61 | 10,638.0 | -5,341.4 | -233.9 | 5,345.2 | 0.00 | 0.00 | 0.00 |
| 16,800.0 | 90.00 | 179.61 | 10,638.0 | -5,441.4 | -233.2 | 5,445.2 | 0.00 | 0.00 | 0.00 |
| 16,900.0 | 90.00 | 179.61 | 10,638.0 | -5,541.4 | -232.5 | 5,545.1 | 0.00 | 0.00 | 0.00 |
| 17,000.0 | 90.00 | 179.61 | 10,638.0 | -5,641.4 | -231.8 | 5,645.1 | 0.00 | 0.00 | 0.00 |
| 17,100.0 | 90.00 | 179.61 | 10,638.0 | -5,741.4 | -231.1 | 5,745.1 | 0.00 | 0.00 | 0.00 |
| 17,200.0 | 90.00 | 179.61 | 10,638.0 | -5,841.4 | -230.4 | 5,845.0 | 0.00 | 0.00 | 0.00 |
| 17,300.0 | 90.00 | 179.61 | 10,638.0 | -5,941.4 | -229.7 | 5,945.0 | 0.00 | 0.00 | 0.00 |
| 17,400.0 | 90.00 | 179.61 | 10,638.0 | -6,041.4 | -229.1 | 6,044.9 | 0.00 | 0.00 | 0.00 |
| 17,500.0 | 90.00 | 179.61 | 10,638.0 | -6,141.4 | -228.4 | 6,144.9 | 0.00 | 0.00 | 0.00 |
| 17,600.0 | 90.00 | 179.61 | 10,638.0 | -6,241.4 | -227.7 | 6,244.9 | 0.00 | 0.00 | 0.00 |
| 17,700.0 | 90.00 | 179.61 | 10,638.0 | -6,341.4 | -227.0 | 6,344.8 | 0.00 | 0.00 | 0.00 |
| 17,800.0 | 90.00 | 179.61 | 10,638.0 | -6,441.4 | -226.3 | 6,444.8 | 0.00 | 0.00 | 0.00 |
| 17,900.0 | 90.00 | 179.61 | 10,638.0 | -6,541.4 | -225.6 | 6,544.7 | 0.00 | 0.00 | 0.00 |
| 18,000.0 | 90.00 | 179.61 | 10,638.0 | -6,641.4 | -225.0 | 6,644.7 | 0.00 | 0.00 | 0.00 |
| 18,100.0 | 90.00 | 179.61 | 10,638.0 | -6,741.4 | -224.3 | 6,744.7 | 0.00 | 0.00 | 0.00 |
| 18,200.0 | 90.00 | 179.61 | 10,638.0 | -6,841.4 | -223.6 | 6,844.6 | 0.00 | 0.00 | 0.00 |
| 18,300.0 | 90.00 | 179.61 | 10,638.0 | -6,941.4 | -222.9 | 6,944.6 | 0.00 | 0.00 | 0.00 |
| 18,400.0 | 90.00 | 179.61 | 10,638.0 | -7,041.4 | -222.2 | 7,044.5 | 0.00 | 0.00 | 0.00 |
| 18,500.0 | 90.00 | 179.61 | 10,638.0 | -7,141.4 | -221.5 | 7,144.5 | 0.00 | 0.00 | 0.00 |

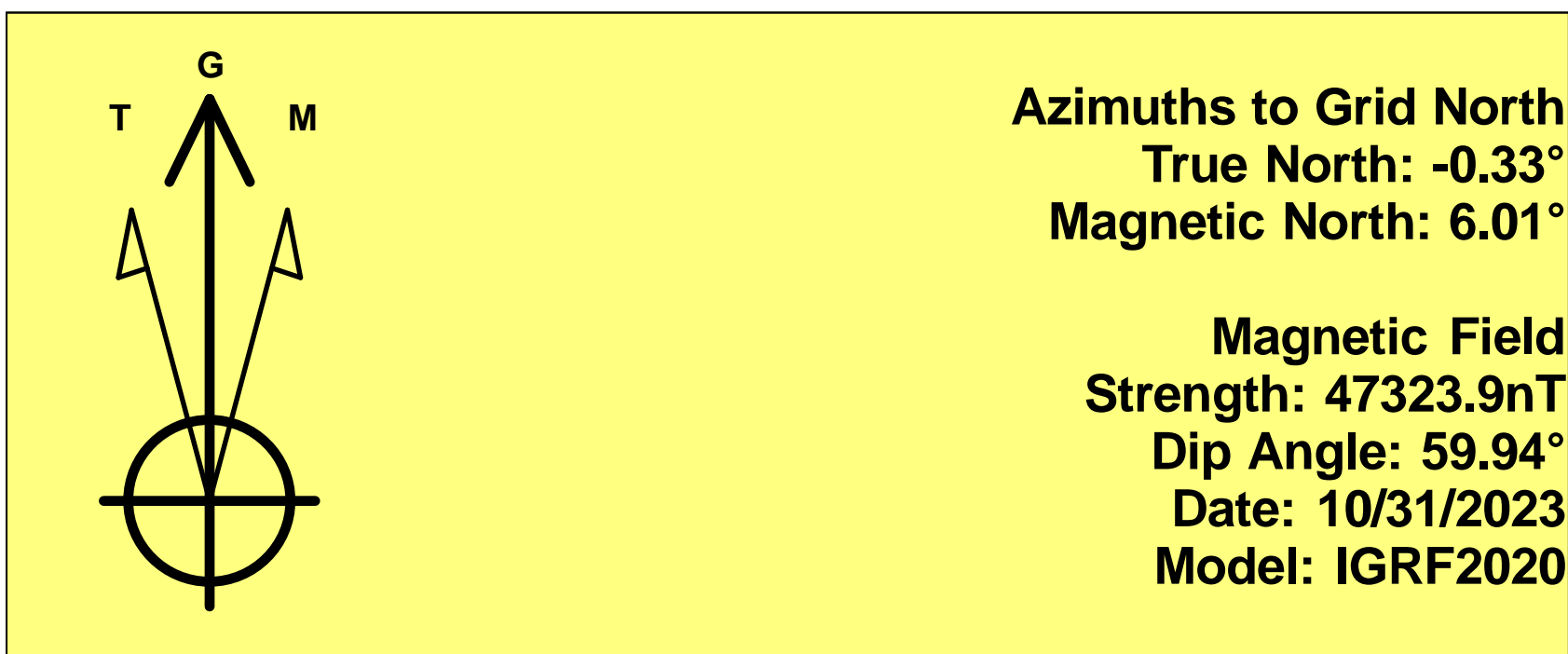
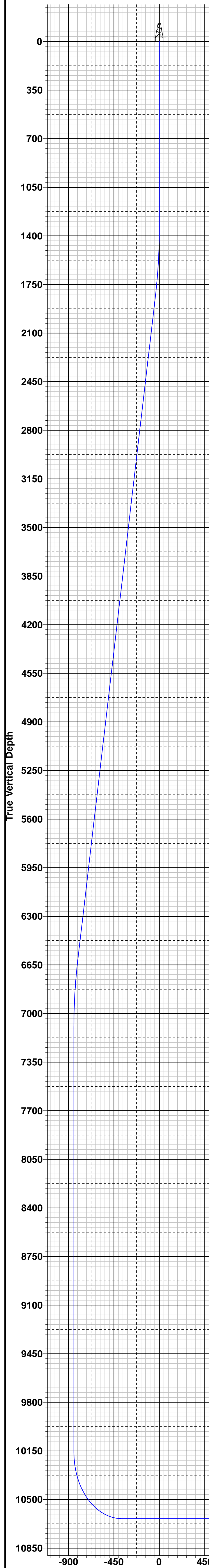


Planning Report

| | | | |
|------------------|-----------------------------|-------------------------------------|---------------------|
| Database: | PEDM | Local Co-ordinate Reference: | Well #505H |
| Company: | Midland | TVD Reference: | kb=25' @ 3678.0usft |
| Project: | Lea County, NM (NAD 83 NME) | MD Reference: | kb=25' @ 3678.0usft |
| Site: | Amazing 19 Fed | North Reference: | Grid |
| Well: | #505H | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | OH | | |
| Design: | Plan #0.1 RT | | |

| Planned Survey | | | | | | | | | | |
|-----------------------|-----------------|-------------|-----------------------|--------------|--------------|-------------------------|-------------------------|------------------------|-----------------------|--|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) | |
| 18,600.0 | 90.00 | 179.61 | 10,638.0 | -7,241.4 | -220.8 | 7,244.5 | 0.00 | 0.00 | 0.00 | |
| 18,700.0 | 90.00 | 179.61 | 10,638.0 | -7,341.4 | -220.2 | 7,344.4 | 0.00 | 0.00 | 0.00 | |
| 18,800.0 | 90.00 | 179.61 | 10,638.0 | -7,441.4 | -219.5 | 7,444.4 | 0.00 | 0.00 | 0.00 | |
| 18,900.0 | 90.00 | 179.61 | 10,638.0 | -7,541.4 | -218.8 | 7,544.3 | 0.00 | 0.00 | 0.00 | |
| 19,000.0 | 90.00 | 179.61 | 10,638.0 | -7,641.4 | -218.1 | 7,644.3 | 0.00 | 0.00 | 0.00 | |
| 19,100.0 | 90.00 | 179.61 | 10,638.0 | -7,741.4 | -217.4 | 7,744.3 | 0.00 | 0.00 | 0.00 | |
| 19,200.0 | 90.00 | 179.61 | 10,638.0 | -7,841.4 | -216.7 | 7,844.2 | 0.00 | 0.00 | 0.00 | |
| 19,300.0 | 90.00 | 179.61 | 10,638.0 | -7,941.4 | -216.1 | 7,944.2 | 0.00 | 0.00 | 0.00 | |
| 19,400.0 | 90.00 | 179.61 | 10,638.0 | -8,041.4 | -215.4 | 8,044.1 | 0.00 | 0.00 | 0.00 | |
| 19,500.0 | 90.00 | 179.61 | 10,638.0 | -8,141.4 | -214.7 | 8,144.1 | 0.00 | 0.00 | 0.00 | |
| 19,600.0 | 90.00 | 179.61 | 10,638.0 | -8,241.4 | -214.0 | 8,244.1 | 0.00 | 0.00 | 0.00 | |
| 19,700.0 | 90.00 | 179.61 | 10,638.0 | -8,341.4 | -213.3 | 8,344.0 | 0.00 | 0.00 | 0.00 | |
| 19,800.0 | 90.00 | 179.61 | 10,638.0 | -8,441.4 | -212.6 | 8,444.0 | 0.00 | 0.00 | 0.00 | |
| 19,900.0 | 90.00 | 179.61 | 10,638.0 | -8,541.4 | -212.0 | 8,543.9 | 0.00 | 0.00 | 0.00 | |
| 20,000.0 | 90.00 | 179.61 | 10,638.0 | -8,641.4 | -211.3 | 8,643.9 | 0.00 | 0.00 | 0.00 | |
| 20,100.0 | 90.00 | 179.61 | 10,638.0 | -8,741.4 | -210.6 | 8,743.9 | 0.00 | 0.00 | 0.00 | |
| 20,200.0 | 90.00 | 179.61 | 10,638.0 | -8,841.3 | -209.9 | 8,843.8 | 0.00 | 0.00 | 0.00 | |
| 20,300.0 | 90.00 | 179.61 | 10,638.0 | -8,941.3 | -209.2 | 8,943.8 | 0.00 | 0.00 | 0.00 | |
| 20,400.0 | 90.00 | 179.61 | 10,638.0 | -9,041.3 | -208.5 | 9,043.7 | 0.00 | 0.00 | 0.00 | |
| 20,500.0 | 90.00 | 179.61 | 10,638.0 | -9,141.3 | -207.8 | 9,143.7 | 0.00 | 0.00 | 0.00 | |
| 20,600.0 | 90.00 | 179.61 | 10,638.0 | -9,241.3 | -207.2 | 9,243.7 | 0.00 | 0.00 | 0.00 | |
| 20,700.0 | 90.00 | 179.61 | 10,638.0 | -9,341.3 | -206.5 | 9,343.6 | 0.00 | 0.00 | 0.00 | |
| 20,800.0 | 90.00 | 179.61 | 10,638.0 | -9,441.3 | -205.8 | 9,443.6 | 0.00 | 0.00 | 0.00 | |
| 20,900.0 | 90.00 | 179.61 | 10,638.0 | -9,541.3 | -205.1 | 9,543.5 | 0.00 | 0.00 | 0.00 | |
| 20,915.7 | 90.00 | 179.61 | 10,638.0 | -9,557.0 | -205.0 | 9,559.2 | 0.00 | 0.00 | 0.00 | |

| Design Targets | | | | | | | | | | |
|---|---------------|--------------|------------|--------------|--------------|-----------------|----------------|------------------|-------------------|--|
| Target Name - hit/miss target - Shape | Dip Angle (°) | Dip Dir. (°) | TVD (usft) | +N/-S (usft) | +E/-W (usft) | Northing (usft) | Easting (usft) | Latitude | Longitude | |
| KOP(Amazing 19 Fed #4 - plan hits target center - Point | 0.00 | 0.00 | 10,160.5 | 852.0 | -275.0 | 504,052.00 | 733,874.00 | 32° 23' 2.994 N | 103° 42' 34.613 W | |
| FTP(Amazing 19 Fed #5 - plan hits target center - Point | 0.00 | 0.00 | 10,373.2 | 802.0 | -275.0 | 504,002.00 | 733,874.00 | 32° 23' 2.499 N | 103° 42' 34.616 W | |
| PBHL(Amazing 19 Fed # - plan hits target center - Point | 0.00 | 0.01 | 10,638.0 | -9,557.0 | -205.0 | 493,643.00 | 733,944.00 | 32° 21' 19.990 N | 103° 42' 34.504 W | |



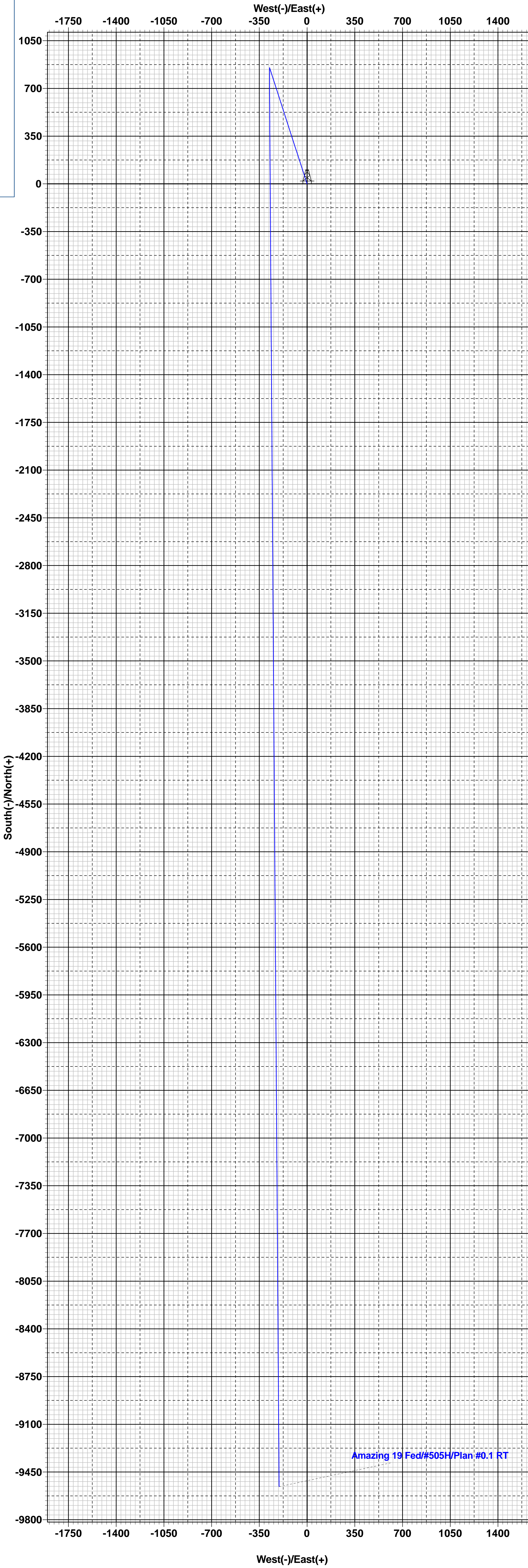
To convert a Magnetic Direction to a Grid Direction, Add 6.01°
To convert a Magnetic Direction to a True Direction, Add 6.34° East
To convert a True Direction to a Grid Direction, Subtract 0.33°

| WELL DETAILS: #505H | | | | |
|----------------------------|-----------|------------------|-------------------|--|
| kb=25' @ 3678.0usft 3653.0 | | | | |
| Northing | Easting | Latitude | Longitude | |
| 503200.00 | 734149.00 | 32° 22' 54.547 N | 103° 42' 31.464 W | |

| SECTION DETAILS | | | | | | | | | | |
|-----------------|---------|-------|--------|---------|---------|--------|-------|--------|--------|----------------------------|
| Sec | MD | Inc | Azi | TVD | +N/-S | +E/-W | Dleg | TFace | VSect | Target |
| 1 | 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.0 | |
| 2 | 1356.0 | 0.00 | 0.00 | 1356.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.0 | |
| 3 | 1839.4 | 9.67 | 342.11 | 1837.1 | 38.7 | -12.5 | 2.00 | 342.11 | -38.4 | |
| 4 | 6686.0 | 9.67 | 342.11 | 6614.9 | 813.3 | -262.5 | 0.00 | 0.00 | -807.5 | |
| 5 | 7169.4 | 0.00 | 0.00 | 7096.0 | 852.0 | -275.0 | 2.00 | 180.00 | -845.9 | |
| 6 | 10233.9 | 0.00 | 0.00 | 10160.5 | 852.0 | -275.0 | 0.00 | 0.00 | -845.9 | KOP(Amazing 19 Fed #505H) |
| 7 | 10454.4 | 26.46 | 180.00 | 10373.2 | 802.0 | -275.0 | 12.00 | 180.00 | -795.9 | FTP(Amazing 19 Fed #505H) |
| 8 | 10983.9 | 90.00 | 179.61 | 10637.9 | 374.5 | -273.0 | 12.00 | -0.44 | -368.6 | |
| 9 | 20915.7 | 90.00 | 179.61 | 10638.0 | -9557.0 | -205.0 | 0.00 | 0.00 | 9559.2 | PBHL(Amazing 19 Fed #505H) |

| CASING DETAILS |
|-----------------------------|
| No casing data is available |

| WELLBORE TARGET DETAILS (MAP CO-ORDINATES) | | | | | |
|--|---------|---------|--------|-----------|-----------|
| Name | TVD | +N/-S | +E/-W | Northing | Easting |
| KOP(Amazing 19 Fed #505H) | 10160.5 | 852.0 | -275.0 | 504052.00 | 733874.00 |
| FTP(Amazing 19 Fed #505H) | 10373.2 | 802.0 | -275.0 | 504002.00 | 733874.00 |
| PBHL(Amazing 19 Fed #505H) | 10638.0 | -9557.0 | -205.0 | 493643.00 | 733944.00 |



Vertical Section at 181.23°

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

| | |
|-----------------------|----------------------------|
| OPERATOR'S NAME: | EOG RESOURCES INCORPORATED |
| WELL NAME & NO.: | AMAZING 19 FED 505H |
| SURFACE HOLE FOOTAGE: | 905'/N 1051'/E |
| BOTTOM HOLE FOOTAGE: | 100'/S 1320'/E |
| LOCATION: | SECTION 19, T22S, R32E |
| COUNTY: | Lea County, New Mexico |

All previous COAs still apply

COA

| | | | |
|----------------------------------|--|--|---|
| H2S | <input checked="" type="radio"/> Yes | <input type="radio"/> No | |
| Potash | <input checked="" type="radio"/> None | <input type="radio"/> Secretary | <input type="radio"/> R-111-P |
| Cave/Karst Potential | <input checked="" type="radio"/> Low | <input type="radio"/> Medium | <input type="radio"/> High |
| Cave/Karst Potential | <input type="radio"/> Critical | | |
| Variance | <input type="radio"/> None | <input checked="" type="radio"/> Flex Hose | <input type="radio"/> Other |
| Wellhead | <input type="radio"/> Conventional | <input checked="" type="radio"/> Multibowl | <input type="radio"/> Both |
| Wellhead Variance | <input type="radio"/> Diverter | | |
| Other | <input type="checkbox"/> 4 String | <input type="checkbox"/> Capitan Reef | <input type="checkbox"/> WIPP |
| Other | <input checked="" type="checkbox"/> Fluid Filled | <input type="checkbox"/> Pilot Hole | <input type="checkbox"/> Open Annulus |
| Cementing | <input type="checkbox"/> Contingency Cement Squeeze | <input type="checkbox"/> EchoMeter | <input type="checkbox"/> Primary Cement Squeeze |
| Special Requirements | <input type="checkbox"/> Water Disposal | <input type="checkbox"/> COM | <input type="checkbox"/> Unit |
| Special Requirements | <input type="checkbox"/> Batch Sundry | | |
| Special Requirements Variance | <input checked="" type="checkbox"/> Break Testing | <input checked="" type="checkbox"/> Offline Cementing | <input checked="" type="checkbox"/> Casing Clearance |

A. CASING

NOTE: INTERMEDIATE CASING SET POINTS ADJUSTED BASED ON BLM GEOLOGY RECOMMENDATION AND ORIGINAL APD SET DEPTH

Primary Casing Design:

1. The **13-3/8** inch surface casing shall be set at approximately **940** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature

survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement in Design A.

2. The **9-5/8** inch intermediate casing shall be set at approximately **4,452** feet TVD. **Cement excess < 25% CFO recommendation. Please review cement volumes to achieve below mentioned tie-back.** The minimum required fill of cement behind the **9-5/8** inch intermediate casing is:

Option 1 (Single Stage):

- Cement to surface. If cement does not circulate see B.1.a, c-d above.
3. The **5-1/2** inch production casing shall be set at approximately **20,916** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

Option 1 (Single Stage):

- Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Alternate Casing Design:

1. The **10-3/4** inch surface casing shall be set at approximately **940** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
 - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - f. Wait on cement (WOC) time for a primary cement job will be a minimum of **8**

- hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - h. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement in Design B.

2. The **8-5/8** inch intermediate casing shall be set at approximately **4,452** feet TVD. The minimum required fill of cement behind the **8-5/8** inch intermediate casing is:

Option 1 (Single Stage):

- Cement to surface. If cement does not circulate see B.1.a, c-d above.
3. The **5-1/2** inch production casing shall be set at approximately **20,916** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

Option 1 (Single Stage):

- a. Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

B. SPECIAL REQUIREMENT (S)

**(Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system)
BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (**Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP**)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (**575-706-2779**) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.

- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR part 3170 Subpart 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

Offline Cementing

OK for surface and intermediate intervals. Notify the BLM prior to the commencement of any offline cementing procedure.

Casing Clearance:

- Salt annular clearance variance in place
- Overlap clearance OK in the production interval

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

☒ Eddy County

EMAIL or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

BLM_NM_CFO_DrillingNotifications@BLM.GOV

(575) 361-2822

☒ Lea County

Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240,

(575) 689-5981

1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.

- Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in **43 CFR part 3170 Subpart 3172** and **API STD 53 Sec. 5.3**.
2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.

- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in **43 CFR part 3170 Subpart 3172** must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
 - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR part 3170 Subpart 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
 - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall

have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.

- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR part 3170 Subpart 3172**.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

KPI 11/21/2023



Salt Section Annular Clearance Variance Request

Daniel Moose

Current Design (Salt Strings)

0.422" Annular clearance requirement

- Casing collars shall have a minimum clearance of 0.422 inches on all sides in the hole/casing annulus, with recognition that variances can be granted for justified exceptions.

- 12.25" Hole x 9.625" 40# J55/HCK55 LTC Casing
 - 1.3125" Clearance to casing OD
 - 0.8125" Clearance to coupling OD
- 9.875" Hole x 8.75" 38.5# P110 Sprint-SF Casing
 - 0.5625" Clearance to casing OD
 - 0.433" Clearance to coupling OD

Annular Clearance Variance Request

EOG request permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues

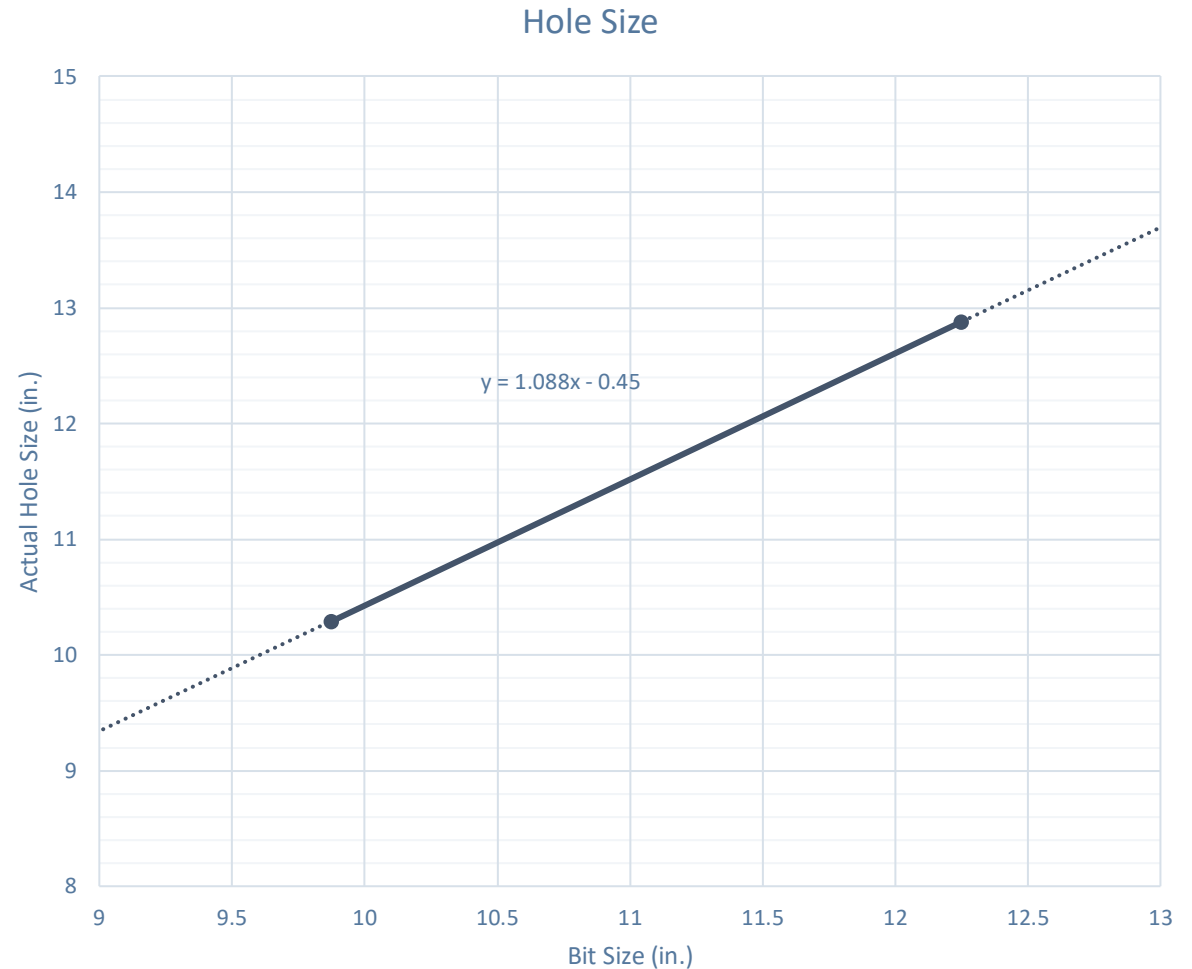
Volumetric Hole Size Calculation

Hole Size Calculations Off Cement Volumes

- Known volume of cement pumped
- Known volume of cement returned to surface
- Must not have had any losses
- Must have bumped plug

Average Hole Size

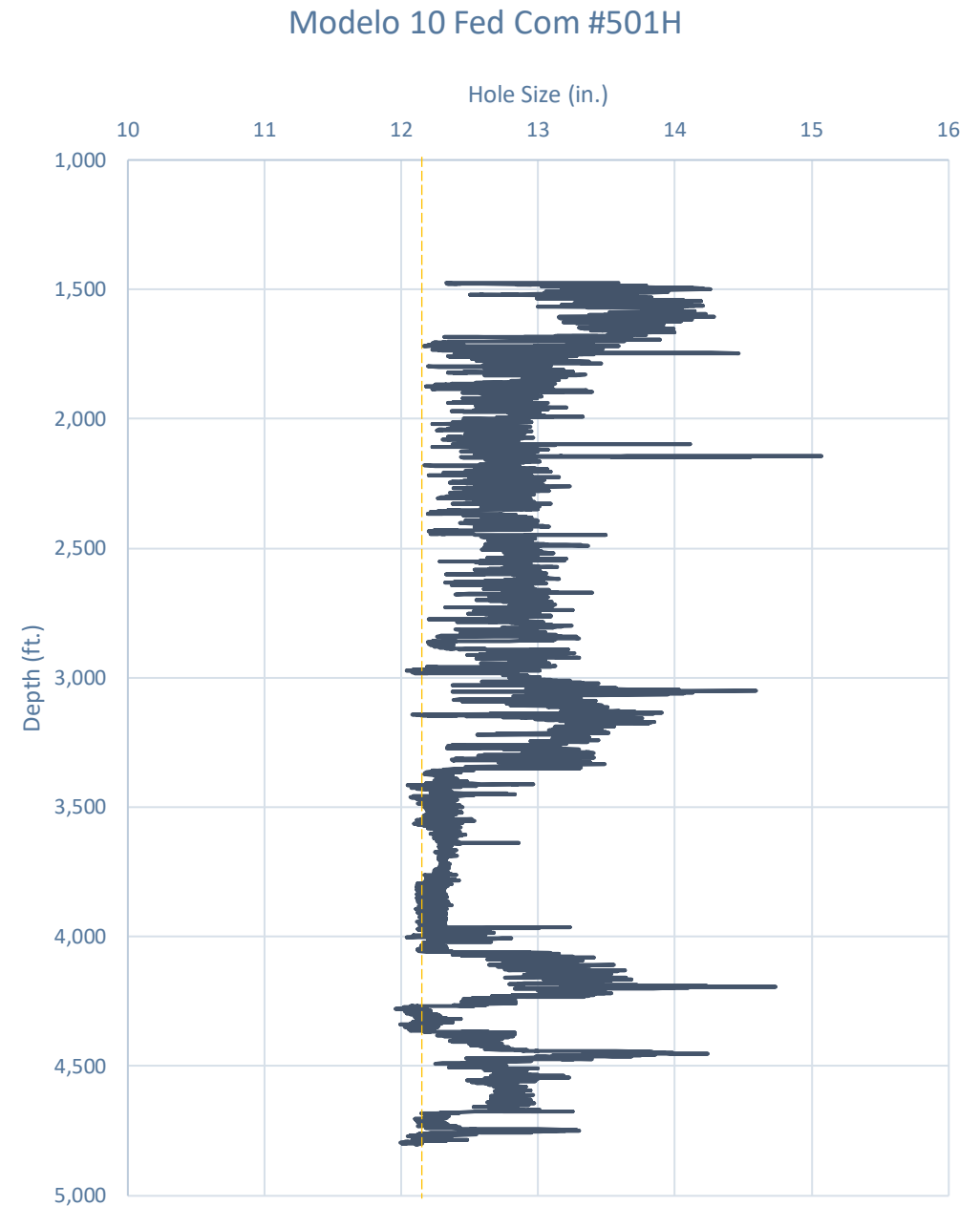
- 12.25" Hole
 - 12.88" Hole
 - 5.13% diameter increase
 - 10.52% area increase
 - 0.63" Average enlargement
 - 0.58" Median enlargement
 - 179 Well Count
- 9.875" Hole
 - 10.30" Hole
 - 4.24% diameter increase
 - 9.64% area increase
 - 0.42" Average enlargement
 - 0.46" Median enlargement
 - 11 Well Count



Caliper Hole Size (12.25")

Average Hole Size

- 12.25" Bit
 - 12.76" Hole
 - 4.14% diameter increase
 - 8.44% area increase
 - 0.51" Average enlargement
 - 0.52" Median enlargement
 - Brine

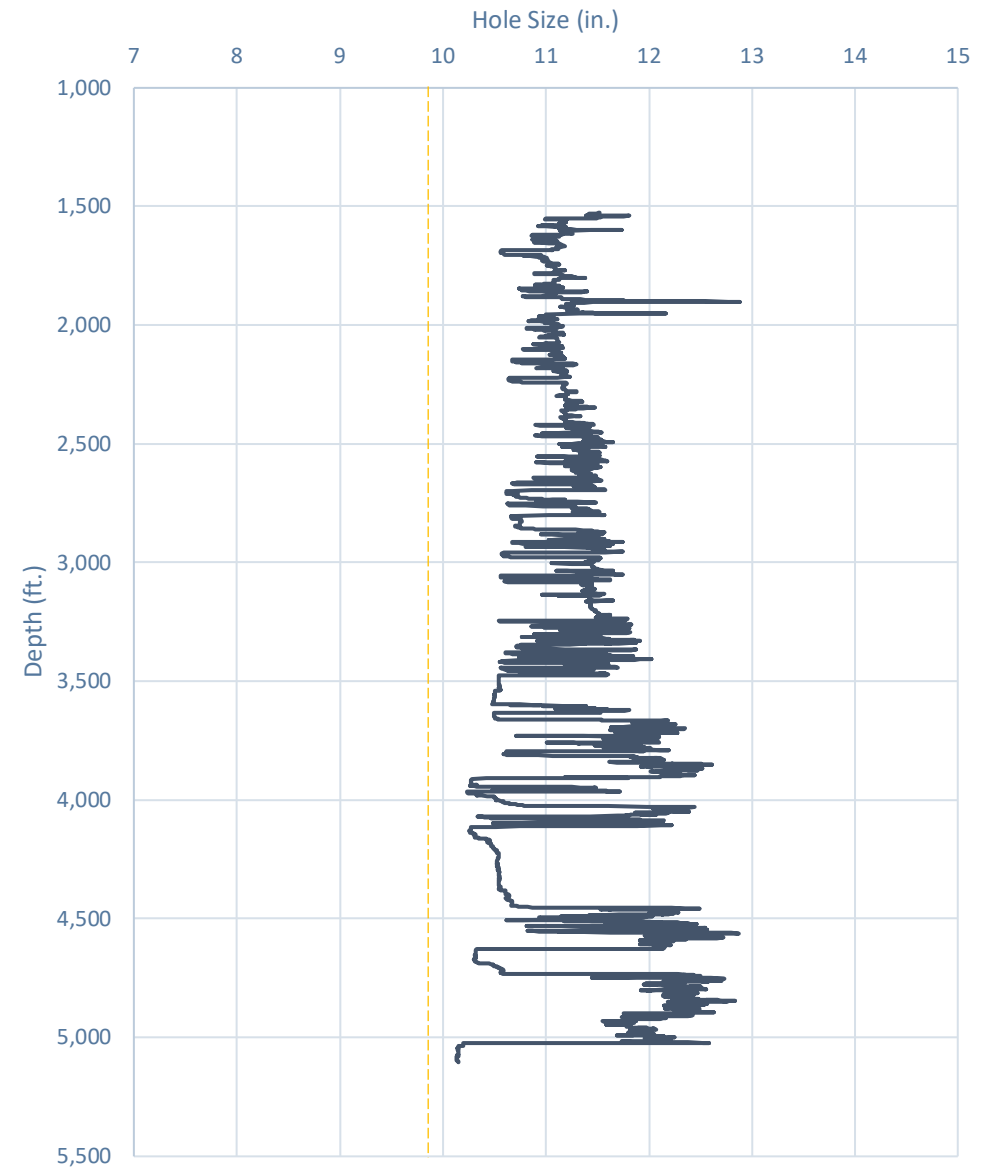


Caliper Hole Size (9.875")

Average Hole Size

- 9.875" Hole
 - 11.21" Hole
 - 13.54% diameter increase
 - 28.92% area increase
 - 1.33" Average enlargement
 - 1.30" Median enlargement
 - EnerLite

Whirling Wind 11 Fed Com #744H



Design A

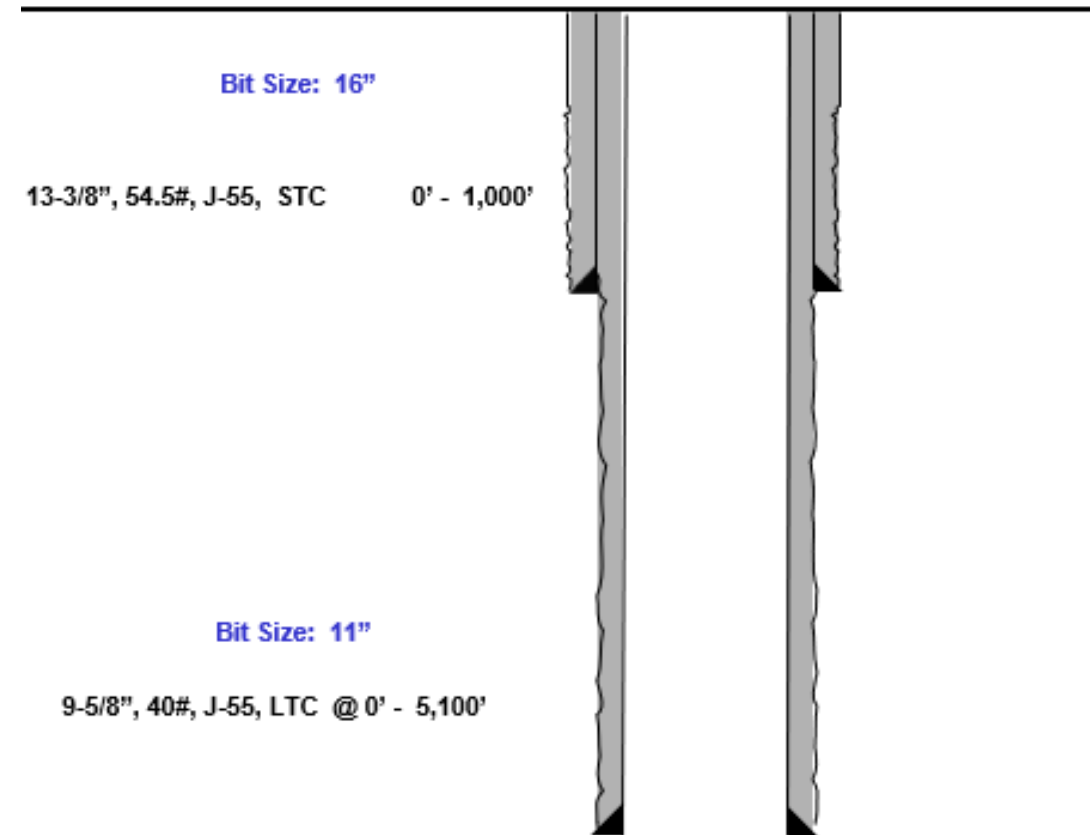
Proposed 11" Hole with 9.625" 40# J55/HCK55 LTC Casing

- 11" Bit + 0.52" Average hole enlargement = 11.52" Hole Size
 - 0.9475" Clearance to casing OD

$$= \frac{11.52 - 9.625}{2}$$
 - 0.4475" Clearance to coupling OD

$$= \frac{11.52 - 10.625}{2}$$
- Previous Shoe – 13.375" 54.5# J55 STC
 - 0.995" Clearance to coupling OD (~1,200' overlap)

$$= \frac{12.615 - 10.625}{2}$$



Design B

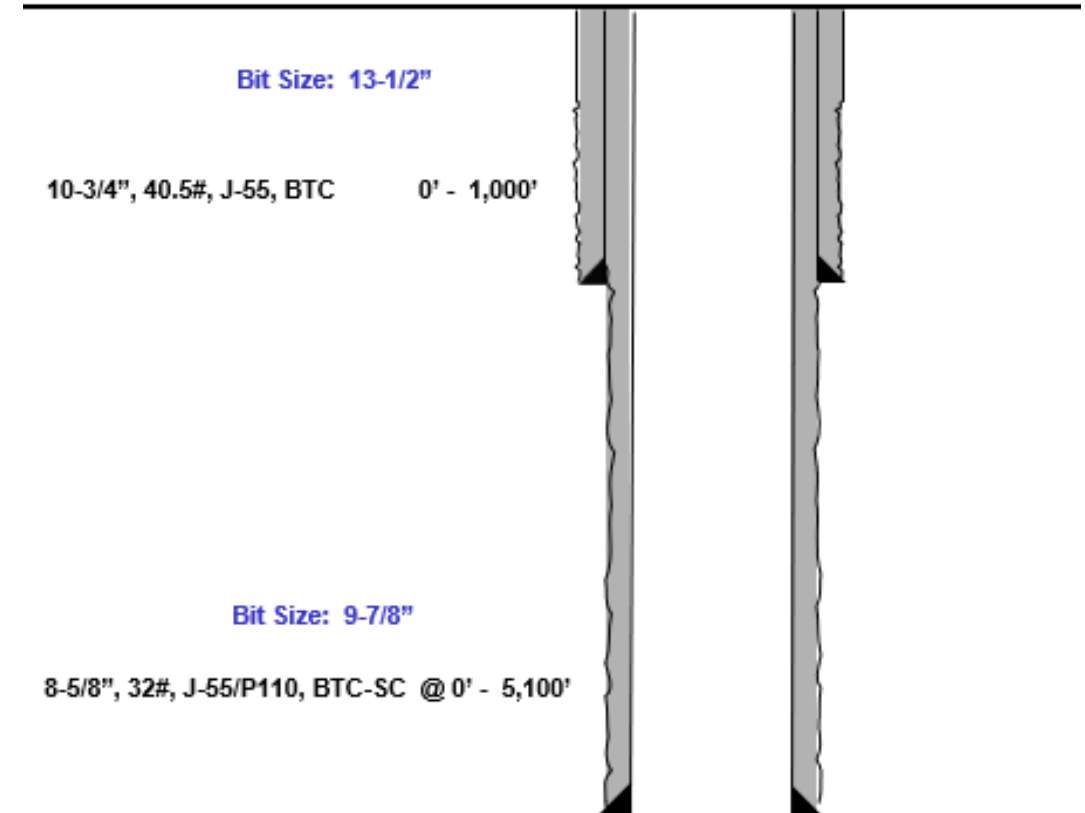
Proposed 9.875" Hole with 8.625" 32# J55/P110 BTC-SC Casing

- 9.875" Bit + 0.42" Average hole enlargement = 10.295" Hole Size
 - 0.835" Clearance to casing OD

$$= \frac{10.295 - 8.625}{2}$$
 - 0.585" Clearance to coupling OD

$$= \frac{10.295 - 9.125}{2}$$
- Previous Shoe – 10.75" 40.5# J55 STC
 - 0.4625" Clearance to coupling OD (~1,200' overlap)

$$= \frac{10.05 - 9.125}{2}$$





Index

Casing Spec Sheets

PERFORMANCE DATA

API LTC

Technical Data Sheet

9.625 in

40.00 lbs/ft

K55 HC

Tubular Parameters

| | | | | | |
|---------------------|--------|--------|------------------------------|-------|------|
| Size | 9.625 | in | Minimum Yield | 55 | ksi |
| Nominal Weight | 40.00 | lbs/ft | Minimum Tensile | 95 | ksi |
| Grade | K55 HC | | Yield Load | 629 | kips |
| PE Weight | 38.94 | lbs/ft | Tensile Load | 1088 | kips |
| Wall Thickness | 0.395 | in | Min. Internal Yield Pressure | 3,950 | psi |
| Nominal ID | 8.835 | in | Collapse Pressure | 3600 | psi |
| Drift Diameter | 8.750 | in | | | |
| Nom. Pipe Body Area | 11.454 | in² | | | |

Connection Parameters

| | | |
|------------------------------|--------|-------|
| Connection OD | 10.625 | in |
| Coupling Length | 10.500 | in |
| Threads Per Inch | 8 | tpi |
| Standoff Thread Turns | 3.50 | turns |
| Make-Up Loss | 4.750 | in |
| Min. Internal Yield Pressure | 3,950 | psi |

Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55

PDF

New Search »

« Back to Previous List

USC ☒ Metric

6/8/2015 10:04:37 AM

| Mechanical Properties | Pipe | BTC | LTC | STC | |
|----------------------------------|--------|--------|-----|--------|----------|
| Minimum Yield Strength | 55,000 | -- | -- | -- | psi |
| Maximum Yield Strength | 80,000 | -- | -- | -- | psi |
| Minimum Tensile Strength | 75,000 | -- | -- | -- | psi |
| Dimensions | Pipe | BTC | LTC | STC | |
| Outside Diameter | 13.375 | 14.375 | -- | 14.375 | in. |
| Wall Thickness | 0.380 | -- | -- | -- | in. |
| Inside Diameter | 12.615 | 12.615 | -- | 12.615 | in. |
| Standard Drift | 12.459 | 12.459 | -- | 12.459 | in. |
| Alternate Drift | -- | -- | -- | -- | in. |
| Nominal Linear Weight, T&C | 54.50 | -- | -- | -- | lbs/ft |
| Plain End Weight | 52.79 | -- | -- | -- | lbs/ft |
| Performance | Pipe | BTC | LTC | STC | |
| Minimum Collapse Pressure | 1,130 | 1,130 | -- | 1,130 | psi |
| Minimum Internal Yield Pressure | 2,740 | 2,740 | -- | 2,740 | psi |
| Minimum Pipe Body Yield Strength | 853.00 | -- | -- | -- | 1000 lbs |
| Joint Strength | -- | 909 | -- | 514 | 1000 lbs |
| Reference Length | -- | 11,125 | -- | 6,290 | ft |
| Make-Up Data | Pipe | BTC | LTC | STC | |
| Make-Up Loss | -- | 4.81 | -- | 3.50 | in. |
| Minimum Make-Up Torque | -- | -- | -- | 3,860 | ft-lbs |
| Maximum Make-Up Torque | -- | -- | -- | 6,430 | ft-lbs |

Casing Spec Sheets

Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55

PDF

New Search »

« Back to Previous List

USC ☒ Metric

6/8/2015 10:14:05 AM

| Mechanical Properties | Pipe | BTC | LTC | STC | |
|----------------------------------|--------|--------|-----|--------|----------|
| Minimum Yield Strength | 55,000 | -- | -- | -- | psi |
| Maximum Yield Strength | 80,000 | -- | -- | -- | psi |
| Minimum Tensile Strength | 75,000 | -- | -- | -- | psi |
| Dimensions | Pipe | BTC | LTC | STC | |
| Outside Diameter | 10.750 | 11.750 | -- | 11.750 | in. |
| Wall Thickness | 0.350 | -- | -- | -- | in. |
| Inside Diameter | 10.050 | 10.050 | -- | 10.050 | in. |
| Standard Drift | 9.894 | 9.894 | -- | 9.894 | in. |
| Alternate Drift | -- | -- | -- | -- | in. |
| Nominal Linear Weight, T&C | 40.50 | -- | -- | -- | lbs/ft |
| Plain End Weight | 38.91 | -- | -- | -- | lbs/ft |
| Performance | Pipe | BTC | LTC | STC | |
| Minimum Collapse Pressure | 1,580 | 1,580 | -- | 1,580 | psi |
| Minimum Internal Yield Pressure | 3,130 | 3,130 | -- | 3,130 | psi |
| Minimum Pipe Body Yield Strength | 629.00 | -- | -- | -- | 1000 lbs |
| Joint Strength | -- | 700 | -- | 420 | 1000 lbs |
| Reference Length | -- | 11,522 | -- | 6,915 | ft |
| Make-Up Data | Pipe | BTC | LTC | STC | |
| Make-Up Loss | -- | 4.81 | -- | 3.50 | in. |
| Minimum Make-Up Torque | -- | -- | -- | 3,150 | ft-lbs |
| Maximum Make-Up Torque | -- | -- | -- | 5,250 | ft-lbs |



API 5CT, 10th Ed. Connection Data Sheet

| O.D. (in) | WEIGHT (lb/ft) | WALL (in) | GRADE | *API DRIFT (in) | RBW % |
|-----------|------------------------------------|-----------|-------|-----------------|-------|
| 8.625 | Nominal: 32.00 Plain End: 31.13 | 0.352 | J55 | 7.796 | 87.5 |

| Material Properties (PE) | | Pipe Body Data (PE) | |
|---------------------------|--------|--|-----------------------|
| Pipe | | Geometry | |
| Minimum Yield Strength: | 55 ksi | Nominal ID: | 7.92 inch |
| Maximum Yield Strength: | 80 ksi | Nominal Area: | 9.149 in ² |
| Minimum Tensile Strength: | 75 ksi | *Special/Alt. Drift: | 7.875 inch |
| Coupling | | Performance | |
| Minimum Yield Strength: | 55 ksi | Pipe Body Yield Strength: | 503 kips |
| Maximum Yield Strength: | 80 ksi | Collapse Resistance: | 2,530 psi |
| Minimum Tensile Strength: | 75 ksi | Internal Yield Pressure: (API Historical) | 3,930 psi |

| API Connection Data | | API Connection Torque | |
|---------------------------------------|--|--|--|
| Coupling OD: 9.625" | | STC Torque (ft-lbs) | |
| STC Performance | | Min: 2,793 Opti: 3,724 Max: 4,655 | |
| STC Internal Pressure: | | LTC Torque (ft-lbs) | |
| STC Joint Strength: | | Min: 3,130 Opti: 4,174 Max: 5,217 | |
| LTC Performance | | BTC Torque (ft-lbs) | |
| LTC Internal Pressure: | | follow API guidelines regarding positional make up | |
| LTC Joint Strength: | | | |
| SC-BTC Performance - Cplg OD = 9.125" | | | |
| BTC Internal Pressure: | | | |
| BTC Joint Strength: | | | |

*Alt. Drift will be used unless API Drift is specified on order.

**If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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Rev 3, 7/30/2021

10/21/2022 15:24



Annular Clearance Variance

**Break-test BOP & Offline Cementing:**

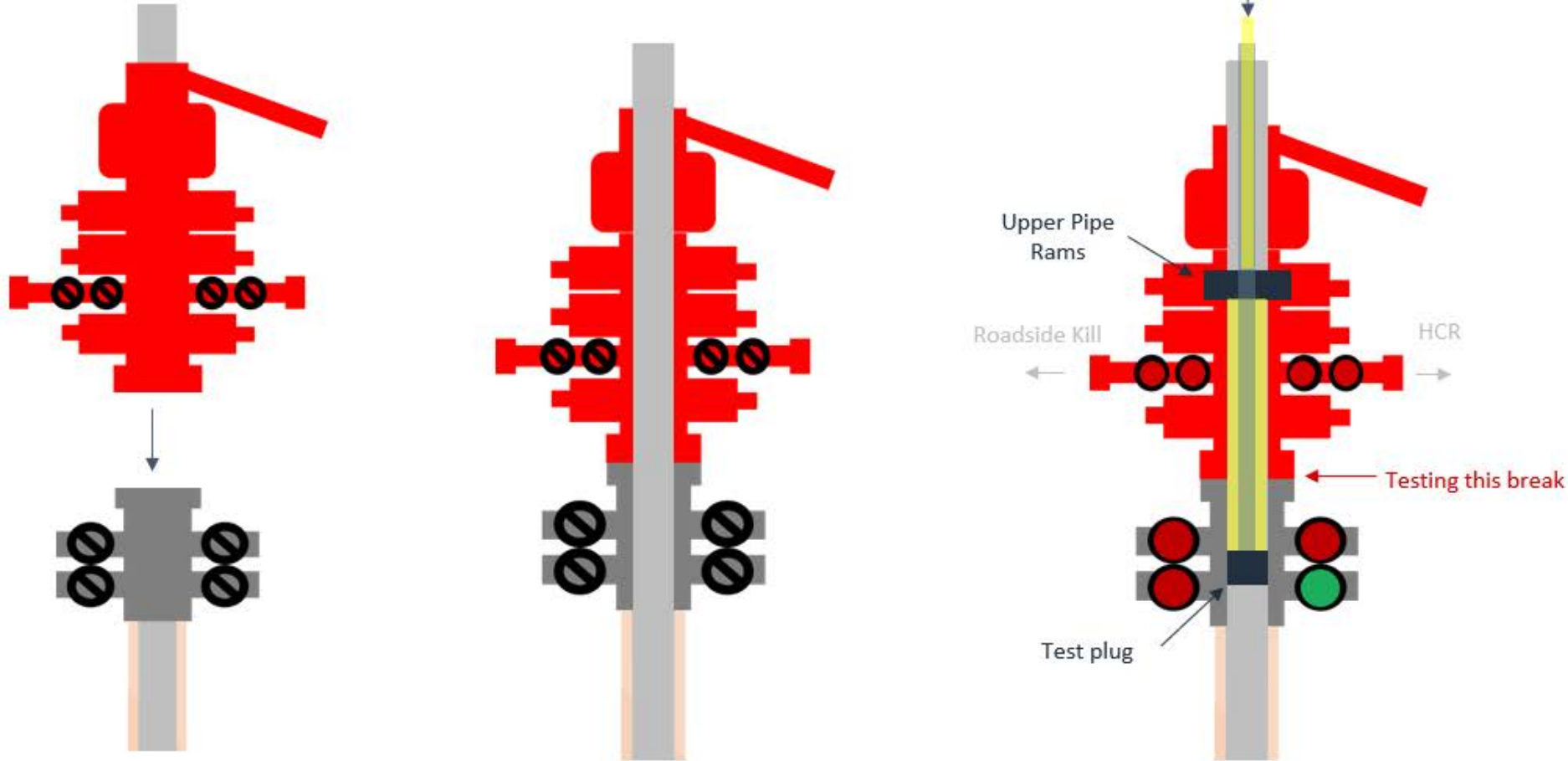
EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
 - Annular ð during each full BOPE test
 - Upper Pipe Rams ð On trip ins where FIT required
 - Blind Rams ð Every trip
 - Lower Pipe Rams ð during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

The diagrams show the process of well intervention. The first diagram shows a red plug at the top of a wellbore. The second diagram shows the plug being moved down. The third diagram shows the plug at the bottom, with labels for 'Blind Rams', 'Roadside Kill', 'HCR', 'Testing this break', and 'Test plug'.

1. Set plug in wellhead (lower barrier)
2. Close Blind Rams (upper barrier)
3. Close roadside kill
4. Open HCR (pressure application)
5. Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
6. Tie BOP testers high pressure line to main choke manifold crown valve
7. Pressure up to test break
8. Bleed test pressure from BOP testing unit

Break Test Diagram (Test Joint)



Steps

1. Set plug in with test joint wellhead (lower barrier)
2. Close Upper Pipe Rams (upper barrier)
3. Close roadside kill
4. Close HCR
5. Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
6. Tie BOP testers high pressure line to top of test joint
7. Pressure up to test break
8. Bleed test pressure from BOP testing unit



Offline Intermediate Cementing Procedure

2/24/2022

Cement Program

1. No changes to the cement program will take place for offline cementing.

Summarized Operational Procedure for Intermediate Casing

1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
 - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
2. Land production casing on mandrel hanger through BOP.
 - a. If casing is unable to be landed with a mandrel hanger, then the **casing will be cemented online**.
3. Break circulation and confirm no restrictions.
 - a. Ensure no blockage of float equipment and appropriate annular returns.
 - b. Perform flow check to confirm well is static.
4. Set pack-off
 - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
 - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
 - a. Minimum 4 hrs notice.
6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
 - a. **Note, if any of the barriers fail to test, the BOP stack will not be nipples down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.**
7. Skid/Walk rig off current well.
8. Confirm well is static before removing TA Plug.
 - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
 - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
 - c. Well control plan can be seen in Section B, Well Control Procedures.
 - d. If need be, rig can be moved back over well and BOP nipples back up for any further remediation.



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- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
9. Rig up return lines to take returns from wellhead to pits and rig choke.
 - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
 - b. If either test fails, perform corrections and retest before proceeding.
 - c. Return line schematics can be seen in Figure 3.
10. Remove TA Plug from the casing.
11. Install offline cement tool.
 - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
12. Rig up cement head and cementing lines.
 - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
13. Break circulation on well to confirm no restrictions.
 - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
 - b. Max anticipated time before circulating with cement truck is 6 hrs.
14. Pump cement job as per plan.
 - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
 - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
15. Confirm well is static and floats are holding after cement job.
 - a. With floats holding and backside static:
 - i. Remove cement head.
 - b. If floats are leaking:
 - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
 - c. If there is flow on the backside:
 - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
16. Remove offline cement tool.
17. Install night cap with pressure gauge for monitoring.
18. Test night cap to 5,000 psi for 10 min.



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Example Well Control Plan Content

A. Well Control Component Table

The table below, which covers the cementing of the **5M MASP (Maximum Allowable Surface Pressure) portion of the well**, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nipped up to the wellhead.

Intermediate hole section, 5M requirement

| Component | RWP |
|--------------------------|-----|
| Pack-off | 10M |
| Casing Wellhead Valves | 10M |
| Annular Wellhead Valves | 5M |
| TA Plug | 10M |
| Float Valves | 5M |
| 2" 1502 Lo-Torque Valves | 15M |

B. Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

General Procedure While Circulating

1. Sound alarm (alert crew).
2. Shut down pumps.
3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
4. Confirm shut-in.
5. Notify tool pusher/company representative.



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6. Read and record the following:
 - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
 - b. Pit gain
 - c. Time
 - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

General Procedure While Cementing

1. Sound alarm (alert crew).
2. Shut down pumps.
3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
4. Confirm shut-in.
5. Notify tool pusher/company representative.
6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
7. Continue to place cement until plug bumps.
8. At plug bump close rig choke and cement head.
9. Read and record the following
 - a. SICP and AP
 - b. Pit gain
 - c. Time
 - d. Shut-in annulus valves on wellhead

General Procedure After Cementing

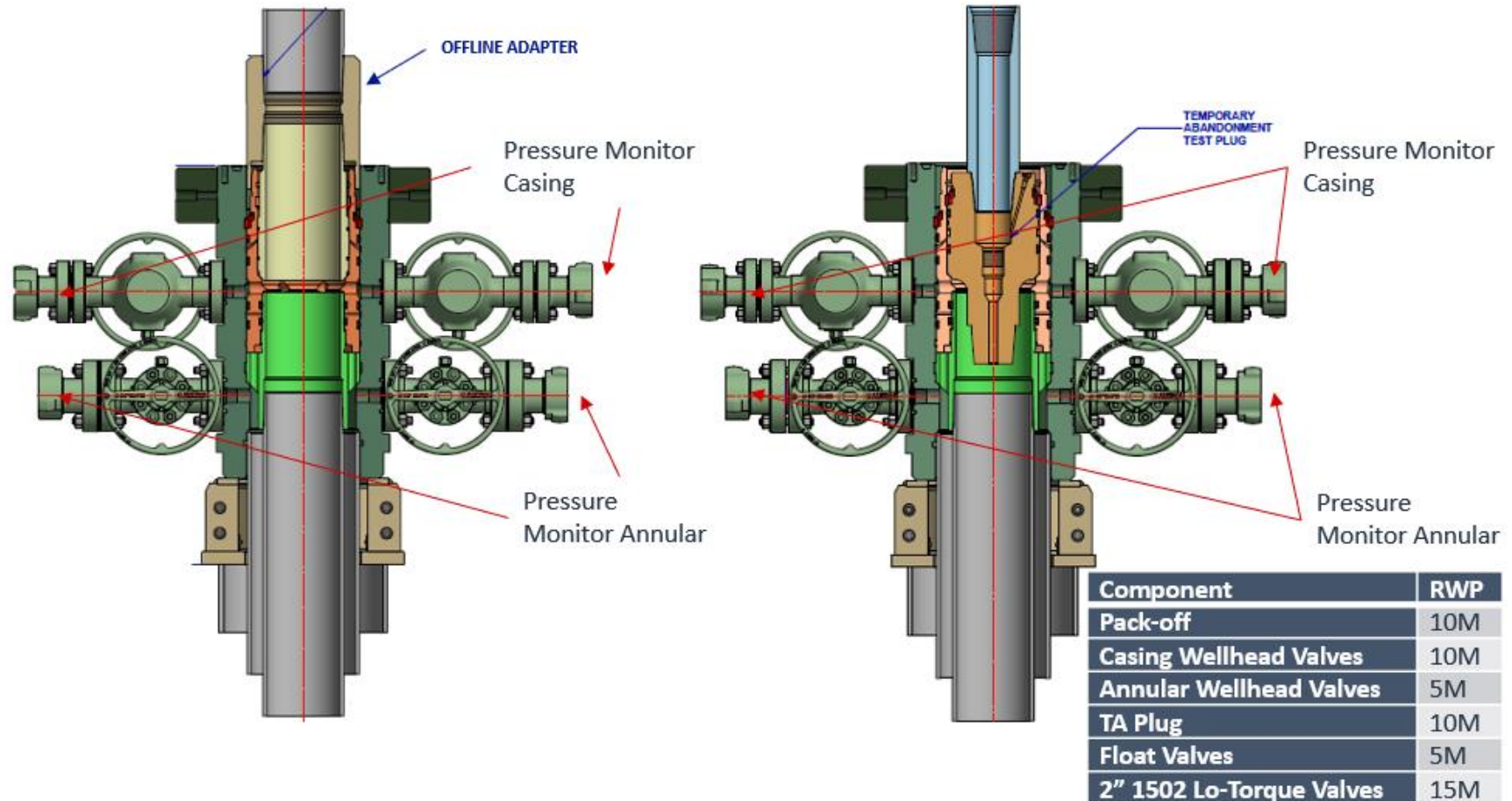
1. Sound alarm (alert crew).
2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
3. Confirm shut-in.
4. Notify tool pusher/company representative.
5. Read and record the following:
 - a. SICP and AP
 - b. Pit gain
 - c. Time
 - d. Shut-in annulus valves on wellhead



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Figure 1: Cameron TA Plug and Offline Adapter Schematic

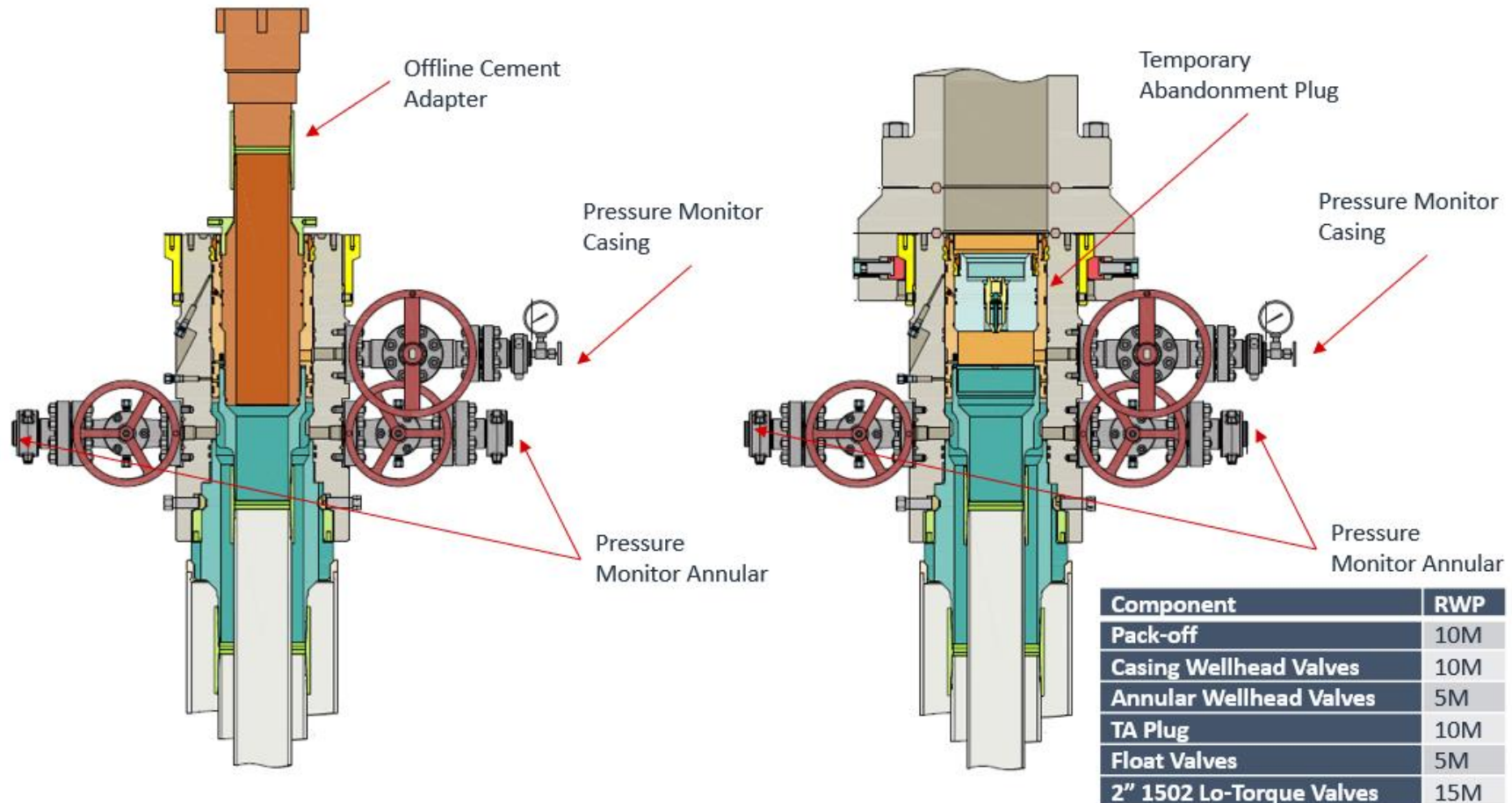




Offline Intermediate Cementing Procedure

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Figure 2: Cactus TA Plug and Offline Adapter Schematic

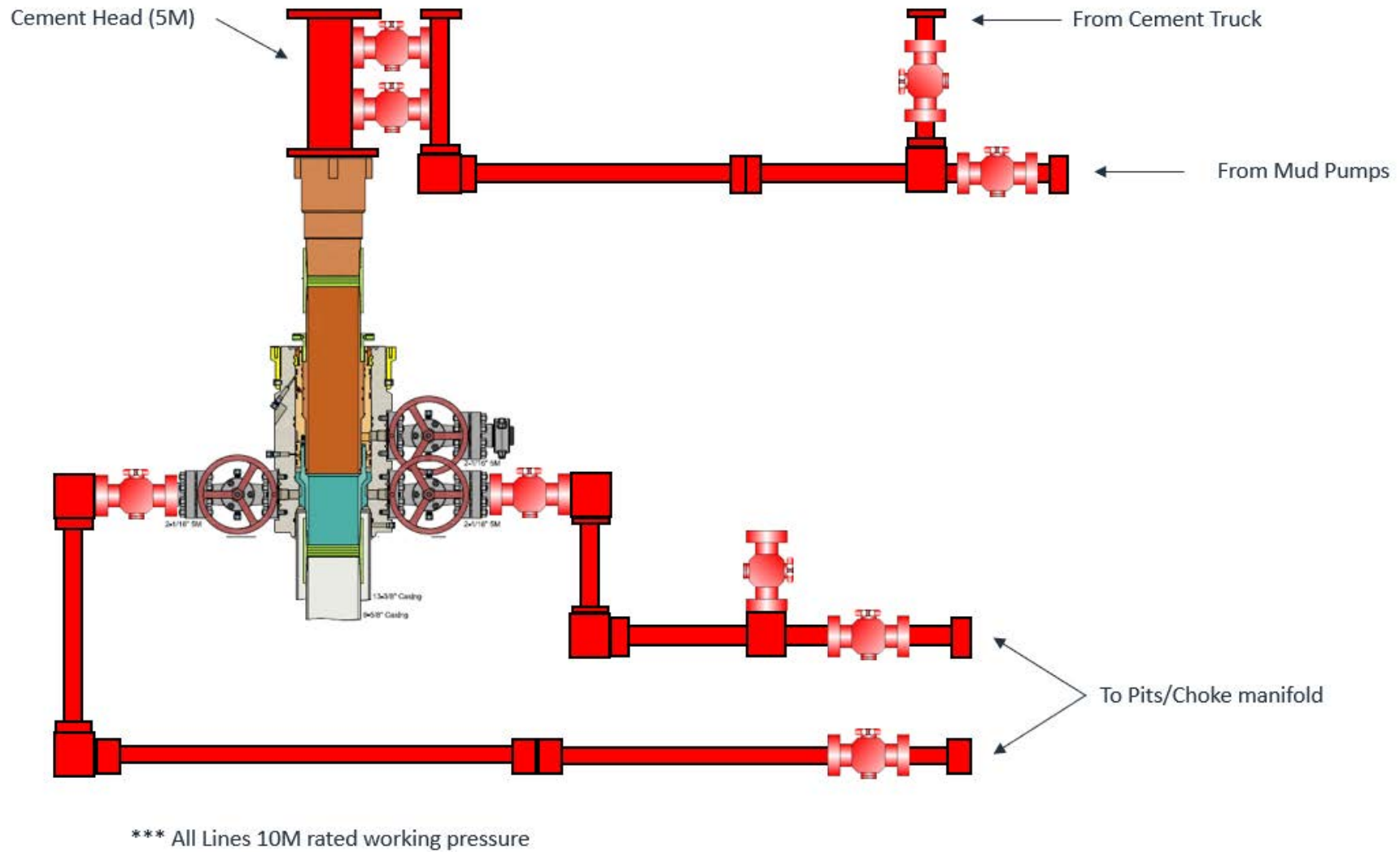




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Figure 3: Back Yard Rig Up

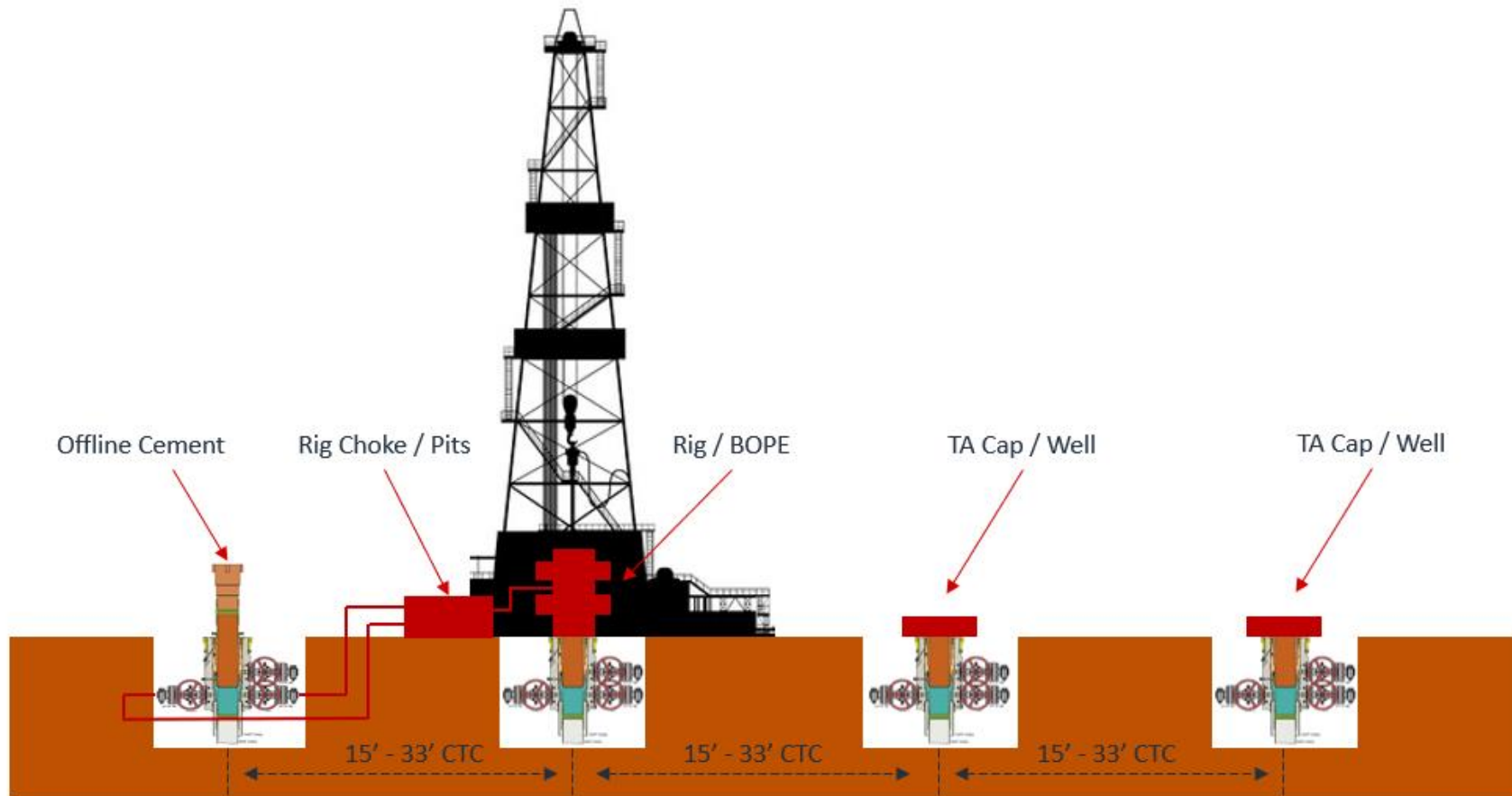




Offline Intermediate Cementing Procedure

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Figure 4: Rig Placement Diagram



**Amazing 19 Fed Package**

| Wells in package: | Tgt TVD |
|--------------------------|----------------|
| Jefe 29 Fed Com #102H | 8,818 |
| Jefe 29 Fed Com #103H | 8,818 |
| Jefe 29 Fed Com #104H | 8,818 |
| Jefe 29 Fed Com #105H | 8,818 |
| Jefe 29 Fed Com #106H | 8,818 |
| Jefe 29 Fed Com #107H | 8,818 |
| Jefe 29 Fed Com #108H | 8,818 |
| Jefe 29 Fed Com #201H | 8,907 |
| Jefe 29 Fed Com #202H | 8,907 |
| Jefe 29 Fed Com #203H | 8,907 |
| Jefe 29 Fed Com #204H | 9,094 |
| Jefe 29 Fed Com #205H | 9,094 |
| Jefe 29 Fed Com #206H | 9,094 |
| Jefe 29 Fed Com #207H | 9,094 |
| Jefe 29 Fed Com #208H | 8,907 |
| Jefe 29 Fed Com #209H | 8,907 |
| Jefe 29 Fed Com #210H | 8,907 |
| Jefe 29 Fed Com #211H | 8,907 |
| Jefe 29 Fed Com #212H | 8,907 |
| Jefe 29 Fed Com #213H | 8,907 |
| Jefe 29 Fed Com #214H | 8,907 |
| Jefe 29 Fed Com #215H | 8,907 |
| Jefe 29 Fed Com #301H | 9,499 |
| Jefe 29 Fed Com #302H | 9,499 |
| Jefe 29 Fed Com #303H | 9,499 |
| Jefe 29 Fed Com #304H | 9,499 |
| Jefe 29 Fed Com #305H | 9,499 |
| Jefe 29 Fed Com #306H | 9,499 |
| Jefe 29 Fed Com #581H | 10,960 |
| Jefe 29 Fed Com #582H | 10,960 |
| Jefe 29 Fed Com #584H | 10,960 |
| Jefe 29 Fed Com #586H | 10,960 |

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1625 N. French Dr., Hobbs, NM 88240
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District II
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District III
1000 Rio Brazos Rd., Aztec, NM 87410
Phone:(505) 334-6178 Fax:(505) 334-6170
District IV
1220 S. St Francis Dr., Santa Fe, NM 87505
Phone:(505) 476-3470 Fax:(505) 476-3462

State of New Mexico
Energy, Minerals and Natural Resources
Oil Conservation Division
1220 S. St Francis Dr.
Santa Fe, NM 87505

CONDITIONS

Action 288691

CONDITIONS

| | |
|--|--|
| Operator: EOG RESOURCES INC P.O. Box 2267 Midland, TX 79702 | OGRID: 7377 |
| | Action Number: 288691 |
| | Action Type: [C-103] NOI Change of Plans (C-103A) |

CONDITIONS

| Created By | Condition | Condition Date |
|------------|-----------|----------------|
| pkautz | None | 12/27/2023 |