Form 3160-5 (June 2019)

UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

BUR	EAU OF LAND MANAGEMENT	5. L	5. Lease Serial No. NMNM108503			
Do not use this t	IOTICES AND REPORTS ON W form for proposals to drill or to Use Form 3160-3 (APD) for suc		6. If Indian, Allottee or Tribe Name			
SUBMIT IN	TRIPLICATE - Other instructions on pag	7. If	Unit of CA/Agree	ement, N	Name and/or No.	
1. Type of Well Oil Well Gas W	Vell Other		8. W	ell Name and No.	ANTER	RO 14 FED COM/741H
2. Name of Operator EOG RESOURG	CES INCORPORATED		9. A	PI Well No. 30-02	25-5181	11
	BY 2, HOUSTON, TX 77(3b. Phone No. (713) 651-70	(include area code,) 10.1	Field and Pool or I	Explorat	tory Area
4. Location of Well (Footage, Sec., T., R SEC 14/T25S/R33E/NMP			11. 0	Country or Parish,		VE SFIXING
	CV THE ADDDODDIATE DOV(ES) TO IN	DICATE MATURE			IED DA	TA
	CK THE APPROPRIATE BOX(ES) TO IN				1EK DA	IIA
TYPE OF SUBMISSION			PE OF ACTION			W
Notice of Intent	Acidize Deep Alter Casing Hydr	raulic Fracturing	Reclamati	n (Start/Resume)	=	Water Shut-Off Well Integrity
Cubecoment Demont		Construction	Recomple		=	Other
Subsequent Report		and Abandon	Temporar	ily Abandon		
Final Abandonment Notice	Convert to Injection Plug	Back	Water Dis	posal		
completion of the involved operation completed. Final Abandonment Notice is ready for final inspection.) Antero 14 Fed Com 101H (FK EOG respectfully requests an Change name from Antero 14 Change SHL from T-25-S, R-3 to T-25-S, R-33-E, Sec 14, 26. Change BHL from T-25-S, R-3 to T-25-S, R-33-E, Sec 11, 100 Continued on page 3 additional	amendment to our approved APD for the Fed Com 741H to Antero 14 Fed Com 63-E, Sec 14, 2639' FNL, 531' FWL, Lea 28' FNL, 1271' FWL, Lea Co., N.M. 33-E, Sec 11, 100' FNL, 787' FWL, Lea Co' FNL, 1600' FWL, Lea Co., N.M.	is well to reflect the control of th	letion in a new ination, have been ation, have been the following characters.	interval, a Form 3 n completed and t	160-4 m	ust be filed once testing has been
STAR HARRELL / Ph: (432) 848-9	, , , , , , , , , , , , , , , , , , , ,	Regulatory	/ Specialist			
Signature (Electronic Submission	on)	Date		01/30/20	024	
	THE SPACE FOR FED	ERAL OR STA	ATE OFICE	USE		
Approved by						
CHRISTOPHER WALLS / Ph: (575	5) 234-2234 / Approved	Petro Title	leum Enginee		Date	02/15/2024
	hed. Approval of this notice does not warran equitable title to those rights in the subject le duct operations thereon.		RLSBAD	'		
Tid- 10 H C C Cti 1001 1 Tid- 4	2 II C C C+: 1212			4 1 4 1-		-4

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

DISTRICT I

1625 N. French Dr., Hobbs, NM 88240
Phone: (575) 393-0161 Fax: (575) 393-0720

DISTRICT II

81 I S. First St., Artesin, NM 88210
Phone: (575) 748-9720

DISTRICT III

1000 Rio Brazos Rd., Aztec, NM 87410
Phone: (505) 334-6178 Fax: (505) 334-6170

DISTRICT IV

1220 S. St. Francis Dr., Santa Fe, NM 87505
Phone: (505) 476-3460 Fax: (505) 476-3462

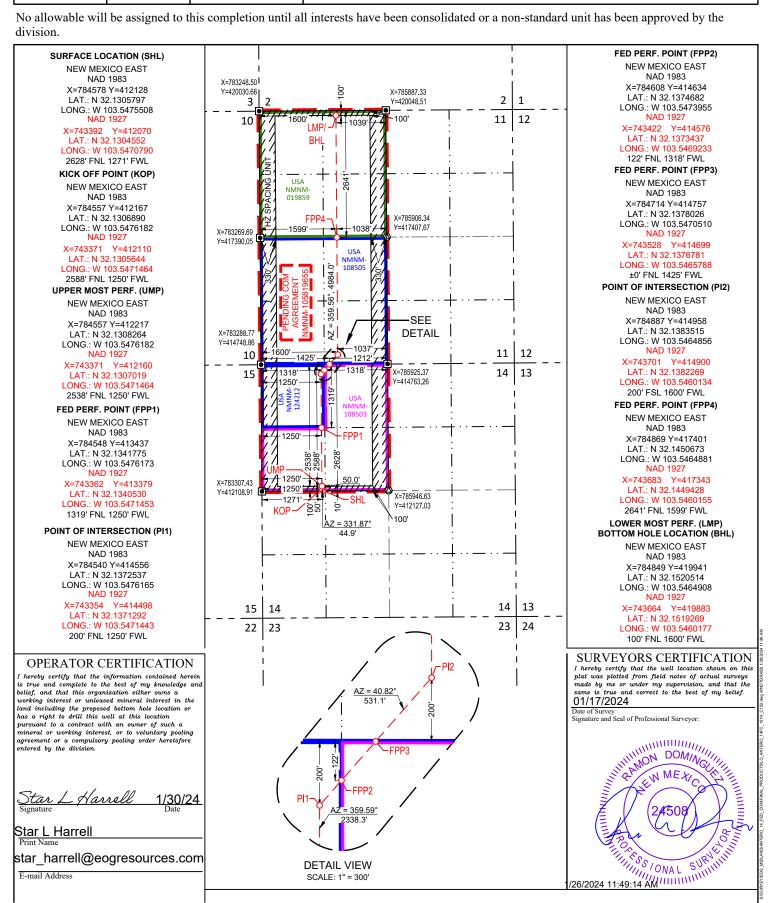
State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, New Mexico 87505

Form C-102
Revised August 1, 2011
Submit one copy to appropriate
District Office

☐ AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

1	PI Number 80-025-51	811	1	Pool Code 51020		Pool Name Red Hills; Lower Bone Spring				
Property Coo			_		Property Name			Well Num	iber	
326481				Α	NTERO 14 FE	ED COM		10)1H	
OGRID N	lo.				Operator Name			Elevatio	on	
7377	,			EC	G RESOURC	ES, INC.		33	57'	
	Surface Location									
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County	
Е	14	25-S	33-E	-	2628'	28' NORTH 1271'		WEST	LEA	
			Bottom Ho	le Locatio	n If Different F	From Surface		•		
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County	
С	11	25-S	33-E	-	100'	NORTH	WEST	LEA		
Dedicated Acres	Joint or I	nfill	Consolidated Code	Orde	er No.	-				
480.00			PENDING COM AGREEMENT: NMNM-105819655							





Revised Permit Information 01/11/2024:

Well Name: Antero 14 Fed Com 101H

Location: SHL: 2628' FNL & 1271' FWL, Section 14, T-25-S, R-33-E, Lea Co., N.M.

BHL: 100' FNL & 1600' FWL, Section 11, T-25-S, R-33-E, Lea Co., N.M.

1. CASING PROGRAM A:

Hole	Interv	al MD	Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
16"	0	1,250	0	1,250	13-3/8"	54.5#	J-55	STC
11"	0	4,990	0	4,990	9-5/8"	40#	J-55	LTC
6-3/4"	0	17,108	0	9,490	5-1/2"	20#	P110-EC	DWC/C IS MS

Variance is requested to waive the centralizer requirements for the 9-5/8" casing in the 11" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 11" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

2. CEMENTING PROGRAM:

Depth	No. Sacks	Wt.	Yld Ft3/sk	Slurry Description
1,250' 13-3/8"	330	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake (TOC @ Surface)
	160	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1,050')
4,990' 9-5/8''	480	12.7	2.22	Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	170	14.8	1.32	Tail: Class C + 10% NaCL + 3% MagOx (TOC @ 3,990')
17,108' 5-1/2''	320	10.5	3.21	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,490')
	580	13.2	1.52	Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 9020')



Additive	Purpose				
Bentonite Gel	Lightweight/Lost circulation prevention				
Calcium Chloride	Accelerator				
Cello-flake	Lost circulation prevention				
Sodium Metasilicate	Accelerator				
MagOx	Expansive agent				
Pre-Mag-M	Expansive agent				
Sodium Chloride	Accelerator				
FL-62	Fluid loss control				
Halad-344	Fluid loss control				
Halad-9	Fluid loss control				
HR-601	Retarder				
Microbond	Expansive Agent				

Note: Cement volumes based on bit size plus at least 25% excess in the open hole plus 10% excess in the cased-hole overlap section.

3. MUD PROGRAM:

Depth (TVD)	Type	Weight (ppg)	Viscosity	Water Loss
0 – 1,250'	Fresh - Gel	8.6-8.8	28-34	N/c
1,250' – 4,990'	Brine	9.0-10.5	28-34	N/c
4,990' – 17,108'	Oil Base	8.8-9.5	58-68	N/c - 6

4. VARIANCE REQUESTS:

EOG requests the additional variance(s) in the attached document(s):

- Break-test BOP
- Offline Cementing
- Salt Section Annular Clearance



5. TUBING REQUIREMENTS

EOG respectively requests an exception to the following NMOCD rule:

• 19.15.16.10 Casing AND TUBING RQUIREMENTS:

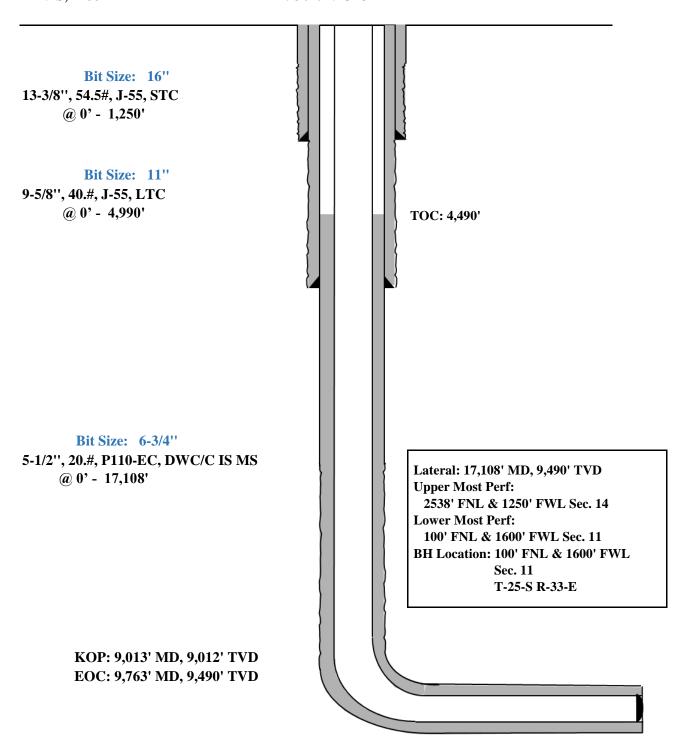
J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.

2628' FNL Revised Wellbore A: KB: 3382'
1271' FWL GL: 3357'

Section 14

T-25-S, R-33-E API: 30-025-51811





Revised Permit Information 01/11/2024:

Well Name: Antero 14 Fed Com 101H

Location: SHL: 2628' FNL & 1271' FWL, Section 14, T-25-S, R-33-E, Lea Co., N.M.

BHL: 100' FNL & 1600' FWL, Section 11, T-25-S, R-33-E, Lea Co., N.M.

1. CASING PROGRAM B:

Hole	Interv	al MD	Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
13-1/2"	0	1,250	0	1,250	10-3/4"	40.5#	J-55	STC
9-7/8"	0	4,990	0	4,990	8-5/8"	32#	J-55	BTC-SC
6-3/4"	0	17,108	0	9,490	5-1/2"	20#	P110-EC	DWC/C IS MS

Variance is requested to waive the centralizer requirements for the 8-5/8" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues.

2. CEMENTING PROGRAM:

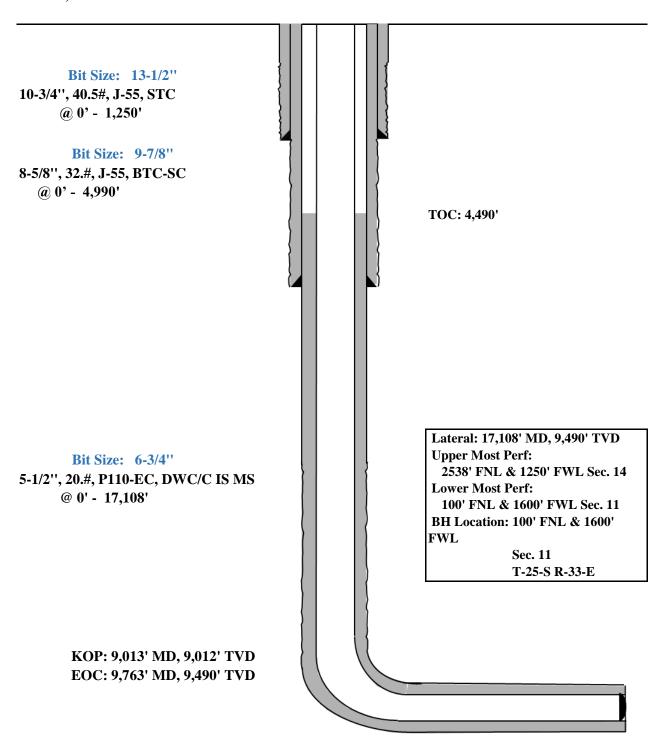
		Wt.	Yld	
Depth	No. Sacks		Ft3/sk	Slurry Description
1,250' 10-3/4''	410	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello- Flake (TOC @ Surface)
	110	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium Metasilicate (TOC @ 1,050')
4,990' 8-5/8"	390	12.7	2.22	Lead: Class C + 10% NaCl + 6% Bentonite Gel + 3% MagOx (TOC @ Surface)
	640	14.8	1.32	Tail: Class C + 10% NaCL + 3% MagOx (TOC @ 3,990')
17,108' 5-1/2"	430	10.5	3.21	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC @ 4,490')
	800	13.2	1.52	Tail: Class H + 5% NEX-020 + 0.2% NAC-102 + 0.15% NAS-725 + 0.5% NFL-549 + 0.2% NFP-703 + 1% NBE-737 + 0.3% NRT-241 (TOC @ 9020')



2628' Revised Wellbore B: KB: 3382'
1271' GL: 3357'

Section 14

T-25-S, R-33-E API: 30-025-51811





GEOLOGIC NAME OF SURFACE FORMATION:

Permian

ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

Rustler	1,150'
Tamarisk Anhydrite	1,225'
Top of Salt	1,500'
Base of Salt	4,890'
Lamar	5,065'
Bell Canyon	5,080'
Cherry Canyon	6,121'
Brushy Canyon	7,685'
Bone Spring Lime	9,240'
Leonard (Avalon) Shale	9,280'
1st Bone Spring Sand	10,215'
2nd Bone Spring Shale	10,440'
2nd Bone Spring Sand	10,810'
3rd Bone Spring Carb	11,270'
3rd Bone Spring Sand	11,875'
TD	9,490'

ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

MATED DEFINS OF ANTICIPATE	D F KESH W	AIEK, OIL O
Upper Permian Sands	0-400'	Fresh Water
Bell Canyon	5,080'	Oil
Cherry Canyon	6,121'	Oil
Brushy Canyon	7,685'	Oil
Leonard (Avalon) Shale	9,280'	Oil
1st Bone Spring Sand	10,215'	Oil
2nd Bone Spring Shale	10,440'	Oil
2nd Bone Spring Sand	10,810'	Oil



Midland

Lea County, NM (NAD 83 NME) Antero 14 Fed Com #101H

OH

Plan: Plan #0.2

Standard Planning Report

29 January, 2024



Planning Report

PEDM Database:

Company: Midland Project: Lea County, NM (NAD 83 NME)

Antero 14 Fed Com Site:

Well: #101H Wellbore: OH Plan #0.2 Design:

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

Minimum Curvature

Project Lea County, NM (NAD 83 NME)

US State Plane 1983 Map System: North American Datum 1983 Geo Datum: New Mexico Eastern Zone Map Zone:

System Datum:

Mean Sea Level

Antero 14 Fed Com Site

Northing: 412,174.00 usft Site Position: Latitude: 32° 7' 50.590 N From: Мар Easting: 783,931.00 usft Longitude: 103° 32' 58.705 W

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 "

Well #101H

Well Position +N/-S 0.0 usft Northing: 412,128.00 usft Latitude: 32° 7' 50.088 N +E/-W 0.0 usft Easting: 784,578.00 usft Longitude: 103° 32' 51.185 W 3,357.0 usft

Position Uncertainty 0.0 usft Wellhead Elevation: usft **Ground Level:**

0.42° **Grid Convergence:**

ОН Wellbore

Model Name Declination Field Strength Magnetics Sample Date Dip Angle (°) (°) (nT) 47,270.27480580 IGRF2020 5/1/2023 6.31 59.76

Design Plan #0.2

Audit Notes:

Phase: PLAN Tie On Depth: 0.0 Version:

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°) 0.0 0.0 0.0 1.99

Plan Survey Tool Program Date 1/29/2024

Depth From Depth To

(usft) (usft) Survey (Wellbore) **Tool Name** Remarks

17,107.9 EOG MWD+IFR1 0.0 Plan #0.2 (OH)

MWD + IFR1



Planning Report

Database: Company:

Project:

PEDM Midland

Lea County, NM (NAD 83 NME)

Site: Antero 14 Fed Com

 Well:
 #101H

 Wellbore:
 OH

 Design:
 Plan #0.2

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,470.0	0.00	0.00	1,470.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,490.7	0.41	331.70	1,490.7	0.1	0.0	2.00	2.00	0.00	331.70	
7,611.5	0.41	331.70	7,611.3	38.9	-21.0	0.00	0.00	0.00	0.00	
7,632.2	0.00	0.00	7,632.0	39.0	-21.0	2.00	-2.00	0.00	180.00	
9,012.7	0.00	0.00	9,012.5	39.0	-21.0	0.00	0.00	0.00	0.00	KOP(Antero 14 Fed C
9,233.1	26.46	0.00	9,225.2	89.0	-21.0	12.00	12.00	0.00	0.00	FTP(Antero 14 Fed C
9,762.6	90.00	359.53	9,489.9	516.4	-23.4	12.00	12.00	-0.09	-0.53	
10,555.2	90.00	359.53	9,490.0	1,309.0	-30.0	0.00	0.00	0.00	0.00	Fed Perf 1(Antero 14
11,174.3	90.00	358.99	9,490.0	1,928.0	-38.0	0.09	0.00	-0.09	-89.17	
11,484.5	90.00	17.61	9,490.0	2,233.6	6.6	6.00	0.00	6.00	90.01	
12,324.3	90.00	17.61	9,490.0	3,034.1	260.6	0.00	0.00	0.00	0.00	
12,624.8	90.00	359.58	9,490.0	3,330.0	305.3	6.00	0.00	-6.00	-90.00	
14,567.9	90.00	359.58	9,490.0	5,273.0	291.0	0.00	0.00	0.00	0.00	Fed Perf 4(Antero 14
17,107.9	90.00	359.52	9,490.0	7,813.0	271.0	0.00	0.00	0.00	-90.00	PBHL(Antero 14 Fed

beog resources

Planning Report

Database: PEDM Company: Midland

Company: Midland
Project: Lea County, NM (NAD 83 NME)

Site: Antero 14 Fed Com

 Well:
 #101H

 Wellbore:
 OH

 Design:
 Plan #0.2

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

Design.	F Id II #U.Z								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
0.008	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,470.0	0.00	0.00	1,470.0	0.0	0.0	0.0	0.00	0.00	0.00
1,490.7	0.41	331.70	1,490.7	0.1	0.0	0.1	2.00	2.00	0.00
1,500.0	0.41	331.70	1,500.0	0.1	-0.1	0.1	0.00	0.00	0.00
1,600.0	0.41	331.70	1,600.0	0.8	-0.4	0.7	0.00	0.00	0.00
1,700.0	0.41	331.70	1,700.0	1.4	-0.4	1.4	0.00	0.00	0.00
1,800.0	0.41	331.70	1,800.0	2.0	-1.1	2.0	0.00	0.00	0.00
1,900.0	0.41	331.70	1,900.0	2.7	-1.4	2.6	0.00	0.00	0.00
2,000.0	0.41	331.70	2,000.0	3.3	-1.8	3.2	0.00	0.00	0.00
2,100.0	0.41	331.70	2,100.0	3.9	-2.1	3.9	0.00	0.00	0.00
2,200.0	0.41	331.70	2,200.0	4.6	-2.5	4.5	0.00	0.00	0.00
2,300.0	0.41	331.70	2,300.0	5.2	-2.8	5.1	0.00	0.00	0.00
2,400.0	0.41	331.70	2,400.0	5.8	-3.1	5.7	0.00	0.00	0.00
2,500.0	0.41	331.70	2,500.0	6.5	-3.5	6.4	0.00	0.00	0.00
2,600.0	0.41	331.70	2,600.0	7.1	-3.8	7.0	0.00	0.00	0.00
2,700.0	0.41	331.70	2,700.0	7.7	-4.2	7.6	0.00	0.00	0.00
2,800.0	0.41	331.70	2,800.0	8.4	-4.5	8.2	0.00	0.00	0.00
2,900.0	0.41	331.70	2,900.0	9.0	-4.9	8.8	0.00	0.00	0.00
3,000.0	0.41	331.70	3,000.0	9.7	-5.2	9.5	0.00	0.00	0.00
3,100.0	0.41	331.70	3,100.0	10.3	-5.5	10.1	0.00	0.00	0.00
3,200.0	0.41	331.70	3,200.0	10.9	-5.9	10.7	0.00	0.00	0.00
3,300.0	0.41	331.70	3,300.0	11.6	-6.2	11.3	0.00	0.00	0.00
3,400.0		331.70		12.2		12.0	0.00	0.00	0.00
	0.41		3,400.0		-6.6				
3,500.0	0.41	331.70	3,499.9	12.8	-6.9	12.6	0.00	0.00	0.00
3,600.0	0.41	331.70	3,599.9	13.5	-7.2	13.2	0.00	0.00	0.00
3,700.0	0.41	331.70	3,699.9	14.1	-7.6	13.8	0.00	0.00	0.00
3,800.0	0.41	331.70	3,799.9	14.7	-7.9	14.4	0.00	0.00	0.00
3,900.0	0.41	331.70	3,899.9	15.4	-8.3	15.1	0.00	0.00	0.00
4,000.0	0.41	331.70	3,999.9	16.0	-8.6	15.7	0.00	0.00	0.00
4,100.0	0.41	331.70	4,099.9	16.6	-9.0	16.3	0.00	0.00	0.00
4,200.0	0.41	331.70	4,199.9	17.3	-9.3	16.9	0.00	0.00	0.00
4,300.0	0.41	331.70	4,299.9	17.9	-9.6	17.6	0.00	0.00	0.00
4,400.0	0.41	331.70	4,399.9	18.5	-10.0	18.2	0.00	0.00	0.00
4,500.0	0.41	331.70	4,499.9	19.2	-10.3	18.8	0.00	0.00	0.00
4,600.0	0.41	331.70	4,599.9	19.8	-10.7	19.4	0.00	0.00	0.00
4,700.0	0.41	331.70	4,699.9	20.4	-11.0	20.1	0.00	0.00	0.00
4,800.0	0.41	331.70	4,799.9	21.1	-11.4	20.7	0.00	0.00	0.00
4,900.0	0.41	331.70	4,899.9	21.7	-11.7	21.3	0.00	0.00	0.00
5,000.0	0.41	331.70	4,999.9	22.4	-12.0	21.9	0.00	0.00	0.00
5,100.0	0.41	331.70	5,099.9	23.0	-12.4	22.5	0.00	0.00	0.00

eog resources

Planning Report

Database: F Company: N

Project:

PEDM Midland

Lea County, NM (NAD 83 NME)

Site: Antero 14 Fed Com

 Well:
 #101H

 Wellbore:
 OH

 Design:
 Plan #0.2

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

Design:	Plan #0.2								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,200.0	0.41	331.70	5,199.9	23.6	-12.7	23.2	0.00	0.00	0.00
5,300.0	0.41	331.70	5,299.9	24.3	-13.1	23.8	0.00	0.00	0.00
5,400.0	0.41	331.70	5,399.9	24.9	-13.4	24.4	0.00	0.00	0.00
5,500.0	0.41	331.70	5,499.9	25.5	-13.7	25.0	0.00	0.00	0.00
5,600.0	0.41	331.70	5,599.9	26.2	-14.1	25.7	0.00	0.00	0.00
5,700.0	0.41	331.70	5,699.9	26.8	-14.4	26.3	0.00	0.00	0.00
5,800.0	0.41	331.70	5,799.9	27.4	-14.8	26.9	0.00	0.00	0.00
5,900.0	0.41	331.70	5,899.9	28.1	-15.1	27.5	0.00	0.00	0.00
6,000.0	0.41	331.70	5,999.9	28.7	-15.5	28.1	0.00	0.00	0.00
6,100.0	0.41	331.70	6,099.9	29.3	-15.8	28.8	0.00	0.00	0.00
6,200.0	0.41	331.70	6,199.9	30.0	-16.1	29.4	0.00	0.00	0.00
6,300.0	0.41	331.70	6,299.9	30.6	-16.5	30.0	0.00	0.00	0.00
6,400.0	0.41	331.70	6,399.9	31.2	-16.8	30.6	0.00	0.00	0.00
6,500.0	0.41	331.70	6,499.9	31.9	-17.2	31.3	0.00	0.00	0.00
6,600.0	0.41	331.70 331.70	6,599.9	32.5	-17.5 -17.8	31.9 32.5	0.00	0.00	0.00
6,700.0	0.41		6,699.9	33.1			0.00	0.00	0.00
6,800.0	0.41	331.70	6,799.9	33.8	-18.2	33.1	0.00	0.00	0.00
6,900.0	0.41	331.70	6,899.9	34.4	-18.5	33.8	0.00	0.00	0.00
7,000.0	0.41	331.70	6,999.9	35.1	-18.9	34.4	0.00	0.00	0.00
7,100.0 7,200.0	0.41 0.41	331.70 331.70	7,099.9 7,199.9	35.7 36.3	-19.2 -19.6	35.0 35.6	0.00 0.00	0.00 0.00	0.00 0.00
7,300.0	0.41	331.70	7,299.8	37.0	-19.9	36.2	0.00	0.00	0.00
7,400.0	0.41	331.70	7,399.8	37.6	-20.2	36.9	0.00	0.00	0.00
7,500.0 7,600.0	0.41 0.41	331.70 331.70	7,499.8 7,599.8	38.2 38.9	-20.6 -20.9	37.5 38.1	0.00 0.00	0.00 0.00	0.00 0.00
7,600.0	0.41	331.70	7,611.3	38.9	-20.9	38.2	0.00	0.00	0.00
7,632.2 7,700.0	0.00	0.00 0.00	7,632.0 7,699.8	39.0 39.0	-21.0 -21.0	38.2 38.2	2.00 0.00	-2.00 0.00	0.00
7,700.0	0.00 0.00	0.00	7,799.8	39.0	-21.0 -21.0	38.2	0.00	0.00	0.00 0.00
7,900.0	0.00	0.00	7,899.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,000.0	0.00	0.00	7,999.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,100.0	0.00	0.00	8,099.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,200.0	0.00	0.00	8,199.8	39.0	-21.0 -21.0	38.2	0.00	0.00	0.00
8,300.0	0.00	0.00	8,299.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,400.0	0.00	0.00	8,399.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,500.0	0.00	0.00	8,499.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,600.0	0.00	0.00	8,599.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,700.0	0.00	0.00	8,699.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,800.0	0.00	0.00	8,799.8	39.0	-21.0	38.2	0.00	0.00	0.00
8,900.0	0.00	0.00	8,899.8	39.0	-21.0	38.2	0.00	0.00	0.00
9,000.0	0.00	0.00	8,999.8	39.0	-21.0	38.2	0.00	0.00	0.00
9,012.7	0.00	0.00	9,012.5	39.0	-21.0	38.2	0.00	0.00	0.00
9,025.0	1.48	0.00	9,024.8	39.2	-21.0	38.4	12.00	12.00	0.00
9,050.0	4.48	0.00	9,049.8	40.5	-21.0	39.7	12.00	12.00	0.00
9,075.0	7.48	0.00	9,074.7	43.1	-21.0	42.3	12.00	12.00	0.00
9,100.0	10.48	0.00	9,099.4	47.0	-21.0	46.2	12.00	12.00	0.00
9,125.0	13.48	0.00	9,123.8	52.2	-21.0	51.4	12.00	12.00	0.00
9,150.0	16.48	0.00	9,148.0	58.6	-21.0	57.9	12.00	12.00	0.00
9,175.0	19.48	0.00	9,171.7	66.3	-21.0	65.6	12.00	12.00	0.00
9,200.0	22.48	0.00	9,195.1	75.3	-21.0	74.5	12.00	12.00	0.00
9,225.0	25.48	0.00	9,217.9	85.4	-21.0	84.7	12.00	12.00	0.00
9,233.1	26.46	0.00	9,225.2	89.0	-21.0	88.2	12.00	12.00	0.00
9,250.0	28.48	359.96	9,240.2	96.8	-21.0	96.0	12.00	12.00	-0.23
9,275.0	31.48	359.91	9,261.8	109.3	-21.0	108.5	12.00	12.00	-0.20

beog resources

Planning Report

Database: Company:

Project:

PEDM Midland

Lea County, NM (NAD 83 NME)

Site: Antero 14 Fed Com

 Well:
 #101H

 Wellbore:
 OH

 Design:
 Plan #0.0

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

Design:	Plan #0.2								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,300.0	34.48	359.87	9,282.8	122.9	-21.0	122.1	12.00	12.00	-0.17
9,325.0	37.48	359.83	9,303.0	137.6	-21.1	136.8	12.00	12.00	-0.14
9,350.0	40.48	359.80	9,322.5	153.3	-21.1	152.5	12.00	12.00	-0.12
9,375.0	43.48	359.77	9,341.0	170.0	-21.2	169.2	12.00	12.00	-0.11
9,400.0	46.48	359.75	9,358.7	187.7	-21.3	186.8	12.00	12.00	-0.10
9,425.0	49.48	359.73	9,375.5	206.3	-21.4	205.4	12.00	12.00	-0.09
9,450.0	52.48	359.71	9,391.2	225.7	-21.4	224.8	12.00	12.00	-0.08
9,475.0	55.48	359.69	9,405.9	245.9	-21.6	245.0	12.00	12.00	-0.08
9,500.0 9,525.0 9,550.0	58.48 61.48 64.48	359.65 359.64	9,419.5 9,432.0 9,443.4	266.9 288.5 310.8	-21.7 -21.8 -21.9	266.0 287.6 309.8	12.00 12.00 12.00	12.00 12.00 12.00	-0.07 -0.07 -0.06
9,575.0	67.48	359.62	9,453.5	333.6	-22.1	332.6	12.00	12.00	-0.06
9,600.0	70.48	359.61	9,462.5	356.9	-22.2	356.0	12.00	12.00	-0.06
9,625.0	73.48	359.60	9,470.2	380.7	-22.4	379.7	12.00	12.00	-0.05
9,650.0	76.48	359.58	9,476.7	404.9	-22.6	403.8	12.00	12.00	-0.05
9,675.0	79.48	359.57	9,481.9	429.3	-22.8	428.3	12.00	12.00	-0.05
9,700.0	82.48	359.56	9,485.8	454.0	-22.9	452.9	12.00	12.00	-0.05
9,725.0	85.48	359.54	9,488.5	478.9	-23.1	477.8	12.00	12.00	-0.05
9,750.0	88.48	359.53	9,489.8	503.8	-23.3	502.7	12.00	12.00	-0.05
9,762.6	90.00	359.53	9,489.9	516.4	-23.4	515.3	12.00	12.00	-0.05
9,800.0	90.00	359.53	9,489.9	553.8	-23.8	552.7	0.00	0.00	0.00
9,900.0	90.00	359.53	9,490.0	653.8	-24.6	652.6	0.00	0.00	0.00
10,000.0	90.00	359.53	9,490.0	753.8	-25.4	752.5	0.00	0.00	0.00
10,100.0	90.00	359.53	9,490.0	853.8	-26.2	852.4	0.00	0.00	0.00
10,200.0	90.00	359.53	9,490.0	953.8	-27.1	952.3	0.00	0.00	0.00
10,300.0	90.00	359.53	9,490.0	1,053.8	-27.9	1,052.2	0.00	0.00	0.00
10,400.0	90.00	359.53	9,490.0	1,153.8	-28.7	1,152.1	0.00	0.00	0.00
10,500.0	90.00	359.53	9,490.0	1,253.8	-29.5	1,252.0	0.00	0.00	0.00
10,555.2	90.00	359.53	9,490.0	1,309.0	-30.0	1,307.2	0.00	0.00	0.00
10,600.0	90.00	359.49	9,490.0	1,353.8	-30.4	1,351.9	0.09	0.00	-0.09
10,700.0	90.00	359.40	9,490.0	1,453.8	-31.4	1,451.8	0.09	0.00	-0.09
10,800.0	90.00	359.32	9,490.0	1,553.8	-32.5	1,551.7	0.09	0.00	-0.09
10,900.0	90.00	359.23	9,490.0	1,653.8	-33.7	1,651.6	0.09	0.00	-0.09
11,000.0	90.00	359.14	9,490.0	1,753.8	-35.2	1,751.5	0.09	0.00	-0.09
11,100.0	90.00	359.06	9,490.0	1,853.7	-36.7	1,851.4	0.09	0.00	-0.09
11,174.3	90.00	358.99	9,490.0	1,928.0	-38.0	1,925.5	0.09	0.00	-0.09
11,200.0	90.00	0.54	9,490.0	1,953.7	-38.1	1,951.2	6.00	0.00	6.00
11,250.0	90.00	3.54	9,490.0	2,003.7	-36.3	2,001.2	6.00	0.00	6.00
11,300.0	90.00	6.54	9,490.0	2,053.5	-31.9	2,051.2	6.00	0.00	6.00
11,350.0	90.00	9.54	9,490.0	2,103.0	-24.9	2,100.9	6.00	0.00	6.00
11,400.0	90.00	12.54	9,490.0	2,152.1	-15.4	2,150.2	6.00	0.00	6.00
11,450.0	90.00	15.54	9,490.0	2,200.6	-3.3	2,199.1	6.00	0.00	6.00
11,484.5	90.00	17.61	9,490.0	2,233.6	6.6	2,232.5	6.00	0.00	6.00
11,500.0	90.00	17.61	9,490.0	2,248.4	11.3	2,247.4	0.00	0.00	0.00
11,600.0	90.00	17.61	9,490.0	2,343.7	41.5	2,343.8	0.00	0.00	0.00
11,700.0	90.00	17.61	9,490.0	2,439.0	71.8	2,440.1	0.00	0.00	0.00
11,800.0	90.00	17.61	9,490.0	2,534.4	102.0	2,536.4	0.00	0.00	0.00
11,900.0	90.00	17.61	9,490.0	2,629.7	132.3	2,632.7	0.00	0.00	0.00
12,000.0	90.00	17.61	9,490.0	2,725.0	162.5	2,729.0	0.00	0.00	0.00
12,000.0	90.00	17.61	9,490.0	2,725.0	192.8	2,729.0	0.00	0.00	0.00
12,100.0	90.00	17.61	9,490.0	2,820.3	192.8	2,825.3	0.00	0.00	0.00
12,200.0	90.00	17.61	9,490.0	2,915.6	223.0	2,921.6	0.00	0.00	0.00
12,300.0	90.00	17.61	9,490.0	3,010.9	253.3	3,017.9	0.00	0.00	0.00
12,324.3	90.00	17.61	9,490.0	3,034.1	260.6	3,041.3	0.00	0.00	0.00
12,350.0	90.00	16.06	9,490.0	3,058.7	268.1	3,066.1	6.00	0.00	-6.00



Planning Report

Database: PEDM Company: Midland

Company: Midland
Project: Lea County, NM (NAD 83 NME)

Site: Antero 14 Fed Com

 Well:
 #101H

 Wellbore:
 OH

 Design:
 Plan #0.2

Local Co-ordinate Reference:

TVD Reference:
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North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

sign:	Plan #0.2								
anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
12,400.0	90.00	13.06	9,490.0	3,107.1	280.6	3,114.9	6.00	0.00	-6.00
12,450.0	90.00	10.06	9,490.0	3,156.1	290.7	3,164.2	6.00	0.00	-6.00
12,500.0	90.00	7.06	9,490.0	3,205.5	298.1	3,213.9	6.00	0.00	-6.00
12,550.0	90.00	4.06	9,490.0	3,255.3	302.9	3,263.8	6.00	0.00	-6.00
12,600.0	90.00	1.06	9,490.0	3,305.2	305.2	3,313.8	6.00	0.00	-6.00
12,624.8	90.00	359.58	9,490.0	3,330.0	305.3	3,338.5	6.00	0.00	-6.00
12,700.0	90.00	359.58	9,490.0	3,405.2	304.8	3,413.7	0.00	0.00	0.00
12,800.0	90.00	359.58	9,490.0	3,505.2	304.0	3,513.6	0.00	0.00	0.00
12,900.0	90.00	359.58	9,490.0	3,605.2	303.3	3,613.5	0.00	0.00	0.00
13,000.0	90.00	359.58	9,490.0	3,705.2	302.6	3,713.4	0.00	0.00	0.00
13,100.0	90.00	359.58	9,490.0	3,805.2	301.8	3,813.4	0.00	0.00	0.00
13,200.0	90.00	359.58	9,490.0	3,905.2	301.1	3,913.3	0.00	0.00	0.00
13,300.0	90.00	359.58	9,490.0	4,005.2	300.3	4,013.2	0.00	0.00	0.00
13,400.0	90.00	359.58	9,490.0	4,105.2	299.6	4,113.1	0.00	0.00	0.00
13,500.0	90.00	359.58	9,490.0	4,205.2	298.9	4,213.0	0.00	0.00	0.00
13,600.0	90.00	359.58	9,490.0	4,305.2	298.1	4,312.9	0.00	0.00	0.00
13,700.0	90.00	359.58	9,490.0	4,405.2	297.4	4,412.8	0.00	0.00	0.00
13,800.0	90.00	359.58	9,490.0	4,505.2	296.7	4,512.7	0.00	0.00	0.00
13,900.0	90.00	359.58	9,490.0	4,605.2	295.9	4,612.7	0.00	0.00	0.00
14,000.0	90.00	359.58	9,490.0	4,705.2	295.2	4,712.6	0.00	0.00	0.00
14,100.0	90.00	359.58	9,490.0	4,805.2	294.4	4,812.5	0.00	0.00	0.00
14,200.0	90.00	359.58	9,490.0	4,905.2	293.7	4,912.4	0.00	0.00	0.00
14,300.0	90.00	359.58	9,490.0	5,005.2	293.0	5,012.3	0.00	0.00	0.00
14,400.0	90.00	359.58	9,490.0	5,105.1	292.2	5,112.2	0.00	0.00	0.00
14,500.0	90.00	359.58	9,490.0	5,205.1	291.5	5,212.1	0.00	0.00	0.00
14,567.9	90.00	359.58	9,490.0	5,273.0	291.0	5,279.9	0.00	0.00	0.00
14,600.0	90.00	359.58	9,490.0	5,305.1	290.8	5,312.0	0.00	0.00	0.00
14,700.0	90.00	359.57	9,490.0	5,405.1	290.0	5,411.9	0.00	0.00	0.00
14,800.0	90.00	359.57	9,490.0	5,505.1	289.3	5,511.9	0.00	0.00	0.00
14,900.0	90.00	359.57	9,490.0	5,605.1	288.5	5,611.8	0.00	0.00	0.00
15,000.0	90.00	359.57	9,490.0	5,705.1	287.8	5,711.7	0.00	0.00	0.00
15,100.0	90.00	359.57	9,490.0	5,805.1	287.0	5,811.6	0.00	0.00	0.00
15,200.0	90.00	359.56	9,490.0	5,905.1	286.3	5,911.5	0.00	0.00	0.00
15,300.0	90.00	359.56	9,490.0	6,005.1	285.5	6,011.4	0.00	0.00	0.00
15,400.0	90.00	359.56	9,490.0	6,105.1	284.7	6,111.3	0.00	0.00	0.00
15,500.0	90.00	359.56	9,490.0	6,205.1	284.0	6,211.2	0.00	0.00	0.00
15,600.0	90.00	359.55	9,490.0	6,305.1	283.2	6,311.1	0.00	0.00	0.00
15,700.0	90.00	359.55	9,490.0	6,405.1	282.4	6,411.1	0.00	0.00	0.00
15,800.0	90.00	359.55	9,490.0	6,505.1	281.6	6,511.0	0.00	0.00	0.00
15,900.0	90.00	359.55	9,490.0	6,605.1	280.8	6,610.9	0.00	0.00	0.00
16,000.0	90.00	359.55	9,490.0	6,705.1	280.0	6,710.8	0.00	0.00	0.00
16,100.0	90.00	359.54	9,490.0	6,805.1	279.2	6,810.7	0.00	0.00	0.00
16,200.0	90.00	359.54	9,490.0	6,905.1	278.4	6,910.6	0.00	0.00	0.00
16,300.0	90.00	359.54	9,490.0	7,005.1	277.6	7,010.5	0.00	0.00	0.00
16,400.0	90.00	359.54	9,490.0	7,105.1	276.8	7,110.4	0.00	0.00	0.00
16,500.0	90.00	359.53	9,490.0	7,205.1	276.0	7,210.3	0.00	0.00	0.00
16,600.0	90.00	359.53	9,490.0	7,305.1	275.2	7,310.2	0.00	0.00	0.00
16,700.0	90.00	359.53	9,490.0	7,405.1	274.4	7,410.1	0.00	0.00	0.00
16,800.0	90.00	359.53	9,490.0	7,505.1	273.6	7,510.0	0.00	0.00	0.00
16,900.0	90.00	359.52	9,490.0	7,605.1	272.7	7,610.0	0.00	0.00	0.00
17,000.0	90.00	359.52	9,490.0	7,705.1	271.9	7,709.9	0.00	0.00	0.00
17,107.9	90.00	359.52	9,490.0	7,813.0	271.0	7,817.7	0.00	0.00	0.00



Planning Report

PEDM Database:

Company: Midland

Project: Lea County, NM (NAD 83 NME) Antero 14 Fed Com Site:

Well: #101H ОН Wellbore: Design: Plan #0.2 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well #101H

kb = 26' @ 3387.0usft kb = 26' @ 3387.0usft

Grid

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
KOP(Antero 14 Fed Con - plan hits target cen - Point	0.00 ter	0.00	9,012.5	39.0	-21.0	412,167.00	784,557.00	32° 7′ 50.475 N	103° 32' 51.426 W
FTP(Antero 14 Fed Com - plan hits target cen - Point	0.00 ter	0.00	9,225.2	89.0	-21.0	412,217.00	784,557.00	32° 7' 50.970 N	103° 32' 51.422 W
PI2(Antero 14 Fed Com - plan misses target - Point	0.00 center by 107	0.00 9usft at 1214	9,490.0 14.4usft MD	2,830.0 (9490.0 TVD,	309.0 2862.6 N, 200	414,958.00 6.2 E)	784,887.00	32° 8′ 18.069 N	103° 32' 47.351 W
PI1(Antero 14 Fed Com - plan misses target - Point	0.00 center by 101	0.00 3usft at 1165	9,490.0 56.3usft MD	2,428.0 (9490.0 TVD,	-38.0 2397.4 N, 58.	414,556.00 5 E)	784,540.00	32° 8′ 14.117 N	103° 32' 51.421 W
PBHL(Antero 14 Fed Co - plan hits target cen - Point	0.00 ter	0.00	9,490.0	7,813.0	271.0	419,941.00	784,849.00	32° 9' 7.380 N	103° 32' 47.370 W
Fed Perf 2(Antero 14 Fe - plan hits target cen - Point	0.00 ter	0.00	9,490.0	2,506.0	93.0	414,634.00	784,671.00	32° 8′ 14.879 N	103° 32' 49.891 W
Fed Perf 1(Antero 14 Fe - plan hits target cen - Point	0.00 ter	0.00	9,490.0	1,309.0	-30.0	413,437.00	784,548.00	32° 8' 3.043 N	103° 32' 51.423 W
Fed Perf 4(Antero 14 Fe - plan hits target cen - Point	0.00 ter	0.00	9,490.0	5,273.0	291.0	417,401.00	784,869.00	32° 8' 42.245 N	103° 32' 47.353 W
Fed Perf 3(Antero 14 Fe - plan hits target cen - Point	0.00 ter	0.00	9,490.0	2,629.0	132.1	414,757.00	784,710.10	32° 8′ 16.093 N	103° 32' 49.426 W



1500

2100

2400

2700-

3000

3600-

4200

ু 4800-ই 4800-

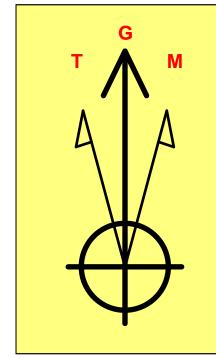
5700-

6300

6900-

7500-

8100



Azimuths to Grid North True North: -0.42° Magnetic North: 5.89°

Magnetic Field Strength: 47270.3nT Dip Angle: 59.76° Date: 5/1/2023 Model: IGRF2020

To convert a Magnetic Direction to a Grid Direction, Add 5.89° To convert a Magnetic Direction to a True Direction, Add 6.31° East To convert a True Direction to a Grid Direction, Subtract 0.42°

Lea County, NM (NAD 83 NME)

Antero 14 Fed Com #101H

Plan #0.2

PROJECT DETAILS: Lea County, NM (NAD 83 NME)

Geodetic System: US State Plane 1983
Datum: North American Datum 1983

Ellipsoid: GRS 1980
Zone: New Mexico Eastern Zone

-|-|-|-|-

System Datum: Mean Sea Level

WELL DETAILS: #101H

3357.0

kb = 26' @ 3387.0usft
Northing Easting Latittude

 Northing
 Easting
 Latittude
 Longitude

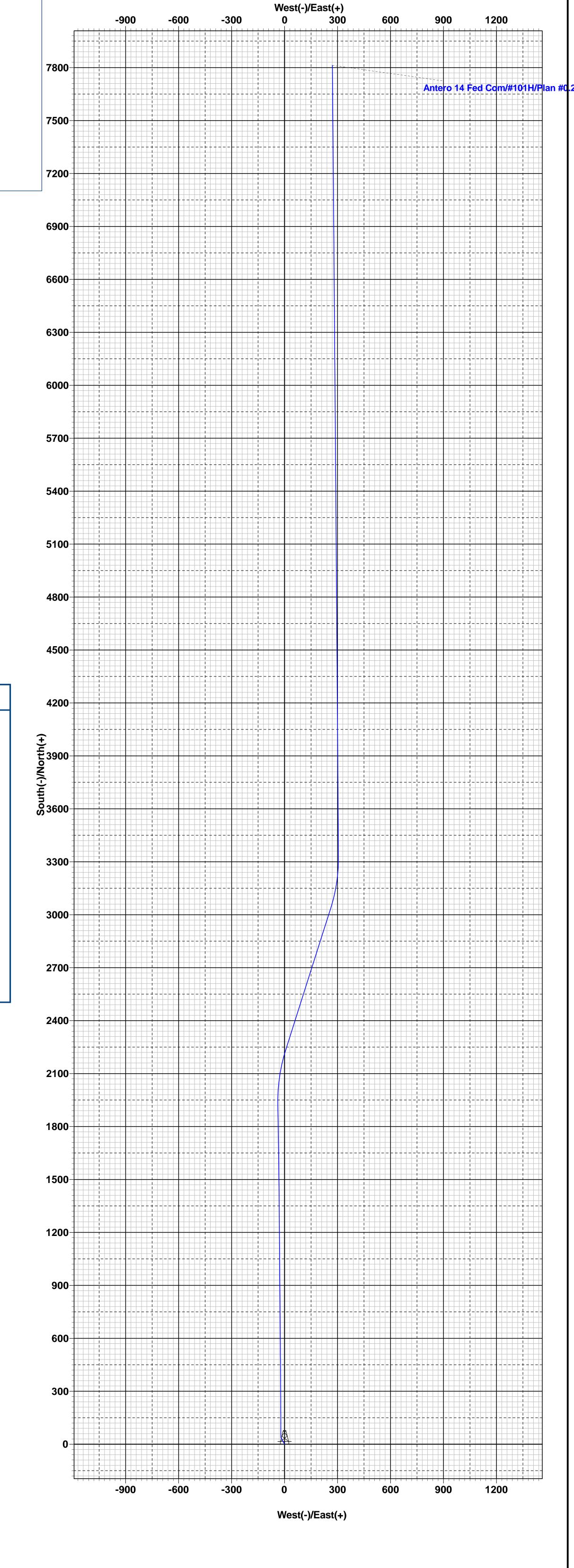
 412128.00
 784578.00
 32° 7' 50.088 N
 103° 32' 51.185 W

SECTION DETAILS										
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	1470.0	0.00	0.00	1470.0	0.0	0.0	0.00	0.00	0.0	
3	1490.7	0.41	331.70	1490.7	0.1	0.0	2.00	331.70	0.1	
4	7611.5	0.41	331.70	7611.3	38.9	-21.0	0.00	0.00	38.2	
5	7632.2	0.00	0.00	7632.0	39.0	-21.0	2.00	180.00	38.2	
6	9012.7	0.00	0.00	9012.5	39.0	-21.0	0.00	0.00	38.2	KOP(Antero 14 Fed Com #741H)
7	9233.1	26.46	0.00	9225.2	89.0	-21.0	12.00	0.00	88.2	FTP(Antero 14 Fed Com #741H)
8	9762.6	90.00	359.53	9489.9	516.4	-23.4	12.00	-0.53	515.3	
9	10555.2	90.00	359.53	9490.0	1309.0	-30.0	0.00	0.00	1307.2	Fed Perf 1(Antero 14 Fed Com #741H)
10	11174.3	90.00	358.99	9490.0	1928.0	-38.0	0.09	-89.17	1925.5	· · · · · · · · · · · · · · · · · · ·
11	11484.5	90.00	17.61	9490.0	2233.6	6.6	6.00	90.01	2232.5	
12	12324.3	90.00	17.61	9490.0	3034.1	260.6	0.00	0.00	3041.3	
13	12624.8	90.00	359.58	9490.0	3330.0	305.3	6.00	-90.00	3338.5	
14	14567.9	90.00	359.58	9490.0	5273.0	291.0	0.00	0.00	5279.9	Fed Perf 4(Antero 14 Fed Com #741H)
15	17107.9	90.00	359.52	9490.0	7813.0	271.0	0.00	-90.00	7817.7	PBHL(Antero 14 Fed Com #741H)

CASING DETAILS

No casing data is available

WELLBORE TA	WELLBORE TARGET DETAILS (MAP CO-ORDINATES)									
Name	TVD	+N/-S	+E/-W	Northing	Easting					
KOP(Antero 14 Fed Com #741H)	9012.5	39.0	-21.0	412167.00	784557.00					
FTP(Antero 14 Fed Com #741H)	9225.2	89.0	-21.0	412217.00	784557.00					
Fed Perf 1(Antero 14 Fed Com #741H)	9490.0	1309.0	-30.0	413437.00	784548.00					
Fed Perf 4(Antero 14 Fed Com #741H)	9490.0	5273.0	291.0	417401.00	784869.00					
PBHL(Antero 14 Fed Com #741H)	9490.0	7813.0	271.0	419941.00	784849.00					
Fed Perf 2(Antero 14 Fed Com #741H)	9490.0	2506.0	93.0	414634.00	784671.00					
Fed Perf 3(Antero 14 Fed Com #741H)	9490.0	2629.0	132.1	414757.00	784710.10					
PI1(Antero 14 Fed Com #741H)	9490.0	2428.0	-38.0	414556.00	784540.00					
Pl2(Antero 14 Fed Com #741H)	9490.0	2830.0	309.0	414958.00	784887.00					



9300 Antelo 14 Fed Com/#101H/P 9600 0 250 700 1050 1400 1750 2300 2450 2800 3850 4300 4550 4900 5250 5600 5050 6300 6650 7000 7250 77

Vertical Section at 1.99°

Lea County, NM (NAD 83 NME)
Antero 14 Fed Com
#101H
OH
Plan #0.2
16:13, January 29 2024

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:
WELL NAME & NO.:
SURFACE HOLE FOOTAGE:
BOTTOM HOLE FOOTAGE
LOCATION:
COUNTY:

EOG RESOURCES INCORPORATED
ANTERO 14 FED COM 101H
2628'/N & 1271'/W
100'/N & 1600'/W
Section 14, T.25 S., R.33 E.
Lea County, New Mexico

COA

H2S	• Yes	O No	
Potash	None	O Secretary	© R-111-P
Cave/Karst Potential	• Low	O Medium	O High
Cave/Karst Potential	O Critical		
Variance	O None	Flex Hose	Other
Wellhead	Conventional	Multibowl	O Both
Wellhead Variance	O Diverter		
Other	□4 String	☐ Capitan Reef	□WIPP
Other	☐ Fluid Filled	☐ Pilot Hole	☐ Open Annulus
Cementing	☐ Contingency	☐ EchoMeter	☐ Primary Cement
	Cement Squeeze		Squeeze
Special Requirements	☐ Water Disposal	☑ COM	□ Unit
Special Requirements	☐ Batch Sundry		
Special Requirements	✓ Break Testing	✓ Offline	✓ Casing
Variance		Cementing	Clearance

A. CASING

Primary Casing Design:

- 1. The 13-3/8 inch surface casing shall be set at approximately 1,250 feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set at approximately 4,990 feet TVD.
 - Mud weight could brine up to 10.2ppg. Reviewed and OK
 - Keep casing full during run for collapse SF

The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

Option 1 (Single Stage):

- Cement to surface. If cement does not circulate see B.1.a, c-d above.
- 3. The **5-1/2** inch production casing shall be set at approximately **17,108** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

Option 1 (Single Stage):

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Alternative Design:

- 1. The **10-3/4** inch surface casing shall be set at approximately **1,250** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that

string.

2. The 8-5/8 inch intermediate casing shall be set at approximately 4,990 feet TVD. Mud weight can brine up to 10.2ppg and is OK. The minimum required fill of cement behind the 8-5/8 inch intermediate casing is:

Option 1 (Single Stage):

- Cement to surface. If cement does not circulate see B.1.a, c-d above.
- 3. The **5-1/2** inch production casing shall be set at approximately **17,108** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

Option 1 (Single Stage):

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

(Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system) BOPE Break Testing Variance

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR part 3170 Subpart 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

Offline Cementing

Offline cementing OK for surface and intermediate intervals. Notify the BLM prior to the commencement of any offline cementing procedure.

Casing Clearance:

- Overlap OK
- Salt annular variance in place.

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Eddy County
 EMAIL or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,
 BLM_NM_CFO_DrillingNotifications@BLM.GOV (575) 361-2822
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.

- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR part 3170 Subpart 3172 must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
 - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR part 3170 Subpart 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
 - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
 - e. The results of the test shall be reported to the appropriate BLM office.
 - f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
 - g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to

the test at full stack pressure.

h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

KPI 2/12/2024

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Salt Section Annular Clearance Variance Request

Daniel Moose

Current Design (Salt Strings)

0.422" Annular clearance requirement

- Casing collars shall have a minimum clearance of 0.422 inches on all sides in the hole/casing annulus, with recognition that variances can be granted for justified exceptions.
- 12.25" Hole x 9.625"40# J55/HCK55 LTC Casing
 - 1.3125" Clearance to casing OD
 - 0.8125" Clearance to coupling OD
- 9.875" Hole x 8.75" 38.5# P110 Sprint-SF Casing
 - 0.5625" Clearance to casing OD
 - 0.433" Clearance to coupling OD

Annular Clearance Variance Request

EOG request permission to allow deviation from the 0.422" annulus clearance requirement for the intermediate (salt) section from Onshore Order #2 under the following conditions:

- The variance is not applicable within the Potash Boundaries or Capitan Reef areas.
- Operator takes responsibility to get casing to set point in the event that the clearance causes stuck pipe issues

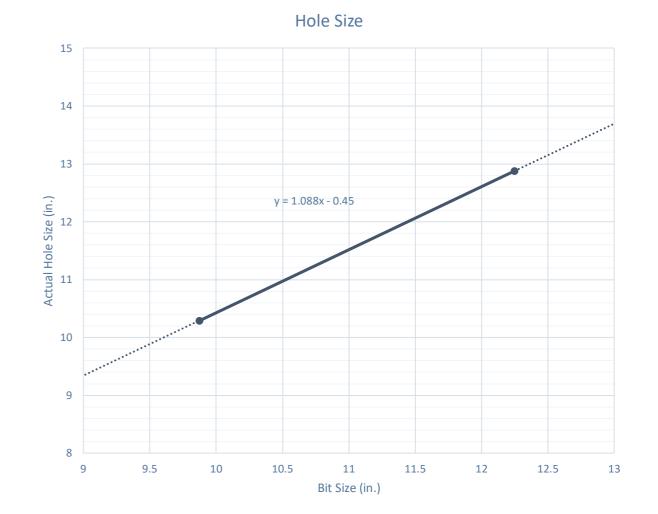
Volumetric Hole Size Calculation

Hole Size Calculations Off Cement Volumes

- Known volume of cement pumped
- Known volume of cement returned to surface
- Must not have had any losses
- Must have bumped plug

Average Hole Size

- 12.25" Hole
 - 12.88" Hole
 - 5.13% diameter increase
 - 10.52% area increase
 - 0.63" Average enlargement
 - 0.58" Median enlargement
 - 179 Well Count
- 9.875" Hole
 - 10.30" Hole
 - 4.24% diameter increase
 - 9.64% area increase
 - 0.42" Average enlargement
 - 0.46" Median enlargement
 - 11 Well Count

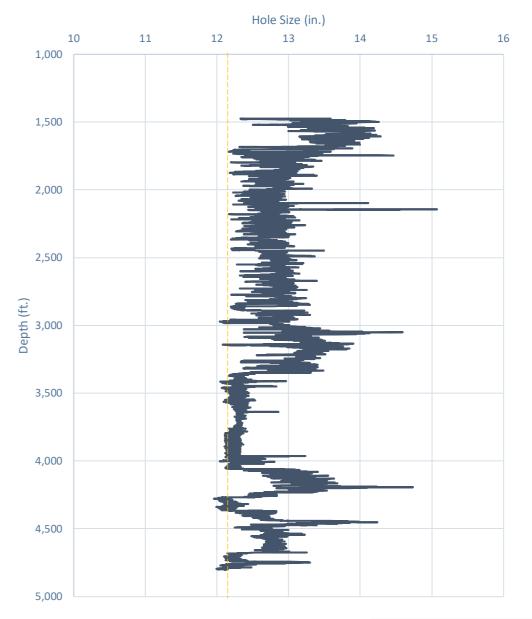


Modelo 10 Fed Com #501H

Caliper Hole Size (12.25")

Average Hole Size

- 12.25" Bit
 - 12.76" Hole
 - 4.14% diameter increase
 - 8.44% area increase
 - 0.51" Average enlargement
 - 0.52" Median enlargement
 - Brine

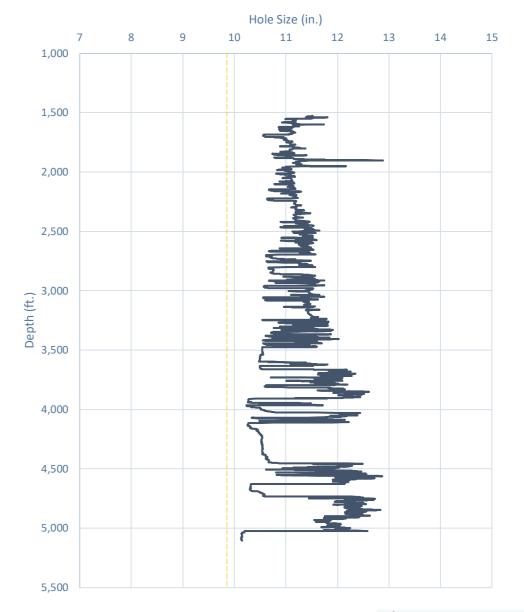


Caliper Hole Size (9.875")

Average Hole Size

- 9.875" Hole
 - 11.21" Hole
 - 13.54% diameter increase
 - 28.92% area increase
 - 1.33" Average enlargement
 - 1.30" Median enlargement
 - EnerLite

Whirling Wind 11 Fed Com #744H



Design A

Proposed 11" Hole with 9.625" 40# J55/HCK55 LTC Casing

- 11" Bit + 0.52" Average hole enlargement = 11.52" Hole Size
 - 0.9475" Clearance to casing OD

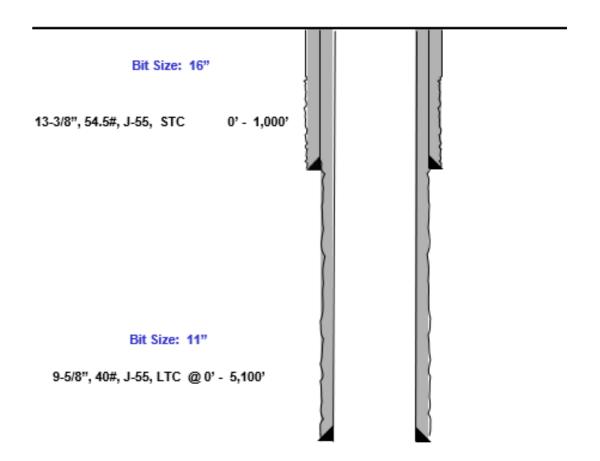
$$=\frac{11.52-9.625}{2}$$

• 0.4475" Clearance to coupling OD

$$=\frac{11.52-10.625}{2}$$

- Previous Shoe 13.375" 54.5# J55 STC
 - 0.995" Clearance to coupling OD (~1,200' overlap)

$$=\frac{12.615-10.625}{^{2}}$$



Design B

Proposed 9.875" Hole with 8.625" 32# J55/P110 BTC-SC Casing

- 9.875" Bit + 0.42" Average hole enlargement = 10.295" Hole Size
 - 0.835" Clearance to casing OD

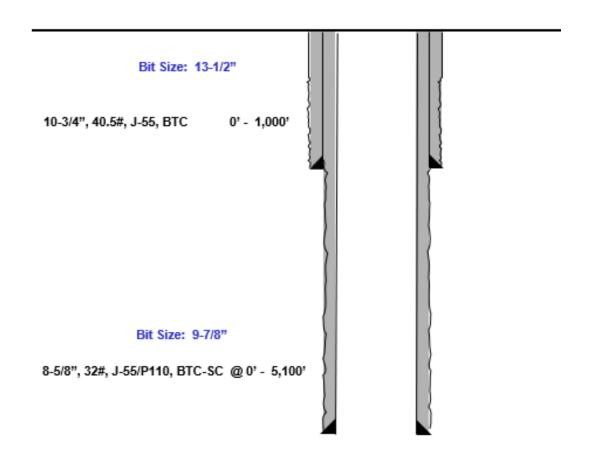
$$=\frac{10.295-8.625}{2}$$

• 0.585" Clearance to coupling OD

$$=\frac{10.295-9.125}{2}$$

- Previous Shoe 10.75" 40.5# J55 STC
 - 0.4625" Clearance to coupling OD (~1,200' overlap)

$$=\frac{10.05-9.125}{2}$$



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Casing Spec Sheets

PERFORMANCE DATA

API LTC 9.625 in K55 HC 40.00 lbs/ft **Technical Data Sheet**

Tubular Parameters					
Size	9.625	in	Minimum Yield	55	ksi
Nominal Weight	40.00	lbs/ft	Minimum Tensile	95	ksi
Grade	K55 HC		Yield Load	629	kips
PE Weight	38.94	lbs/ft	Tensile Load	1088	kips
Wall Thickness	0.395	in	Min. Internal Yield Pressure	3,950	psi
Nominal ID	8.835	in	Collapse Pressure	3600	psi
Drift Diameter	8.750	in		1	1

Connection Parameters									
Connection OD	10.625	in							
Coupling Length	10.500	in							
Threads Per Inch	8	tpi							
Standoff Thread Turns	3.50	turns							
Make-Up Loss	4.750	in							
Min. Internal Yield Pressure	3,950	psi							

11.454

Pipe Body and API Connections Performance Data

13.375 54.50/0.380 J55 PDF

New Search »

« Back to Previous List

6/8/2015 10:04:37 AM					
Mechanical Properties	Ptpe	втс	LTC	STC	
Minimum Yield Strength	55,000	-	-	-	psi
Maximum Yield Strength	80,000	-	-	-	psi
Minimum Tensile Strength	75,000	-	-	-	psi
Dimensions	Ptpe	втс	LTC	STC	
Outside Diameter	13.375	14.375	-	14.375	in.
Wall Thickness	0.380	-	-	-	in.
Inside Diameter	12.615	12.615	-	12.615	in.
Standard Drift	12.459	12.459	-	12.459	in.
Alternate Drift	-	-	-	-	in.
Nominal Linear Weight, T&C	54.50	-	-	-	lbs/ft
Plain End Weight	52.79	-	-	-	lbs/ft
Performance	Pipe	втс	LTC	STC	
Minimum Collapse Pressure	1,130	1,130	-	1,130	psi
Minimum Internal Yield Pressure	2,740	2,740	-	2,740	psi
Minimum Pipe Body Yield Strength	853.00	-	-	-	1000 lbs
Joint Strength		909	-	514	1000 lbs
Reference Length	-	11,125	-	6,290	ft
Make-Up Data	Ptpe	втс	LTC	STC	
Make-Up Loss	-	4.81	-	3.50	in.
Minimum Make-Up Torque	-	-	-	3,860	ft-lbs
Maximum Make-Up Torque	-	-	-	6,430	ft-lbs

Nom. Pipe Body Area

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3,150

5,250

ft-lbs

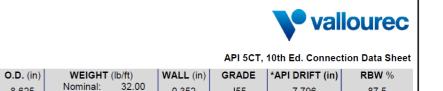
ft-lbs

Casing Spec Sheets

Pipe Body and API Connections Performance Data

10.750 40.50/0.350 J55 PDF

New Search » « Back to Previous List USC Metric 6/8/2015 10:14:05 AM BTC LTC Ptpe STC **Mechanical Properties** Minimum Yield Strength 55,000 psi Maximum Yield Strength 80,000 Minimum Tensile Strength 75,000 psi BTC LTC Pipe STC 11.750 Outside Diamete 10.750 11.750 in. Wall Thickness 0.350 Inside Diameter 10.050 10.050 10.050 Standard Drift 9.894 9.894 in. Alternate Drift in. 40.50 Nominal Linear Weight, T&C lbs/ft 38.91 lbs/ft Plain End Weight Performance Ptpe BTC STC Minimum Collapse Pressure psi Minimum Internal Yield Pressure 3.130 3.130 3.130 629.00 Minimum Pipe Body Yield Strength 1000 lbs 700 420 Joint Strength 1000 lbs Reference Length 11,522 6,915 BTC STC Make-Up Data Ptpe 4.81 Make-Up Loss 3.50 in.



0.352

Material Properties (PE)		
Pipe		
Minimum Yield Strength:	55 ksi	
Maximum Yield Strength:	80 ksi	
Minimum Tensile Strength:	75 ksi	
Coupling		
Minimum Yield Strength:	55 ksi	
Maximum Yield Strength:	80 ksi	
Minimum Tensile Strength:	75 ksi	

Plain End: 31.13

8.625

MADE IN USA

#Od

SLN

#0/M

7.875

DA

S2L2

S

8.625

STAR

VALLOUREC

Pipe Body Data (PE)		
Geometry		
Nominal ID:	7.92 inch	
Nominal Area:	9.149 in ²	
*Special/Alt. Drift:	7.875 inch	
Performance		
Pipe Body Yield Strength:	503 kips	
Collapse Resistance:	2,530 psi	
Internal Yield Pressure: (API Historical)	3,930 psi	

7.796

87.5

Coupling OD: 9.625"			
STC Performance			
STC Internal Pressure:	3,930	psi	
STC Joint Strength:	372	kips	
LTC Performance			
LTC Internal Pressure:	3,930	psi	
LTC Joint Strength:		kips	
SC-BTC Performance - Cplg	OD =	9.125"	
BTC Internal Pressure:	3,930	psi	
BTC Joint Strength:	503	kips	

API Connection Torque					
	STC Torque (ft-lbs)				
Min:	2,793	Opti:	3,724	Max:	4,655
LTC Torque (ft-lbs)					
Min:	3,130	Opti:	4,174	Max:	5,217
BTC Torque (ft-lbs)					
follow API guidelines regarding positional make up					

*Alt. Drift will be used unless API Drift is specified on order.

**If above API connections do not suit your needs, VAM® premium connections are available up to 100% of pipe body ratings.

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Minimum Make-Up Torque

Maximum Make-Up Torque

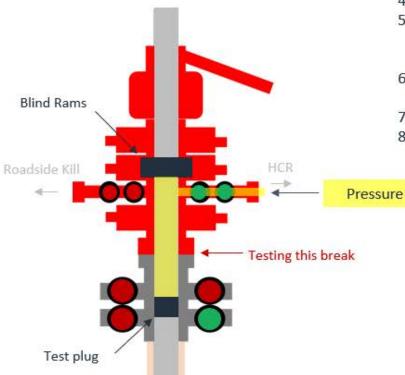


Break-test BOP & Offline Cementing:

EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
 - Annular **à** during each full BOPE test
 - Upper Pipe Rams **à** On trip ins where FIT required
 - Blind Rams **à** Every trip
 - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the
 casing will be monitored via the valve on the TA cap as per standard batch drilling
 ops.

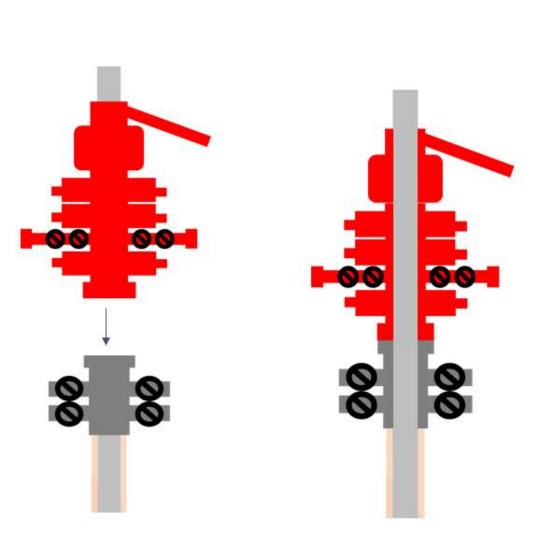
Break Test Diagram (HCR valve)

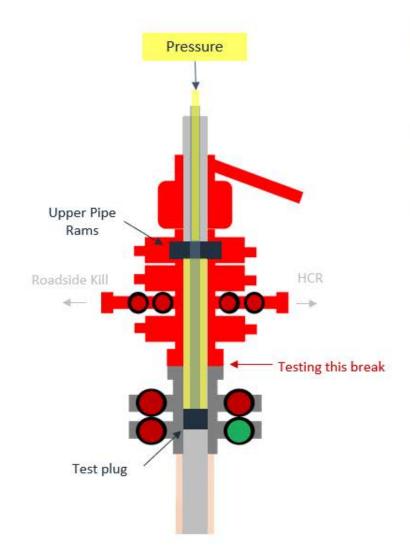


Steps

- 1. Set plug in wellhead (lower barrier)
- 2. Close Blind Rams (upper barrier)
- 3. Close roadside kill
- 4. Open HCR (pressure application)
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to main choke manifold crown valve
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit

Break Test Diagram (Test Joint)





Steps

- Set plug in with test joint wellhead (lower barrier)
- 2. Close Upper Pipe Rams (upper barrier)
- 3. Close roadside kill
- 4. Close HCR
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to top of test joint
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit



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Cement Program

1. No changes to the cement program will take place for offline cementing.

Summarized Operational Procedure for Intermediate Casing

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
 - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
- 2. Land production casing on mandrel hanger through BOP.
 - a. If casing is unable to be landed with a mandrel hanger, then the casing will be cemented online.
- 3. Break circulation and confirm no restrictions.
 - a. Ensure no blockage of float equipment and appropriate annular returns.
 - b. Perform flow check to confirm well is static.
- 4. Set pack-off
 - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
 - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
- 5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
 - a. Minimum 4 hrs notice.
- 6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
 - a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
- 7. Skid/Walk rig off current well.
- 8. Confirm well is static before removing TA Plug.
 - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
 - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
 - c. Well control plan can be seen in Section B, Well Control Procedures.
 - d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.



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- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
- 9. Rig up return lines to take returns from wellhead to pits and rig choke.
 - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
 - If either test fails, perform corrections and retest before proceeding.
 - c. Return line schematics can be seen in Figure 3.
- 10. Remove TA Plug from the casing.
- 11. Install offline cement tool.
 - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
- 12. Rig up cement head and cementing lines.
 - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
- 13. Break circulation on well to confirm no restrictions.
 - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
 - b. Max anticipated time before circulating with cement truck is 6 hrs.
- 14. Pump cement job as per plan.
 - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
 - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
- 15. Confirm well is static and floats are holding after cement job.
 - a. With floats holding and backside static:
 - i. Remove cement head.
 - b. If floats are leaking:
 - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
 - c. If there is flow on the backside:
 - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
- 16. Remove offline cement tool.
- 17. Install night cap with pressure gauge for monitoring.
- 18. Test night cap to 5,000 psi for 10 min.



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Example Well Control Plan Content

A. Well Control Component Table

The table below, which covers the cementing of the <u>5M MASP (Maximum Allowable Surface Pressure) portion of the well</u>, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

B. Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

General Procedure While Circulating

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.

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- 6. Read and record the following:
 - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
 - b. Pit gain
 - c. Time
 - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

General Procedure While Cementing

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.
- 6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
- 7. Continue to place cement until plug bumps.
- 8. At plug bump close rig choke and cement head.
- 9. Read and record the following
 - a. SICP and AP
 - b. Pit gain
 - c. Time
 - d. Shut-in annulus valves on wellhead

General Procedure After Cementing

- 1. Sound alarm (alert crew).
- 2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 3. Confirm shut-in.
- 4. Notify tool pusher/company representative.
- 5. Read and record the following:
 - a. SICP and AP
 - b. Pit gain
 - c. Time
 - d. Shut-in annulus valves on wellhead



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Figure 1: Cameron TA Plug and Offline Adapter Schematic

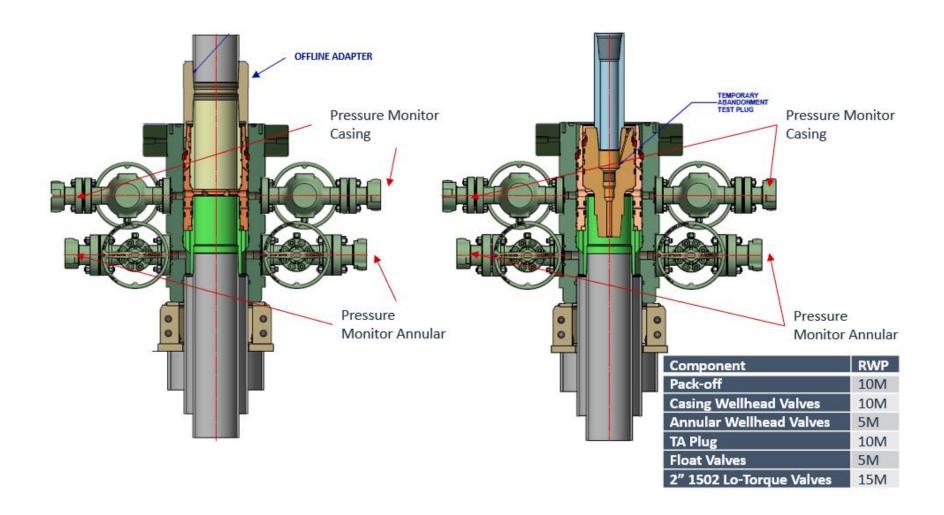
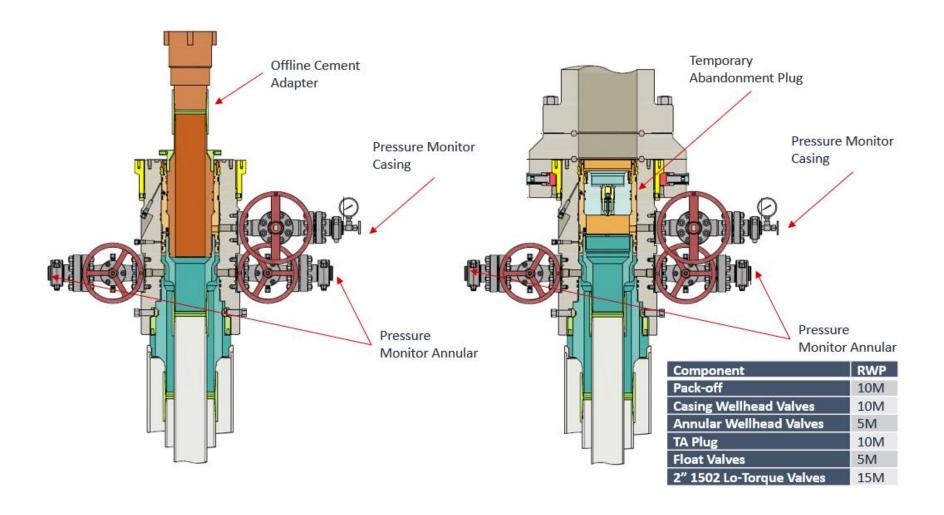




Figure 2: Cactus TA Plug and Offline Adapter Schematic

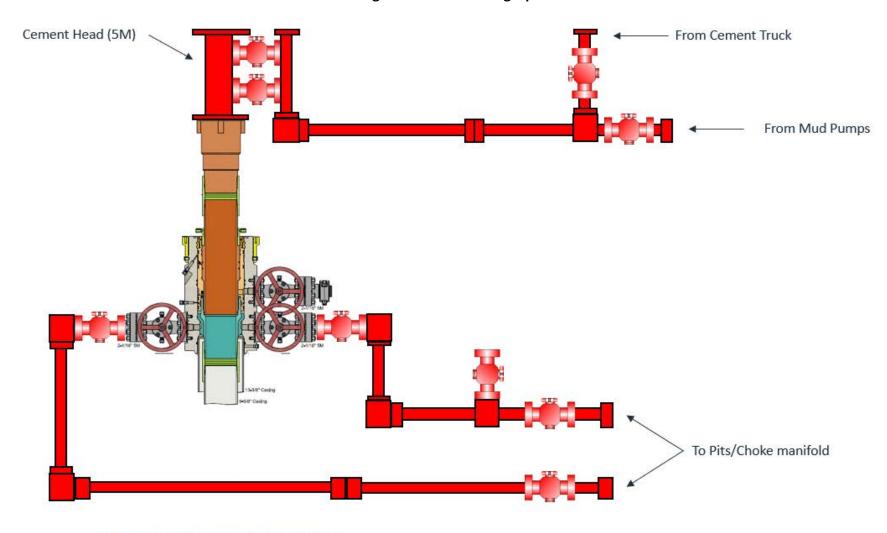


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Figure 3: Back Yard Rig Up



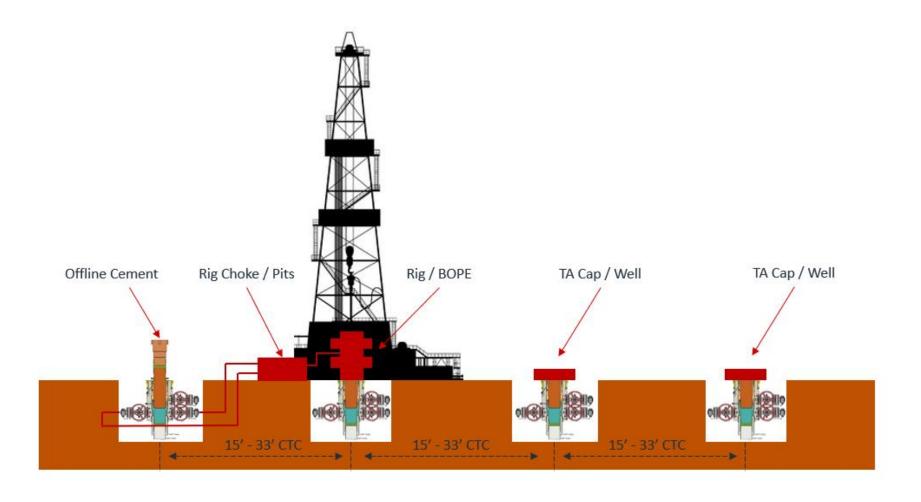
*** All Lines 10M rated working pressure

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Figure 4: Rig Placement Diagram



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State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. **Santa Fe, NM 87505**

CONDITIONS

Action 314926

CONDITIONS

Operator:	OGRID:
EOG RESOURCES INC	7377
5509 Champions Drive	Action Number:
Midland, TX 79706	314926
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

CONDITIONS

Created By	Condition	Condition Date
pkautz	None	3/15/2024