Received by OCD: 3/18/2024 4:55:00 PM U.S. Department of the Interior BUREAU OF LAND MANAGEMENT		Sundry Print Report 03/18/2024
Well Name: ROBIN FED	Well Location: T20S / R34E / SEC 20 / SESE /	County or Parish/State:
Well Number: 134H	Type of Well: OIL WELL	Allottee or Tribe Name:
Lease Number: NMNM13276	Unit or CA Name:	Unit or CA Number:
US Well Number: 3002552587	<b>Well Status:</b> Approved Application for Permit to Drill	Operator: COLGATE OPERATING LLC

### **Notice of Intent**

Sundry ID: 2776501

Type of Submission: Notice of Intent

Date Sundry Submitted: 02/26/2024

Date proposed operation will begin: 03/08/2024

Type of Action: APD Change Time Sundry Submitted: 08:17 59

**Procedure Description:** API# 30-025-52587 Colgate respectfully requests to change the Robin Fed Com 134H APD drilling plan from 3 string to 4 string as it states in our COAs and we would like to add a pilot hole. Please see revised drilling plan, pilot hole directional survey, batch drilling/OLC procedure, BOPs, Choke diagrams, pilot hole procedure and variances attached.

**NOI Attachments** 

### **Procedure Description**

ROBIN\_FED\_134H\_PWP0\_SVY\_RPT\_PH\_20240226081452.pdf

ROBIN\_FED\_134H\_PWP0\_AC\_RPT\_PH\_20240226081452.pdf

Robin\_Fed\_134H\_drilling\_packet\_4\_string\_20240223100946.pdf

k	eceived by OCD: 3/18/2024 4:55:00 PM Well Name: ROBIN FED	Well Location: T20S / R34E / SEC 20 / SESE /	County or Parish/State: Page 2 of 59
	Well Number: 134H	Type of Well: OIL WELL	Allottee or Tribe Name:
	Lease Number: NMNM13276	Unit or CA Name:	Unit or CA Number:
	<b>US Well Number:</b> 3002552587	Well Status: Approved Application for Permit to Drill	<b>Operator:</b> COLGATE OPERATING LLC

# **Conditions of Approval**

### Additional

SEC20\_T20SR34E\_ROBIN\_FED\_AND\_FED\_COM\_\_Lea\_NMNM13276\_COLGATE\_RESOURCES\_11\_28\_2023\_JS\_20240318152601.pdf

ROBIN\_FED\_134H\_COAs\_20240318152601.pdf

### Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

**Operator Electronic Signature: KANICIA SCHLICHTING** 

Name: COLGATE OPERATING LLC

Title: Regulatory Specialist

Street Address: 300 N MARIENFELD ST SUITE 1000

City: MIDLAND

State: TX

Phone: (432) 232-2875

Email address: KANICIA.SCHLICHTING@PERMIANRES.COM

# **Field**

Representative I	Name:
Street Address:	

City:

Phone:

Email address:

State:

Zip:

Signed on: MAR 07, 2024 02:30 PM

### **BLM Point of Contact**

BLM POC Name: CHRISTOPHER WALLS BLM POC Phone: 5752342234 Disposition: Approved Signature: Chris Walls BLM POC Title: Petroleum Engineer BLM POC Email Address: cwalls@blm.gov Disposition Date: 03/18/2024

### Received by OCD: 3/18/2024 4:55:00 PM

eceiveu by OCD. 5/10/202	77 7.33.00 I M			I uge 5 0j
Form 3160-5 (June 2019)	UNITED STAT DEPARTMENT OF THE BUREAU OF LAND MAN	INTERIOR	0	ORM APPROVED MB No. 1004-0137 ires: October 31, 2021
Do not use t		ORTS ON WELLS to drill or to re-enter an APD) for such proposals.	6. If Indian, Allottee o	r Tribe Name
SUBM	T IN TRIPLICATE - Other inst	ructions on page 2	7. If Unit of CA/Agree	ement, Name and/or No.
1. Type of Well	Gas Well Other		8. Well Name and No.	
2. Name of Operator			9. API Well No.	
3a. Address		3b. Phone No. <i>(include area code)</i>	10. Field and Pool or I	Exploratory Area
4. Location of Well (Footage, Sea	c., T.,R.,M., or Survey Description	ı)	11. Country or Parish,	State
12	CHECK THE APPROPRIATE I	BOX(ES) TO INDICATE NATURE	OF NOTICE, REPORT OR OTH	IER DATA
TYPE OF SUBMISSION		TYP	E OF ACTION	
Notice of Intent	Acidize	Deepen Hydraulic Fracturing	Production (Start/Resume) Reclamation	Water Shut-Off Well Integrity
Subsequent Report	Casing Repair Change Plans	New Construction Plug and Abandon	Recomplete     Temporarily Abandon	Other
Final Abandonment Notice		<b>—</b> •	Water Disposal	
the proposal is to deepen dire the Bond under which the wo completion of the involved op	ctionally or recomplete horizonta rk will be perfonned or provide the perations. If the operation results	Ily, give subsurface locations and me he Bond No. on file with BLM/BIA. in a multiple completion or recomple	easured and true vertical depths of Required subsequent reports mu- etion in a new interval, a Form 3	rk and approximate duration thereof. If of all pertinent markers and zones. Attach st be filed within 30 days following 160-4 must be filed once testing has been he operator has detennined that the site

14. I hereby certify that the foregoing is true and correct. Name ( <i>Printed/Typed</i> )			
1	Title		
Signature	Date		
Signature [			
THE SPACE FOR FEDER	RAL OR STATE OF	FICE USE	
Approved by			
	Title	Date	
Conditions of approval, if any, are attached. Approval of this notice does not warrant of certify that the applicant holds legal or equitable title to those rights in the subject leas which would entitle the applicant to conduct operations thereon.			
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any any false, fictitious or fraudulent statements or representations as to any matter within		llfully to make to any department or agency of the Unite	ed States

(Instructions on page 2)

### **GENERAL INSTRUCTIONS**

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

### SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

*Item 13:* Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

### NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

### **Additional Information**

### **Location of Well**

0. SHL: SESE / 10 FSL / 1295 FEL / TWSP: 20S / RANGE: 34E / SECTION: 20 / LAT: 32.5513509 / LONG: -103.5780527 (TVD: 0 feet, MD: 0 feet) PPP: SESE / 100 FSL / 990 FEL / TWSP: 20S / RANGE: 34E / SECTION: 20 / LAT: 32.5516152 / LONG: -103.5770631 (TVD: 10895 feet, MD: 10950 feet) BHL: NENE / 10 FNL / 990 FEL / TWSP: 20S / RANGE: 34E / SECTION: 17 / LAT: 32.5803926 / LONG: -103.5770828 (TVD: 11053 feet, MD: 21312 feet)

# SEC20-T20SR34E\_ROBIN FED AND FED COM \_Lea\_NMNM13276\_COLGATE RESOURCES\_11-28-2023\_JS

13 3/8	/ _	surface csg in a	17 1/2	inch hole.		Design I	actors	/		Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	54.50		j 55	btc	10.09	1.48	1.54	1,552	4	2.67	2.66	84,584
"B"				btc				0				0
	w/	8.4#/g mud, 30min Sfc Csg Tes	t psig: 1,234	Tail Cmt	does not	circ to sfc.	Totals:	1,552	-			84,584
omparison o	f Proposed	to Minimum Required Cem	ent Volumes									
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
17 1/2	0.6946	1210	1621	1078	50	9.50	1022	2M				1.56
10 3/4		casing inside the	13 3/8			Design I	actors		a a	Int 1		
	#/ft	Grade	13 3/0	Coupling	Pady	Collapse		Longth	P@c	a-B	a-C	Wajah
Segment "A"		Grade	; 66	Coupling	Body	-	Burst	Length	B@s			Weigh
A "B"	45.50		j 55	BTC	4.61	1.18	1.31	3,412	2	2.37	2.05	155,24
<b>B</b>							m , 1	0				0
	w/	8.4#/g mud, 30min Sfc Csg Tes			•		Totals:	3,412				155,24
				nded to achieve a top of	0	ft from su		1552				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
12 1/1	0.1882	530	915	719	27	10.00	1509	2M				0.25
12 1/4												Σ%exce
							sum of sx	<u>Σ CuFt</u>				Z%exces
<b>D V Tool(s):</b> by stage % :		#VALUE!	#VALUE!				sum of sx 530	<u>Σ CuFt</u> 915				27
by stage % : class 'H' tail cm 8 5/8	nt yld > 1.20	casing inside the	#VALUE!			Design Fac	530	915	a a	Int 2		27
9 V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment	nt yld > 1.20			 Coupling	Body	Collapse	530 <u>etors</u> Burst		B@s	Int 2 a-B	a-C	27
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A"	nt yld > 1.20	casing inside the		Coupling mo-fxl	<b>Body</b> 5.70		530	915	<b>B@s</b> 4		<b>a-C</b> 2.85	27 Weigh
b V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment	nt yld > 1.20	casing inside the	10 3/4	• •	-	Collapse	530 <u>etors</u> Burst	915		a-B		27 Weigh
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A"	nt yld > 1.20 #/ft 32.00	casing inside the	<b>10 3/4</b> p 110	• •	-	Collapse 1.58	530 <u>ctors</u> Burst 1.67 Totals:	915 Length 5,517		a-B		27 Weigh 176,54 0
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A"	nt yld > 1.20 #/ft 32.00	casing inside the Grade 8.4#/g mud, 30min Sfc Csg Tes	<b>10 3/4</b> p 110 t psig: 1,500	• •	-	Collapse	530 <u>ctors</u> Burst 1.67 Totals:	915 Length 5,517 0		a-B	2.85	27 Weigh 176,54 0
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A"	nt yld > 1.20 #/ft 32.00	casing inside the Grade 8.4#/g mud, 30min Sfc Csg Tes	<b>10 3/4</b> p 110 t psig: 1,500	mo-fxl	5.70	Collapse 1.58	530 <u>ctors</u> Burst 1.67 Totals:	915 Length 5,517 0 5,517		a-B	2.85	27 Weigh 176,54 0 176,54 overlap.
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A" "B" Hole Size	nt yld > 1.20 #/ft 32.00 w/ Annular Volume	casing inside the Grade 8.4#/g mud, 30min Sfc Csg Tes The cement	<b>10 3/4</b> p 110 t psig: 1,500 <b>volume(s) are inter</b>	mo-fxl nded to achieve a top of	5.70 0	Collapse 1.58 ft from su	530 <u>etors</u> Burst 1.67 Totals: rface or a	915 Length 5,517 0 5,517 3412		a-B	2.85	27 Weigh 176,54 0 176,54 overlap. Min Dis
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A" "B" Hole	nt yld > 1.20 #/ft 32.00 w/ Annular	casing inside the Grade 8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage	<b>10 3/4</b> p 110 t psig: 1,500 t <b>volume(s) are inter</b> <b>1 Stage</b>	mo-fxl nded to achieve a top of Min	5.70 0 1 Stage	Collapse 1.58 ft from su Drilling	530 Ctors Burst 1.67 Totals: rface or a Calc	915 Length 5,517 0 5,517 3412 Req'd		a-B	2.85	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp
D V Tool(s): by stage % : Class 'H' tail cm 8 5/8 Segment "A" "B" Hole Size	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261	28.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx	<b>10 3/4</b> p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt	mo-fxl nded to achieve a top of Min Cu Ft 724	5.70 0 1 Stage % Excess 17	Collapse 1.58 ft from su Drilling Mud Wt 9.50	530 2530 25075 Burst 1.67 Totals: rface or a Calc MASP	915 Length 5,517 0 5,517 3412 Req'd BOPE		a-B	2.85	27 Weigh 176,54 0 176,54
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490	<b>10 3/4</b> p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt	mo-fxl nded to achieve a top of Min Cu Ft	5.70 0 1 Stage % Excess 17	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement	530 Etors Burst 1.67 Totals: rface or a Calc MASP 3347	915 Length 5,517 0 5,517 3412 Req'd BOPE		<b>a-B</b> 2.90	2.85	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490 casing inside the	<b>10 3/4</b> p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25%	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u>	530 Etors Burst 1.67 Totals: rface or a Calc MASP 3347	915 Length 5,517 0 5,517 3412 Req'd BOPE	4	<b>a-B</b> 2.90 Prod 1	2.85	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63
D V Tool(s): by stage % : class 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm 5 1/2 Segment	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490	<b>10 3/4</b> p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844	mo-fxl nded to achieve a top of Min Cu Ft 724	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement	530 Etors Burst 1.67 Totals: rface or a Calc MASP 3347	915 Length 5,517 0 5,517 3412 Req'd BOPE		<b>a-B</b> 2.90	2.85 <b>a-C</b>	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63 Weigh
D V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 lass 'C' tail cm 5 1/2 Segment "A"	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490 casing inside the	<b>10 3/4</b> p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25%	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u>	530 tors Burst 1.67 Totals: rface or a Calc MASP 3347 Sators	915 Length 5,517 0 5,517 3412 Req'd BOPE 5M	4	<b>a-B</b> 2.90 Prod 1	2.85	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63 Weigh
D V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 lass 'C' tail cm 5 1/2 Segment	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35 #/ft	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490 casing inside the	10 3/4 p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844 844	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25%	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u> Collapse	530 tors Burst 1.67 Totals: rface or a Calc MASP 3347 Say 2 Say 2 Sa	915 Length 5,517 0 5,517 3412 Req'd BOPE 5M	4 B@s	<b>a-B</b> 2.90 Prod 1 <b>a-B</b>	2.85 <b>a-C</b> 3.32	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63 Weigh
D V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 lass 'C' tail cm 5 1/2 Segment "A"	nt yld > 1.20 #/ft 32.00 %/ Annular Volume 0.1261 nt yld > 1.35 #/ft 20.00 20.00	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490 casing inside the	10 3/4 p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844 844 85/8 p 110 p 110 p 110	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25% Coupling geoconn	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u> Collapse 1.71	530 Etors Burst 1.67 Totals: rface or a Calc MASP 3347 Sagar S	915 Length 5,517 3412 Req'd BOPE 5M Length 11,642	4 B@s 2	а-В 2.90 Ргод 1 а-В 4.10	2.85 <b>a-C</b> 3.32	27 Weigh 176,54 overlap. Min Dis Hole-Cp 0.63 Weigh 232,84
D V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 class 'C' tail cm 5 1/2 Segment "A"	nt yld > 1.20 #/ft 32.00 %/ Annular Volume 0.1261 nt yld > 1.35 #/ft 20.00 20.00	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490 casing inside the Grade 8.4#/g mud, 30min Sfc Csg Tes	10 3/4 p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844 844 844 85/8 p 110 p 110 p 110 t psig: 2,459	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25% Coupling geoconn	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u> Collapse 1.71	530 Etors Burst 1.67 Totals: rface or a Calc MASP 3347 Sagardarian Eactors Burst 2.36 2.36 Totals:	915 Length 5,517 0 5,517 3412 Req'd BOPE 5M Length 11,642 10,011	4 B@s 2	а-В 2.90 Ргод 1 а-В 4.10	2.85 <b>a-C</b> 3.32 3.32	27 Weigl 176,54 overlap. Min Di Hole-Cr 0.63 Weigl 232,84 200,22 433,00
D V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 lass 'C' tail cm 5 1/2 Segment "A"	nt yld > 1.20 #/ft 32.00 %/ Annular Volume 0.1261 nt yld > 1.35 #/ft 20.00 20.00	casing inside the Grade '8.4#/g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 490 casing inside the Grade 8.4#/g mud, 30min Sfc Csg Tes	10 3/4 p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844 844 844 85/8 p 110 p 110 p 110 t psig: 2,459	mo-fxl inded to achieve a top of Min Cu Ft 724 Does not meet CFO 25% Coupling geoconn geoconn	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u> Collapse 1.71 1.91	530 Etors Burst 1.67 Totals: rface or a Calc MASP 3347 Sagardarian Eactors Burst 2.36 2.36 Totals:	915 Length 5,517 0 5,517 3412 Req'd BOPE 5M Length 11,642 10,011 21,653	4 B@s 2	а-В 2.90 Ргод 1 а-В 4.10	2.85 <b>a-C</b> 3.32 3.32	27 Weigl 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63 Weigl 232,84 200,22 433,06 overlap.
D V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 lass 'C' tail cm 5 1/2 Segment "A" "B"	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35 #/ft 20.00 20.00 w/	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	10 3/4 p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844 85/8 p 110 p 110 p 110 t psig: 2,459 volume(s) are inter	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25% Coupling geoconn geoconn geoconn	5.70 0 1 Stage % Excess 17 excess requi Joint 1.26 ∞ 5317	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u> Collapse 1.71 1.91 ft from su	530 250 250 250 200 200 200 200 20	915 Length 5,517 0 5,517 3412 Req'd BOPE 5M Length 11,642 10,011 21,653 200	4 B@s 2	а-В 2.90 Ргод 1 а-В 4.10	2.85 <b>a-C</b> 3.32 3.32	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63 Weigh 232,84 200,22 433,06 overlap. Min Dis
V Tool(s): by stage % : lass 'H' tail cm 8 5/8 Segment "A" "B" Hole Size 9 7/8 lass 'C' tail cm 5 1/2 Segment "A" "B"	nt yld > 1.20 #/ft 32.00 w/ Annular Volume 0.1261 nt yld > 1.35 #/ft 20.00 20.00 w/ Annular	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	10 3/4 p 110 t psig: 1,500 volume(s) are inter 1 Stage CuFt Cmt 844 85/8 p 110 p 110 t psig: 2,459 volume(s) are inter 1 Stage	mo-fxl nded to achieve a top of Min Cu Ft 724 Does not meet CFO 25% Coupling geoconn geoconn nded to achieve a top of Min	5.70 0 1 Stage % Excess 17 excess requi	Collapse 1.58 ft from su Drilling Mud Wt 9.50 rement <u>Design I</u> Collapse 1.71 1.91 ft from su Drilling	530 tors Burst 1.67 Totals: rface or a Calc MASP 3347 Sagar Sagar Calc MASP 3347 Calc MASP 3347 Calc Totals: rface or a Calc	915 Length 5,517 0 5,517 3412 Req'd BOPE 5M 11,642 10,011 21,653 200 Req'd	4 B@s 2	а-В 2.90 Ргод 1 а-В 4.10	2.85 <b>a-C</b> 3.32 3.32	27 Weigh 176,54 0 176,54 overlap. Min Dis Hole-Cp 0.63 Weigh 232,84 200,22 433,06

### **ROBIN FED AND FED COM**

Carlsbad Field Office



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**Released to Imaging: 3/19/2024 7:55:25 AM** 

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

ĺ	OPERATOR'S NAME:	COLGATE OPERATING LLC
	WELL NAME & NO.:	ROBIN FED 134H
	SURFACE HOLE FOOTAGE:	10'/S & 1295'/E
	BOTTOM HOLE FOOTAGE	10'/N & 990'/E
	LOCATION:	Section 20, T.20 S., R.34 E., NMP
	COUNTY:	Lea County, New Mexico

# COA

H2S	• Yes	C No	
Potash	C None	C Secretary	• R-111-P
Cave/Karst Potential	• Low	C Medium	C High
Cave/Karst Potential	Critical		
Variance	C None	Section Flex Hose	C Other
Wellhead	Conventional	Multibowl	C Both
Wellhead Variance	C Diverter		
Other	✓ 4 String	Capitan Reef	□WIPP
Other	□ Fluid Filled	Pilot Hole	Open Annulus
Cementing	Contingency	EchoMeter	Primary Cement
	Cement Squeeze		Squeeze
Special Requirements	🗆 Water Disposal	COM	🗖 Unit
Special Requirements	Batch Sundry		
Special Requirements	Break Testing	☑ Offline	Casing
Variance		Cementing	Clearance

# A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated AT SPUD. As a result, the Hydrogen Sulfide area must meet 43 CFR part 3170 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

# **B.** CASING

### Primary Casing Design:

 The 13-3/8 inch surface casing shall be set at approximately 1620 feet per BLM Geologist (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface. The surface hole shall be 17 1/2 inch in diameter.

- a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>24 hours in the Potash Area</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **10-3/4** inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.
  - In <u>R111 Potash Areas</u> if cement does not circulate to surface on the first two salt protection casing strings, the cement on the 3rd casing salt string must come to surface.
- 3. The minimum required fill of cement behind the **8-5/8** inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef. Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.
- 4. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 50 feet on top of Capitan Reef top or 500 feet into the previous casing, whichever is greater. If cement does not circulate see B.1.a, c-d above.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst, potash or capitan reef.

### C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **13-3/8** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000** (**5M**) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

# **D. SPECIAL REQUIREMENT (S)**

# (Note: For a minimum 5M BOPE or less (Utilizing a 10M BOPE system)

### **BOPE Break Testing Variance**

- BOPE Break Testing is ONLY permitted for 5M BOPE or less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP)
- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (**575-706-2779**) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-689-5981 Lea County) 4 hours prior to BOPE tests.
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per Onshore Oil and Gas Order No. 2.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

### **Offline Cementing**

Contact the BLM prior to the commencement of any offline cementing procedure.

### **Casing Clearance:**

Operator casing variance is approved for the utilization of 10-3/4 inch intermediate casing in a  $12 \frac{1}{4}$  inch intermediate hole.

Operator shall clean up cycles until wellbore is clear of cuttings and any large debris, ensure cutting sizes are adequate "coffee ground or less" before cementing.

# **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

**BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV** (575) 361-2822

- Lea County Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43 CFR part 3170 Subpart 3172** as soon as 2nd Rig is rigged up on well.

- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24 hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

### B. PRESSURE CONTROL

- All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.

- d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
- e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
  - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
  - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
  - e. The results of the test shall be reported to the appropriate BLM office.
  - f. All tests are required to be recorded on a calibrated test chart. A copy of the

BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.

- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

JS 3/18/2024

# NEW MEXICO

(SP) LEA ROBIN PROJECT ROBIN FED 134H

**PILOT HOLE** 

Plan: PHPWP0

# **Standard Planning Report - Geographic**

26 February, 2024

Planning Report - Geographic

Database: Company: Project: Site: Well: Well: Wellbore: Design:		(SP) L Robii Robii Pilot Phpw	MEXICO LEA N PROJECT N FED 134H I HOLE VP0			TVD Ref MD Refe North Re			Well ROBIN F KB @ 3700.00 KB @ 3700.00 Grid Minimum Curv	usft usft	
Project		(SP) LI	EA								
Map System Geo Datum: Map Zone:	1	North Ar	e Plane 1983 nerican Datu xico Eastern	m 1983		System D	atum:	Μ	ean Sea Leve	l	
Site		ROBIN	I PROJECT								
Site Position From: Position Unc		Map t <b>y:</b>	ο 0.0 ι	East	hing: ing: Radius:	773,9	135.84 usft 996.49 usft 3-3/16 "	Latitude: Longitude:			32° 33' 4.851 N 103° 34' 41.691 W
Well		ROBIN	FED 134H								
Well Position Position Unc Grid Conver	certaint	•	0. 0.	.0 usft E	orthing: asting: /ellhead Ele	vation:	565,137.50 774,056.47	usft <b>Lo</b>	titude: ngitude: ound Level:		32° 33' 4.864 N 103° 34' 40.990 W 3,674.0 ust
Wellbore		PILOT	HOLE								
Magnetics		Мос	del Name	Samp	le Date	Declina (°)			Angle °)	Field St (n	
		I	GRF200510	1	2/31/2009		7.78		60.54	48,988	3.41599933
Design		PHPW	P0								
Audit Notes: Version:	:			Pha	se:	PROTOTYPE	Tio	e On Depth:		0.0	
Vertical Sect	tion:		De	epth From (` (usft) 0.0	rvd)	<b>+N/-S</b> (usft) 0.0	- (u	<b>5/-W</b> I <b>sft)</b> 0.0		<b>ection</b> (°) 4.02	
Plan Survey	Tool P	rogram	Date	2/26/2024							
Depth Fi (usft)		Depth (usf		/ (Wellbore)		Tool Name		Remarks			
1	0.0	12,6	622.4 PHPW	P0 (PILOT H	IOLE)	MWD OWSG_Rev	/2_ MWD - S	tar			
Plan Section	าร										
Measured Depth (usft)	Inclin (°		Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0 2,000.0 2,400.0 4,431.7 4,831.7 12,622.4	) ) 7 7	0.00 0.00 8.00 8.00 0.00 0.00	0.00 0.00 64.02 64.02 0.00 0.00	0.0 2,000.0 2,398.7 4,410.6 4,809.3 12,600.0	0.0 0.0 12.2 136.1 148.3 148.3	0.0 0.0 25.1 279.2 304.3 304.3	0.00 0.00 2.00 0.00 2.00 0.00	0.00 0.00 2.00 0.00 -2.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 64.02 0.00 180.00 0.00	

2/26/2024 9:04:13AM

Planning Report - Geographic

Database:	Compass	Local Co-ordinate Reference:	Well ROBIN FED 134H
Company:	NEW MEXICO	TVD Reference:	KB @ 3700.0usft
Project:	(SP) LEA	MD Reference:	KB @ 3700.0usft
Site:	ROBIN PROJECT	North Reference:	Grid
Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Wellbore:	PILOT HOLE	-	
Design:	PHPWP0		

### Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude
									-
0.0		0.00 0.00	0.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W 103° 34' 40.990 W
100.0		0.00	100.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	
200.0		0.00	200.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
300.0			300.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
400.0		0.00	400.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
500.0 600.0		0.00 0.00	500.0 600.0	0.0 0.0	0.0 0.0	565,137.50 565.137.50	774,056.47 774,056.47	32° 33' 4.864 N 32° 33' 4.864 N	103° 34' 40.990 W 103° 34' 40.990 W
700.0		0.00	700.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
800.0		0.00	800.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
900.0		0.00	900.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,000.0		0.00	1,000.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,100.0		0.00	1,100.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,100.0		0.00	1,200.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,300.0		0.00	1,300.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,400.0		0.00	1,400.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,500.0		0.00	1,500.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,600.0		0.00	1,600.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,700.0		0.00	1,700.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,800.0		0.00	1,800.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
1,900.0		0.00	1,900.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
2,000.0		0.00	2,000.0	0.0	0.0	565,137.50	774,056.47	32° 33' 4.864 N	103° 34' 40.990 W
	uild 2.00	0.00	2,000.0	0.0	0.0	000,101.00	111,000.11	02 00 1.00111	
2,100.0		64.02	2,100.0	0.8	1.6	565,138.27	774,058.04	32° 33' 4.871 N	103° 34' 40.971 W
2,200.0		64.02	2,199.8	3.1	6.3	565,140.56	774,062.74	32° 33' 4.893 N	103° 34' 40.916 W
2,300.0	6.00	64.02	2,299.5	6.9	14.1	565,144.38	774,070.57	32° 33' 4.931 N	103° 34' 40.824 W
2,400.0	8.00	64.02	2,398.7	12.2	25.1	565,149.72	774,081.53	32° 33' 4.983 N	103° 34' 40.696 W
Start 20	031.7 hold at	t 2400.0 MD							
2,500.0	8.00	64.02	2,497.7	18.3	37.6	565,155.81	774,094.04	32° 33' 5.042 N	103° 34' 40.549 W
2,600.0	8.00	64.02	2,596.8	24.4	50.1	565,161.91	774,106.55	32° 33' 5.102 N	103° 34' 40.403 W
2,700.0	8.00	64.02	2,695.8	30.5	62.6	565,168.01	774,119.06	32° 33' 5.161 N	103° 34' 40.256 W
2,800.0	8.00	64.02	2,794.8	36.6	75.1	565,174.10	774,131.57	32° 33' 5.220 N	103° 34' 40.109 W
2,900.0	8.00	64.02	2,893.8	42.7	87.6	565,180.20	774,144.08	32° 33' 5.280 N	103° 34' 39.963 W
3,000.0	8.00	64.02	2,992.9	48.8	100.1	565,186.30	774,156.59	32° 33' 5.339 N	103° 34' 39.816 W
3,100.0	8.00	64.02	3,091.9	54.9	112.6	565,192.40	774,169.10	32° 33' 5.399 N	103° 34' 39.669 W
3,200.0		64.02	3,190.9	61.0	125.1	565,198.49	774,181.61	32° 33' 5.458 N	103° 34' 39.523 W
3,300.0		64.02	3,289.9	67.1	137.7	565,204.59	774,194.13	32° 33' 5.518 N	103° 34' 39.376 W
3,400.0		64.02	3,389.0	73.2	150.2	565,210.69	774,206.64	32° 33' 5.577 N	103° 34' 39.229 W
3,500.0		64.02	3,488.0	79.3	162.7	565,216.78	774,219.15	32° 33' 5.637 N	103° 34' 39.083 W
3,600.0		64.02	3,587.0	85.4	175.2	565,222.88	774,231.66	32° 33' 5.696 N	103° 34' 38.936 W
3,700.0		64.02	3,686.0	91.5	187.7	565,228.98	774,244.17	32° 33' 5.755 N	103° 34' 38.789 W
3,800.0		64.02	3,785.1	97.6	200.2	565,235.08	774,256.68	32° 33' 5.815 N	103° 34' 38.643 W
3,900.0		64.02	3,884.1	103.7	212.7	565,241.17	774,269.19	32° 33' 5.874 N	103° 34' 38.496 W
4,000.0		64.02	3,983.1	109.8	225.2	565,247.27	774,281.70	32° 33' 5.934 N	103° 34' 38.349 W
4,100.0		64.02	4,082.2	115.9	237.7	565,253.37	774,294.21	32° 33' 5.993 N	103° 34' 38.203 W
4,200.0		64.02	4,181.2	122.0	250.3	565,259.46	774,306.72	32° 33' 6.053 N	103° 34' 38.056 W
4,300.0		64.02	4,280.2	128.1	262.8	565,265.56	774,319.23	32° 33' 6.112 N	103° 34' 37.909 W
4,400.0		64.02	4,379.2	134.2	275.3	565,271.66	774,331.74	32° 33' 6.172 N	103° 34' 37.763 W
4,431.7		64.02	4,410.6	136.1	279.2	565,273.59	774,335.71	32° 33' 6.190 N	103° 34' 37.716 W
	rop -2.00	04.00	4 470 4	400.0	0074	FOF 077 40	774 040 50	00% 001 0 000 N	4008 041 07 005 144
4,500.0		64.02	4,478.4	139.9	287.1	565,277.40	774,343.53	32° 33' 6.228 N	103° 34' 37.625 W
4,600.0		64.02	4,577.9	144.2	295.9	565,281.70	774,352.35	32° 33' 6.270 N	103° 34' 37.521 W
4,700.0		64.02	4,677.7	147.0	301.6	565,284.48	774,358.05	32° 33' 6.297 N 32° 33' 6.309 N	103° 34' 37.454 W
4,800.0	0.63	64.02	4,777.6	148.2	304.1	565,285.73	774,360.61	32 33 0.309 N	103° 34' 37.424 W

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COMPASS 5000.17 Build 03

Planning Report - Geographic

Database:	Compass	Local Co-ordinate Reference:	Well ROBIN FED 134H
Company:	NEW MEXICO	TVD Reference:	KB @ 3700.0usft
Project:	(SP) LEA	MD Reference:	KB @ 3700.0usft
Site:	ROBIN PROJECT	North Reference:	Grid
Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Wellbore:	PILOT HOLE		
Design:	PHPWP0		

### Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude
4,831.7		0.00	4,809.3	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
Start 7	790.7 hold at	t 4831.7 MD	)						
4,900.0	0.00	0.00	4,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,000.0	0.00	0.00	4,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,100.0	0.00	0.00	5,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,200.0		0.00	5,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,300.0		0.00	5,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,400.0		0.00	5,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,500.0		0.00	5,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,600.0		0.00	5,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,700.0		0.00	5,677.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,800.0		0.00	5,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
5,900.0		0.00	5,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,000.0		0.00	5,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,100.0		0.00	6,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,200.0		0.00	6,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,300.0 6,400.0		0.00 0.00	6,277.6 6,377.6	148.3 148.3	304.3 304.3	565,285.80 565,285.80	774,360.77 774,360.77	32° 33' 6.310 N 32° 33' 6.310 N	103° 34' 37.422 W 103° 34' 37.422 W
6,500.0		0.00	6,377.6 6,477.6	146.3	304.3 304.3	565,285.80 565,285.80		32° 33' 6.310 N	103 34 37.422 W
6,600.0		0.00	6,577.6	148.3	304.3 304.3	565,285.80	774,360.77 774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,700.0		0.00	6,677.6	148.3	304.3 304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,800.0		0.00	6,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
6,900.0		0.00	6,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,000.0		0.00	6,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,100.0		0.00	7,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,200.0		0.00	7,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,300.0		0.00	7,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,400.0		0.00	7,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,500.0		0.00	7,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,600.0		0.00	7,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,700.0		0.00	7,677.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,800.0		0.00	7,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
7,900.0		0.00	7,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,000.0	0.00	0.00	7,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,100.0	0.00	0.00	8,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,200.0	0.00	0.00	8,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,300.0	0.00	0.00	8,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,400.0	0.00	0.00	8,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,500.0	0.00	0.00	8,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,600.0		0.00	8,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,700.0		0.00	8,677.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,800.0		0.00	8,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
8,900.0		0.00	8,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,000.0		0.00	8,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,100.0		0.00	9,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,200.0		0.00	9,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,300.0		0.00	9,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,400.0		0.00	9,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,500.0		0.00	9,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,600.0		0.00	9,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,700.0		0.00	9,677.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,800.0		0.00	9,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
9,900.0		0.00	9,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,000.0	0.00	0.00	9,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W

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Planning Report - Geographic

Database:	Compass	Local Co-ordinate Reference:	Well ROBIN FED 134H
Company:	NEW MEXICO	TVD Reference:	KB @ 3700.0usft
Project:	(SP) LEA	MD Reference:	KB @ 3700.0usft
Site:	ROBIN PROJECT	North Reference:	Grid
Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Wellbore:	PILOT HOLE	•	
Design:	PHPWP0		

### Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Map Northing (usft)	Map Easting (usft)	Latitude	Longitude
. ,			. ,	. ,		. ,	. ,		J
10,100.0		0.00	10,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,200.0		0.00	10,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,300.0		0.00	10,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,400.0		0.00	10,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,500.0		0.00	10,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,600.0		0.00	10,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,700.0		0.00	10,677.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,800.0	0.00	0.00	10,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
10,900.0	0.00	0.00	10,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,000.0	0.00	0.00	10,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,100.0	0.00	0.00	11,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,200.0	0.00	0.00	11,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,300.0	0.00	0.00	11,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,400.0	0.00	0.00	11,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,500.0	0.00	0.00	11,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,600.0	0.00	0.00	11,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,700.0	0.00	0.00	11,677.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,800.0	0.00	0.00	11,777.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
11,900.0	0.00	0.00	11,877.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,000.0	0.00	0.00	11,977.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,100.0	0.00	0.00	12,077.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,200.0	0.00	0.00	12,177.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,300.0	0.00	0.00	12,277.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,400.0	0.00	0.00	12,377.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,500.0	0.00	0.00	12,477.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,600.0	0.00	0.00	12,577.6	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
12,622.4	0.00	0.00	12,600.0	148.3	304.3	565,285.80	774,360.77	32° 33' 6.310 N	103° 34' 37.422 W
TD at 1	2622.4								

### **Plan Annotations**

Measured	Vertical	Local Coordinates		
Depth (usft)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Comment
2,000.0	2,000.0	0.0	0.0	Start Build 2.00
2,400.0	2,398.7	12.2	25.1	Start 2031.7 hold at 2400.0 MD
4,431.7	4,410.6	136.1	279.2	Start Drop -2.00
4,831.7	4,809.3	148.3	304.3	Start 7790.7 hold at 4831.7 MD
12,622.4	12,600.0	148.3	304.3	TD at 12622.4

# NEW MEXICO (SP) LEA

ROBIN PROJECT ROBIN FED 134H

PILOT HOLE PHPWP0

# **Anticollision Report**

26 February, 2024

Anticollision Report

Company: Project: Reference Site: Site Error:	NEW MEXICO (SP) LEA ROBIN PROJECT 0.0 usft	Local Co-ordinate Reference: TVD Reference: MD Reference: North Reference:	Well ROBIN FED 134H KB @ 3700.0usft KB @ 3700.0usft Grid							
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature							
Well Error:	0.0 usft	Output errors are at	2.00 sigma							
Reference Wellbore	PILOT HOLE	Database:	Compass							
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum							
Reference	PHPWP0									
Filter type:	Filter type: NO GLOBAL FILTER: Using user defined selection & filtering criteria									

Results Limited by: Warning Levels Evaluation		Error Surface: Casing Method:	
	Maximum centre distance of 800.0usft	Error Surface:	Pedal Curve
Depth Range:	Unlimited	Scan Method:	Closest Approach 3D
interpolation wethod:	Stations	Error Model:	ISCWSA

Survey Tool P	Program	Date 2/26/2024		
From (usft)	To (usft)	Survey (Wellbore)	Tool Name	Description
	0.0 12,622.	4 PHPWP0 (PILOT HOLE)	MWD	OWSG_Rev2_MWD - Standard

Summary

	Reference	Offset	Dista	nce			
Site Name Offset Well - Wellbore - Design	Measured Depth (usft)	Measured Depth (usft)	Between Centres (usft)	Between Ellipses (usft)	Separation Factor	Warning	
ROBIN PROJECT							
ROBIN FED 133H - OWB - PWP0	1,966.3	1,967.3	60.0	46.1	4.312	CC	
ROBIN FED 133H - OWB - PWP0	2,000.0	2,000.0	60.0	45.9	4.241	ES, SF	
ROBIN FED 134H - OWB - PWP0	2,009.4	2,009.4	0.0	-14.2	0.000	Level 3, CC, SF	
ROBIN FED 134H - OWB - PWP0	10,600.0	10,599.3	0.1	-75.3	0.001	Level 3, ES	
ROBIN FED 203H - OWB - PWP0	2,000.0	2,000.0	30.0	15.8	2.119	CC, ES, SF	
ROBIN FED 204H - OWB - PWP0	1,965.3	1,969.3	30.0	16.1	2.159	CC	
ROBIN FED 204H - OWB - PWP0	2,200.0	2,201.9	30.9	15.4	1.992	ES	
ROBIN FED 204H - OWB - PWP0	2,300.0	2,300.8	32.0	15.8	1.979	SF	

# Offset Design: ROBIN PROJECT - ROBIN FED 133H - OWB - PWP0

	-												Offset Site Error:	0.0 us
Survey Prog Refer	rence	MWD Off			laior Axis		Offset Wellb	ore Centre		Rule Assig			Offset Well Error:	0.0 us
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	+N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
0.0	0.0	1.0	1.0	0.0	0.0	-91.59	-1.7	-60.0	60.0					
100.0	100.0	101.0	101.0	0.3	0.3	-91.59	-1.7	-60.0	60.0	59.5	0.53	112.339		
200.0	200.0	201.0	201.0	0.6	0.6	-91.59	-1.7	-60.0	60.0	58.8	1.25	47.961		
300.0	300.0	301.0	301.0	1.0	1.0	-91.59	-1.7	-60.0	60.0	58.0	1.97	30.489		
400.0	400.0	401.0	401.0	1.3	1.3	-91.59	-1.7	-60.0	60.0	57.3	2.68	22.348		
500.0	500.0	501.0	501.0	1.7	1.7	-91.59	-1.7	-60.0	60.0	56.6	3.40	17.638		
600.0	600.0	601.0	601.0	2.1	2.1	-91.59	-1.7	-60.0	60.0	55.9	4.12	14.568		
700.0	700.0	701.0	701.0	2.4	2.4	-91.59	-1.7	-60.0	60.0	55.2	4.84	12.408		
800.0	800.0	801.0	801.0	2.8	2.8	-91.59	-1.7	-60.0	60.0	54.5	5.55	10.806		
900.0	900.0	901.0	901.0	3.1	3.1	-91.59	-1.7	-60.0	60.0	53.7	6.27	9.570		
1,000.0	1,000.0	1,001.0	1,001.0	3.5	3.5	-91.59	-1.7	-60.0	60.0	53.0	6.99	8.588		
1,100.0	1,100.0	1,101.0	1,101.0	3.8	3.9	-91.59	-1.7	-60.0	60.0	52.3	7.70	7.789		
1,200.0	1,200.0	1,201.0	1,201.0	4.2	4.2	-91.59	-1.7	-60.0	60.0	51.6	8.42	7.126		
1,300.0	1,300.0	1,301.0	1,301.0	4.6	4.6	-91.59	-1.7	-60.0	60.0	50.9	9.14	6.567		
1,400.0	1,400.0	1,401.0	1,401.0	4.9	4.9	-91.59	-1.7	-60.0	60.0	50.1	9.85	6.089		
1,500.0	1,500.0	1,501.0	1,501.0	5.3	5.3	-91.59	-1.7	-60.0	60.0	49.4	10.57	5.676		
1,600.0	1,600.0	1,601.0	1,601.0	5.6	5.6	-91.59	-1.7	-60.0	60.0	48.7	11.29	5.316		
1,700.0	1,700.0	1,701.0	1,701.0	6.0	6.0	-91.59	-1.7	-60.0	60.0	48.0	12.01	4.998		
1,800.0	1,800.0	1,801.0	1,801.0	6.4	6.4	-91.59	-1.7	-60.0	60.0	47.3	12.72	4.716		
1,900.0	1,900.0	1,901.0	1,901.0	6.7	6.7	-91.59	-1.7	-60.0	60.0	46.6	13.44	4.465		

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Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 133H - OWB - PWP0

urvey Prog		MWD							_	Rule Assig	gned:		Offset Well Error:	0.0 us
Refer leasured	Vertical	Offs Measured	set Vertical	Semi M Reference	laior Axis Offset	Highside	Offset Wellb	ore Centre		ance Between	Minimum	Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor	nanng	
1,966.3	1,966.3	1,967.3	1,967.3	7.0	7.0	-91.59	-1.7	-60.0	60.0	46.1	13.91	4.312 CC		
2,000.0	2,000.0	2,000.0	2,000.0	7.1	7.1	-91.59	-1.7	-60.0	60.0	45.9	14.15	4.241 ES,	SF	
2,100.0	2,100.0	2,098.8	2,098.8	7.4	7.4	-155.99	-1.5	-61.7	63.3	48.5	14.85	4.265		
2,200.0	2,199.8	2,196.1	2,195.9	7.8	7.8	-156.94	-0.9	-66.6	73.2	57.7	15.51	4.719		
2,300.0	2,299.5	2,292.0	2,291.5	8.1	8.1	-158.04	0.1	-74.7	89.6	73.4	16.15	5.545		
2,400.0	2,398.7	2,386.1	2,385.0	8.5	8.4	-159.01	1.4	-85.8	112.3	95.6	16.77	6.698		
2,500.0	2,497.7	2,478.3	2,476.1	8.9	8.8	-159.73	3.1	-99.5	139.8	122.4	17.37	8.050		
2,600.0	2,596.8	2,572.8	2,569.1	9.2	9.1	-160.05	5.0	-115.7	169.4	151.4	18.02	9.402		
2,700.0	2,695.8	2,668.3	2,663.2	9.6	9.5	-160.27	7.0	-132.2	199.1	180.4	18.69	10.651		
2,800.0	2,794.8	2,763.7	2,757.2	10.0	9.8	-160.43	8.9	-148.7	228.8	209.4	19.37	11.810		
2,900.0	2,893.8	2,859.2	2,851.2	10.3	10.2	-160.56	10.9	-165.1	258.4	238.4	20.05	12.888		
3,000.0	2,992.9	2,954.7	2,945.3	10.7	10.6	-160.66	12.9	-181.6	288.1	267.4	20.74	13.894		
3,100.0	3,091.9	3,050.2	3,039.3	11.1	11.0	-160.74	14.8	-198.1	317.8	296.4	21.43	14.833		
3,200.0	3,190.9	3,145.7	3,133.4	11.5	11.4	-160.81	16.8	-214.5	347.5	325.4	22.12	15.713		
3,300.0	3,289.9	3,241.2	3,227.4	11.9	11.7	-160.87	18.8	-231.0	377.2	354.4	22.81	16.537		
3,400.0	3,389.0	3,336.7	3,321.4	12.3	12.1	-160.91	20.7	-247.5	406.9	383.4	23.50	17.311		
3,500.0	3,488.0	3,432.2	3,415.5	12.7	12.5	-160.96	22.7	-263.9	436.6	412.4	24.20	18.039		
3,600.0	3,587.0	3,527.7	3,509.5	13.1	12.9	-160.99	24.7	-280.4	466.3	441.4	24.90	18.725		
3,700.0	3,686.0	3,623.2	3,603.6	13.5	13.3	-161.03	26.6	-296.9	496.0	470.4	25.60	19.373		
3,800.0	3,785.1	3,718.7	3,697.6	13.9	13.7	-161.05	28.6	-313.3	525.6	499.3	26.30	19.985		
3,900.0	3,884.1	3,814.1	3,791.6	14.3	14.1	-161.08	30.6	-329.8	555.3	528.3	27.01	20.564		
4,000.0	3,983.1	3,909.6	3,885.7	14.7	14.5	-161.10	32.5	-346.3	585.0	557.3	27.71	21.112		
4,100.0	4,082.2	4,005.1	3,979.7	15.1	14.9	-161.12	34.5	-362.7	614.7	586.3	28.42	21.633		
4,200.0	4,181.2	4,100.6	4,073.8	15.5	15.3	-161.14	36.5	-379.2	644.4	615.3	29.12	22.127		
4,300.0	4,280.2	4,196.1	4,167.8	15.9	15.8	-161.16	38.4	-395.6	674.1	644.3	29.83	22.597		
4,400.0	4,379.2	4,291.6	4,261.8	16.3	16.2	-161.18	40.4	-412.1	703.8	673.2	30.54	23.045		
4,431.7	4,410.6	4,321.8	4,291.6	16.4	16.3	-161.18	41.0	-417.3	713.2	682.4	30.76	23.182		
4,500.0	4,478.4	4,387.3	4,356.1	16.7	16.6	-161.30	42.4	-428.6	732.7	701.5	31.25	23.448		
4,600.0	4,577.9	4,483.9	4,451.2	17.1	17.0	-161.38	44.3	-445.3	758.7	726.7	31.96	23.738		
4,700.0	4,677.7	4,581.2	4,547.1	17.4	17.4	-161.36	46.4	-462.0	781.4	748.7	32.67	23.917		

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

# Offset Design: ROBIN PROJECT - ROBIN FED 134H - OWB - PWP0

Survey Prog Refer Measured Depth (usft) 2,009.4 2,100.0	rence	MWD Off	set	Comi A						Rule Assig	aned:	Offset Well Error	0.0 usft
Measured Depth (usft) 2,009.4	Vertical						Offeet Wellb	ara Cantra	Diet	anaa			
<b>(usft)</b> 2,009.4	Donth	weasureu	Vertical	Reference	Aajor Axis Offset	Highside	Offset Wellb		Between	ance Between	Minimum	Separation Warnin	g
2,009.4	(usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor	-
2 100 0	2,009.4	2,009.4	2,009.4	7.1	7.1	-90.03	0.0	0.0	0.0	-14.2	14.22	0.000 Level 3, CC, SF	
2,100.0	2,100.0	2,100.0	2,100.0	7.4	7.4	-90.03	0.8	1.6	0.0	-14.9	14.86	0.000 Level 3	
2,200.0	2,199.8	2,200.0	2,199.8	7.8	7.8	-90.03	3.1	6.3	0.0	-15.6	15.56	0.000 Level 3	
2,300.0	2,299.5	2,300.0	2,299.5	8.1	8.1	-90.03	6.9	14.1	0.0	-16.3	16.27	0.000 Level 3	
2,400.0	2,398.7	2,400.0	2,398.7	8.5	8.5	-90.03	12.2	25.1	0.0	-17.0	16.98	0.000 Level 3	
2,500.0	2,497.7	2,500.0	2,497.7	8.9	8.9	-90.02	18.3	37.6	0.0	-17.7	17.71	0.000 Level 3	
2,600.0	2,596.8	2,600.0	2,596.8	9.2	9.2	-90.01	24.4	50.1	0.0	-18.4	18.44	0.000 Level 3	
2,700.0	2,695.8	2,700.0	2,695.8	9.6	9.6	-90.01	30.5	62.6	0.0	-19.2	19.19	0.000 Level 3	
2,800.0	2,794.8	2,800.0	2,794.8	10.0	10.0	-90.01	36.6	75.1	0.0	-19.9	19.94	0.000 Level 3	
2,900.0	2,893.8	2,900.0	2,893.8	10.3	10.3	-90.01	42.7	87.6	0.0	-20.7	20.70	0.000 Level 3	
3,000.0	2,992.9	3,000.0	2,992.9	10.7	10.7	-90.01	48.8	100.1	0.0	-21.5	21.46	0.000 Level 3	
3,100.0	3,091.9	3,100.0	3,091.9	11.1	11.1	-90.01	54.9	112.6	0.0	-22.2	22.23	0.000 Level 3	
3,200.0	3,190.9	3,200.0	3,190.9	11.5	11.5	-90.01	61.0	125.1	0.0	-23.0	23.01	0.000 Level 3	
3,300.0	3,289.9	3,300.0	3,289.9	11.9	11.9	-90.01	67.1	137.7	0.0	-23.8	23.78	0.000 Level 3	
3,400.0	3,389.0	3,400.0	3,389.0	12.3	12.3	-90.01	73.2	150.2	0.0	-24.6	24.57	0.000 Level 3	
3,500.0	3,488.0	3,500.0	3,488.0	12.7	12.7	-90.01	79.3	162.7	0.0	-25.3	25.35	0.000 Level 3	
3,600.0	3,587.0	3,600.0	3,587.0	13.1	13.1	-90.01	85.4	175.2	0.0	-26.1	26.14	0.000 Level 3	
3,700.0	3,686.0	3,700.0	3,686.0	13.5	13.5	-90.00	91.5	187.7	0.0	-26.9	26.94	0.001 Level 3	
3,800.0	3,785.1	3,800.0	3,785.1	13.9	13.9	-90.00	97.6	200.2	0.0	-27.7	27.73	0.001 Level 3	
3,900.0	3,884.1	3,900.0	3,884.1	14.3	14.3	-90.00	103.7	212.7	0.0	-28.5	28.53	0.001 Level 3	
4,000.0	3,983.1	4,000.0	3,983.1	14.7	14.7	-90.00	109.8	225.2	0.0	-29.3	29.33	0.001 Level 3	
4,100.0	4,082.2	4,100.0	4,082.2	15.1	15.1	-90.00	115.9	237.7	0.0	-30.1	30.13	0.001 Level 3	
4,200.0	4,181.2	4,200.0	4,181.2	15.5	15.5	-90.00	122.0	250.2	0.0	-30.9	30.93	0.001 Level 3	
4,300.0	4,280.2	4,300.0	4,280.3	15.9	15.9	-177.39	127.9	262.4	0.4	-30.1	30.51	0.014 Level 3	
4,400.0	4,379.2	4,400.0	4,379.5	16.3	16.3	-179.55	133.1	273.0	2.5	-28.8	31.27	0.080 Level 3	
4,431.7	4,410.6	4,431.6	4,411.0	16.4	16.4	-179.68	134.6	276.1	3.5	-28.0	31.51	0.111 Level 3	
4,500.0	4,478.4	4,499.8	4,478.9	16.7	16.7	-179.79	137.5	282.1	5.5	-26.5	32.01	0.172 Level 3	
4,600.0	4,577.9	4,599.7	4,578.4	17.1	17.0	-179.83	141.2	289.7	6.9	-25.8	32.74	0.212 Level 3	
4,700.0	4,677.7	4,699.6	4,678.1	17.4	17.4	-179.82	144.1	295.6	6.6	-26.8	33.46	0.198 Level 3	
4,800.0	4,777.6	4,799.5	4,777.8	17.8	17.8	-179.73	146.3	300.0	4.6	-29.6	34.16	0.133 Level 3	
4,831.7	4,809.3	4,831.1	4,809.4	17.9	17.9	-115.63	146.8	301.1	3.5	-30.8	34.38	0.103 Level 3	
4,900.0	4,877.6	4,899.4	4,877.7	18.1	18.1	-115.18	147.6	302.9	1.6	-33.3	34.84	0.045 Level 3	
5,000.0	4,977.6	4,999.3	4,977.6	18.5	18.5	-106.60	148.3	304.2	0.1	-35.4	35.53	0.004 Level 3	
5,048.2	5,025.9	5,047.6	5,025.9	18.6	18.6	-90.00	148.3	304.2	0.1	-36.0	36.05	0.001 Level 3	
5,100.0	5,077.6	5,099.3	5,077.6	18.8	18.8	-90.00	148.3	304.2	0.1	-36.4	36.41	0.001 Level 3	
5,200.0	5,177.6	5,199.3	5,177.6	19.1	19.1	-90.00	148.3	304.2	0.1	-37.1	37.11	0.001 Level 3	
5,300.0	5,277.6	5,299.3	5,277.6	19.5	19.5	-90.00	148.3	304.2	0.1	-37.8	37.81	0.001 Level 3	
5,400.0	5,377.6	5,399.3	5,377.6	19.8	19.8	-90.00	148.3	304.2	0.1	-38.5	38.51	0.001 Level 3	
5,500.0	5,477.6	5,499.3	5,477.6	20.2	20.2	-90.00	148.3	304.2	0.1	-39.2	39.21	0.001 Level 3	
5,600.0	5,577.6	5,599.3	5,577.6	20.5	20.5	-90.00	148.3	304.2	0.1	-39.9	39.91	0.001 Level 3	
5,700.0	5,677.6	5,699.3	5,677.6	20.9	20.9	-90.00	148.3	304.2	0.1	-40.6	40.61	0.001 Level 3	
5,800.0	5,777.6	5,799.3	5,777.6	21.2	21.2	-90.00	148.3	304.2	0.1	-41.3	41.31	0.001 Level 3	
5,900.0	5,877.6	5,899.3	5,877.6	21.5	21.5	-90.00	148.3	304.2	0.1	-42.0	42.01	0.001 Level 3	
6,000.0	5,977.6	5,999.3	5,977.6	21.9	21.9	-90.00	148.3	304.2	0.1	-42.7	42.72	0.001 Level 3	
6,100.0	6,077.6	6,099.3	6,077.6	22.2	22.2	-90.00	148.3	304.2	0.1	-43.4	43.42	0.001 Level 3	
6,200.0	6,177.6	6,199.3	6,177.6	22.6	22.6	-90.00	148.3	304.2	0.1	-44.1	44.12	0.001 Level 3	
6,300.0	6,277.6	6,299.3	6,277.6	22.9	22.9	-90.00	148.3	304.2	0.1	-44.8	44.83	0.001 Level 3	
6,400.0	6,377.6	6,399.3	6,377.6	23.3	23.3	-90.00	148.3	304.2	0.1	-45.5	45.53	0.001 Level 3	
6,500.0	6,477.6	6,499.3	6,477.6	23.6	23.6	-90.00	148.3	304.2	0.1	-46.2	46.24	0.001 Level 3	
6,600.0	6,577.6	6,599.3	6,577.6	24.0	24.0	-90.00	148.3	304.2	0.1	-46.9	46.94	0.001 Level 3	
6,700.0	6,677.6	6,699.3	6,677.6	24.3	24.3	-90.00	148.3	304.2	0.1	-47.6	47.65	0.001 Level 3	
6,800.0	6,777.6	6,799.3	6,777.6	24.7	24.7	-90.00	148.3	304.2	0.1	-48.3	48.36	0.001 Level 3	

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COMPASS 5000.17 Build 03

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 134H - OWB - PWP0

0	sign		JECI -	ROBIN FE	D 134H ·	- OWB - P\	WP0						Offset Site Error:	0.0 usft
Survey Prog	uram: 0-	MWD								Rule Assig	ned.		Offset Well Error:	0.0 usft
Refere	ence	Off			laior Axis		Offset Wellb	ore Centre		tance		<b>.</b>		0.0 usit
Measured Depth	Vertical Depth	Measured Depth	Vertical Depth	Reference	Offset	Highside Toolface	+N/-S	+E/-W	Between Centres	Between Ellipses	Minimum Separation	Separation Factor	Warning	
(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	(°)	(usft)	(usft)	(usft)	(usft)	(usft)			
6,900.0	6,877.6	6,899.3	6,877.6	25.0	25.0	-90.00	148.3	304.2	0.1	-49.0	49.06	0.001 Lev	/el 3	
7,000.0	6,977.6	6,999.3	6,977.6	25.4	25.4	-90.00	148.3	304.2	0.1	-49.7	49.77	0.001 Lev		
7,100.0	7,077.6	7,099.3	7,077.6	25.7	25.7	-90.00	148.3	304.2	0.1	-50.4	50.48	0.001 Lev		
7,200.0	7,177.6	7,199.3	7,177.6	26.1	26.1	-90.00	148.3	304.2	0.1	-51.1	51.18	0.001 Lev		
7,300.0	7,277.6	7,299.3	7,277.6	26.4	26.4	-90.00	148.3	304.2	0.1	-51.8	51.89	0.001 Lev		
7,400.0	7,377.6	7,399.3	7,377.6	26.8	26.8	-90.00	148.3	304.2	0.1	-52.5	52.60	0.001 Lev	/el 3	
7,500.0	7,477.6	7,499.3	7,477.6	27.1	27.1	-90.00	148.3	304.2	0.1	-53.3	53.31	0.001 Lev	vel 3	
7,600.0	7,577.6	7,599.3	7,577.6	27.5	27.5	-90.00	148.3	304.2	0.1	-54.0	54.02	0.001 Lev	vel 3	
7,700.0	7,677.6	7,699.3	7,677.6	27.8	27.8	-90.00	148.3	304.2	0.1	-54.7	54.72	0.001 Lev	vel 3	
7,800.0	7,777.6	7,799.3	7,777.6	28.2	28.2	-90.00	148.3	304.2	0.1	-55.4	55.43	0.001 Lev		
7,900.0	7,877.6	7,899.3	7,877.6	28.5	28.5	-90.00	148.3	304.2	0.1	-56.1	56.14	0.001 Lev	vel 3	
8,000.0	7,977.6	7,999.3	7,977.6	28.9	28.9	-90.00	148.3	304.2	0.1	-56.8	56.85	0.001 Lev	vel 3	
8,100.0	8,077.6	8,099.3	8,077.6	29.2	29.2	-90.00	148.3	304.2	0.1	-57.5	57.56	0.001 Lev		
8,200.0	8,177.6	8,199.3	8,177.6	29.6	29.6	-90.00	148.3	304.2	0.1	-58.2	58.27	0.001 Lev		
8,300.0	8,277.6	8,299.3	8,277.6	29.9	29.9	-90.00	148.3	304.2	0.1	-58.9	58.98	0.001 Lev		
8,400.0	8,377.6	8,399.3	8,377.6	30.3	30.3	-90.00	148.3	304.2	0.1	-59.6	59.69	0.001 Lev		
0.500.0	0 177 0	0 100 0	0 477 0			~~~~					00.40	0.004.1		
8,500.0	8,477.6	8,499.3	8,477.6	30.6	30.6	-90.00	148.3	304.2	0.1	-60.3	60.40	0.001 Lev		
8,600.0 8,700.0	8,577.6	8,599.3	8,577.6	31.0	31.0	-90.00	148.3	304.2	0.1	-61.1	61.11	0.001 Lev 0.001 Lev		
8,800.0	8,677.6 8,777.6	8,699.3 8,799.3	8,677.6 8,777.6	31.3 31.7	31.3 31.7	-90.00 -90.00	148.3 148.3	304.2 304.2	0.1 0.1	-61.8 -62.5	61.82 62.53	0.001 Lev		
8,900.0	8,877.6	8,899.3	8,877.6	32.0	32.0	-90.00	148.3	304.2 304.2	0.1	-63.2	63.24	0.001 Lev		
0,000.0	0,077.0	0,000.0	0,077.0	52.0	52.0	-30.00	140.0	504.2	0.1	-00.2	05.24	0.001 LC		
9,000.0	8,977.6	8,999.3	8,977.6	32.4	32.4	-90.00	148.3	304.2	0.1	-63.9	63.95	0.001 Lev	vel 3	
9,100.0	9,077.6	9,099.3	9,077.6	32.7	32.7	-90.00	148.3	304.2	0.1	-64.6	64.66	0.001 Lev	vel 3	
9,200.0	9,177.6	9,199.3	9,177.6	33.1	33.1	-90.00	148.3	304.2	0.1	-65.3	65.37	0.001 Lev		
9,300.0	9,277.6	9,299.3	9,277.6	33.4	33.4	-90.00	148.3	304.2	0.1	-66.0	66.09	0.001 Lev		
9,400.0	9,377.6	9,399.3	9,377.6	33.8	33.8	-90.00	148.3	304.2	0.1	-66.7	66.80	0.001 Lev	vel 3	
9,500.0	9,477.6	9,499.3	9,477.6	34.2	34.1	-90.00	148.3	304.2	0.1	-67.5	67.51	0.001 Lev	vel 3	
9,600.0	9,577.6	9,599.3	9,577.6	34.5	34.5	-90.00	148.3	304.2	0.1	-68.2	68.22	0.001 Lev		
9,700.0	9,677.6	9,699.3	9,677.6	34.9	34.8	-90.00	148.3	304.2	0.1	-68.9	68.93	0.001 Lev		
9,800.0	9,777.6	9,799.3	9,777.6	35.2	35.2	-90.00	148.3	304.2	0.1	-69.6	69.64	0.001 Lev	vel 3	
9,900.0	9,877.6	9,899.3	9,877.6	35.6	35.6	-90.00	148.3	304.2	0.1	-70.3	70.35	0.001 Lev	vel 3	
10,000,0	0.077.0	0 000 0	0.077.0	05.0	05.0	00.00	140.0	004.0	0.4	74.0	74.07	0.004.1		
10,000.0	9,977.6	9,999.3	9,977.6	35.9	35.9	-90.00	148.3	304.2	0.1	-71.0	71.07	0.001 Lev		
	10,077.6 10,177.6	10,099.3 10,199.3	10,077.6 10,177.6	36.3 36.6	36.3 36.6	-90.00 -90.00	148.3 148.3	304.2 304.2	0.1	-71.7 -72.4	71.78 72.49	0.001 Lev 0.001 Lev		
	10,177.6	10,199.3	10,177.6	30.0 37.0	36.6 37.0	-90.00	148.3	304.2 304.2	0.1 0.1	-72.4	72.49	0.001 Lev		
	10,277.6	10,299.3	10,277.6	37.3	37.3	-90.00	148.3	304.2	0.1	-73.9	73.92	0.001 Lev		
	-,5	, 500.0		01.0	51.0	- 5.00			0.1	. 0.0	. 0.02	2.50.20		
10,500.0	10,477.6	10,499.3	10,477.6	37.7	37.7	-90.00	148.3	304.2	0.1	-74.6	74.63	0.001 Lev		
	10,543.9	10,565.6	10,543.9	37.9	37.9	-90.00	148.3	304.2	0.1	-75.1	75.10	0.001 Lev		
	10,577.6	10,599.3	10,577.6	38.0	38.0	-84.57	148.3	304.2	0.1	-75.3	75.40	0.001 Lev		
	10,677.6	10,697.8	10,675.4	38.4	38.4	-0.71	158.9	304.2	10.8	-64.9	75.71	0.143 Lev		
10,800.0	10,777.6	10,788.4	10,761.6	38.8	38.7	-0.52	186.1	304.0	41.0	-32.5	73.53	0.558 Lev	/el 3	
10,900.0	10,877.6	10,866.6	10,830.8	39.1	39.0	-0.48	222.3	303.7	87.6	17.2	70.35	1.245 Lev	vel 3	
	10,977.6	10,931.4	10,883.1	39.5	39.2	-0.47	260.6	303.4	146.8	79.8	66.99	2.191		
	11,077.6	10,984.2	10,921.5	39.8	39.3	-0.46	296.7	303.1	215.4	151.5	63.92	3.370		
11,200.0	11,177.6	11,025.0	10,948.3	40.2	39.5	-0.46	327.5	302.9	291.0	229.9	61.07	4.765		
11,300.0	11,277.6	11,062.1	10,970.3	40.5	39.6	-0.46	357.3	302.6	371.6	312.4	59.22	6.275		
44,400.0	44 077 6	44 000 0	40.005.0	10.5	cc 7	0.45	001 5	000 4	150 6	000 5	F7 50	7 000		
	11,377.6	11,090.9 11 114 8	10,985.8	40.9	39.7 30.8	-0.45	381.5	302.4	456.0	398.5	57.56 56.27	7.922		
	11,477.6 11,577.6	11,114.8 11,134.9	10,997.5 11,006.5	41.2 41.6	39.8 39.8	-0.45 -0.45	402.4 420.4	302.3 302.1	543.2 632.6	487.0 577.3	56.27 55.29	9.653 11.442		
	11,577.6		11,006.5	41.0	39.8 39.9	-0.45 -0.45	420.4 434.1	302.1	032.0 723.7	669.2	55.29 54.45	13.289		
11,700.0	. 1,077.0	11,100.0	11,012.0	-1.5	55.5	0.70	1.107	002.0	120.1	000.2	07.70	10.200		

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 203H - OWB - PWP0

Irvey Pro	oram 0.	MWD								Rule Assig	aned:		Offset Well Error:	0.0 u
Refe	rence	Off			laior Axis		Offset Wellb	ore Centre		ance		•		0.0 u
easured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	+N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
0.0	0.0	0.0	0.0	0.0	0.0	-91.55	-0.8	-30.0	30.0					
100.0	100.0	100.0	100.0	0.3	0.3	-91.55	-0.8	-30.0	30.0	29.5	0.53	56.529		
200.0	200.0	200.0	200.0	0.6	0.6	-91.55	-0.8	-30.0	30.0	28.7	1.25	24.041		
300.0	300.0	300.0	300.0	1.0	1.0	-91.55	-0.8	-30.0	30.0	28.0	1.96	15.267		
400.0	400.0	400.0	400.0	1.3	1.3	-91.55	-0.8	-30.0	30.0	27.3	2.68	11.185		
500.0	500.0	500.0	500.0	1.7	1.7	-91.55	-0.8	-30.0	30.0	26.6	3.40	8.825		
600.0	600.0	600.0	600.0	2.1	2.1	-91.55	-0.8	-30.0	30.0	25.9	4.12	7.288		
700.0	700.0	700.0	700.0	2.4	2.4	-91.55	-0.8	-30.0	30.0	25.2	4.83	6.206		
800.0	800.0	800.0	800.0	2.8	2.8	-91.55	-0.8	-30.0	30.0	24.4	5.55	5.405		
900.0	900.0	900.0	900.0	3.1	3.1	-91.55	-0.8	-30.0	30.0	23.7	6.27	4.786		
1,000.0	1,000.0	1,000.0	1,000.0	3.5	3.5	-91.55	-0.8	-30.0	30.0	23.0	6.98	4.295		
1,100.0	1,100.0	1,100.0	1,100.0	3.8	3.8	-91.55	-0.8	-30.0	30.0	22.3	7.70	3.895		
1,200.0	1,200.0	1,200.0	1,200.0	4.2	4.2	-91.55	-0.8	-30.0	30.0	21.6	8.42	3.563		
1,300.0	1,300.0	1,300.0	1,300.0	4.6	4.6	-91.55	-0.8	-30.0	30.0	20.9	9.13	3.283		
1,400.0	1,400.0	1,400.0	1,400.0	4.9	4.9	-91.55	-0.8	-30.0	30.0	20.1	9.85	3.045		
1,500.0	1,500.0	1,500.0	1,500.0	5.3	5.3	-91.55	-0.8	-30.0	30.0	19.4	10.57	2.838		
1,600.0	1,600.0	1,600.0	1,600.0	5.6	5.6	-91.55	-0.8	-30.0	30.0	18.7	11.28	2.658		
1,700.0	1,700.0	1,700.0	1,700.0	6.0	6.0	-91.55	-0.8	-30.0	30.0	18.0	12.00	2.499		
1,800.0	1,800.0	1,800.0	1,800.0	6.4	6.4	-91.55	-0.8	-30.0	30.0	17.3	12.72	2.358		
1,900.0	1,900.0	1,900.0	1,900.0	6.7	6.7	-91.55	-0.8	-30.0	30.0	16.6	13.44	2.232		
2,000.0	2,000.0	2,000.0	2,000.0	7.1	7.1	-91.55	-0.8	-30.0	30.0	15.8	14.15		C, ES, SF	
2,100.0	2,100.0	2,098.9	2,098.9	7.4	7.4	-155.98	-0.4	-31.6	33.2	18.4	14.85	2.239		
2,200.0	2,199.8	2,197.2	2,197.0	7.8	7.8	-156.84	0.8	-36.6	43.0	27.5	15.52	2.770		
2,300.0	2,299.5	2,294.2	2,293.7	8.1	8.1	-157.61	2.8	-44.6	59.2	43.0	16.17	3.659		
2,400.0	2,398.7	2,390.5	2,389.3	8.5	8.4	-158.21	5.5	-55.5	81.4	64.5	16.82	4.838		
2,500.0	2,497.7	2,487.5	2,485.6	8.9	8.8	-158.91	8.4	-67.0	105.7	88.2	17.50	6.039		
2,600.0	2,596.8	2,584.5	2,581.8	9.2	9.2	-159.35	11.3	-78.4	130.0	111.9	18.19	7.150		
2,700.0	2,695.8	2,681.4	2,678.1	9.6	9.5	-159.65	14.1	-89.9	154.4	135.5	18.87	8.180		
2,800.0	2,794.8	2,778.4	2,774.4	10.0	9.9	-159.87	17.0	-101.4	178.7	159.2	19.56	9.136		
2,900.0	2,893.8	2,875.4	2,870.6	10.3	10.2	-160.03	19.8	-112.8	203.1	182.8	20.26	10.026		
3,000.0	2,992.9	2,972.4	2,966.9	10.7	10.6	-160.16	22.7	-124.3	227.4	206.5	20.95	10.855		
3,100.0	3,091.9	3,069.4	3,063.2	11.1	11.0	-160.27	25.6	-135.8	251.8	230.1	21.65	11.631		
3,200.0	3,190.9	3,166.4	3,159.4	11.5	11.3	-160.35	28.4	-147.2	276.1	253.8	22.35	12.357		
3,300.0	3,289.9	3,263.4	3,255.7	11.9	11.7	-160.42	31.3	-158.7	300.5	277.4	23.05	13.037		
3,400.0	3,389.0	3,360.4	3,352.0	12.3	12.1	-160.49	34.1	-170.2	324.8	301.1	23.75	13.677		
3,500.0	3,488.0	3,457.4	3,448.2	12.7	12.4	-160.54	37.0	-181.6	349.2	324.7	24.45	14.279		
3,600.0	3,587.0	3,554.3	3,544.5	13.1	12.8	-160.59	39.9	-193.1	373.5	348.4	25.16	14.847		
3,700.0	3,686.0	3,651.3	3,640.8	13.5	13.2	-160.63	42.7	-204.6	397.9	372.0	25.87	15.383		
3,800.0	3,785.1	3,748.3	3,737.0	13.9	13.6	-160.66	45.6	-216.1	422.2	395.7	26.57	15.889		
3,900.0	3,884.1	3,845.3	3,833.3	14.3	13.9	-160.69	48.4	-227.5	446.6	419.3	27.28	16.369		
4,000.0	3,983.1	3,942.3	3,929.6	14.7	14.3	-160.72	51.3	-239.0	471.0	443.0	27.99	16.824		
4,100.0	4,082.2	4,039.3	4,025.8	15.1	14.7	-160.75	54.1	-250.5	495.3	466.6	28.70	17.256		
4,200.0	4,181.2	4,136.3	4,122.1	15.5	15.1	-160.77	57.0	-261.9	519.7	490.2	29.42	17.666		
4,300.0	4,280.2	4,233.3	4,218.4	15.9	15.5	-160.79	59.9	-273.4	544.0	513.9	30.13	18.057		
4,400.0	4,379.2	4,330.3	4,314.6	16.3	15.9	-160.81	62.7	-284.9	568.4	537.5	30.84	18.429		
4,431.7	4,410.6	4,361.0	4,345.1	16.4	16.0	-160.82	63.6	-288.5	576.1	545.0	31.07	18.543		
4,500.0	4,478.4	4,427.4	4,411.1	16.7	16.2	-160.91	65.6	-296.4	592.0	560.4	31.55	18.760		
4,600.0	4,577.9	4,525.3	4,508.2	17.1	16.6	-160.94	68.5	-307.9	612.5	580.3	32.27	18.982		
4,700.0	4,677.7	4,628.9	4,611.1	17.4	17.0	-160.83	71.5	-320.0	629.6	596.6	33.03	19.064		
4,800.0	4,777.6	4,739.6	4,721.2	17.4	17.5	-160.64	74.2	-331.1	642.0	608.2	33.83	18.975		
4,831.7	4,809.3	4,774.9	4,756.3	17.9	17.6	-96.55	75.0	-334.2	644.9	610.8	34.09	18.918		
4,900.0	4,877.6	4,851.0	4,832.2	18.1	17.9	-96.36	76.5	-340.2	650.1	615.4	34.63	18.772		
.,000.0	.,511.0						jent point, SF							

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

# Offset Design: ROBIN PROJECT - ROBIN FED 203H - OWB - PWP0

urvey Pro	gram: 0- rence	MWD	set	Sami B	lajor Axis		Offset Wellb	oro Contro	Diet	Rule Assig	gned:		Offset Well Error:	0.0 ust
Refe Neasured		Measured		Reference		Highside			Between	ance Between	Minimum	Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
5,000.0	4,977.6	4,962.8	4,943.7	18.5	18.3	-96.14	78.3	-347.2	656.1	620.7	35.41	18.528		
5,100.0	5,077.6	5,074.8	5,055.6	18.8	18.7	-95.98	79.5	-352.1	660.4	624.2	36.19	18.249		
5,200.0	5,177.6	5,186.9	5,167.7	19.1	19.1	-95.90	80.2	-354.9	662.8	625.9	36.95	17.938		
5,300.0	5,277.6	5,296.8	5,277.6	19.5	19.5	-95.88	80.4	-355.6	663.4	625.7	37.69	17.602		
5,400.0	5,377.6	5,396.8	5,377.6	19.8	19.8	-95.88	80.4	-355.6	663.4	625.0	38.39	17.281		
5,500.0	5,477.6	5,496.8	5,477.6	20.2	20.2	-95.88	80.4	-355.6	663.4	624.3	39.09	16.972		
5,600.0	5,577.6	5,596.8	5,577.6	20.5	20.5	-95.88	80.4	-355.6	663.4	623.6	39.79	16.673		
5,700.0	5,677.6	5,696.8	5,677.6	20.9	20.8	-95.88	80.4	-355.6	663.4	622.9	40.49	16.384		
5,800.0	5,777.6	5,796.8	5,777.6	21.2	21.2	-95.88	80.4	-355.6	663.4	622.2	41.19	16.105		
5,900.0	5,877.6	5,896.8	5,877.6	21.5	21.5	-95.88	80.4	-355.6	663.4	621.5	41.90	15.835		
6,000.0	5,977.6	5,996.8	5,977.6	21.9	21.9	-95.88	80.4	-355.6	663.4	620.8	42.60	15.573		
6,100.0	6,077.6	6,096.8	6,077.6	22.2	22.2	-95.88	80.4	-355.6	663.4	620.1	43.30	15.320		
6,200.0	6,177.6	6,196.8	6,177.6	22.6	22.6	-95.88	80.4	-355.6	663.4	619.4	44.01	15.075		
6,300.0	6,277.6	6,296.8	6,277.6	22.9	22.9	-95.88	80.4	-355.6	663.4	618.7	44.71	14.838		
6,400.0	6,377.6	6,396.8	6,377.6	23.3	23.2	-95.88	80.4	-355.6	663.4	618.0	45.42	14.607		
6,500.0	6,477.6	6,496.8	6,477.6	23.6	23.6	-95.88	80.4	-355.6	663.4	617.3	46.12	14.384		
6,600.0	6,577.6	6,596.8	6,577.6	24.0	23.9	-95.88	80.4	-355.6	663.4	616.6	46.83	14.167		
6,700.0	6,677.6	6,696.8	6,677.6	24.3	24.3	-95.88	80.4	-355.6	663.4	615.9	47.53	13.957		
6,800.0	6,777.6	6,796.8	6,777.6	24.7	24.6	-95.88	80.4	-355.6	663.4	615.2	48.24	13.753		
	6,877.6	6,896.8		24.7	24.0 25.0	-95.88	80.4	-355.6	663.4	614.5	48.95	13.554		
6,900.0 7,000.0	6,977.6	6,996.8	6,877.6 6,977.6	25.4	25.0	-95.88	80.4	-355.6	663.4	613.8	48.95	13.361		
7,100.0	7,077.6	7,096.8	7,077.6	25.7	25.7	-95.88	80.4	-355.6	663.4	613.1	50.36	13.174		
7,200.0	7,177.6	7,196.8	7,177.6	26.1	26.0	-95.88	80.4	-355.6	663.4	612.4	51.07	12.991		
7,300.0	7,277.6	7,296.8	7,277.6	26.4	26.4	-95.88	80.4	-355.6	663.4	611.6	51.77	12.814		
7,400.0 7,500.0	7,377.6 7,477.6	7,396.8 7,496.8	7,377.6 7,477.6	26.8 27.1	26.7 27.1	-95.88 -95.88	80.4 80.4	-355.6 -355.6	663.4 663.4	610.9 610.2	52.48 53.19	12.641 12.473		
7,600.0	7,577.6	7,596.8	7,577.6	27.5	27.4	-95.88	80.4	-355.6	663.4	609.5	53.90	12.309		
7,700.0	7,677.6	7,696.8	7,677.6	27.8	27.8	-95.88	80.4	-355.6	663.4	608.8	54.61	12.149		
7,800.0	7,777.6	7,796.8	7,777.6	28.2	28.1	-95.88	80.4	-355.6	663.4	608.1	55.32	11.993		
7,900.0	7,877.6	7,896.8	7,877.6	28.5	28.5	-95.88	80.4	-355.6	663.4	607.4	56.02	11.841		
8,000.0	7,977.6	7,996.8	7,977.6	28.9	28.8	-95.88	80.4	-355.6	663.4	606.7	56.73	11.693		
8,100.0	8,077.6	8,096.8	8,077.6	29.2	29.2	-95.88	80.4	-355.6	663.4	606.0	57.44	11.549		
8,200.0	8,177.6	8,196.8	8,177.6	29.6	29.5	-95.88	80.4	-355.6	663.4	605.3	58.15	11.408		
8,300.0	8,277.6	8,296.8	8,277.6	29.9	29.9	-95.88	80.4	-355.6	663.4	604.6	58.86	11.271		
8,400.0	8,377.6	8,396.8	8,377.6	30.3	30.2	-95.88	80.4	-355.6	663.4	603.8	59.57	11.136		
8,500.0	8,477.6	8,496.8	8,477.6	30.6	30.6	-95.88	80.4	-355.6	663.4	603.1	60.28	11.005		
8,600.0	8,577.6	8,596.8	8,577.6	31.0	30.9	-95.88	80.4	-355.6	663.4	602.4	60.99	10.877		
8,700.0	8,677.6	8,696.8	8,677.6	31.3	31.3	-95.88	80.4	-355.6	663.4	601.7	61.70	10.752		
8,800.0	8,777.6	8,796.8	8,777.6	31.7	31.6	-95.88	80.4	-355.6	663.4	601.0	62.41	10.629		
8,900.0	8,877.6	8,896.8	8,877.6	32.0	32.0	-95.88	80.4	-355.6	663.4	600.3	63.12	10.510		
9,000.0	8,977.6	8,996.8	8,977.6	32.4	32.3	-95.88	80.4	-355.6	663.4	599.6	63.84	10.393		
9,100.0	9,077.6	9,096.8	9,077.6	32.7	32.7	-95.88	80.4	-355.6	663.4	598.9	64.55	10.278		
9,200.0	9,177.6	9,196.8	9,177.6	33.1	33.0	-95.88	80.4	-355.6	663.4	598.2	65.26	10.166		
9,300.0	9,277.6	9,296.8	9,277.6	33.4	33.4	-95.88	80.4	-355.6	663.4	597.4	65.97	10.057		
9,400.0	9,377.6	9,396.8	9,377.6	33.8	33.7	-95.88	80.4	-355.6	663.4	596.7	66.68	9.949		
9,500.0	9,477.6	9,496.8	9,477.6	34.2	34.1	-95.88	80.4	-355.6	663.4	596.0	67.39	9.844		
9,600.0	9,577.6	9,596.8	9,577.6	34.5	34.4	-95.88	80.4	-355.6	663.4	595.3	68.10	9.741		
9,000.0 9,700.0	9,677.6	9,590.8 9,696.8	9,577.6 9,677.6	34.5 34.9	34.4 34.8	-95.88	80.4	-355.6	663.4	595.5 594.6	68.81	9.741 9.641		
9,800.0	9,777.6	9,796.8	9,777.6	35.2	35.2	-95.88	80.4	-355.6	663.4	593.9	69.53	9.542		
9,900.0	9,877.6	9,896.8 0.006.8	9,877.6 9,977.6	35.6	35.5	-95.88	80.4 80.4	-355.6 355.6	663.4	593.2	70.24	9.445		
10,000.0	9,977.6	9,996.8	9,977.6	35.9	35.9	-95.88	80.4	-355.6	663.4	592.5	70.95	9.350		
10,100.0	10,077.6	10,096.8	10,077.6	36.3	36.2	-95.88	80.4	-355.6	663.4	591.8	71.66	9.258		

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 203H - OWB - PWP0

Offset De	esign:RC	DRIN PRO	JECT -	ROBIN FE	D 203H ·	- OWB - P	WP0						Offset Site Error:	0.0 usft
Survey Prog Refer		MWD Off	set	Semi N	laior Axis		Offset Wellbo	ore Centre	Dis	Rule Assig	gned:		Offset Well Error:	0.0 usft
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	+N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
10,200.0	10,177.6	10,196.8	10,177.6	36.6	36.6	-95.88	80.4	-355.6	663.4	591.0	72.37	9.166		
10,300.0	10,277.6	10,296.8	10,277.6	37.0	36.9	-95.88	80.4	-355.6	663.4	590.3	73.09	9.077		
10,400.0	10,377.6	10,396.8	10,377.6	37.3	37.3	-95.88	80.4	-355.6	663.4	589.6	73.80	8.989		
10,500.0	10,477.6	10,496.8	10,477.6	37.7	37.6	-95.88	80.4	-355.6	663.4	588.9	74.51	8.904		
10,600.0	10,577.6	10,596.8	10,577.6	38.0	38.0	-95.88	80.4	-355.6	663.4	588.2	75.22	8.819		
10,700.0	10,677.6	10,696.8	10,677.6	38.4	38.3	-95.88	80.4	-355.6	663.4	587.5	75.94	8.736		
10,800.0	10,777.6	10,809.1	10,789.1	38.8	38.7	-94.90	91.7	-355.7	662.5	585.8	76.69	8.640		
10,900.0	10,877.6	10,911.9	10,886.3	39.1	39.1	-92.05	124.6	-356.0	660.8	583.3	77.41	8.536		
10,944.0	10,921.6	10,951.9	10,921.8	39.3	39.2	-90.47	142.9	-356.1	660.4	582.7	77.71	8.499		
11,000.0	10,977.6	10,997.8	10,960.5	39.5	39.4	-88.33	167.5	-356.3	661.1	583.1	78.05	8.470		
11,100.0	11,077.6	11,066.4	11,013.6	39.8	39.5	-84.59	210.9	-356.6	667.0	588.6	78.42	8.505		
11,200.0	11,177.6	11,120.4	11,050.7	40.2	39.7	-81.24	250.2	-356.9	681.0	602.7	78.29	8.698		
11,300.0	11,277.6	11,163.1	11,076.6	40.5	39.8	-78.41	284.0	-357.2	704.5	627.0	77.55	9.085		
11,400.0	11,377.6	11,200.0	11,096.6	40.9	39.9	-75.86	315.0	-357.4	738.0	661.7	76.29	9.674		
11,500.0	11,477.6	11,225.0	11,108.8	41.2	40.0	-74.10	336.9	-357.6	780.9	706.3	74.51	10.479		

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 204H - OWB - PWP0

urvey Pro		MWD								Rule Assi	gned:		Offset Well Error:	0.0 u
	rence Vertical	Off Measured		Semi M Reference	lajor Axis	Highside	Offset Wellb	ore Centre		ance	Minimum	Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Separation (usft)		warning	
0.0	0.0	4.0	4.0	0.0	0.0	88.47	0.8	30.0	30.0					
100.0	100.0	104.0	104.0	0.3	0.3	88.47	0.8	30.0	30.0	29.5	0.53	56.585		
200.0	200.0	204.0	204.0	0.6	0.6	88.47	0.8	30.0	30.0	28.8	1.25	24.065		
300.0	300.0	304.0	304.0	1.0	1.0	88.47	0.8	30.0	30.0	28.1	1.96	15.282		
400.0	400.0	404.0	404.0	1.3	1.3	88.47	0.8	30.0	30.0	27.3	2.68	11.196		
500.0	500.0	504.0	504.0	1.7	1.7	88.47	0.8	30.0	30.0	26.6	3.40	8.834		
600.0	600.0	604.0	604.0	2.1	2.1	88.47	0.8	30.0	30.0	25.9	4.12	7.295		
700.0	700.0	704.0	704.0	2.4	2.4	88.47	0.8	30.0	30.0	25.2	4.83	6.213		
800.0	800.0	804.0	804.0	2.8	2.8	88.47	0.8	30.0	30.0	24.5	5.55	5.410		
900.0	900.0	904.0	904.0	3.1	3.1	88.47	0.8	30.0	30.0	23.8	6.27	4.791		
1,000.0	1,000.0	1,004.0	1,004.0	3.5	3.5	88.47	0.8	30.0	30.0	23.0	6.98	4.299		
1,100.0	1,100.0	1,104.0	1,104.0	3.8	3.8	88.47	0.8	30.0	30.0	22.3	7.70	3.899		
1,200.0	1,200.0	1,204.0	1,204.0	4.2	4.2	88.47	0.8	30.0	30.0	21.6	8.42	3.567		
1,300.0	1,300.0	1,304.0	1,304.0	4.6	4.6	88.47	0.8	30.0	30.0	20.9	9.13	3.287		
1,400.0	1,400.0	1,404.0	1,404.0	4.9	4.9	88.47	0.8	30.0	30.0	20.2	9.85	3.048		
1,500.0	1,500.0	1,504.0	1,504.0	5.3	5.3	88.47	0.8	30.0	30.0	19.5	10.57	2.841		
1,600.0	1,600.0	1,604.0	1,604.0	5.6	5.6	88.47	0.8	30.0	30.0	18.7	11.28	2.660		
1,700.0	1,700.0	1,704.0	1,704.0	6.0	6.0	88.47	0.8	30.0	30.0	18.0	12.00	2.501		
1,800.0	1,800.0	1,804.0	1,804.0	6.4	6.4	88.47	0.8	30.0	30.0	17.3	12.72	2.360		
1,900.0	1,900.0	1,904.0	1,904.0	6.7	6.7	88.47	0.8	30.0	30.0	16.6	13.44	2.234		
1,965.3	1,965.3	1,969.3	1,969.3	7.0	7.0	88.47	0.8	30.0	30.0	16.1	13.90	2.159 CC		
2,000.0	2,000.0	2,004.0	2,004.0	7.1	7.1	88.47	0.8	30.0	30.0	15.9	14.15	2.121		
2,100.0	2,100.0	2,102.9	2,102.9	7.4	7.4	25.47	1.0	31.8	30.3	15.5	14.84	2.041		
2,200.0	2,199.8	2,201.9	2,201.7	7.8	7.8	28.48	1.7	37.1	30.9	15.4	15.51	1.992 ES		
2,300.0	2,299.5	2,300.8	2,300.2	8.1	8.1	33.27	2.7	45.7	32.0	15.8	16.16	1.979 SF		
2,400.0	2,398.7	2,400.0	2,398.7	8.5	8.5	39.42	4.2	57.7	33.8	17.0	16.83	2.009		
2,500.0	2,497.7	2,498.3	2,495.8	8.9	8.8	44.43	6.1	72.9	37.9	20.4	17.46	2.169		
2,600.0	2,596.8	2,598.1	2,594.1	9.2	9.2	47.36	8.2	90.1	43.7	25.5	18.18	2.403		
2,700.0	2,695.8	2,697.9	2,692.4	9.6	9.6	49.60	10.4	107.3	49.6	30.7	18.91	2.624		
2,800.0	2,794.8	2,797.7	2,790.7	10.0	10.0	51.35	12.5	124.5	55.6	35.9	19.64	2.830		
2,900.0	2,893.8	2,897.5	2,889.0	10.3	10.3	52.77	14.6	141.7	61.6	41.2	20.38	3.022		
3,000.0	2,992.9	2,997.4	2,987.3	10.7	10.7	53.93	16.7	158.9	67.7	46.5	21.13	3.202		
3,100.0	3,091.9	3,097.2	3,085.6	11.1	11.1	54.90	18.9	176.1	73.7	51.8	21.88	3.369		
3,200.0	3,190.9	3,197.0	3,183.9	11.5	11.5	55.72	21.0	193.3	79.8	57.2	22.64	3.526		
3,300.0	3,289.9	3,296.8	3,282.1	11.9	11.9	56.43	23.1	210.5	85.9	62.5	23.40	3.672		
3,400.0	3,389.0	3,396.6	3,380.4	12.3	12.4	57.04	25.2	227.7	92.0	67.9	24.16	3.809		
3,500.0	3,488.0	3,496.4	3,478.7	12.7	12.8	57.58	27.4	244.9	98.2	73.2	24.93	3.937		
3,600.0	3,587.0	3,596.2	3,577.0	13.1	13.2	58.05	29.5	262.1	104.3	78.6	25.71	4.057		
3,700.0	3,686.0	3,696.0	3,675.3	13.5	13.6	58.47	31.6	279.3	110.4	83.9	26.48	4.170		
3,800.0	3,785.1	3,795.8	3,773.6	13.9	14.0	58.85	33.7	296.5	116.6	89.3	27.26	4.276		
3,900.0	3,884.1	3,895.6	3,871.9	14.3	14.4	59.19	35.9	313.7	122.7	94.7	28.04	4.376		
4,000.0	3,983.1	3,995.4	3,970.2	14.7	14.9	59.49	38.0	330.9	128.9	100.1	28.83	4.471		
4,100.0	4,082.2	4,095.2	4,068.5	15.1	15.3	59.77	40.1	348.1	135.0	105.4	29.61	4.560		
4,200.0	4,181.2	4,195.1	4,166.8	15.5	15.7	60.02	42.2	365.3	141.2	110.8	30.40	4.644		
4,300.0	4,280.2	4,294.9	4,265.1	15.9	16.1	60.26	44.4	382.5	147.4	116.2	31.19	4.724		
4,400.0	4,379.2	4,394.7	4,363.4	16.3	16.6	60.47	46.5	399.7	153.5	121.5	31.99	4.800		
4,431.7	4,410.6	4,426.3	4,394.5	16.4	16.7	60.54	47.2	405.2	155.5	123.2	32.24	4.823		
4,500.0	4,478.4	4,494.5	4,461.6	16.7	17.0	60.49	48.6	416.9	160.1	127.3	32.77	4.885		
4,600.0	4,577.9	4,594.1	4,559.7	17.1	17.4	59.60	50.7	434.1	168.3	134.8	33.51	5.023		
4,700.0	4,677.7	4,693.4	4,657.5	17.4	17.9	57.88	52.9	451.2	178.4	144.2	34.20	5.216		
4,800.0	4,777.6	4,792.3	4,754.9	17.8	18.3	55.52	55.0	468.3	190.6	155.8	34.86	5.469		
4,831.7	4,809.3	4,823.5	4,785.7	17.9	18.4	118.69	55.6	473.6	195.0	159.9	35.06	5.563		

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 204H - OWB - PWP0

Survey Pro		MWD		0			046-4144-11	one Contra		Rule Assi	gned:		Offset Well Error:	0.0 usft
Refe Measured	rence Vertical	Off Measured		Semi N Reference	laior Axis Offset	Highside	Offset Wellb	ore Centre	Dist Between	tance Between	Minimum	Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor	· ·	
4,900.0	4,877.6	4,890.8	4,851.9	18.1	18.7	116.76	57.1	485.2	204.8	169.3	35.48	5.771		
5,000.0	4,977.6	4,989.3	4,948.9	18.5	19.2	114.25	59.2	502.2	219.5	183.4	36.12	6.077		
5,100.0	5,077.6	5,087.8	5,045.9	18.8	19.6	112.05	61.3	519.2	234.6	197.8	36.77	6.379		
5,200.0	5,177.6	5,186.2	5,142.9	19.1	20.0	110.12	63.3	536.1	249.9	212.5	37.43	6.678		
5,300.0	5,277.6	5,284.7	5,239.9	19.5	20.5	108.42	65.4	553.1	265.5	227.5	38.09	6.971		
5,400.0	5,377.6	5,383.2	5,336.9	19.8	20.9	106.90	67.5	570.1	281.4	242.6	38.76	7.258		
5,500.0	5,477.6	5,481.7	5,433.9	20.2	21.3	105.55	69.6	587.1	297.4	257.9	39.44	7.539		
5,600.0	5,577.6	5,580.2	5,530.8	20.5	21.8	104.33	71.7	604.0	313.5	273.4	40.12	7.813		
5,700.0	5,677.6	5,678.6	5,627.8	20.9	22.2	103.23	73.8	621.0	329.8	288.9	40.81	8.080		
5,800.0	5,777.6	5,777.1	5,724.8	21.2	22.6	102.24	75.9	638.0	346.1	304.6	41.50	8.340		
5,900.0	5,877.6	5,875.6	5,821.8	21.5	23.1	101.33	78.0	654.9	362.6	320.4	42.19	8.593		
6,000.0	5,977.6	5,974.1	5,918.8	21.9	23.5	100.51	80.1	671.9	379.1	336.2	42.89	8.839		
6,100.0	6,077.6	6,072.6	6,015.8	22.2	23.9	99.75	82.2	688.9	395.7	352.2	43.59	9.079		
6,200.0	6,177.6	6,171.0	6,112.7	22.6	24.4	99.05	84.3	705.9	412.4	368.1	44.29	9.312		
6,300.0	6,277.6	6,269.5	6,209.7	22.9	24.8	98.41	86.4	722.8	429.2	384.2	44.99	9.538		
6,400.0	6,377.6	6,368.0	6,306.7	23.3	25.2	97.82	88.5	739.8	445.9	400.2	45.70	9.758		
6,500.0	6,477.6	6,466.5	6,403.7	23.6	25.7	97.27	90.6	756.8	462.7	416.3	46.40	9.972		
6,600.0	6,577.6	6,565.0	6,500.7	24.0	26.1	96.75	92.7	773.7	479.6	432.5	47.11	10.181		
6,700.0	6,677.6	6,663.5	6,597.7	24.3	26.6	96.28	94.8	790.7	496.5	448.7	47.82	10.383		
6,800.0	6,777.6	6,761.9	6,694.7	24.7	27.0	95.83	96.9	807.7	513.4	464.9	48.53	10.580		
6,900.0	6,877.6	6,860.4	6,791.6	25.0	27.4	95.41	99.0	824.7	530.4	481.1	49.24	10.772		
7,000.0	6,977.6	6,958.9	6,888.6	25.4	27.9	95.02	101.1	841.6	547.4	497.4	49.95	10.958		
7,100.0	7,077.6	7,057.4	6,985.6	25.7	28.3	94.65	103.2	858.6	564.4	513.7	50.66	11.140		
7,200.0	7,177.6	7,155.9	7,082.6	26.1	28.7	94.30	105.3	875.6	581.4	530.0	51.38	11.316		
7,300.0	7,277.6	7,254.3	7,179.6	26.4	29.2	93.98	107.4	892.6	598.4	546.3	52.09	11.488		
7,400.0	7,377.6	7,352.8	7,276.6	26.8	29.6	93.67	109.5	909.5	615.5	562.7	52.81	11.656		
7,500.0	7,477.6	7,460.3	7,382.4	27.1	30.1	93.36	111.7	927.7	632.4	578.7	53.61	11.797		
7,600.0	7,577.6	7,587.2	7,508.1	27.5	30.6	93.07	113.9	945.1	645.9	591.4	54.53	11.846		
7,700.0	7,677.6	7,715.4	7,635.8	27.8	31.1	92.89	115.4	957.0	655.1	599.7	55.36	11.833		
7,800.0	7,777.6	7,844.5	7,764.7	28.2	31.6	92.80	116.1	963.2	659.9	603.8	56.11	11.761		
7,900.0	7,877.6	7,961.4	7,881.6	28.5	31.9	92.78	116.2	964.1	660.6	603.8	56.79	11.633		
8,000.0	7,977.6	8,061.4	7,981.6	28.9	32.3	92.78	116.2	964.1	660.6	603.1	57.48	11.493		
8,100.0	8,077.6	8,161.4	8,081.6	29.2	32.6	92.78	116.2	964.1	660.6	602.4	58.17	11.356		
8,200.0	8,177.6	8,261.4	8,181.6	29.6	32.9	92.78	116.2	964.1	660.6	601.7	58.86	11.223		
8,300.0	8,277.6	8,361.4	8,281.6	29.9	33.2	92.78	116.2	964.1	660.6	601.1	59.56	11.092		
8,400.0	8,377.6	8,461.4	8,381.6	30.3	33.5	92.78	116.2	964.1	660.6	600.4	60.25	10.965		
8,500.0	8,477.6	8,561.4	8,481.6	30.6	33.8	92.78	116.2	964.1	660.6	599.7	60.94	10.840		
8,600.0	8,577.6	8,661.4	8,581.6	31.0	34.1	92.78	116.2	964.1	660.6	599.0	61.64	10.718		
8,700.0	8,677.6	8,761.4	8,681.6	31.3	34.4	92.78	116.2	964.1	660.6	598.3	62.33	10.598		
8,800.0 8,900.0	8,777.6 8,877.6	8,861.4 8,961.4	8,781.6 8,881.6	31.7 32.0	34.8 35.1	92.78 92.78	116.2 116.2	964.1 964.1	660.6 660.6	597.6 596.9	63.03 63.72	10.481 10.367		
9,000.0	8,977.6	9,061.4	8,981.6	32.4	35.4			964.1	660.6	596.2	64.42	10.254		
9,000.0 9,100.0	8,977.6 9,077.6	9,061.4 9,161.4	8,961.6 9,081.6	32.4 32.7	35.4 35.7	92.78 92.78	116.2 116.2	964.1 964.1	660.6	596.2 595.5	64.42 65.12	10.254		
9,100.0	9,077.6	9,101.4 9,261.4	9,081.0 9,181.6	32.7	36.0	92.78	116.2	964.1 964.1	660.6	595.5 594.8	65.82	10.145		
9,200.0 9,300.0	9,177.6	9,261.4 9,361.4	9,181.6 9,281.6	33.1 33.4	36.0 36.4	92.78 92.78	116.2	964.1 964.1	660.6	594.8 594.1	66.51	9.932		
9,300.0 9,400.0	9,277.6 9,377.6	9,361.4 9,461.4	9,281.6 9,381.6	33.4 33.8	36.4 36.7	92.78	116.2	964.1 964.1	660.6	594.1 593.4	67.21	9.932 9.829		
9,500.0	9,477.6	9,561.4	9,481.6	34.2	37.0	92.78	116.2	964.1	660.6	592.7	67.91	9.728		
9,600.0	9,477.0 9,577.6	9,661.4	9,581.6	34.2 34.5	37.3	92.78	116.2	964.1	660.6	592.0	68.61	9.629		
9,700.0	9,677.6	9,761.4	9,681.6	34.9	37.6	92.78	116.2	964.1	660.6	591.3	69.31	9.531		
9,800.0	9,777.6	9,861.4	9,781.6	35.2	37.0	92.78	116.2	964.1	660.6	590.6	70.01	9.436		
9,900.0	9,877.6	9,961.4 9,961.4	9,881.6	35.6	38.3	92.78	116.2	964.1	660.6	589.9	70.01	9.343		
10,000.0	9,977.6	10,061.4	9,981.6	35.9	38.6	92.78	116.2	964.1	660.6	589.2	71.41	9.251		

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COMPASS 5000.17 Build 03

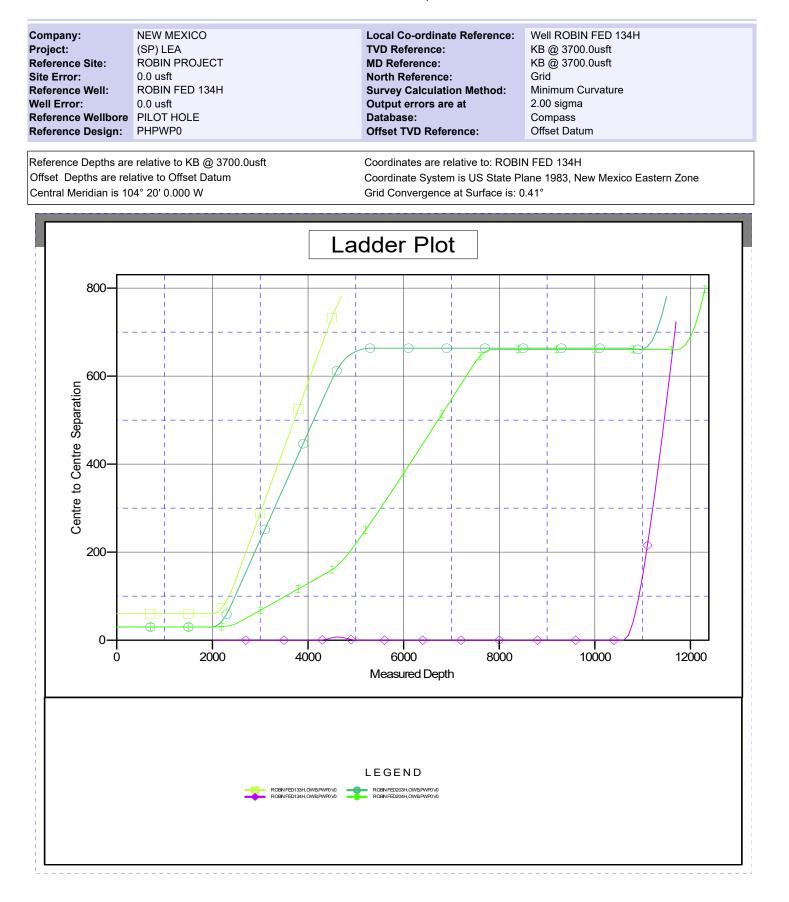
Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

### Offset Design: ROBIN PROJECT - ROBIN FED 204H - OWB - PWP0

Offset De	esign: <sup>RC</sup>	DRIN PRO	JECI -	ROBIN FE	D 204H	- OWB - P\	WP0						Offset Site Error:	0.0 usft
Survey Pro	oram: 0-	MWD								Rule Assig	ned:		Offset Well Error:	0.0 usft
Refei Measured	rence	Off Measured			Aajor Axis Offset	Highside	Offset Wellbo	ore Centre	Dis Between	tance Between	-	Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)		warning	
10,100.0	10,077.6	10,161.4	10,081.6	36.3	38.9	92.78	116.2	964.1	660.6	588.5	72.11	9.161		
10,200.0	10,177.6	10,261.4	10,181.6	36.6	39.3	92.78	116.2	964.1	660.6	587.8	72.81	9.073		
10,300.0	10,277.6	10,361.4	10,281.6	37.0	39.6	92.78	116.2	964.1	660.6	587.1	73.51	8.986		
10,400.0	10,377.6	10,461.4	10,381.6	37.3	39.9	92.78	116.2	964.1	660.6	586.4	74.21	8.902		
10,500.0	10,477.6	10,561.4	10,481.6	37.7	40.2	92.78	116.2	964.1	660.6	585.7	74.91	8.818		
10,600.0	10,577.6	10,661.4	10,581.6	38.0	40.6	92.78	116.2	964.1	660.6	585.0	75.62	8.736		
10,700.0	10,677.6	10,761.4	10,681.6	38.4	40.9	92.78	116.2	964.1	660.6	584.3	76.32	8.656		
10,800.0	10,777.6	10,861.4	10,781.6	38.8	41.2	92.78	116.2	964.1	660.6	583.6	77.02	8.577		
10,900.0	10,877.6	10,961.4	10,881.6	39.1	41.6	92.78	116.2	964.1	660.6	582.9	77.72	8.499		
11,000.0	10,977.6	11,061.4	10,981.6	39.5	41.9	92.78	116.2	964.1	660.6	582.2	78.43	8.423		
11,100.0	11,077.6	11,161.4	11,081.6	39.8	42.2	92.78	116.2	964.1	660.6	581.5	79.13	8.348		
11,200.0	11,177.6	11,261.4	11,181.6	40.2	42.6	92.78	116.2	964.1	660.6	580.8	79.84	8.275		
11,300.0	11,277.6	11,361.4	11,281.6	40.5	42.9	92.78	116.2	964.1	660.6	580.1	80.54	8.202		
11,400.0	11,377.6	11,461.4	11,381.6	40.9	43.2	92.78	116.2	964.1	660.6	579.4	81.24	8.131		
11,500.0	11,477.6	11,562.6	11,482.8	41.2	43.6	92.76	116.5	964.1	660.6	578.7	81.95	8.061		
11,600.0	11,577.6	11,668.4	11,587.3	41.6	43.9	91.46	131.5	964.0	660.0	577.3	82.63	7.987		
11,670.5	11,648.1	11,736.8	11,652.1	41.8	44.1	89.56	153.4	963.8	659.6	576.4	83.12	7.935		
11,700.0	11,677.6	11,763.4	11,676.3	41.9	44.2	88.61	164.3	963.8	659.7	576.3	83.33	7.916		
11,800.0	11,777.6	11,843.2	11,744.8	42.3	44.4	85.08	205.0	963.4	662.6	578.6	84.00	7.889		
11,900.0	11,877.6	11,907.7	11,794.6	42.7	44.6	81.57	245.9	963.1	671.7	587.3	84.41	7.957		
12,000.0	11,977.6	11,959.1	11,830.1	43.0	44.7	78.43	283.1	962.8	689.1	604.7	84.35	8.169		
12,100.0	12,077.6	12,000.0	11,855.4	43.4	44.8	75.77	315.2	962.6	715.8	632.1	83.71	8.551		
12,200.0	12,177.6	12,033.5	11,873.9	43.7	44.9	73.51	343.1	962.4	752.1	669.6	82.54	9.112		
12,300.0	12,277.6	12,060.6	11,887.5	44.1	45.0	71.65	366.5	962.2	797.4	716.4	80.99	9.846		

Anticollision Report

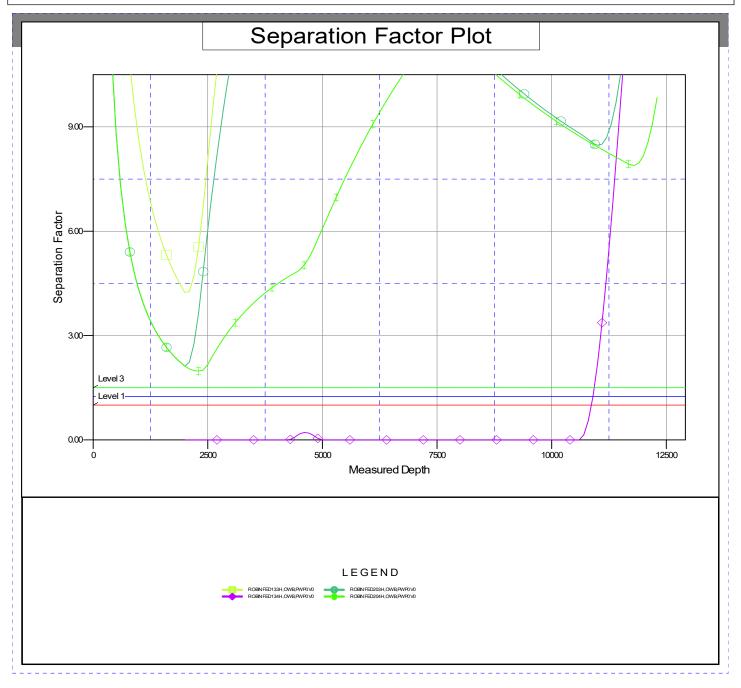


CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Anticollision Report

Company:	NEW MEXICO	Local Co-ordinate Reference:	Well ROBIN FED 134H
Project:	(SP) LEA	TVD Reference:	KB @ 3700.0usft
Reference Site:	ROBIN PROJECT	MD Reference:	KB @ 3700.0usft
Site Error:	0.0 usft	North Reference:	Grid
Reference Well:	ROBIN FED 134H	Survey Calculation Method:	Minimum Curvature
Well Error:	0.0 usft	Output errors are at	2.00 sigma
Reference Wellbore	PILOT HOLE	Database:	Compass
Reference Design:	PHPWP0	Offset TVD Reference:	Offset Datum

Reference Depths are relative to KB @ 3700.0usft Offset Depths are relative to Offset Datum Central Meridian is 104° 20' 0.000 W Coordinates are relative to: ROBIN FED 134H Coordinate System is US State Plane 1983, New Mexico Eastern Zone Grid Convergence at Surface is: 0.41°



### Permian Resources - Robin Fed 134H

### 1. Geologic Formations

Formation	Lithology	Elevation	TVD	Target
Rustler	Sandstone	2177	1527	No
Top of Salt	Salt	2067	1637	No
Yates	Anhydrite/Shale	317	3387	No
Seven Rivers	Limestone	NP	NP	No
Capitan	Sandstone	82	3622	No
Delaware Sands	Sandstone	-1863	5567	No
Brushy Canyon	Sandstone	-3103	6807	No
Bone Spring Lime	Limestone/Shale	-4833	8537	No
1st Bone Spring Sand	Sandstone/Limestone/Shale	-5808	9512	No
2nd Bone Spring Sand	Sandstone/Limestone/Shale	-6383	10087	No
3rd Bone Spring Sand	Sandstone/Limestone/Shale	-7143	10847	Yes
Wolfcamp	Shale	-7391	11095	No

### 2. Blowout Prevention

BOP installed and tested before drilling	Size?	Min. Required WP	Туре		x	Tested to:			
			Anr	nular	х	2500 psi			
			Blind	Ram	х	2500 psi 5000 psi 2500 psi 5000 psi			
12.25	13-5/8"	5M Pipe Ram		х	5000 nai				
			Double	e Ram		- 3000 psi			
		Other*							
			Anr	Annular		2500 psi			
			Blind	Ram	х				
9.875	13-5/8"	5M	Pipe	Ram	х	5000 poi			
			Double	e Ram		5000 psi			
			Other*			5000 psi 2500 psi			
			Annular		х	2500 psi			
			Blind	Ram	х				
7.875	13-5/8"	5M	Pipe	Ram	х	5000 poi			
			Double	e Ram		5000 psr			
			Other*						

Equipment: BOPE with working pressure ratings in excess of anticipated maximum surface pressure will be utilized for well control from drill out of surface casing to TMD. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. All BOPE connections shall be flanged, welded or clamped. All choke lines shall be straight unless targeted with running tees or tee blocks are used, and choke lines shall be anchored to prevent whip and reduce vibrations. All valves in the choke line & the choke manifold shall be full opening as to not cause restrictions and to allow for straight fluid paths to minimize potential erosion. All gauges utilized in the well control system shall be of a type designed for drilling fluid service. A top drive inside BOP valve will be utilized at all times. Subs equipped with full opening valves sized to fit the drill pipe and collars will be available on the rig floor in the open position. The key to operate said valve equipped subs will be on the rig floor at all times. The accumulator system will have sufficient capacity to open the HCR and close all three sets of rams plus the annular preventer while retaining at least 300 psi above precharge on the closing manifold (accumulator system shall be capable of doing so without using the closing unit pumps). The fluid reservoir capacity will be double the usable fluid volume of the accumulator system capacity, and the fluid level will be maintained at the manufacturer's recommended level. Prior to connecting the closing unit to the BOP stack, an accumulator precharge pressure test shall be performed to ensure the precharge pressure is within 100 psi of the desired precharge pressure (only nitrogen gas will be used to precharge). Two independent power sources will be made available at all times to power the closing unit pumps so that the pumps can automatically start when the closing valve manifold pressure has decreased to the preset level. Closing unit pumps will be sized to allow opening of HCR and closing of annular preventer on 5" drill pipe achieving at least 200 psi above precharge pressure with the accumulator system isolated from service in less than two minutes. A valve shall be installed in the closing line as close to the annular preventer as possible to act as a locking device; the valve shall be maintained in the open position and shall be closed only when the power source for the accumulator system is inoperative. Remote controls capable of opening and closing all preventers & the HCR shall be readily accessible to the driller; master controls with the same capability will be operable at the accumulator. The wellhead will be a multibowl speed head allowing for hangoff of intermediate casing & isolation of the 133/8 x 95/8 annulus without breaking the connection between the BOP & wellhead to install an additional casing head. A wear bushing will be installed & inspected frequently to guard against internal wear to wellhead. VBRs (variablebore rams) will be run in upper rambody of BOP stack to provide redundancy to annular preventer while RIH w/ production casing;

#### Requesting Variance? YES

Variance request: Break testing, flex hose, and offline cement variances, see attachments in section 8. Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order II requirements. The BOP test shall be performed before drilling out of the surface casing shoe and will occur at a minimum: a. when initially installed b. whenever any seal subject to test pressure is broken c. following related repairs d. at 30 day intervals e. checked daily as to mechanical operating conditions. The ram type preventer(s) will be tested using a test plug to 250 psi (low) and 5,000 psi (high) (casinghead WP) with a test plug upon its installation onto the 13 surface casing. If a test plug is not used, the ram type preventer(s) shall be tested to 70% of the minimum internal yield pressure of the casing. The annular type preventer(s) shall be tested to 3500 psi. Pressure will be maintained for at least 10 minutes or until provisions of the test are met, whichever is longer. A Sundry Notice (Form 3160 5), along with a copy of the BOP test report, shall be submitted to the local BLM office within 5 working days following the test. If the bleed line is connected into the buffer tank (header), all BOP equipment including the buffer tank and associated valves will be rated at the required BOP pressure. The BLM office will be provided with a minimum of four (4) hours notice of BOP testing to allow witnessing. The BOP Configuration, choke manifold layout, and accumulator system, will be in compliance with Onshore Order 2 for a 5,000 psi system. A remote accumulator and a multi-bowl system will be used, please see attachment in section 8 for multi-bowl procedure. Pressures, capacities, and specific placement and use of the manual and/or hydraulic controls, accumulator controls, bleed lines, etc., will be identified at the time of the BLM 'witnessed BOP test. Any remote controls will be capable of both opening and closing all preventers and shall be readily accessible.

Pipe rams will be operationally checked each 24-hour period. Blind rams will be operationally checked on each trip out of the hole. These checked will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP), choke lines, and choke manifold. See attached schematics.

Choke Diagram Attachment: 5M Choke Manifold BOP Diagram Attachment: BOP Schematics

### 3. Casing

String	Hole Size	Casing Size	Тор	Bottom	Top TVD	Bottom TVD	Length	Grade	Weight	Connection	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
Surface	17.5	13.375	0	1552	0	1552	1552	J55	54.5	BTC	1.47	1.91	Dry	4.92	Dry	4.62
Intermediate 1	12.25	10.75	0	3412	0	3412	3412	J55	45.5	BTC	6.82	3.65	Dry	4.16	Dry	4.07
Intermediate 2	9.875	8.625	0	5517	0	5517	5517	P110 HS	32	MO-FXL	4.63	2.28	Dry	2.85	Dry	4.14
Production	7.875	5.5	0	11347	0	11053	11347	P110RY	20	GeoConn	1.93	2.02	Dry	2.00	Dry	2.00
Production	7.875	5.5	11347	21289	11053	11053	9942	P110RY	20	GeoConn	1.93	2.02	Dry	2.00	Dry	2.00
								<b>BLM Mi</b>	n Safe	ety Factor	1.125	1		1.6		1.6

Non API casing spec sheets and casing design assumptions attached.

### 4. Cement

String	Lead/Tail	Top MD	Bottom MD	Quanity (sx)	Yield	Density	Cu Ft	Excess %	CementType	Additives
Surface	Tail	0	1552	1210	1.34	14.8	1620	50%	Class C	Accelerator
Intermediate 1	Lead	0	2720	380	1.88	12.9	700	50%		EconoCem-HLC + 5% Salt + 5% Kol-Seal
Intermediate 1	Tail	2720	3412	150	1.34	14.8	200	50%	Class C	Retarder
Intermediate 2	Lead	0	4410	350	1.88	12.9	650	50%		EconoCem-HLC + 5% Salt + 5% Kol-Seal
Intermediate 2	Tail	4410	5517	140	1.33	14.8	180	25%	Class C	Salt
Production	Lead	5017	10597	560	2.41	11.5	1330	40%		POZ, Extender, Fluid Loss, Dispersant, Retarder
Production	Tail	10597	21289	1350	1.73	12.5	2320	25%		POZ, Extender, Fluid Loss, Dispersant, Retarder
Plug Back	Tail	10275	12600	470	0.97	17.5	450	10%	Class C	Defoamer, HR-601, Salt

If losses are encountered while drilling intermediate 2 a stage tool will be added and cement will be adjusted accordingly.

### 5. Circulating Medium

Mud System Type: Closed

### Will an air or gas system be used: No

**Describe what will be on location to control well or mitigate oter conditions**: Sufficient quantities of mud materials will be on the well site at all times for the purpose of assuring well control and maintaining wellbore integrity. Surface interval will employ fresh water mud. The intermediate hole will utilize a saturated brine fluid to inhibit salt washout. The production hole will employ brine based and oil base fluid to inhibit formation reactivity and of the appropriate density to maintain well control.

**Describe the mud monitoring system utilized:** Centrifuge separation system. Open tank monitoring with EDR will be used for drilling fluids and return volumes. Open tank monitoring will be used for cement and cuttings return volumes. Mud properties will be monitored at least every 24 hours using industry accepted mud check practices.

### Cuttings Volume: 10570 Cu Ft

	Circulating Medium Table								
Top Depth	Bottom Depth	Mud Type	Min Weight	Max Weight					
0	1552	Spud Mud	8.6	9.5					
1552	3412	Salt Saturated	10	10					
3412	5517	Water Base Mud	8.6	9.5					
5517	11347	Brine	9	10					
11347	21289	OBM	9	10					

### 6. Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures: Will utilize MWD/LWD (Gamma Ray logging) from intermediate hole to TD of the well. List of open and cased hole logs run in the well: DIRECTIONAL SURVEY,GAMMA RAY LOG, OPEN HOLE WL LOGS IN PILOT Coring operation description for the well: N/A

#### 7. Pressure

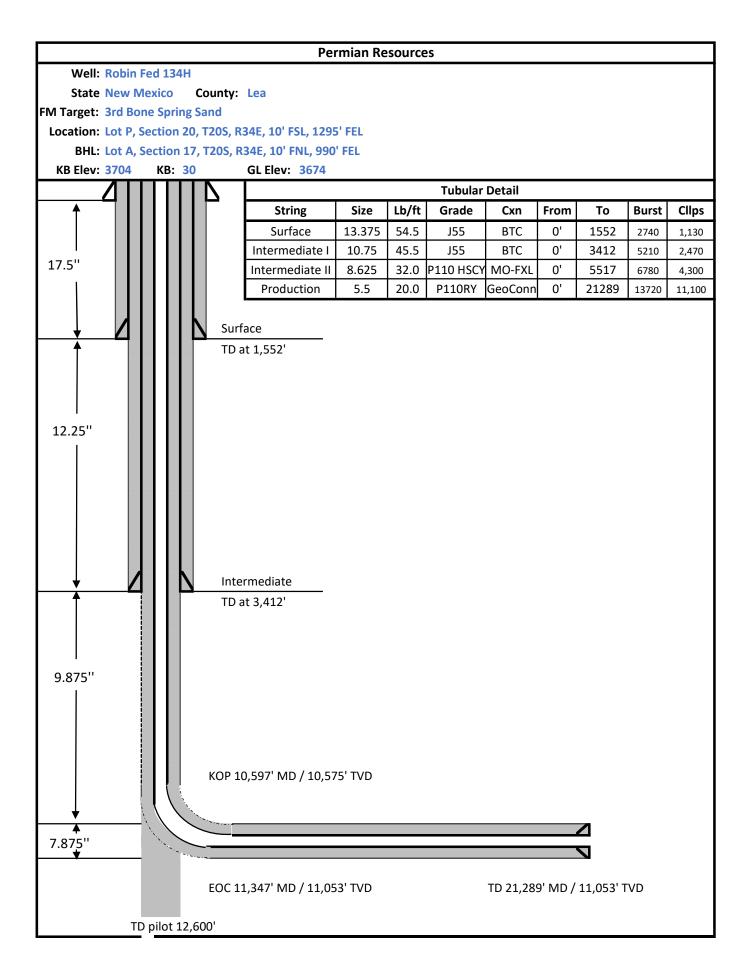
Anticipated Bottom Hole Pressure	5750	psi
Anticipated Surface Pressure	3316	psi
Anticipated Bottom Hole Temperature	165	°F
Anticipated Abnormal pressure, temp, or geo hazards	No	

#### 8. Waste Management

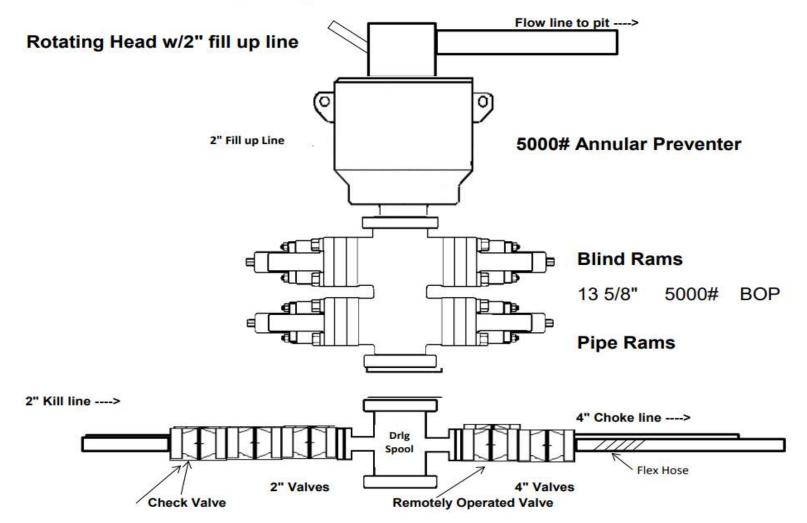
Waste Type:	Drilling
Waste content description:	Fresh water based drilling fluid
Amount of waste:	1500 bbls
Waste disposal frequency:	Weekly (after drilling all surfaces)
Safe containment description:	Steel tanks with plastic-lined containment berms
Waste disposal type:	Haul to commercial facility
Disposal location ownership:	Commercial
Waste Type:	Grey Water & Human Waste
Waste content description:	Grey Water/Human Waste
Amount of waste:	5000 gallons
Waste disposal frequency:	Weekly
Safe containment description:	Approved waste storage tanks with containment
Waste disposal type:	Haul to commercial facility
Disposal location ownership:	Commercial
Waste Type:	Garbage
Waste content description:	General trash/garbage
Amount of waste:	5000 lbs
Waste disposal frequency:	Weekly
Safe containment description:	Enclosed trash trailer
Waste disposal type:	Haul to commercial facility
Disposal location ownership:	Commercial
Waste Type:	Drilling
Waste content description:	Drill Cuttings
Amount of waste:	10570 Cu Ft
Waste disposal frequency:	Per well
Safe containment description:	Steel tanks
Waste disposal type:	Haul to commercial facility
Disposal location ownership:	Commercial
Waste Type:	Drilling
Waste content description:	Brine water based drilling fluid
Amount of waste:	1500 bbls
Waste disposal frequency:	Monthly
Safe containment description:	Steel tanks with plastic-lined containment berms
Waste disposal type:	Haul to commercial facility
Disposal location ownership:	Commercial

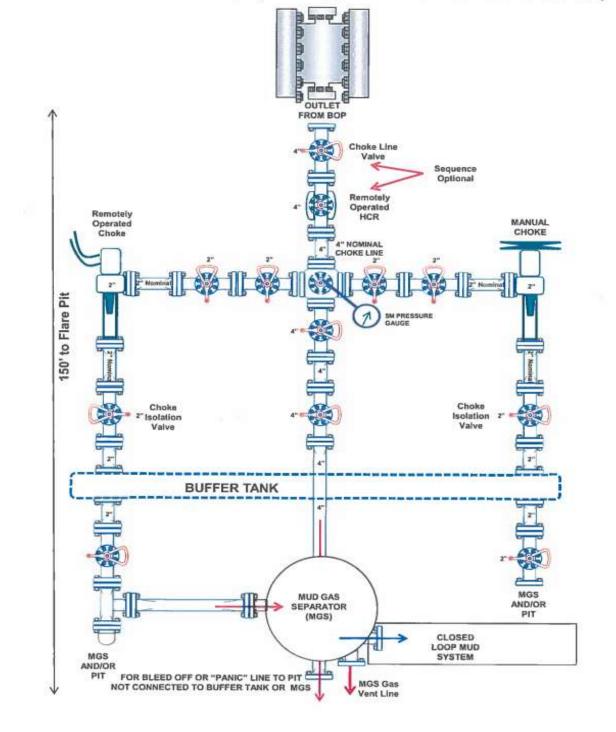
### 9. Other Information

Well Plan and AC Report: attached Batching Drilling Procedure: attached WBD: attached Flex Hose Specs: attached Offline Cementing Procedure: attached Break Testing Procedure: attached



# 5,000 psi BOP Schematic





# 5M Choke Manifold Equipment (WITH MGS + CLOSED LOOP)

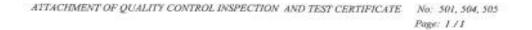


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INSPECTIO	JALITY CON		ATE	CERT. )	4÷.	504	
URCHASER: ContiTech Oil & Marine Corp. P.D. Nº:			§ 8	450040965	9		
CONTITECH HUBBER order Nº: 538236 HOSE TYPE: 3" ID Choke and Kill Hos				Kill Hose			
HOSE SERIAL Nº.	67255	NOMINAL / ACTUAL LENGTH: 10,67 m / 10,77			/ 10,77 m	,77 m	
W.P. 68,9 MPa	10000 psi	T.P. 103,4	MPa 150	00 pei	Duration:	60	min
1000 ANS	Min	See attachme	ent. (1 pag	e)			
→ 10 mm = 20 COUPLINGS	MPs Type	Serial	N°	ä	unity	Heat	10
3" coupling	with	9251	9254	AIS	61 4130	A0578	- HE .
A 1HET TOK ADLE	Flange end		· · · · · · · · ·				
a inte TOK API D.W.				AIS	81 4130	03560	IN
Not Designe	d For Well To	esting		AIS	AP	ossec 9 Spec 16 erature ra	3N X8 C
Not Designe All metal parts are flawles WE CERTIFY THAT THE AB	8 IOVE HOSE HAS BE	EN MANUFACTUR		ANCE WIT	AF Temp	9 Spec 16 erature ra	3N 28 C te:"B"
Not Designe	s ICVE HOSE HAS BE TESTED AS ABO MITY. We hereby a of the above Purc ed standards, codes	EN MANUFACTUR	CTORY RESUL e terrs/equipro at these female of meet the rele	ANCE WIT T. equipment v vari scopiled	AF Tempo H THE TERMS	PI Spec 16 prature rail of THE ORDE	IN IS C C te:"B" R tested in

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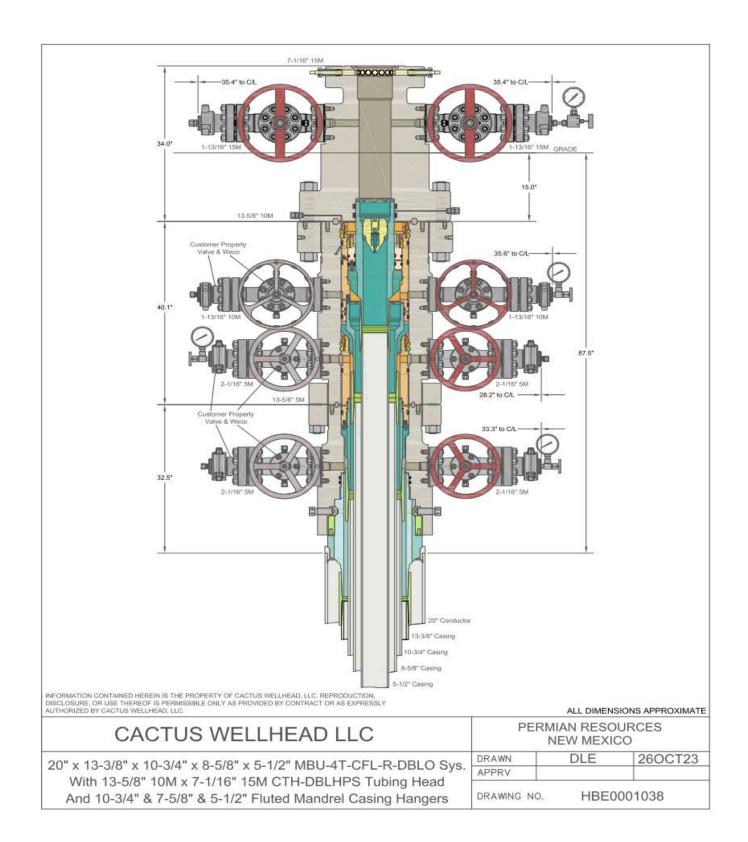


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#### **Hose Data Sheet**

CRI Order No.	538236
Customer	ContiTech Oil & Marine Corp.
Customer Order No	4500409859
Item No.	1
Hose Type	Flexible Hose
Standard	API SPEC 16 C
Inside dia in inches	3
Length	35 ft
Type of coupling one end	FLANGE 4.1/16" 10K API SPEC 6A TYPE 6BX FLANGE C/W BX155 R.GR.SOUR
Type of coupling other end	FLANGE 4.1/16* 10K API SPEC 6A TYPE 6BX FLANGE C/W BX155 R.GR.SOUR
H2S service NACE MR0175	Yes
Working Pressure	10 000 psi
Design Pressure	10 000 psi
Test Pressure	15 000 psi
Safety Factor	2,25
Marking	USUAL PHOENIX
Cover	NOT FIRE RESISTANT
Outside protection	St.steel outer wrap
Internal stripwound tube	No
Lining	OIL + GAS RESISTANT SOUR
Safety clamp	No
Lifting collar	No
Element C	No
Safety chain	No
Safety wire rope	No
Max.design temperature [°C]	100
Min.design temperature [°C]	-20
Min. Bend Radius operating [m]	0,90
Min. Bend Radius storage [m]	0,90
Electrical continuity	The Hose is electrically continuous
Type of packing	WOODEN CRATE ISPM-15

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### Permian Resources Casing Design Criteria

A sundry will be requested if any lesser grade or different size casing is substituted. All casing will be centralized as specified in On Shore Order II. Casing will be tested as specified in On Shore Order II.

### **Casing Design Assumptions:**

### Surface

- 1) Burst Design Loads
  - a) Displacement to Gas
    - (1) Internal: Assumes a full column of gas in the casing with a gas gradient of 0.7 psi/ft in the absence of better information. It is limited to the controlling pressure based on the maximum expected pore pressure within the next drilling interval.
    - (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
  - b) Casing Pressure Test
    - Internal: Displacement fluid plus surface pressure required to comply with regulatory casing test pressure requirements of Onshore Oil and Gas Order No. 2 and NM NMAC 19.15.16 of NMOCD regulations.
    - (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
- Collapse Loads
  - a) Cementing
    - (1) Internal: Displacement fluid density.
    - (2) External: Mud weight from TOC to surface and cement slurry weight from TOC to shoe.
  - b) Lost Returns with Mud Drop
    - Internal: Lost circulation at the TD of the next hole section and the fluid level falls to a depth where the hydrostatic pressure of the mud column equals pore pressure at the depth of the lost circulation zone.
    - (2) External: Mud weight to TOC and cement slurry(s) density below TOC.
- 3) Tension Loads
  - a) Overpull Force
    - 1. Axial: Buoyant weight of the string plus planned 100,000 lbs applied in stuck pipe situation.
  - b) Green Cement Casing Test
    - 1. Axial: Buoyant weight of the string plus cement plug bump pressure load.

### Intermediate I

- 1) Burst Design Loads
  - a) Displacement to Gas
    - (1) Internal: Assumes a full column of gas in the casing with a gas gradient of 0.7 psi/ft in the absence of better information. It is limited to the controlling pressure based on the maximum expected pore pressure within the next drilling interval.
    - (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
  - b) Casing Pressure Test
    - Internal: Displacement fluid plus surface pressure required to comply with regulatory casing test pressure requirements of Onshore Oil and Gas Order No. 2 and NM NMAC 19.15.16 of NMOCD regulations.

- (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
- 2) Collapse Loads
  - a) Cementing
    - (1) Internal: Displacement fluid density.
    - (2) External: Mud weight from TOC to surface and cement slurry weight from TOC to shoe.
  - b) Lost Returns with Mud Drop
    - Internal: Lost circulation at the TD of the next hole section and the fluid level falls to a depth where the hydrostatic pressure of the mud column equals pore pressure at the depth of the lost circulation zone.
    - (2) External: Mud weight to TOC and cement slurry(s) density below TOC.
- 3) Tension Loads
  - a) Overpull Force
    - 1. Axial: Buoyant weight of the string plus planned 100,000 lbs applied in stuck pipe situation.
  - b) Green Cement Casing Test
    - 1. Axial: Buoyant weight of the string plus cement plug bump pressure load.

### Intermediate or Intermediate II

- 1) Burst Design Loads
  - a) Gas Kick Profile
    - Internal: Load profile based on influx encountered in lateral portion of wellbore with a maximum influx volume of 150 bbl and a kick intensity of 1.5 ppg using maximum anticipated MW of 9.9 ppg.
    - (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
  - b) Casing Pressure Test
    - Internal: Displacement fluid plus surface pressure required to comply with regulatory casing test pressure requirements of Onshore Oil and Gas Order No. 2 and NM NMAC 19.15.16 of NMOCD regulations.
    - (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
- 2) Collapse Loads
- a) Cementing
  - (1) Internal: Displacement fluid density.
  - (2) External: Mud weight from TOC to surface and cement slurry weight from TOC to shoe.
  - b) Lost Returns with Mud Drop
    - Internal: Lost circulation at the deepest TVD of the next hole section and the fluid level falls to a depth where the hydrostatic pressure of the mud column equals pore pressure at the depth of the lost circulation zone.
    - (2) External: Mud weight to TOC and cement slurry(s) density below TOC.
- 3) Tension Loads
  - a) Overpull Force
    - 1. Axial: Buoyant weight of the string plus planned 100,000 lbs applied in stuck pipe situation.
  - b) Green Cement Casing Test
    - 1. Axial: Buoyant weight of the string plus cement plug bump pressure load.

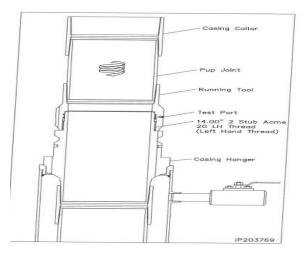
### Production

- 1) Burst Design Loads
  - a) Injection Down Casing
    - (1) Internal: Surface pressure plus injection fluid gradient.
    - (2) External: Mud base-fluid density to top of cement and cement mix water gradient (8.4 ppg) below TOC.
  - b) Casing Pressure Test (Drilling)
    - Internal: Displacement fluid plus surface pressure required to comply with regulatory casing test pressure requirements of Onshore Oil and Gas Order No. 2 and NM NMAC 19.15.16 of NMOCD regulations.
    - (2) External: Mud weight to TOC and cement mix water gradient (8.4 ppg) below TOC.
  - c) Casing Pressure Test (Production)
    - (1) Internal: The design pressure test should be the greater of the planned test pressure prior to simulation down the casing, the regulatory test pressure, and the expected gas lift system pressure. The design test fluid should be the fluid associated with the pressure test having the greatest pressure.
    - (2) External: Mud base-fluid density to top of cement and cement mix water gradient (8.4 ppg) below TOC.
  - d) Tubing Leak
    - (1) Internal: SITP plus a packer fluid gradient to the top of packer.
    - (2) External: Mud base-fluid density to top of cement and cement mix water gradient (8.4 ppg) below TOC.
- 2) Collapse Loads
- a) Cementing
  - (1) Internal: Displacement fluid density.
  - (2) External: Mud weight to TOC and cement slurry(s) density below TOC.
  - b) Full Evacuation
    - (1) Internal: Full void pipe.
    - (2) External: Mud weight to TOC and cement slurry(s) density below TOC.
- 3) Tension Loads
  - a) Overpull Force
    - 1. Axial: Buoyant weight of the string plus planned 100,000 lbs applied in stuck pipe situation.
  - b) Green Cement Casing Test
    - 1. Axial: Buoyant weight of the string plus cement plug bump pressure load.

### Permian Resources Multi-Well Pad Batch Drilling & Off Line Cement Procedure

<u>Surface Casing</u> - PR intends to Batch set and offline cement all surface casing to a depth approved in the APD. Surface Holes will be batch drilled by a big rig. Appropriate notifications will be made prior to spudding the well, running, and cementing casing and prior to skidding to the rig to the next well on pad.

- 1. Drill Surface hole to Approved Depth with Surface Preset Rig and perform wellbore cleanup cycles. Trip out and rack back drilling BHA.
- 2. Run casing with Cactus Multibowl system, with baseplate supported by Conductor.
- 3. Circulate 1.5 csg capacity.
- 4. Flow test Confirm well is static.
- 5. Install cap flange.
- 6. Skid rig to next well on pad
- 7. Remove cap flange (confirm well is static before removal)
  - a) If well is not static use the casing outlet valves to kill well
  - b) Drillers method will be used in well control event
  - c) High pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
  - d) Kill mud will be circulated once influx is circulated out of hole
  - e) Confirm well is static and remove cap flange to start offline cement operations
- 8. Install offline cement tool.
- 9. Rig up cementers.
- 10. Circulate bottoms up with cement truck
- 11. Commence planned cement job, take returns through the annulus wellhead valve
- 12. After plug is bumped confirm floats hold and well is static
- 13. Perform green cement casing test.
  - a) Test Surface casing (.22 psi/ft or 1500 psi whichever is greater) not to exceed 70% casing burst.
- 14. Rig down cementers and equipment
- 15. Install night cap with pressure gauge to monitor.

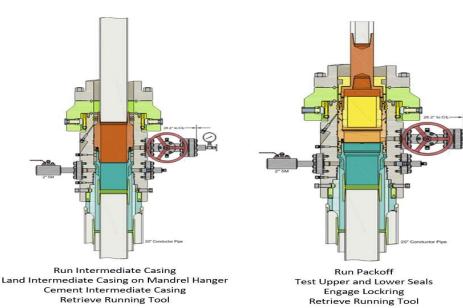


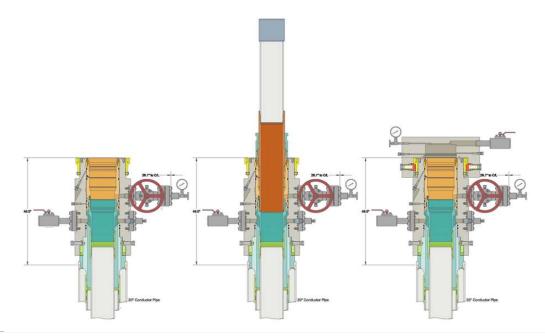
<u>Intermediate 1 Casing</u> – PR intends to Batch set all intermediate 1 casing strings to a depth approved in the APD, typically set into end of salts. Appropriate notifications will be made prior Testing BOPE, and prior to running/cementing all casing strings.

Rig will remove the nightcap and install and test BOPE (testing will be performed on the first Intermediate 1 as per requested break testing variance).

Install wear bushing then drill out 20" shoe-track.

- 1. Drill Intermediate 1 hole to approved casing point. Trip out of hole with BHA to run Casing.
- 2. Remove wear bushing then run and land Intermediate 1 casing with mandrel hanger in wellhead.
- 3. Flow test Confirm well is static.
- 4. Set Annular packoff and pressure test. Test to 5k.
- 5. Install BPV, Nipple down BOP and install cap flange.
- 6. Skid rig to next well on pad
- 7. Remove cap flange (confirm well is static before removal)
  - a) If well is not static use the casing outlet valves to kill well
  - b) Drillers method will be used in well control event
  - c) High pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
  - d) Kill mud will be circulated once influx is circulated out of hole
  - e) Confirm well is static and remove cap flange to start offline cement operations
- 8. Install offline cement tool.
- 9. Rig up cementers.
- 10. Circulate bottoms up with cement truck
- 11. Commence planned cement job, take returns through the annulus wellhead valve
- 12. After plug is bumped confirm floats hold and well is static
- 13. Perform green cement casing test.
  - a) Test casing (.22 psi/ft or 1500 psi whichever is greater) not to exceed 70% casing burst.
- 14. Rig down cementers and equipment
- 15. Install night cap with pressure gauge to monitor.





<u>Intermediate 2 Casing</u> – PR intends to Batch set all Intermediate 2 casing strings to a depth approved in the APD, typically set into Captain past losses. Appropriate notifications will be made prior Testing BOPE, and prior to running/cementing all casing strings.

- 1. Rig will remove the nightcap and install and test BOPE (testing will be performed on the first Intermediate 2 as per requested break testing variance).
- 2. Install wear bushing then drill out Intermediate 1 shoe-track.
- 3. Drill Intermediate 2 hole to approved casing point. Trip out of hole with BHA to run Casing.
- 4. Remove wear bushing then run and land Intermediate 2 casing with mandrel hanger in wellhead.
- 5. Flow test Confirm well is static.
- 6. Set Annular packoff and pressure test. Test to 5k.
- 7. Install BPV, Nipple down BOP and install cap flange.
- 8. Skid rig to next well on pad
- 9. Remove cap flange (confirm well is static before removal)
  - a) If well is not static use the casing outlet valves to kill well
  - b) Drillers method will be used in well control event
  - c) High pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
  - d) Kill mud will be circulated once influx is circulated out of hole
  - e) Confirm well is static and remove cap flange to start offline cement operations
- 10. Install offline cement tool.
- 11. Rig up cementers.
- 12. Circulate bottoms up with cement truck
- 13. Commence planned cement job, take returns through the annulus wellhead valve
- 14. After plug is bumped confirm floats hold and well is static
- 15. Perform green cement casing test.
  - a) Test casing (.22 psi/ft or 1500 psi whichever is greater) not to exceed 70% casing burst.
- 16. Rig down cementers and equipment
- 17. Install night cap with pressure gauge to monitor.

<u>Production Casing</u> – PR intends to Batch set all Production casings. Appropriate notifications will be made prior Testing BOPE, and prior to running/cementing all casing strings.

- 1. Rig will remove the nightcap and install and test BOPE.
- 2. Install wear bushing then drill Intermediate shoe-track.
- 3. Drill Vertical hole to KOP Trip out for Curve BHA.
- 4. Drill Curve, landing in production interval Trip for Lateral BHA.
- 5. Drill Lateral / Production hole to Permitted BHL, perform cleanup cycles and trip out to run Production Casing.
- 6. Remove wear bushing then run Production casing to TD landing casing mandrel in wellhead.
- 7. Cement Production string to surface with floats holding.

## Permian Resources BOP Break Testing Variance Procedure

**Subject:** Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE). Permian Resources requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

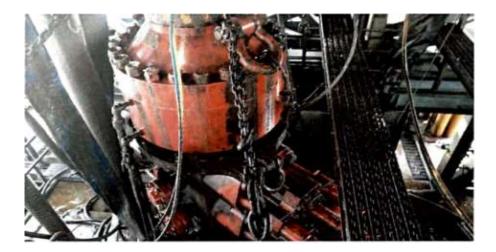
### **Background**

Title 43 CFR 3172, Drilling Operations, Sections 6.b.9.iv states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. 43 CFR 3172.13, Variances from minimum standards states, "An operator may request the authorized officer to approve a variance from any of the minimum standards prescribed in §§ 3172.6 through 3172.12. All such requests shall be submitted in writing to the appropriate authorized officer and provide information as to the circumstances which warrant approval of the variance(s) requested and the proposed alternative methods by which the related minimum standard(s) are to be satisfied. The authorized officer, after considering all relevant factors, if appropriate, may approve the requested variance(s) if it is determined that the proposed alternative(s) meet or exceed the objectives of the applicable minimum standard(s).". Permian Resources feels the break testing the BOPE is such a situation. Therefore, as per 43 CFR 3172.13, Permian Resources submits this request for the variance.

### **Supporting Documentation**

The language used in 43 CFR 3172 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time, there have been significant changes in drilling technology. The BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since 43 CFR 3172 was originally released. The Permian Resources drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.

Figure 1: Winch System attached to BOP Stack



### Figure 2: BOP Winch System



American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. 43 CFR 3172 recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

	Pressure Test-Low	Pressure Test-High Pressure*			
Component to be Pressure Tested	Pressure** psig (MPa)	Change Out of Component, Elastomer, or Ring Gasket	No Change Out of Component, Elastomer, or Ring Gasket		
Annular preventer*	250 to 350 (1.72 to 2.41)	RWP of annular preventer	MASP or 70% annular RWP, whichever is lower.		
Fixed pipe, variable bore, blind, and BSR preventers <sup>32</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventer or wellhead system, whichever is lower	ЧTI		
Choke and kill line and BOP side outlet valves below ram preventers (both sides)	250 to 350 (1.72 to 2 41)	RWP of side outlet valve or wellhead system, whichever is lower	ITP		
Choke manifold—upstream of chokes*	250 to 350 (1.72 to 2.41)	RWP of ram preventers or wellhead system, whichever is lower	ITP		
Choke manifold—downstream of chokes*	250 to 350 (1.72 to 2.41)	RWP of valve(s), line(s), or MASP for the well program, whichever is lower			
Kelly, kelly valves, drill pipe safety valves, IBOPs	250 to 350 (1.72 to 2.41)	MASP for the well program			
<ul> <li>Annular(s) and VBR(s) shall be pre- For pad drilling operations, moving pressure-controlling connections</li> <li>For surface offshore operations, the</li> </ul>	during the evaluation period. The p ssure tested on the largest and sm. from one wellhead to another within when the integray of a pressure se- ie ram BOPs shall be pressure test land operations, the ram BOPs sha	vessure shall not decrease below the allest OD drill pipe to be used in well in the 21 days, pressure testing is req al is broken. ted with the ram locks engaged and ill be pressure tested with the ram loc	program. wred for pressure-containing an the closing and locking pressure		

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

Permian Resources feels break testing and our current procedures meet the intent of 43 CFR 3172 and often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. Permian Resources internal standards require complete BOPE tests more often than that of 43 CFR 3172 (every 21 days). In addition to function testing the annular, pipe rams and blind rams after each BOP nipple up, Permian Resources performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of 43 CFR 3172.

### **Procedures**

1) Permian Resources will use this document for our break testing plan for New Mexico Delaware Basin. The summary below will be referenced in the APD or Sundry Notice and receive approval prior to implementing this variance.

2) Permian Resources will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.

a)A full BOP test will be conducted on the first well on the pad.

b)The first intermediate hole section drilled on the pad will be the deepest. All the remaining hole sections will be the same formation depth or shallower.

c) A full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.

d) A full BOP test will be required prior to drilling any production hole.

3) After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.

a) Between the HCV valve and choke line connection

b)Between the BOP quick connect and the wellhead

4) The BOP is then lifted and removed from the wellhead by a hydraulic system.

5) After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.

6) The connections mentioned in 3a and 3b will then be reconnected.

7) Install test plug into the wellhead using test joint or drill pipe.

8) A shell test is performed against the upper pipe rams testing the two breaks.

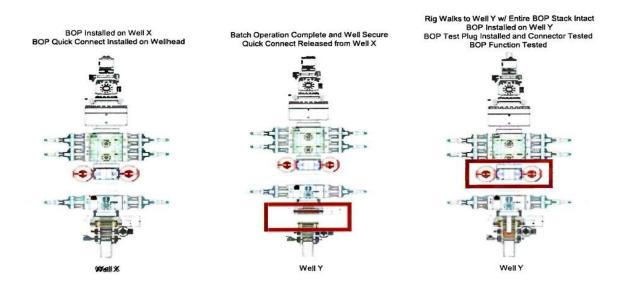
9) The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).

10) Function tests will be performed on the following components: lower pipe rams, blind rams, and annular.

11) For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.

12) A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.

### Note: Picture below highlights BOP components that will be tested during batch operations



### **Summary**

A variance is requested to ONLY test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operations, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control

event occurs prior to the commencement of a BOPE Break Testing operation.

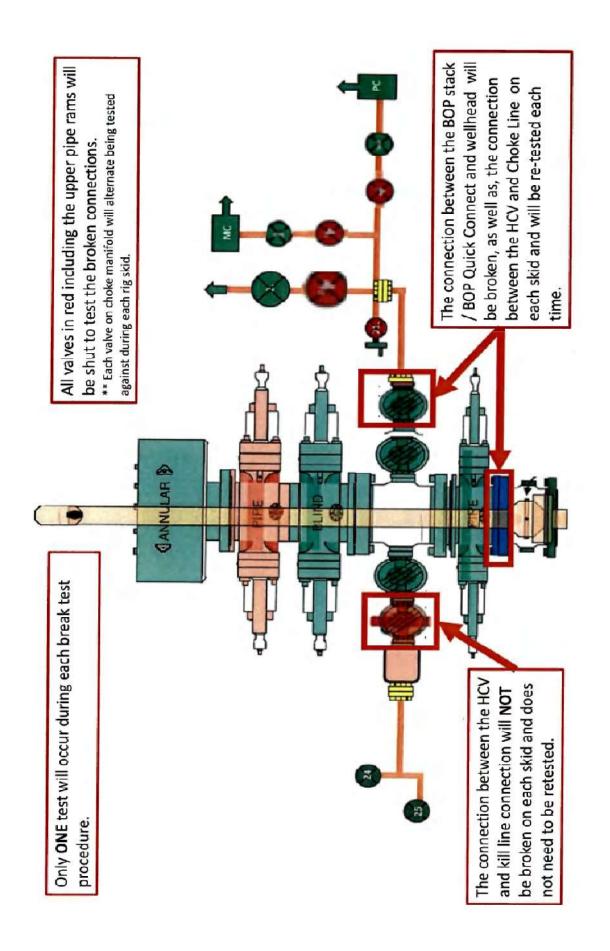
Based on public data and the supporting documentation submitted herein to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

1) After a full BOP test is conducted on the first well on the pad.

2) The first intermediate hole section drilled on the pad will be the deepest. All the remaining hole sections will be the same depth or shallower.

3) A full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.

4) A full BOP test will be required prior to drilling the production hole.



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etal One Corp.	MO-FX			MO-FXL 8		
	WO-FX	-	CDS#	P110H		
Metal One		*1 Pipe Body: BMP P110HSCY MinYS125ksi Min95%WT		MinYS125ksi		
	Min95%W			Min959		
	Connection Da	ta Sheet	Date	8-Sep-21		
	Geometry	Imperia	1	<u>S.I.</u>		
	Pipe Body					
	Grade *1	P110HSCY		P110HSCY		
	MinYS *1	125	ksi	125	ksi	
	Pipe OD (D)	8 5/8	in	219.08	mm	
MO-FXL	Weight	32.00	lb/ft	47.68	kg/m	
	Actual weight	31.10		46.34	kg/m	
	Wall Thickness (t)	0.352	in	8.94	mm	
	Pipe ID (d)	7.921	in	201.19	mm	
	Pipe body cross section	9.149	in <sup>2</sup>	5,902	mm <sup>2</sup>	
	Drift Dia.	7.796	in	198.02	mm	
	-	-	-	-	-	
	<b>0</b>	-				
	Connection	0.005		040.00		
↑ ↔	Box OD (W)	8.625	in	219.08	mm	
	PIN ID	7.921	in	201.19	mm	
Box	Make up Loss	3.847	in	97.71	mm	
crit	Box Critical Area	5.853	in <sup>2</sup>	3686	mm <sup>2</sup>	
are		69	%	69 %		
		Thread Taper 1 / 10 ( 1.2" per ft )				
		Number of Threads 5 TPI				
Make up	Performance	Performance				
	<ul> <li>D Performance Propertie</li> </ul>					
			kips	5.087		
	S.M.Y.S. *1	1,144	кіра		kN	
	M.I.Y.P. *1	1,144 9,690	psi	66.83	MPa	
	M.I.Y.P. *1 Collapse Strength *1	9,690 4,300	psi psi	66.83 29.66	MPa MPa	
Pin	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Spec	9,690 4,300 cified Minimum YIE	psi psi LD Stre	66.83 29.66 ngth of Pipe bo	MPa MPa dy	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini	9,690 4,300 cified Minimum YIE imum Internal Yiek	psi psi LD Stre Pressu	66.83 29.66 ngth of Pipe bo re of Pipe body	MPa MPa dy	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY:	9,690 4,300 cified Minimum YIE imum Internal Yiek S125ksi, Min95%V	psi psi LD Stre Pressu VT, Colla	66.83 29.66 ngth of Pipe bo re of Pipe body	MPa MPa dy	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie	9,690 4,300 cified Minimum YIE imum Internal Yiek S125ksi, Min95%V s for Connectio	psi psi ELD Stre d Pressu VT, Colla n	66.83 29.66 ngth of Pipe bo re of Pipe body spse Strength 4	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load	9,690 4,300 cified Minimum YIE imum Internal Yield \$125ksi, Min95%V s for Connectio 789 kips	psi psi ELD Stre Pressu VT, Colla n ( 69%	66.83 29.66 ngth of Pipe bo re of Pipe body apse Strength 4 of S.M.Y.S.)	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield	9,690 4,300 cified Minimum YIE imum Internal Yield \$125ksi, Min95%V s for Connectio 789 kips 789 kips	psi psi ELD Stre d Pressu VT, Colla n (69% (69%	66.83 29.66 ngth of Pipe body apse Strength 4 of S.M.Y.S. ) of S.M.Y.S. )	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure	9,690 4,300 cified Minimum YIE imum Internal Yield \$125ksi, Min95%V s for Connectio 789 kips	psi psi ELD Stre d Pressu VT, Colla n ( 69% ( 69% ( 70%	66.83 29.66 ngth of Pipe body upse Strength 4 of S.M.Y.S. ) of S.M.Y.S. )	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure External Pressure	9,690 4,300 cified Minimum YIE imum Internal Yield \$125ksi, Min95%V s for Connectio 789 kips 789 kips	psi psi ELD Stre d Pressu VT, Colla n ( <u>69%</u> ( <u>69%</u> ( <u>70%</u> 100% (	66.83 29.66 ngth of Pipe body apse Strength 4 of S.M.Y.S. ) of S.M.Y.S. ) of M.I.Y.P. ) of Collapse S	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure	9,690 4,300 cified Minimum YIE imum Internal Yield \$125ksi, Min95%V s for Connectio 789 kips 789 kips	psi psi ELD Stre d Pressu VT, Colla n ( <u>69%</u> ( <u>69%</u> ( <u>70%</u> 100% (	66.83 29.66 ngth of Pipe body upse Strength 4 of S.M.Y.S. ) of S.M.Y.S. )	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY3 Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure External Pressure Max. DLS ( deg. /100ft) Recommended Torque	9,690 4,300 cified Minimum YIE imum Internal Yiek \$125ksi, Min95%V s for Connectio 789 kips 6,780 psi (	psi psi ELD Stre d Pressu VT, Colla n ( 69% ( 69% ( 70% 100% ( 2	66.83 29.66 ngth of Pipe body opse Strength 4 of S.M.Y.S. ) of S.M.Y.S. ) of M.I.Y.P. ) of Collapse S 9	MPa MPa dy ,300psi	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure External Pressure Max. DLS ( deg. /100ft) Recommended Torque Min.	9,690 4,300 cified Minimum YIE imum Internal Yield S125ksi, Min95%V s for Connectio 789 kips 6,780 psi ( 6,780 psi (	psi psi ELD Stred Pressu VT, Colla n ( 69% ( 69% ( 70% 100% ( 2 ft-lb	66.83 29.66 ngth of Pipe body opse Strength 4 of S.M.Y.S. ) of S.M.Y.S. ) of M.I.Y.P. ) of Collapse S 9	MPa MPa dy ,300psi trength	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure External Pressure Max. DLS ( deg. /100ft) Recommended Torque Min. Opti.	9,690 4,300 cified Minimum YIE imum Internal Yiek \$125ksi, Min95%V \$ for Connectio 789 kips 6,780 psi 6,780 psi 13,600 14,900	psi psi ELD Stred Pressu VT, Colla n ( 69% ( 69% ( 70% 100% ( 2 ft-lb ft-lb	66.83 29.66 ngth of Pipe body upse Strength 4 of S.M.Y.S. ) of S.M.Y.S. ) of M.I.Y.P. ) of Collapse S 9 18,400 20,200	MPa MPa dy ,300psi trength	
Pin criti	M.I.Y.P. *1 Collapse Strength *1 Note S.M.Y.S.= Sper M.I.Y.P. = Mini *1: BMP P110HSCY: MinY: Performance Propertie Tensile Yield load Min. Compression Yield Internal Pressure External Pressure Max. DLS ( deg. /100ft) Recommended Torque Min.	9,690 4,300 cified Minimum YIE imum Internal Yield S125ksi, Min95%V s for Connectio 789 kips 6,780 psi ( 6,780 psi (	psi psi ELD Stred Pressu VT, Colla n ( 69% ( 69% ( 70% 100% ( 2 ft-lb	66.83 29.66 ngth of Pipe body opse Strength 4 of S.M.Y.S. ) of S.M.Y.S. ) of M.I.Y.P. ) of Collapse S 9	MPa MPa dy ,300psi trength	

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al One Corp.	GEOCON		Page		SeAH PRY 95%
	Pipe Body: SeAH P110RY(SMY	S110ksi) & 95%RBW *1			6.050 P110CY
Metal <mark>O</mark> ne	Coupling: P110CY (S		Date	29-	Sep-21
	Connection Da	ata Sheet	Rev.		0
	Geometry	Impe	erial	S.	L
	Pipe Body				-
	Grade "1	SeAH P110RY	-	SeAH P110RY	
	SMYS	110	ksi	110	ksi
	Pipe OD ( D )	5.500	in	139.70	mm
GEOCONN-SC	Weight	20.00	lb/ft	29.80	kg/m
	Wall Thickness (t)	0.361	in	9.17	mm
	Pipe ID ( d )	4.778	in	121.36	mm
Wsc1	Drift Dia.	4.653	in	118.19	mm
lD	Connection				
	Coupling SMYS	110	ksi	110	ksi
♦ 3	Coupling OD (Wsc1)	6.050	in	153.67	mm
b {	Coupling Length ( NL )	8.350	in	212.09	mm
8	Make up Loss	4.125	in	104.78	mm
- E	Pipe Critical Area	5.83	in <sup>2</sup>	3,760	mm <sup>2</sup>
1 E					
8	Box Critical Area	6.00	in <sup>2</sup>	3,874	mm²
5	Thread Taper			3/4" per ft )	
5	Number of Threads		0	TPI	
	Performance Performance Properties for			<u>S.</u>	
	S.M.Y.S.	641	kips	2,852	kN
ι ş	M.I.Y.P. *1 Collapse Strength	13,720	psi psi	94.62 76.55	MPa MPa
	M.I.Y.P. = M *1 Pipe: SeAH P110RY (SMYS Performance Properties fo				
2	Min. Connection Joint Strength		100%	of S.M.Y.S.	
- E	Min. Compression Yield		100%	of S.M.Y.S.	
1	Internal Pressure		100% of M.I.)		
1	External Pressure		100% of Colla	pse Strength	
+   8	Max. DLS ( deg. /100ft)		1	>90	
t	Recommended Torque				
	Min.	14,600	ft-lb	19,700	N-m
	Opti.	16,200	ft-lb	21,900	N-m
	Max.	17,800	ft-lb	24,100	N-m
	Operational Max. Note : Operational Max. torg	19,500	ft-lb	26,400	N-m
a of information contained herein. The int da, without regard to safety-related factor ation. wents regarding the suitability of products tatements are not binding statements ab cation is suitable for use in a particular piece.		for informational purposes only, an alors and users of the subject corne One's knowledge of typical requirer tion. It is the customer's responsibili	d was prepared by refer ctors. Metal One assur ments that are often plac by to validate that a pert	ence to engineering information rea no responsibility for any en- ed on Metal One products in a icular product with the properti	n that is specific to the sul rors with respect to this bandard well configuration
roducts described in this Connection Data	Sheet are not recommended for use in deep water <u>87 1.pdf</u> the contents of which are incorporated by			<u>http://www.mtio.co.ja/mo-</u>	

District I 1625 N. French Dr., Hobbs, NM 88240 Phone:(575) 393-6161 Fax:(575) 393-0720 District II

811 S. First St., Artesia, NM 88210 Phone:(575) 748-1283 Fax:(575) 748-9720

District III

1000 Rio Brazos Rd., Aztec, NM 87410 Phone:(505) 334-6178 Fax:(505) 334-6170

District IV 1220 S. St Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3470 Fax: (505) 476-3462

# **State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division** 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
COLGATE OPERATING, LLC	371449
300 North Marienfeld Street	Action Number:
Midland, TX 79701	324458
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

CONDITIONS

CONDITIC		
Created By	Condition	Condition Date
pkautz	Must circulate cement on surface casing, Intermediate1 and intermediate2 casing strings.	3/19/2024
pkautz	IF ON ANY STRING CEMENT DOES NOT CIRCULATE, A CBL MUST BE RUN ON THAT STRING OF CASING.	3/19/2024

CONDITIONS

Action 324458