Received by QCD i 0/31/2024 3:09:11 PM	f State of New M	lexico		Form C-103				
Office District I – (575) 393-6161	Energy, Minerals and Nat	tural Resources		Revised August 1, 2011				
1625 N. French Dr., Hobbs, NM 88240			WELL API NO.					
<u>District II</u> – (575) 748-1283	OIL CONSERVATIO	N DIVISION		ND 30-025-42139				
811 S. First St., Artesia, NM 88210 District III – (505) 334-6178	1220 South St. Fra		5. Indicate Type					
1000 Rio Brazos Rd., Aztec, NM 87410	-		STATE					
District IV - (505) 476-3460	Santa Fe, NM 8	\$7505	6. State Oil & C	as Lease No.				
1220 S. St. Francis Dr., Santa Fe, NM			V07530-0001					
87505 SUNDRY NOTICI	ES AND REPORTS ON WELL	\$	7 Lesse Name	or Unit Agreement Name				
(DO NOT USE THIS FORM FOR PROPOSA			Linam AGI	of Ohn Agreement Name				
DIFFERENT RESERVOIR. USE "APPLICA			Linani AOI					
PROPOSALS.)			8. Wells Numbe	er 1 and 2				
<i>V</i> 1	as Well 🛛 Other		01 11 0110 1 (01110)					
2. Name of Operator			9. OGRID Num	iber 36/85				
DCP Operating Company, LP			10 D 1	XX7'1 1 4				
3. Address of Operator	CO 80227		10. Pool name or Wildcat					
6900 E. Layton Ave, Suite 900, Denv	/er CO 80237		Wildcat					
4. Well Location								
Unit Letter K; 1980 feet from	n the South line and 1980 feet fi	rom the West line						
Section 30	Township 18S	Range 37E	NMPM	County Lea				
	11. Elevation <i>(Show whether D.</i> 3,736 GR	R, RKB, RT, GR, etc.,						
12. Check Appropriate Box to Ir	ndicate Nature of Notice, R	Report or Other Da	ata					
		REMEDIAL WOR						
	CHANGE PLANS	COMMENCE DRI		P AND A				
	MULTIPLE COMPL	CASING/CEMEN	I JOB					
DOWNHOLE COMMINGLE	_							
OTHER:			Summary Report a oursuant to NMOC	and Notification parameter C R12546-K				
13. Describe proposed or complete	d operations. (Clearly state all							

of starting any proposed work). SEE RULE 19.15.7.14 NMAC. For Multiple Completions: Attach wellbore diagram of proposed completion or recompletion.

# Annual Report for the period from January 1 through December 31, 2023 Pursuant to NMOCC Orders R-12546-K and ACO-275 for Linam AGI #1 and AGI #2 and Request to Continue with Approved Immediate Notification Parameters for Operation of Both Wells

This is an annual summary submittal of data as agreed to between DCP and NMOCD relative to injection pressure, TAG temperature and casing annulus pressure for Linam AGI #1 (API #30-025-38576) and for Linam AGI #2 (API #30-025-42139) which was brought online in October 2015.

The analyses of data from both wells have been submitted monthly. The AGI #1 well was successfully worked over as planned in June 2017 and was used exclusively until May 2019 when flow switched primarily to AGI #2 through June 2020. Both the AGI #1 and AGI #2 operated in July 2020 until AGI #1 operated exclusively from August through February 2021. AGI #2 alone was used from March 2021 through January 2022, after which, AGI #1 and AGI #2 operated simultaneously and briefly in February 2022 before switching exclusively to AGI #1 through June 2023. AGI #2 was used exclusively from July 2023 through December 2023. The effects of the simultaneous and switching of well use are noted in the attached annual summary of the data. The purpose of this submittal is to provide NMOCD with the required summary of data for the 2023 calendar year for the operation of the Linam Ranch AGI Facility and to request to keep the approved immediate notification parameters in place for the 2024 calendar year.

The summary of the data and supporting tables and figures are attached.

 TITLE Consultant to DCP Midstream/ Geolex, Inc. DATE 1/21/2024E-mail address: <a href="mailto:aag@geolex.com">aag@geolex.com</a>PHONE: <a href="mailto:505-842-8000">505-842-8000</a>

Page 1 of 15

DATE

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# ANALYSIS OF 2023 ANNUAL TRENDS AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS FOR OPERATION OF LINAM AGI #1 AND LINAM AGI #2 (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-All

This document presents the results from the analyses of the injection parameter data collected from the Linam AGI #1 and #2 wells which serve the Linam Ranch Gas Processing Facility near Hobbs, NM. Data from the Linam AGI #1 has been collected continuously since 2012 and has been analyzed on a monthly basis by Geolex and transmitted to DCP for reporting to NMOCD as required by ACO-275 and the approved post-workover C-103. In addition, the Linam AGI #2 well was completed and brought online in October 2015. The AGI #2 well was completed in the same injection zone as the AGI #1 approximately 450 feet to the southwest of AGI #1. From the time that the AGI #2 was brought online, injection has been either into both wells simultaneously or solely into one of the two wells. AGI #2 was operated in conjunction with AGI #1 from October 2015 to January 2016 when a switch was made to operate only AGI #1 for the remainder of 2016. In May 2017, DCP switched over to injecting into AGI #2 to allow for the workover of AGI #1. The workover was completed on June 8, 2017, and AGI #1 was brought back online in July 2017 with bottom hole sensors installed. These sensors are now serving to monitor downhole and reservoir conditions since the downhole sensors in AGI #2 failed due to a lightning strike shortly after installation (2015) and will not be able to be repaired until sometime in the future when AGI #2 is worked over. In the meantime, to obtain reservoir data which would have been provided by the downhole PT sensors in AGI #2, a slick line with a pressure recorder was placed into AGI #2 and downhole pressure data are collected under both injection and non-injection conditions for the AGI #2 and AGI #1. Since that time, the downhole sensors in AGI #1 provide the reservoir data needed to evaluate the performance of the two wells. The system continued operating through 2018 with only AGI #1 active while waiting for independent flow meters to be installed/repaired in both wells so that reliable flow information would be available for each well independently. This operational mode (utilizing only AGI #1) continued through April 2019, and, to date, separate volume meters have not been installed/repaired. In May 2019, however, DCP began dividing the flow of acid gas between the two wells by using one or the other well exclusively (see Figure 3). This practice continues today with all flow having gone to AGI #1 from January 2022 through May 2023 and was switched entirely to AGI #2 for the rest of the year. Presently, surface data from both wells is being collected relative to the following parameters:

- Treated Acid Gas (TAG) surface injection pressure (both wells)
- TAG injection temperature (both wells)
- Annular pressure (both wells)
- Bottom Hole pressure and temperature (AGI #1 only beginning 7/2017)
- Overall total TAG flow rate from compressors

The parameters above are currently being measured in both wells in order to monitor the operations of the wells, prevent hydrate formation, and reduce corrosion potential. While improvements have been implemented in the placement of temperature controls, dehydration of TAG during compression, and other systems improvements at the AGI facility, there continue to be variations in the desired and normal

operating levels of the above-referenced parameters. Since these parameters are useful indicators and predictors of potential operational or mechanical problems in the well, various levels of alarms have been established for each of these parameters. These parameters include three which are measured directly (TAG injection pressure, TAG injection temperature, and annular pressure) and one (differential pressure) which is a calculated value (the difference between the two measured parameters of injection and annular pressure). The analyses of the long-term trends in these values have been useful in smoothing out shorter-term variations which can be observed from detailed inspection of hourly data and in the development of appropriate alarm bands for each parameter.

The Linam AGI #1 experienced a tubing leak in late 2011 which was partially addressed in a workover conducted in April/May 2012. At the beginning of 2012 (until the time of the workover) the injection parameters were reviewed, analyzed, and reported weekly to the NMOCD. Following the workover in which the tubing leak was repaired, some compromised production casing was detected immediately above the packer depth. At that time, we recommended keeping only approximately 250 psig on the annular space between the tubing and casing in AGI #1 since, with annular pressure at this level under normal operating conditions, this parameter can serve as a useful indicator of when activity should be initiated to prevent damage to the well or trigger an NMOCD shutdown and/or immediate notification requirements. Concern about this compromised casing was eliminated by stacking packers when the well was worked over again in June 2017. Data from January 2012 through December 2015 are included in our analysis, but only the post-workover data have been used to develop the recommended alarm and emergency shutdown (ESD) levels in conjunction with the requirements of NMOCD Order 12546-All, ACO-275, and the post-workover C-103.

Furthermore, a similar process has been employed on the Linam AGI #2 since it was brought online in October 2015. As described above, this well is equipped with bottom hole (just at top of packer) pressure and temperature measurement capability both inside and outside the tubing. The immediate notification parameters for both wells were developed from long-term analysis of the injection data. Initial testing of the Linam AGI #2 indicated that the pressure variations induced by flow rate and temperature fluctuations in the Linam AGI #1 are influencing the reservoir as measured in the AGI #2 location. This is to be expected as the newer well is completed in the same zone at a distance away from the initial well which we predicted would see the edge of the plume in about 7 years. The Linam AGI #1 has been injecting since 2007.

Data from the AGI #1 was continuously collected and analyzed weekly prior to the original workover in April/May 2012. This data collection, analysis, and reporting continues monthly as mandated by NMOCD. Since it is necessary to evaluate the data from both wells to know how the system is operating overall, the surface data from AGI #2 are also being collected, analyzed, and reported monthly although the reporting requirement for the AGI #2 is quarterly.

The NMOCD also requires that immediate notification parameters and levels be discussed and agreed upon with the agency and that these be periodically reviewed and updated as needed based on operational or regulatory changes. The immediate notification parameters for both wells have been approved by NMOCD and DCP requests no changes in these approved values. With this requirement in mind and for the purpose of protecting the mechanical integrity and safety of both wells and the overall AGI facility, Geolex monitors these data under contract to DCP to prevent damage to the wells or violation of regulatory requirements or permit constraints.

Geolex has carefully and continuously assembled and analyzed the performance data and trends for the Linam AGI #1 and AGI #2 since 2012 and 2015, respectively. Several important observations can be made from analyzing this data and taking into consideration important system modifications that have occurred in the post-workover period from June 2012 through December 2023. These include the following:

- 1. AGI #1 Post-Workover MIT completed in May 2012
- 2. AGI #1 MIT test completed November 14, 2012
- 3. Bleeding of diesel from casing annular space immediately after the November 2012 AGI #1 MIT test.
- 4. AGI #1 MIT test completed April 30, 2013
- 5. Addition of diesel in annular space after April 2013 AGI #1 MIT and May 2013 plant shutdown
- 6. AGI #1 MIT test completed October 30, 2013
- 7. Failure of the VFD for the cooler on the AGI compressor from February 4 through 9, 2014.
- 8. AGI #1 MIT test completed April 30, 2014
- 9. Addition of diesel in annular space after April 2014 AGI #1 MIT
- 10. AGI #1 MIT test completed September 19, 2014
- 11. AGI #1 MIT test completed March 19, 2015
- 12. AGI #1 MIT test completed September 15, 2015
- 13. AGI #2 brought online with startup in October-November 2015 and operated until January 2016
- 14. AGI #1 MIT test completed March 22, 2016
- 15. AGI #2 MIT test completed April 1, 2016
- 16. AGI #2 TAG lines bled to flare on June 13, 2016 to remove static TAG in line when well is not operating
- 17. AGI #1 MIT test completed September 14, 2016
- 18. AGI #2 MIT test completed February 16, 2017
- 19. AGI #1 Workover completed June 8, 2017 including stacked packer, bottom hole PT gauges
- 20. AGI #1 MIT test completed June 7, 2017 after workover completion
- 21. AGI #2 MIT test completed February 15, 2018
- 22. AGI #1 MIT test completed June 19, 2018
- 23. AGI #2 MIT test completed February 15, 2019
- 24. AGI #1 MIT test completed February 15, 2019
- 25. AGI #1 MIT test completed February 4, 2020
- 26. AGI #2 MIT test completed February 4, 2020
- 27. AGI #1 MIT test completed February 9, 2021
- 28. AGI #2 MIT test completed February 9, 2021
- 29. AGI #1 MIT test completed August 12, 2021
- 30. AGI #1 MIT test completed February 14, 2022
- 31. AGI #2 MIT test completed February 14, 2022

- 32. AGI #1 MIT test completed August 17, 2022
- 33. AGI #1 MIT test completed February 14, 2023
- 34. AGI #2 MIT test completed February 14, 2023
- 35. AGI #1 MIT test completed November 1, 2023

The following trends have been observed in the AGI well data and are reflected in Figures 1-4:

- TAG injection pressure, which was on a slight increasing trend due to slightly increasing average temperature of injected TAG, began to level off due to temperature decreases in 2017. This trend continued over the last six months of 2018 until flow began cycling between AGI #1 and AGI #2 in May 2019. The TAG injection pressure and rate has been more variable since 2016 due to inlet flow variations.
- AGI #1 was used exclusively following the workover from July 2017 through April 2019. Beginning in May 2019, the flow of TAG was split between the two wells with either one or the other being used with simultaneous operation occurring for only brief periods of time, if at all (Figure 3).
- 3. The TAG injection temperature is significantly lower during periods of low flow or no flow when the other well is being used.
- 4. Pressure in the casing annulus has been consistently tracked; the correlative behavior of annular pressure with flowrate, injection pressure, and temperature confirms both wells have good integrity and are functioning as expected (Figures 1 and 2). The injection temperature is the largest influencer of this parameter under normal conditions.
- 5. The pressure differential between the casing annulus and the TAG injection pressure clearly indicates that no communication currently exists between the tubing and the casing annulus.
- 6. The generally low annular pressures observed, especially in recent years, indicate that the production casing and cement continue to have good integrity.
- 7. TAG injection temperatures can now be lower due to the improvement of water reduction in compression which reduces the potential for hydrate formation at lower temperatures. This has allowed for relatively lower injection temperatures from 2018 to 2023 in AGI #1 and, generally, more stable operational temperatures in AGI #2.
- 8. The behavior of the reservoir in terms of pressure and temperature when switching between wells clearly demonstrates that the bottom hole sensors in AGI #1 are sufficient for recording reservoir conditions in both wells (Figure 4).
- 9. The behavior of the reservoir in response to injection demonstrates that the reservoir is not pressuring up significantly and responds quickly to reduction of pressure upon cessation of injection.

There is no current indication of the reservoir being pressured up to any significant degree by the injection from Linam AGI #1. This was confirmed during the drilling and testing of AGI #2. Upon startup from any shutdown that lasts more than 6-8 hours it is critical to inject methanol along with the TAG for the initial startup period to prevent the formation of hydrates. While this may no longer be necessary due to the changes which were made in the water removal efficiency of the AGI compressor system, it is a good preventative measure. Prior to the increased water removal efficiency, this effect was observed in the period of March 2013 when hydrate formation during one of these events caused a spike

in TAG injection pressure of approximately 35% over normal pressures due to partial blockage of the injection line and tubing created by hydrate formation. This persisted for several hours until the situation was alleviated by the stabilization of the compressor and the simultaneous injection of methanol to cause the hydrates to be reabsorbed into the TAG. Subsequently, injection pressures and temperatures returned to normal.

It is also critical to maintain temperature control on the injected TAG and to avoid rapid temperature or pressure fluctuations during periods when power failures or other mechanical failures may occur. The extensive and wide variation in TAG injection temperatures resulted in the formation of free water and corrosion within the tubing resulting in a tubing leak which had to be repaired in April/May 2012. Temperature control changes were implemented and helped to significantly control downward swings in temperature and prevent the formation of hydrates. However, in February 2014, there was a failure in the VFD for the cooler on the AGI compressor which persisted for five days. During this time, the TAG temperature increased to at least 150 °F and resulted in a dramatic increase in the annular pressure due to the heating of the diesel fluid in the annular space. TAG temperature as well as annular pressure returned to the normal range once the VFD on the cooler was repaired. The significant spread between TAG injection pressure and the annular pressure maintained even during this heating episode confirms the continued integrity of the well, packer, casing, and tubing. However, the rise in annular pressure has the potential to damage the integrity of the compromised casing in the well and should be avoided in subsequent operations. In response to these issues, DCP undertook and successfully completed a project in 2015 to address the temperature fluctuations resulting from compression controls and to increase the efficiency of water removal to the point where all free water is removed from the TAG prior to injection. This significantly reduces hydrate formation potential in the entire system regardless of temperature variations. This has provided for lower average injection temperatures observed without resulting in hydrate formation.

In October 2015, AGI #2 began operating in a startup mode, switching operation back and forth with AGI #1. This effect is reflected in the trend data shown in Figure 2. Due to a volume meter sensor failure and configuration issues, only total flow to the AGI system can be reliably measured through 2019. For 2021, AGI #1 operated exclusively from January through February with AGI #2 operating the remainder of the year and through February 2022, after which, AGI #1 was operated exclusively through June 2023. AGI #2 was operated exclusively from July 2023 through December 2023. On the rare occasion that both wells are in operation simultaneously, this typically occurs only briefly. See Figure 3 for total flowrate and flowrate of both the AGI #1 and AGI #2 wells.

## REVIEW OF STATISTICAL ANALYSIS OF INJECTION PARAMETERS, DEVELOPMENT OF AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-All

The statistical analyses of the injection parameter data were initially conducted for the purpose of establishing normal operating levels for the parameters that are automatically monitored. Several data filtering steps were undertaken to take the hourly data, which forms the basis of the analysis, in order to smooth out variability and to account for the physical changes in the well and its operation after the repair of the tubing leak and the workover completed in May 2012. Because the configuration of the well changed dramatically after the workover, only data after the well had stabilized post-workover were used in this analysis. Additionally, in June 2017 during a workover, AGI #1 was equipped with a stacked packer configuration. The bottom hole pressure and temperature sensors installed during the 2017 workover of AGI #1 have been providing excellent data, as shown in Figure 4. During 2018, communication issues between the Halliburton BHPT panel and the plant DCS system were corrected. BHPT readings had been inaccurately reported from November 2017 to June 2018 until this issue was detected. In 2018, for the period affected, we downloaded the data directly from the Halliburton panel and corrected the values. A C-103 was submitted with these corrections in July 2018. The corrected values are used in this analysis. No problems with BHPT readings occurred from 2019 through 2023. It is clear from the variation in these parameters when flow is switched between wells that the conditions measured in the BHPT gauge in AGI #1 reflect the values in the reservoir which would be very similar to AGI #2 if the BHPT gauges in the well were operational.

All the data are summarized in Table 1 and the calculated statistical parameters of arithmetic mean and standard deviation were used to establish base levels and variability for each parameter. The results of these analyses resulted in the immediate notification parameters which were approved both for AGI #2 and the parameters required under ACO-275 for AGI #1.

Based on the analysis of observed trends, the immediate notification parameters which were approved for AGI #1 and the parameters previously approved for AGI# 2 and continued through 2023 remain appropriate to continue through 2024. This is DCPs request and the approved immediate notification parameters are detailed below:

The approved immediate notification parameters for Linam AGI #1 are summarized below:

- 1. Exceedance of the approved MAOP of 2,644 psig for a period greater than two hours.
- 2. Failure of a mechanical integrity test (MIT) of the well.
- 3. Confirmation of any condition that indicates a tubing, packer or casing leak.
- 4. Any increase of the annular pressure to a value that is greater than 1,200 psig
- 5. Any instance in which differential pressure between the injection tubing and injection tubing annulus is less than 100 psig.
- 6. Any release of H<sub>2</sub>S at the well which results in an activation of the facility's approved Rule 11 H<sub>2</sub>S contingency plan.
- 7. Any workover or maintenance activity that requires intrusive work in the well.

The approved immediate notification parameters for the Linam AGI #2 are summarized below:

- 1. Exceedance of the approved MAOP of 2,644 psig for a period greater than two hours.
- 2. Failure of a mechanical integrity test (MIT) of the well.
- 3. Confirmation of any condition that indicates a tubing, packer or casing leak.
- 4. Any increase of the annular pressure to a value that is more than 80% of the injection pressure.
- 5. Any release of H<sub>2</sub>S at the well which results in an activation of the facility's approved Rule 11 H<sub>2</sub>S contingency plan.
- 6. Any workover or maintenance activity that requires intrusive work in the well.

 TABLE 1 SUMMARY DATA ANALYSIS OF LINAM AGI #1 AND AGI #2 TRENDS FOR JANUARY 2012 THROUGH DECEMBER 2023

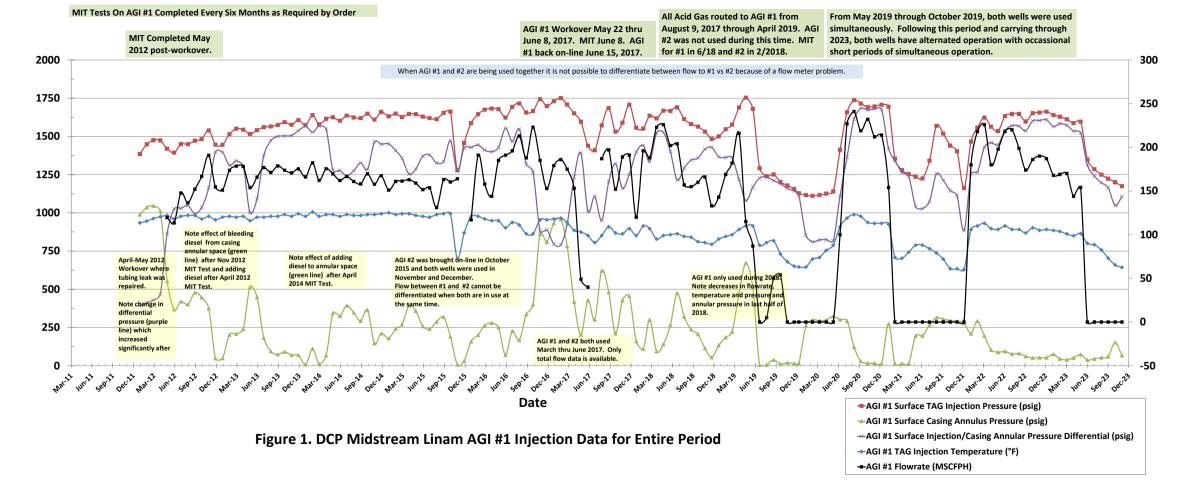
Month	Ended		-	AGI #1 TAG Injection Temperature (°F)	AGI #1 Surface Casing Annulus Pressure (psig)	Total Flowrate (MSCFPH)	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	Bottom Hole	AGI #1 Average Bottom Hole Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #1 Flowrate AGI #2 Flowrate (MSCFPH) (MSCFPH)	AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)	Total CO2 Sequestered per month (Metric Ton) Notes
iry	2012	Jan-12	1385	114						(199.8/	(190.8)		N/A 0		No Flow Data Available
iary		Feb-12	1448	116		N/A	412						N/A 0	D	No Flow Data Available
h		Mar-12	1475	118									N/A 0	)	No Flow Data Available
		Apr-12	1474	121									N/A 0	0	No Flow Data Available
		May-12	1419	122									120 0	0	3693 Plant Workover and Shutdown
	2012	Jun-12 Jul-12	1394 1450	118									113 0		3392 Plant Workover and Shutdown 4562
st	2012 2012	Aug-12	1450	121									148 0 137 0	1	4562 4218
mber	2012	Sep-12	1445	122									152 0	)	4547
ber		Oct-12	1482	118									167 0	0	5150
mber		Nov-12	1539	121									191 0	0	5702 November 14, 2012 MIT Test
nber	2012	Dec-12	1446	117									155 0	0	4775
ry	2013	Jan-13	1445	120									151 0	0	4664
iry		Feb-13	1515 1550	121									174 0 179 0		4845 5514
		Mar-13 Apr-13	1550	120									179 0	1	5321 April 30, 2013 MIT Test
		May-13	1544	110									178 0	)	4753
	2013	Jun-13	1510	120					1	1	1	1	166 0	)	4957
	2013	Jul-13	1560	120	182	177	1375						177 0	)	5461
		Aug-13	1565	121									171 0	)	5291
nber	2013	Sep-13	1575	121							l		179 0	0	5343
er	2013	Oct-13	1594	123							+		174 0		5369 October 30, 2013 MIT Test
iber ber		Nov-13 Dec-13	1576 1607	121							ł		171 0 175 0		5103 5414
v	2013	Jan-14	1607	122							1		1/5 0	)	5414 5131
ary .		Feb-14	1639	126									182 0	0	5083
<i>'</i>		Mar-14	1579	121									162 0	)	5011
	2014	Apr-14	1615	123		175	1547	r					175 0	0	5244 April 30, 2014 MIT Test
		May-14	1625	123									170 0	)	5239
	2014	Jun-14	1603	121									162 0	0	4844
	2014	Jul-14	1636	123									167 0	0	5144
-		Aug-14	1624 1620	122									161 0		4971 4728 September 19, 2014 MIT Test
nber er	2014 2014	Sep-14 Oct-14	1620	122									158 0 170 0	1	5241
ber		Nov-14	1648	123									158 0	)	4716
iber		Dec-14	1660	124									168 0	0	5173
ry -	2015	Jan-15	1631	125			1451						151 0	)	4666
ary		Feb-15	1649	123									161 0	)	4491
		Mar-15	1627	124									161 0	0	4984 March 19, 2015 MIT Test
	2015	Apr-15	1647	124									163 0	)	4869
	2015 2015	May-15 Jun-15	1645 1629	122									159 0 152 0		4911 4531
	2015	Jun-15 Jul-15	1629	121									152 0	1	4531 4746
t	2015	Aug-15	1613	123									134 0	)	4048
nber	2015	Sep-15	1654	124									163 0	0	4875 September 15, 2015 MIT Test
er	2015	Oct-15	1662	124			1471						160 0	0	4954 AGI #2 Operations Began October 2015
ber	2015	Nov-15	1280	73						1430			9 164 0	10:	
ber		Dec-15	1457	102						1498				10	
y		Jan-16	1587	121						1094		7		10	
iry		Feb-16	1645	121						1603		4		16	
		Mar-16 Apr-16	1675 1682	118					+	1679		. 5		0 16 0 16	
		May-16	1682	116						1685		7		16	
	2010		10/8	110	230	185	1420	1	1	108.			100	10	AGI #2 not in use. TAG trapped in blocked off section of A
	2016	Jun-16	1624	108			1554	k		2	2 1	. 8	1 191 0	, ,	1 5709 pipe blown down
	2016	Jul-16	1693	114		196	1467			2	2 1	. 8		)	1 6053 AGI #2 not in use
		Aug-16	1715	111							3 1	. 7		)	2 6578 AGI #2 not in use
ber		Sep-16	1657	101						3	3 1	. 7		0	2 5619 AGI #2 not in use
r		Oct-16	1666	101						2	2 0	6		)	2 6887 AGI #2 not in use
ber bor		Nov-16	1743 1698	117						1		5			1 5529 AGI #2 not in use 1 4725 AGI #2 not in use
ber V	2016 2017	Dec-16 Jan-17	1698	117					1			4.		2	4/25 AGI #2 not in use     5528 AGI #2 not in use
y ry	2017	Feb-17	1730	118						10	278			-20	
<u>'</u>			1,50	11.		100	,,,,				2/0				
	2017	Mar-17	1708	114	1 782	186	927	,		1701	373	104	4 175 11	13.	Both wells used; #2 flow meter not functioning. AGI #1 fl           27         5745 month and AGI #2 only from 3-13 to 3-16 and 3-21 to 3-1           Both wells used. Flow meter for #2 not working. TAG rot
															well exclusively, both wells simultaneously and #2 well e All TAG routed to #2 from 4-26 onward in anticipation o
	2017	Apr-17	1651	105	5 418	194	1234			1862	2 296	10	0 153 41	15	Both wells used. #2 Flow Meter not working. TAG Route #2 save for 19 hour period from 5-17 to 5-18 when it wa to AGI #1. AGI #1 workover 5-22 thru 6-8. AGI #2 experi
	2017	May-17	1596	103	3 203	155	1390	)		1842	266	104	4 49 150	17	
	2017	Jun-17	1439	qc	429	147	1010			1838			3 40 107	7 18	Both wells used. #2 used from 6-2 through 6-15. Work completed 6-8 and sucessful MIT performed 6-8; #1 ba 15. #1 and #2 used simultaneously from 6-15 to 6-30 Mechanical Problem with flow meter for #2 well. Only can be measured; no way to differentiate between #1. 4394 when they are used together.

Мо	nth Ende	d	-	Injection	AGI #1 Surface Casing Annulus Pressure (psig)	Total Flowrate	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	Bottom Hole	AGI #1 Average Bottom Hole Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #1 Flowrate (MSCFPH)	AGI #2 Surface Injection/Casing AGI #2 Flowrate (MSCFPH) Differential (psig)	Total CO2 Sequestered per month (Metric Ton)	Notes
July	2017	Jul-17	1409	91	302	171	1108	4392	137	, 1810	) sensor error	10	12	0 n/a	5281	Both wells used. Annular Pressure Meter for AGI #2 malfunctioning for month of July. Mechanical problem with flow meter for #2 well persists. Bottomhole sensors added to #1 Well as part of workover completed in June and began recording data on 7-20-17
August	2017		1572	99	621	187		4514	134				33 187		1064 5775	Both wells used. Mechanical problem with flow meter for #2 well persists. Only total flow data available. Annular Pressure meter for AGI #2 back in service 8-11-17. Annular Pressure and differential pressure readings are for period 8-11-17 through 8-31.
September	2017		1685	109		197	1203	4578	13-	1267			77 197			Only AGI #1 used. Entire plant shut down from Sept 19 to Sept 30th for a scheduled turnaround. Data available only for first 19 3 days of September
October	2017	Oct-17	1531	102	211	152	1321	4250	136	5 872	2 9	7 6	53 152	0	776 4694	Plant shutdown 9-19 through 10-3 for a turnaround. Only AGI #1 used during remainder of month. Major software upgrade in DCS. BH sensors not yet integrated into DCS. Only AGI #1 in use in November. BH sensors not reconnected to
November	2017		1589	101				4080	136				56 189			DCS until 11-29.
December January	2017 2018	Dec-17 Jan-18	1707 1557	99	456 160			4080	136				14 191 11 120			Only AGI #1 in use. Only AGI #1 in use.
February	2018		1557	110				4410	133							3 Only AGI #1 in use.
March	2018		1635	107				4503	133				58 188			Only AGI #1 in use.
April	2018 2018		1618 1668	95	95 141			4576 4646	131				53 223 79 226			Only AGI #1 in use. Only AGI #1 in use.
June	2018		1667	100				4615	133							7 Only AGI #1 in use.
July	2018		1690	101				4627	132							Only AGI #1 in use.
August	2018	ů.	1614	98	321			4565	131				32 157			Only AGI #1 in use.
September October	2018 2018		1581 1564	97	237			4534 4525	130				72 155 51 160			Only AGI #1 in use.
November	2018	Nov-18	1531	91	115			4529	129							l Only AGI #1 in use.
December	2018	Dec-18	1483	89	55	133	1428	4480	128	1152	2 8	5 6	59 133	0	1067 4108	3 Only AGI #1 in use.
January	2019	Jan-19	1500	95	133	143	1367	4457	129	925	5 6	8 6	i9 143	0	858 4417	7
February	2019	Feb-19	1547	98	185	169	1362	4484	129	936	5 19	4 7	73 169	0	724 4714	1
March	2019		1577	100				4511	131	442	2 23	8 7	78 182	0	161 5621	
April	2019		1689	100		216		4577	133				2 216		-215 6456	
May	2019		1753	100				4516	133						1450 6949	
ividy	2019		1/33	110		199		4310	136							
June	2019		1080	88	513	207	1167	4433	138						1528 5948 1487 6393	
July				00	5											
August	2019	Ŭ	1240	91	6	182		4224	138						1419 5621	
September	2019	Sep-19	1251	93	38	169		4171	137						1371 5051	
October	2019		1202	78	11	231	1191	4156	137						1451 7134	
November	2019	Nov-19	1179	69	19	204		4143	137				10 0		1396 6097	
December	2019	Dec-19	1156	64	15	195	1142	4116	138	1494	4 13	5 11	1 (	195	1359 6023	3
January	2020	Jan-20	1128	63	17	188	1111	4096	138	1481	1 5	4 11	10 0	188	1427 5806	5
February	2020	Feb-20	1116	63	262	191	854	4085	138	1462	2 13	7 10	07 (	191	1324 5518	Perfrom MIT on both wells adjust backside pressure
March	2020	Mar-20	1111	72	300	217	811	4085	138	1509	9 5:	9 10	09 (	217	1450 6702	2
April	2020	Apr-20	1117	74	294	228	823	4095	138	1519	9 3	5 10	9 0	228	1485 6815	5
May	2020	May-20	1126	82	300	212	825	4098	138	1501	1 10	0 10	08 0	212	1491 6548	3
June	2020	Jun-20	1140	88	323	226	817	4109	138	1500	12	7 11	17 (	226	1373 6755	5
July	2020	Jul-20	1412	109	302	219	1109	4212	139	1409	9 10	3 10	9 100	119	1307 6764	4 Switch flow from #2 to #1 16 July 9am
August	2020	Aug-20	1658	119	293	227	1364	4332	141	1113	3 18	1 9	98 227	0	932 7011	
September	2020	Sep-20	1737	123	123	241	1613	4389	143	1125	5 21	7 8	37 241	0	909 7203	3
October	2020		1715	121		219			142				79 219	0	973 6764	
November	2020		1692	114		232		4447	140						1032 6934	
December	2020		1696	114		232									1085 6548	
	2020		1707	113		212									1102 6609	
January									136							
February	2021		1694	112				4521								
March	2021		1355			229		4336								Flow switched to AGI #2 on 3/1/2021
April	2021		1279	73					138						1606 6785	
May	2021		1254	80		220			139						1582 6795	
June	2021		1236	88	196				139						1479 6605	
July	2021	Jul-21	1225	88				4187	139			3 11	.6 0	237	1545 7320	
August	2021	Aug-21	1341	84	266	189	1075	4167	139	1558	8 14	3 11	0 0	189	1415 5837	7
September	2021	Sep-21	1569	79	314	214	1255	4145	139	1552	2 35	6 11	2 0	214	1197 6396	5
October	2021	Oct-21	1518	72	305	224	1213	4140	139	1574	4 30	2 11	4 (	224	1272 6918	3

Мо	nth Ende	d		Injection	AGI #1 Surface Casing Annulus Pressure (psig)	Total Flowrate (MSCFPH)	AGI #1 Surface Injection/Casing Annular Pressure Differential (psig)	Bottom Hole	AGI #1 Average Bottom Hole Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	AGI #2 Surface TAG Injection Temperature (°F)			AGI #2 Surface Injection/Casing Annular Pressure Differential (psig)	Total CO2 Sequestered per month (Metric Ton)	Notes
November	2021	Nov-21	1440	61	1 295	214	1145	5 4133	139	151	2 9	0 10	9 0	214	1422	6396	5
December	2021	Dec-21	1402	61	1 291	218	1111	4129	139	150	0 5	6 10	8 0	218	1444	6733	8
January	2022	Jan-22	1162	60	278	192	885	5 4116	139	148	6 7	1 10	8 0	192	1415	5930	
February	2022	Feb-22	1466	106	5 210	183	1256	5 4262	134	123	0 14	2 6	3 180	3	1089	5105	Flow switched to AGI #1 on 2/1/2022
March	2022	Mar-22	1557	110	292	218	1265	i 4319	130	5 111	8 21	0 7	1 218	0	908	6733	8
April	2022	Apr-22	1623	113	3 195	226	1429	4361	138	3 112	7 18	4 8	1 226	0	943	6755	5
May	2022	May-22	1563	107	7 104	180	1459	4334	13	7 115	0 18	6 9	0 180	0	964	5559	)
June	2022	Jun-22	1535	106	5 89	198	1446	5 4328	13	5 116	9 18	0 9	5 198	0	989	5918	3
July	2022	Jul-22	1633	110	94	218	1538	3 4417	130	5 122	3 17	8 9	9 218	0	1045	6733	3
August	2022	Aug-22	1647	106	5 77	220	1570	4478	13	5 125	3 21	3 9	5 220	0	1041	6795	
September	2022	Sep-22	1647	106	5 80	199	1567	7 4499	134	128	0 27	6 9	4 199	0	1004	5948	3
October	2022	Oct-22	1598	102	2 61	174	1537	7 4493	132	2 126	5 23	1 8	0 174	0	1034	5374	
November	2022	Nov-22	1652	108	8 51	186	1601	4508	134	126	0 20	8 6	4 186	0	1052	5559	)
December	2022	Dec-22	1656	105	5 53	190	1604	4539	133	3 128	8 18	8 6	3 190	0	1100	5868	3
January	2023	Jan-23	1662	106	5 53	187	1609	4549	133	3 129	4 17	9 6	2 187	0	1115	5557	7
February	2023	Feb-23	1640	105	5 75	168	1565	4533	133	3 129	4 25	8 6	3 168	0	1036	4669	}
March	2023	Mar-23	1628	104	4 45	169	1583	4536	132	2 129	1 33	9 7	1 169	0	951	5210	)
April	2023	Apr-23	1612	101	1 39	170	1572	2 4534	13:	129	7 33	9 7	7 170	0	958	5083	3
May	2023	May-23	1587	99	9 52	144	1535	5 4511	132	2 131	1 34	3 8	7 144	0	968	4243	3
June	2023	Jun-23	1597	101	1 73	162	1523	4509	133	2 131	3 34	6 9	6 154	9	966	4863	3
July	2023	Jul-23	1349	90	37	157	1312	4331	13	7 151	7 4	0 10	6 0	157	1476	4864	
August	2023	Aug-23	1286	88	8 45	163	1241	4260	138	3 147	3	3 10	2 0	163	1470	5005	;
September	2023	Sep-23	1250	83	3 53	160	1197	7 4226	138	3 142	0	2 9	8 0	160	1418	4749	
October	2023	Oct-23	1224	73	3 60	151	1164	4190	138	3 142	6 1	2 10	2 0	151	1414	4483	3
November	2023	Nov-23	1199	65	5 152	139	1048	3 4162	138	3 139	4 7	7 10	2 0	139	1316	4148	3
December	2023	Dec-23	1174	63	3 67	151	1107	4136	138	3 140	3 4	1 10	3 0	151	1363	4658	3
Average for 202	23		1434		63	160	1371		13				9 83	78	1204		
Standard Devia	tion 2023		192	15	5 29	12	204	163	1	3 7	6 14	4 1	6 83	76	213	382	
Average for En			1526.7	104.9	9 254.5	180.8	1271.6	5 4351.1	135.0	5 1201.	2 141.	8 86.	2 135.7	43.8	1050.5	5477	
Standard Devia	tion Entire	Period	168.2	17.8	8 231.6	28.5	257.6	5 173.6	3.4	478.	5 115.	1 21.	7 74.5	80.1	478.9	883	
OPERATIN	G CONS	TRAINTS	BASED ON NM	OCC ORDER AND	ACO-275										Total for 2023 <sup>1</sup> (metric ton)	57530	
MAOP in NMO	CC Order is	2,644 psig												Total	for Entire Period <sup>2</sup> (metric ton)	766811	L
														2023 Car	bon credit in USD (at \$85/ton)	\$ 4,890,074.66	

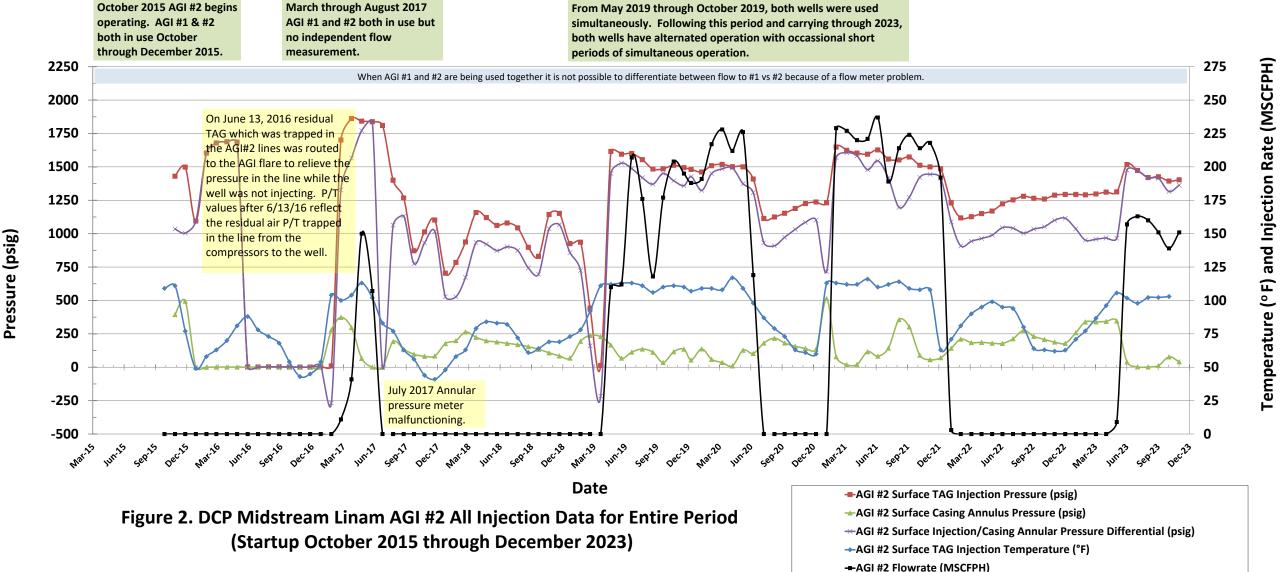
<sup>1</sup> - Based on data from Ron Tabery, 180- day trend from 4/4/23

<sup>2</sup> - Assumes a stream of 80% CO2

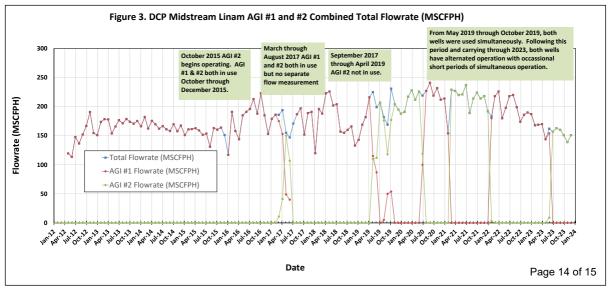


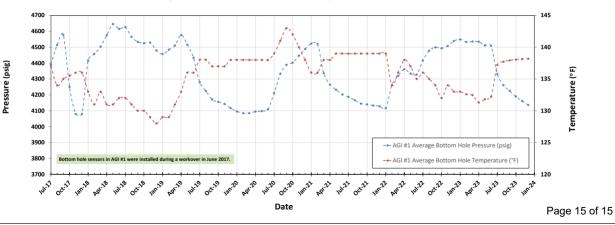
Pressure (psig)

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### Figure 4. Bottom Hole Pressure and Temperature - AGI #1

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III

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District IV 1220 S. St Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3470 Fax: (505) 476-3462

**State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
DCP OPERATING COMPANY, LP	36785
6900 E. Layton Ave	Action Number:
Denver, CO 80237	310102
	Action Type:
	[C-103] Sub. General Sundry (C-103Z)

## CONDITIONS

Created By		Condition Date
anthony.harris	None	2/2/2024

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Action 310102