U.S. Department of the Interior BUREAU OF LAND MANAGEMENT



Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
STEEL GUITAR	443H	3001555941	NMNM19609	NMNM19609	WPX ENERGY
STEEL GUITAR	444H	3001555942	NMNM41646	NMNM41646	WPX ENERGY

## **Notice of Intent**

**Sundry ID: 2832325** 

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/16/2025 Time Sundry Submitted: 02:48

Date proposed operation will begin: 01/17/2025

**Procedure Description:** Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan to add a 4 string design as contingency for the Steel Guitar 35-26 Fed Com 443H and 444H wells. Please see attachments. Batch sundry to only include attachments by pad for the drilling plan for the deepest well (TVD). NOTE - Batch Sundry ID 2828321 still in process for these two wells which requests the addition of slim hole design to casing plan.

# **NOI Attachments**

#### **Procedure Description**

STEEL\_GUITAR\_35\_26\_FED\_COM\_444H\_Combined\_w\_Mud\_BOP\_REV2\_20250130083842.pdf

5.5\_20lb\_P110HP\_TALON\_RD\_20250116143650.pdf

7.625\_29.7lb\_P110\_HP\_Talon\_SFC\_20250116143531.pdf

9.625\_40lb\_J55\_SeAH\_20250116143455.pdf

13.375\_54.5lb\_J55\_20250116143436.pdf

# **Conditions of Approval**

## **Specialist Review**

Steel\_Guitar\_35\_26\_Fed\_Com\_443H\_Sundry\_ID\_2832325\_20250205135911.pdf

# **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Signed on: JAN 30, 2025 08:38 AM

Name: WPX ENERGY PERMIAN LLC

Title: Regulatory Professional

Street Address: 333 WEST SHERIDAN AVENUE

City: OKLAHOMA CITY State: OK

Phone: (405) 552-6137

Email address: AMY.BROWN@DVN.COM

**Field** 

**Representative Name:** 

**Street Address:** 

City: State: Zip

Phone:

**Email address:** 

# **BLM Point of Contact**

Signature: Long Vo

BLM POC Name: LONG VO BLM POC Title: Petroleum Engineer

BLM POC Phone: 5759885402 BLM POC Email Address: LVO@BLM.GOV

**Disposition:** Approved **Disposition Date:** 02/05/2025

#### STEEL GUITAR 35-26 FED COM 444H

# 1. Geologic Formations

TVD of target	10675	Pilot hole depth	N/A
MD at TD:	17508	Deepest expected fresh water	

#### Basin

	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	386		
Salt	1261		
Base of Salt	2967		
Delaware	2967		
Cherry Canyon	3981		
Brushy Canyon	5070		
1st Bone Spring Lime	6701		
Bone Spring 1st	7627		
Bone Spring 2nd	8224		
3rd Bone Spring Lime	8687		
Bone Spring 3rd	9527		
Wolfcamp	9839		

<sup>\*</sup>H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade Conn		From (MD)	To (MD)	From (TVD)	To (TVD)
13 1/2	9 5/8	40	J-55	ВТС	0	411	0	411
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	10027	0	10027
6 3/4	5 1/2	20	P110HP	TALON RD	0	17508	0	10675

<sup>•</sup> All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

3. Cementing Program (Primary Design)

Casing	# Sks	TOC	Wt.	Yld (ft3/sack)	Slurry Description
Surface	228	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	200	Surf	9	3.27	Lead: Class C Cement + additives
1111. 1	457	5070	13.2	1.44	Tail: Class H / C + additives
Int 1	454	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	200	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	457	5070	13.2	1.44	Tail: Class H / C + additives
Production	62	8127	9	3.27	Lead: Class H /C + additives
Floduction	471	10127	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements.

2. Casing Program (Secondary Design)

Hole Size	Csg. Size	Wt (PPF)	Grade	Conn	Top (MD)	Bottom (MD)	Top (TVD)	Bottom (TVD)
17 1/2	13 3/8	54.5	J-55	BTC	0.0	411 MD	0	411 TVD
12 1/4	9 5/8	40.0	J-55	BTC	0.0	3100 MD	0	3100 TVD
8 3/4	7 5/8	29.7	P110HP	Talon SFC	0	10127 MD	0	10127 TVD
6 3/4	5 1/2	20.0	P110HP	Talon RD	0	17508 MD	0	10675 TVD

- •All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.
- The Rustler top will be validated via drilling parameters (i.e. reduction in ROP), and the surface casing setting depth will be revised accordingly. In addition, surface casing will be set a minimum of 25' above the top of the salt.

3. Cementing Program (Secondary Design)

Casing	# Sks	TOC	Wt. (lb/gal)	Yld (ft3/sack)	Slurry Description
Surface	335	Surf	13.2	1.44	Lead: Class C Cement + additives
Int	318	Surf	9	3.27	Lead: Class C Cement + additives
Int	154	2600	13.2	1.44	Tail: Class H / C + additives
Int 2	165	Surf	9	3.27	Lead: Class C Cement + additives
Int 2	466	5070	13.2	1.44	Tail: Class H / C + additives
Int 2	375	Surf	9	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	165	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	466	5070	13.2	1.44	Tail: Class H / C + additives
Production	62	8127	9	3.27	Lead: Class H /C + additives
Floduction	471	10127	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Casing String	% Excess
Surface	50%
Intermediate	30%
Intermediate 2 (Two Stage)	25%
Prod	10%

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements.

**4. Pressure Control Equipment (Three String Design)** 

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		✓	Tested to:
			Anı	nular	X	50% of rated working pressure
Int 1	13-5/8"	5M	Bline	d Ram	X	
IIIL I	13-3/6	JIVI	Pipe	Ram		5M
			Doub	le Ram	X	3101
			Other*			
			Annul	ar (5M)	X	50% of rated working pressure
Dun dun sti nu	13-5/8"	5M	Blind Ram		X	
Production			Pipe Ram			5M
			Doub	le Ram	X	JIVI
			Other*			
			Annular (5M)			
			Blind Ram			
			Pipe	Ram		
			Doub	le Ram		
			Other*			
N A variance is requested for	the use of	a diverter or	n the surface	e casing. See	attached for	schematic.
Y A variance is requested to	run a 5 M a	nnular on a	10M system	1		

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, (	Logging, Coring and Testing			
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the			
X	Completion Report and shumitted to the BLM.			
	No logs are planned based on well control or offset log information.			
	Drill stem test? If yes, explain.			
	Coring? If yes, explain.			

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5829
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

encountered measured values and formations will be provided to the BEN.		
	N	H2S is present
ı	Y	H2S plan attached.

**4. Pressure Control Equipment (Four String Design)** 

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	T	ype	✓	Tested to:									
	13-5/8"	5M	Anı	nular	X	50% of rated working pressure									
Int 1 & 2			Bline	d Ram	X										
IIIt 1 & 2	13-3/6		J1 <b>V1</b>		Ram		5M								
			Doub	le Ram	X	J1V1									
			Other*												
	13-5/8"		Annul	ar (5M)	X	50% of rated working pressure									
Production		53.4	Bline	d Ram	X										
Production		15-5/8 51/1	15-5/8 5101	5M	SIVI	SIVI	Pipe	Ram		5M					
															Doub
			Other*												
			Annular (5M)												
	Blind Ram		d Ram												
			Pipe	Ram		1									
			Doub	le Ram		]									
			Other*			1									
N A variance is requested for	the use of a diverter on the surface casing. See attached for schematic.														
Y A variance is requested to:	A variance is requested to run a 5 M annular on a 10M system														

5. Mud Program (Four String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate 1 &2	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, (	Logging, Coring and Testing			
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the			
X	Completion Report and shumitted to the BLM.			
	No logs are planned based on well control or offset log information.			
	Drill stem test? If yes, explain.			
	Coring? If yes, explain.			

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5829
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

encountered measured values and formations will be provided to the BEN.		
	N	H2S is present
ı	Y	H2S plan attached.

#### STEEL GUITAR 35-26 FED COM 444H

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments				
X	Directional Plan			
	Other, describe			



# U. S. Steel Tubular Products 5.500" 20.00lb/ft (0.361" Wall)

#### 2/21/2024 7:48:59 AM

# Olb/ft (0.361" Wall) P110 HP USS-TALON HTQ™ RD

MECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		
Critical Area	5.828	5.828	sq. in.	
Joint Efficiency		100.0	%	[2]
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		
Minimum Collapse Pressure	13,150	13,150	psi	
Minimum Internal Yield Pressure	14,360	14,360	psi	
Minimum Pipe Body Yield Strength	729,000		lb	
Joint Strength		729,000	lb	
Compression Rating		729,000	lb	
Reference Length		24,300	ft	[5]
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		
Make-Up Loss		5.58	in.	
Minimum Make-Up Torque		18,400	ft-lb	[4]
Maximum Make-Up Torque		21,400	ft-lb	[4]
Maximum Operating Torque		44,400	ft-lb	[4]

#### **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3. Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

#### **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com

5/15/2024 6:31:14 PM

# U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall)

# P110 HP USS-TALON SFC™

		7		
MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	
Joint Efficiency		85.8	%	[2]
PERFORMANCE	Pipe	USS-TALON SFC™		
Minimum Collapse Pressure	7,260	7,260	psi	
Minimum Internal Yield Pressure	10,750	10,750	psi	
Minimum Pipe Body Yield Strength	1,068,000		lb	
Joint Strength		916,000	lb	
Compression Rating		916,000	lb	
Reference Length		20,560	ft	[5]
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON SFC™		
Make-Up Loss		5.08	in.	
Minimum Make-Up Torque		30,000	ft-lb	[4]
Maximum Make-Up Torque		33,000	ft-lb	[4]
Maximum Operating Torque		80,500	ft-lb	[4]

#### **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- Coupling must meet minimum mechanical properties of the pipe.

#### **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com



9.625" 40# .395" J-55

# **Dimensions (Nominal)**

Outside Diameter Wall Inside Diameter Drift	9.625 0.395 8.835 8.750	in. in. in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.
Performance Properties		
Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
ВТС	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
ВТС	714	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.



# 13-3/8" 54.50# .380 J-55

# **Dimensions (Nominal)**

<b>Outside Diameter</b>	13.375	in.
Wall	0.380	in.
Inside Diameter	12.615	in.
Drift	12.459	in.
Weight, T&C	54.500	lbs/ft
Weight, PE	52.790	lbs/ft

# **Performance Ratings, Minimum**

Collapse, PE	1130	psi
Internal Yields Pressure		
PE	2730	psi
STC	2730	PSI
ВТС	2730	psi
Yield Strength, Pipe Body	853	1000 lbs
Joint Strength, STC	514	1000 lbs
Joint Strength, BTC	909	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.





Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
STEEL GUITAR	443H	3001555941	NMNM19609	NMNM19609	WPX ENERGY
STEEL GUITAR	444H	3001555942	NMNM41646	NMNM41646	WPX ENERGY

# **Notice of Intent**

**Sundry ID: 2832325** 

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/16/2025 Time Sundry Submitted: 02:48

Date proposed operation will begin: 01/17/2025

**Procedure Description:** Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan to add a 4 string design as contingency for the Steel Guitar 35-26 Fed Com 443H and 444H wells. Please see attachments. Batch sundry to only include attachments by pad for the drilling plan for the deepest well (TVD). NOTE - Batch Sundry ID 2828321 still in process for these two wells which requests the addition of slim hole design to casing plan

# **NOI Attachments**

### **Procedure Description**

STEEL\_GUITAR\_35\_26\_FED\_COM\_444H\_Combined\_w\_Mud\_BOP\_REV2\_20250130083842.pdf

5.5\_20lb\_P110HP\_TALON\_RD\_20250116143650.pdf

7.625\_29.7lb\_P110\_HP\_Talon\_SFC\_20250116143531.pdf

9.625\_40lb\_J55\_SeAH\_20250116143455.pdf

13.375\_54.5lb\_J55\_20250116143436.pdf

# **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Signed on: JAN 30, 2025 08:38 AM

Name: WPX ENERGY PERMIAN LLC

Title: Regulatory Professional

Street Address: 333 WEST SHERIDAN AVENUE

City: OKLAHOMA CITY State: OK

Phone: (405) 552-6137

Email address: AMY.BROWN@DVN.COM

R	e	pr	es	er	าta	tiv	'e	N	la	m	e	:
---	---	----	----	----	-----	-----	----	---	----	---	---	---

**Street Address:** 

City: State: Zip

Phone:

**Email address:** 

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:

LOCATION: Section 26, T.26 S., R.29 E., NMPM
COUNTY: Eddy County, New Mexico

WELL NAME & NO.: Steel Guitar 35-26 Fed Com 443H
ATS/API ID: 3001555941
APD ID: 10400095628

WELL NAME & NO.: Steel Guitar 35-26 Fed Com 444H
ATS/API ID: 3001555942
APD ID: 10400095624
Sundry ID: 2832325

2832325

**Sundry ID:** 

COA

**Primary Design:** 

	<del>, ·</del>		
H2S	Yes		
Potash	None <u></u>	None	
Cave/Karst Potential	High ▼		
Cave/Karst Potential	Critical		
Variance	None	☑ Flex Hose	C Other
Wellhead	Conventional and Multibov	vl 🔻	
Other	□4 String □5 String	Capitan Reef None	□WIPP
Other	Pilot Hole  None	☐ Open Annulus	
Cementing	Contingency Squeeze None	Echo-Meter Int 1	Primary Cement Squeeze None
Special Requirements	☐ Water Disposal/Injection	▼ COM	☐ Unit
Special Requirements	■ Batch Sundry	Waste Prevention None	
Special Requirements Variance	☐ BOPE Break Testing ☐ Offline BOPE Testing	✓ Offline Cementing	☐ Casing Clearance

**Alternate Design:** 

Potash	None	None	
Cave/Karst Potential	High ▼		
Cave/Karst Potential	Critical		
Other	✓ 4 String ☐ 5 String	Capitan Reef None	□WIPP
Other	Pilot Hole  None	□ Open Annulus	
Cementing	Contingency Squeeze  None	Echo-Meter Int 2	Primary Cement Squeeze None

#### A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. As a result, the Hydrogen Sulfide area must meet **43 CFR part 3170 Subpart 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

# **Primary Design**

#### **B. CASING**

- 1. The 9-5/8 inch surface casing shall be set at approximately 411 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 13 1/2 inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### **Option 2:**

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 5070'.
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 454 sxs Class C)
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 200 feet into previous casing string.
     Operator shall provide method of verification.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### **Alternate Design**

#### C. CASING

- 4. The 13-3/8 inch surface casing shall be set at approximately 411 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 17 1/2 inch in diameter.
  - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature

- survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- f. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- h. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 5. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
  - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
- 6. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- c. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 5070'.
- d. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 375 sxs Class C)
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 7. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 200 feet into previous casing string.
     Operator shall provide method of verification.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

#### D. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

#### Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **3000 (3M)** psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 9-5/8 or the 7-5/8 intermediate casing shoe shall be 5000 (5M) psi.

#### **Option 2:**

- a. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 13-3/8 inch or the 9-5/8 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

#### E. SPECIAL REQUIREMENT (S)

#### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

#### **Offline Cementing**

Operator has been (**Approved**) to pump the proposed cement program offline in the 1<sup>st</sup> **Intermediate(s) interval**, 4-string alternate design ONLY.

Offline cementing should commence within 24 hours of landing the casing for the interval.

Notify the BLM 4hrs prior to cementing offline at Eddy County: 575-361-2822.

### **Batch Sundry:**

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes above the deepest well shoe(s) set depth.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)
- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

# **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

## **☑** Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

**BLM\_NM\_CFO\_DrillingNotifications@BLM.GOV** (575) 361-2822

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

#### A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or

- if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.

- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been

done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

Long Vo (LVO) 2/5/2025

Form 3160-5 (June 2019)

# UNITED STATES DEPARTMENT OF THE INTERIOR

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

BUREAU OF LAND MANAGEMENT	5. Lease Serial No.		
SUNDRY NOTICES AND REPORTS ON V Do not use this form for proposals to drill or to abandoned well. Use Form 3160-3 (APD) for su	6. If Indian, Allottee or Tribe Name		
SUBMIT IN TRIPLICATE - Other instructions on pag	ge 2	7. If Unit of CA/Agreement, N	lame and/or No.
1. Type of Well Oil Well Gas Well Other	•	8. Well Name and No.	
2. Name of Operator		9. API Well No.	
3a. Address 3b. Phone No.	. (include area code)	10. Field and Pool or Explorate	ory Area
4. Location of Well (Footage, Sec., T.,R.,M., or Survey Description)		11. Country or Parish, State	
12. CHECK THE APPROPRIATE BOX(ES) TO IN	DICATE NATURE OI	F NOTICE, REPORT OR OTH	IER DATA
TYPE OF SUBMISSION	TYPE	OF ACTION	
Notice of Intent Acidize Deep Alter Casing Hyd	pen	Production (Start/Resume) Reclamation	Water Shut-Off Well Integrity
Subsequent Report	Construction and Abandon	Recomplete Temporarily Abandon	Other
	g Back	Water Disposal	
completed. Final Abandonment Notices must be filed only after all requiremen is ready for final inspection.)	is, including reclamati	on, nave been completed and ti	ne operator has detennined that the site
14. I hereby certify that the foregoing is true and correct. Name ( <i>Printed/Typed</i> )	Title		
Signature	Date		
THE SPACE FOR FED	ERAL OR STAT	E OFICE USE	
Approved by	Title	r	Date
Conditions of approval, if any, are attached. Approval of this notice does not warrar certify that the applicant holds legal or equitable title to those rights in the subject leads which would entitle the applicant to conduct operations thereon.	nt or	1	, m.
Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.			

(Instructions on page 2)

#### **GENERAL INSTRUCTIONS**

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

#### SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

#### **NOTICES**

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

### **Additional Information**

#### **Batch Well Data**

STEEL GUITAR 35-26 FED COM 444H, US Well Number: 3001555942, Case Number: NMNM41646, Lease Number: NMNM41646, Operator: WPX ENERGY PERMIAN LLC

STEEL GUITAR 35-26 FED COM 443H, US Well Number: 3001555941, Case Number: NMNM19609, Lease Number: NMNM19609, Operator: WPX ENERGY PERMIAN LLC

#### STEEL GUITAR 35-26 FED COM 444H

# 1. Geologic Formations

TVD of target	10675	Pilot hole depth	N/A
MD at TD:	17508	Deepest expected fresh water	

#### Basin

Formation	Depth (TVD)	Water/Mineral Bearing/Target	Hazards*
Rustler	<b>from KB</b> 386	Zone?	
Salt	1261		
Base of Salt	2967		
Delaware	2967		
Cherry Canyon	3981		
Brushy Canyon	5070		
1st Bone Spring Lime	6701		
Bone Spring 1st	7627		
Bone Spring 2nd	8224		
3rd Bone Spring Lime	8687		
Bone Spring 3rd	9527		
Wolfcamp	9839		

<sup>\*</sup>H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
13 1/2	9 5/8	40	J-55	ВТС	0	411	0	411
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	10027	0	10027
6 3/4	5 1/2	20	P110HP	TALON RD	0	17508	0	10675

<sup>•</sup> All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

3. Cementing Program (Primary Design)

Casing	# Sks	TOC	Wt.	Yld (ft3/sack)	Slurry Description
Surface	228	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	200	Surf	9	3.27	Lead: Class C Cement + additives
1111.1	457	5070	13.2	1.44	Tail: Class H / C + additives
Int 1	454	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	200	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	457	5070	13.2	1.44	Tail: Class H / C + additives
Production	62	8127	9	3.27	Lead: Class H /C + additives
Floduction	471	10127	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements.

2. Casing Program (Secondary Design)

Hole Size	Csg. Size	Wt (PPF)	Grade	Conn	Top (MD)	Bottom (MD)	Top (TVD)	Bottom (TVD)
17 1/2	13 3/8	54.5	J-55	BTC	0.0	411 MD	0	411 TVD
12 1/4	9 5/8	40.0	J-55	BTC	0.0	3100 MD	0	3100 TVD
8 3/4	7 5/8	29.7	P110HP	Talon SFC	0	10127 MD	0	10127 TVD
6 3/4	5 1/2	20.0	P110HP	Talon RD	0	17508 MD	0	10675 TVD

- •All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.
- The Rustler top will be validated via drilling parameters (i.e. reduction in ROP), and the surface casing setting depth will be revised accordingly. In addition, surface casing will be set a minimum of 25' above the top of the salt.

3. Cementing Program (Secondary Design)

Casing	# Sks	TOC	Wt. (lb/gal)	Yld (ft3/sack)	Slurry Description
Surface	335	Surf	13.2	1.44	Lead: Class C Cement + additives
Int	318	Surf	9	3.27	Lead: Class C Cement + additives
IIII	154	2600	13.2	1.44	Tail: Class H / C + additives
Int 2	165	Surf	9	3.27	Lead: Class C Cement + additives
III 2	466	5070	13.2	1.44	Tail: Class H / C + additives
Int 2	375	Surf	9	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	165	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	466	5070	13.2	1.44	Tail: Class H / C + additives
Production	62	8127	9	3.27	Lead: Class H /C + additives
FIOGUCTION	471	10127	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Casing String	% Excess
Surface	50%
Intermediate	30%
Intermediate 2 (Two Stage)	25%
Prod	10%

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements.

**4. Pressure Control Equipment (Three String Design)** 

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	T	ype	✓	Tested to:						
			Anı	nular	X	50% of rated working pressure						
Int 1	13-5/8"	5M	5M	Blind	d Ram	X						
Int 1	13-3/6	JIVI		Ram		5M						
			Doub	le Ram	X	J1V1						
			Other*									
			Annul	ar (5M)	X	50% of rated working pressure						
Production	13-5/8" 5M	5M	Blind	d Ram	X							
Production			Pipe Ram			5M						
										Doub	le Ram	X
			Other*									
			Annul	ar (5M)								
			Blind	d Ram								
			Pipe Ram									
			Doub	le Ram		]						
			Other*									
N A variance is requested for	the use of	a diverter or	n the surface	casing. See	attached for	schematic.						
Y A variance is requested to:	A variance is requested to run a 5 M annular on a 10M system											

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, Coring and Testing			
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the		
X	Completion Report and shumitted to the BLM.		
	No logs are planned based on well control or offset log information.		
	Drill stem test? If yes, explain.		
	Coring? If yes, explain.		

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5829
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

L	encountered measured values and formations with be provided to the BLM.		
	N	H2S is present	
	Y	H2S plan attached.	

**4. Pressure Control Equipment (Four String Design)** 

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	T	ype	✓	Tested to:																									
			Anı	nular	X	50% of rated working pressure																									
Int 1 & 2	13-5/8"	5M	Blind	d Ram	X																										
IIIt 1 & 2	13-3/6	3101	Pipe	Ram		5M																									
			Doub	le Ram	X	31V1																									
			Other*																												
			Annul	ar (5M)	X	50% of rated working pressure																									
Production	13-5/8" 5M	5M	Blind	d Ram	X																										
Production		13-3/8	13-3/8	13-3/8 3IVI	SIVI	JIVI		3101	31 <b>V</b> 1	31 <b>VI</b>	3101	5 3101	.3-3/8 31/1	3101	3101	J1V1	3101	3101	J1 <b>V1</b>	31 <b>V1</b>	3101	3111	3101	3101	3101	3171	5101	Pipe	Ram		5M
								Doub	le Ram	X	3101																				
								Other*																							
			Annul	ar (5M)																											
			Blind	d Ram																											
			Pipe	Ram																											
			Doub	le Ram																											
			Other*																												
N A variance is requested for	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.																														
Y A variance is requested to	A variance is requested to run a 5 M annular on a 10M system																														

5. Mud Program (Four String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate 1 &2	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, Coring and Testing			
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the		
X	Completion Report and shumitted to the BLM.		
	No logs are planned based on well control or offset log information.		
	Drill stem test? If yes, explain.		
	Coring? If yes, explain.		

Additional logs planned		Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5829
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

encountered	measured values and formations will be provided to the BEW.
N	H2S is present
Y	H2S plan attached.

#### STEEL GUITAR 35-26 FED COM 444H

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
- The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachme	ents
X	Directional Plan
	Other, describe

2/21/2024 7:48:59 AM



## U. S. Steel Tubular Products 5.500" 20.00lb/ft (0.361" Wall)

## P110 HP USS-TALON HTQ™ RD

MECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		
Critical Area	5.828	5.828	sq. in.	
Joint Efficiency		100.0	%	[2]
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		
Minimum Collapse Pressure	13,150	13,150	psi	
Minimum Internal Yield Pressure	14,360	14,360	psi	
Minimum Pipe Body Yield Strength	729,000		lb	
Joint Strength		729,000	lb	
Compression Rating		729,000	lb	
Reference Length		24,300	ft	[5]
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		
Make-Up Loss		5.58	in.	
Minimum Make-Up Torque		18,400	ft-lb	[4]
Maximum Make-Up Torque		21,400	ft-lb	[4]
Maximum Operating Torque		44,400	ft-lb	[4]

## **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3. Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

## **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com

5/15/2024 6:31:14 PM

## U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall)

## P110 HP USS-TALON SFC™

		7		
MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	
Joint Efficiency		85.8	%	[2]
PERFORMANCE	Pipe	USS-TALON SFC™		
Minimum Collapse Pressure	7,260	7,260	psi	
Minimum Internal Yield Pressure	10,750	10,750	psi	
Minimum Pipe Body Yield Strength	1,068,000		lb	
Joint Strength		916,000	lb	
Compression Rating		916,000	lb	
Reference Length		20,560	ft	[5]
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON SFC™		
Make-Up Loss		5.08	in.	
Minimum Make-Up Torque		30,000	ft-lb	[4]
Maximum Make-Up Torque		33,000	ft-lb	[4]
Maximum Operating Torque		80,500	ft-lb	[4]

## **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3. Uniaxial bend rating shown is structural only
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

#### **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com



9.625" 40# .395" J-55

## **Dimensions (Nominal)**

**BTC** 

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.
Performance Properties		
Collapse, PE	2570	psi
• ,		•
Internal Yield Pressure at Minimum	Yield	
PE	3950	psi
LTC	3950	psi
втс	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

714

1000 lbs.



# <u>13-3/8"</u> <u>54.50#</u> <u>.380</u> <u>J-55</u>

## **Dimensions (Nominal)**

<b>Outside Diameter</b>	13.375	in.
Wall	0.380	in.
Inside Diameter	12.615	in.
Drift	12.459	in.
Weight, T&C	54.500	lbs/ft
Weight, PE	52.790	lbs/ft

## **Performance Ratings, Minimum**

Collapse, PE	1130	psi
Internal Yields Pressure		
PE	2730	psi
STC	2730	PSI
ВТС	2730	psi
Yield Strength, Pipe Body	853	1000 lbs
Joint Strength, STC	514	1000 lbs
Joint Strength, BTC	909	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

#### Steel Guitar 35-26 Fed Com

9 5/8		surface csg in a	13 1/2 i	nch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	а-В	a-C	Weigh
"A"	40.00		j 55	btc	38.32	13.37	0.72	411	22	1.21	25.26	16,440
"B"				btc				0				0
	V	//8.4#/g mud, 30min Sfc Csg Te	st psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	411				16,44
Comparison o		to Minimum Required Cen										
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
13 1/2	0.4887	228	328	201	63	9.00	3263	5M				1.44
Burst Frac Grad	lient(s) for S	egment(s) A, B = , b All > 0	0.70, OK.									
7.70						Danisus				lmt 1		
7 5/8	ше	casing inside the	9 5/8	Caumlina	laint	Design		l amanth	D@-	Int 1	- 0	\A/a i au la
Segment	#/ft	Grade	<b>- 110</b>	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	29.70		p 110	talon sfc	3.08	1.33	1.85	10,027	2	3.09	2.22	
"B"							_ ,	0				0
	٧	u/8.4#/g mud, 30min Sfc Csg Te					Totals:	10,027				297,80
				ed to achieve a top of	0	ft from su		411				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Di
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
8 3/4	0.1005	657	1312	1011	30	10.50	3474	5M				0.43
D V Tool(s):			5070				sum of sx	Σ CuFt				Σ%exce
, ,	t yld > 1.35	163	27				1111	1966				94
Class 'C' tail cm	t yld > 1.35					Docing Fa		1966		Prod 1		94
Tail cmt 5 1/2		casing inside the	7 5/8	Coupling	loint	Design Fa	ctors		B.O.	Prod 1		
Tail cmt 5 1/2 Segment	#/ft		7 5/8	Coupling	Joint 2 44	Collapse	ctors Burst	Length	B@s	а-В	a-C	Weigh
Tail cmt 5 1/2 Segment "A"		casing inside the		Coupling talon rd	Joint 3.41		ctors	Length 17,508	<b>B@s</b> 2		<b>a-C</b> 3.79	<b>Weigh</b> 350,16
Tail cmt 5 1/2 Segment "A" "B"	#/ft	casing inside the	7 5/8			Collapse	ctors Burst	Length 17,508	_	а-В		Weigh 350,16
Tail cmt 5 1/2 Segment "A" "B" "C"	#/ft	casing inside the	7 5/8			Collapse	ctors Burst	Length 17,508 0	_	а-В		Weigh 350,16 0
Tail cmt 5 1/2 Segment "A" "B"	#/ft 20.00	casing inside the Grade	<b>75/8</b> p 110			Collapse	ctors Burst 2.47	Length 17,508 0 0	_	а-В		Weigh 350,16 0 0
Tail cmt 5 1/2 Segment "A" "B" "C"	#/ft 20.00	casing inside the Grade	<b>75/8</b> p 110 st psig: 2,349	talon rd	3.41	Collapse 2.26	Ctors Burst 2.47 Totals:	Length 17,508 0 0 17,508	_	а-В	3.79	Weigh 350,16 0 0 0 0 350,16
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 20.00	casing inside the Grade v/8.4#/g mud, 30min Sfc Csg Te The cement	7 5/8 p 110 st psig: 2,349 volume(s) are intende	talon rd	3.41 9827	Collapse 2.26	Ctors Burst 2.47  Totals:	Length 17,508 0 0 17,508 200	_	а-В	3.79	Weigh 350,16 0 0 0 350,16 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 20.00	casing inside the Grade v/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage	talon rd ed to achieve a top of	3.41 9827 1 Stage	Collapse 2.26  ft from su Drilling	Ctors Burst 2.47  Totals: rface or a Calc	Length 17,508 0 0 0 17,508 200 Req'd	_	а-В	3.79	Weigh 350,16 0 0 0 350,16 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	#/ft 20.00	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx	7 5/8  p 110  st psig: 2,349 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	9827 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.47  Totals:	Length 17,508 0 0 17,508 200	_	а-В	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4	#/ft 20.00 Annular Volume 0.0835	casing inside the Grade v/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage	talon rd ed to achieve a top of	3.41 9827 1 Stage	Collapse 2.26  ft from su Drilling	Ctors Burst 2.47  Totals: rface or a Calc	Length 17,508 0 0 0 17,508 200 Req'd	_	а-В	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4	#/ft 20.00 Annular Volume 0.0835	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx	7 5/8  p 110  st psig: 2,349 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	9827 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.47  Totals: rface or a Calc	Length 17,508 0 0 0 17,508 200 Req'd	_	а-В	3.79	Weigh 350,16 0 0 0 350,16
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4	#/ft 20.00 Annular Volume 0.0835	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx	7 5/8  p 110  st psig: 2,349 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	9827 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.47  Totals: rface or a Calc	Length 17,508 0 0 0 17,508 200 Req'd	_	а-В	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm	#/ft 20.00 Annular Volume 0.0835 tyld>1.35	casing inside the Grade  W/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533	7 5/8  p 110  st psig: 2,349 volume(s) are intende 1 Stage CuFt Cmt	ed to achieve a top of Min Cu Ft 642	9827 1 Stage % Excess 37	ft from su Drilling Mud Wt	Totals: rface or a Calc MASP	Length 17,508 0 0 0 17,508 200 Req'd	2	а-В	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis Hole-Cp
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment	#/ft 20.00 Annular Volume 0.0835	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage CuFt Cmt 881	ed to achieve a top of Min Cu Ft 642  Coupling	9827 1 Stage % Excess	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 17,508 0 0 17,508 200 Req'd BOPE	2	<b>a-B</b> 4.13	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis Hole-Cp 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm	#/ft 20.00 Annular Volume 0.0835 tyld>1.35	casing inside the Grade  W/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage CuFt Cmt 881	ed to achieve a top of Min Cu Ft 642  Coupling 0.00	9827 1 Stage % Excess 37	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 17,508 0 0 0 17,508 200 Reg'd BOPE	2	a-B 4.13	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis Hole-Cp 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm	#/ft 20.00 Annular Volume 0.0835 tyld>1.35	casing inside the Grade  W/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage CuFt Cmt 881	ed to achieve a top of Min Cu Ft 642  Coupling	9827 1 Stage % Excess 37	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 17,508 0 0 17,508 200 Req'd BOPE  Length 0	2	a-B 4.13	3.79	Weigl 350,16 0 0 350,16 0 overlap. Min Di Hole-Cp 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm	#/ft 20.00 Annular Volume 0.0835 tyld > 1.35	casing inside the Grade  d/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533  Grade	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage CuFt Cmt 881	talon rd  ed to achieve a top of Min Cu Ft 642  Coupling 0.00 0.00	9827 1 Stage % Excess 37	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP  Factors Burst Totals:	Length 17,508 0 0 17,508 200 Req'd BOPE  Length 0 0	2	a-B 4.13	3.79	Weigl 350,16 0 0 350,16 overlap. Min Di Hole-C <sub>1</sub> 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm	#/ft 20.00 Annular Volume 0.0835 ttyld>1.35	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533  Grade  //8.4#/g mud, 30min Sfc Csg Te Cmt vol of	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage CuFt Cmt 881	talon rd  ed to achieve a top of Min Cu Ft 642  Coupling 0.00 0.00  his csg, TOC intended	9827 1 Stage % Excess 37 #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Totals: Totals: Totals: Totals:	Length 17,508 0 0 17,508 200 Req'd BOPE  Length 0 0 4N/A	2	a-B 4.13	3.79	Weigl 350,16 0 0 350,16 overlap. Min Di Hole-C <sub>1</sub> 0.43 Weigl 0 0 0 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B"	#/ft 20.00 Annular Volume 0.0835 tyld > 1.35	casing inside the Grade  d/8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533  Grade	7 5/8 p 110 st psig: 2,349 volume(s) are intended. 1 Stage CuFt Cmt 881 5 1/2 st psig: calc below includes th	talon rd  ed to achieve a top of Min Cu Ft 642  Coupling 0.00 0.00  his csg, TOC intended Min	9827 1 Stage % Excess 37 #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Totals: rfactors Burst  Totals: rface or a Calc	Length 17,508 0 0 17,508 200 Req'd BOPE  Length 0 0 #N/A Req'd	2	a-B 4.13	3.79	Weigl 350,16 0 0 0 350,16 overlap. Min Di: Hole-Cr 0.43 Weigl 0 0 0 overlap.
5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail on  #N/A 0 Segment "A" "B"	#/ft 20.00 Annular Volume 0.0835 ttyld>1.35	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533  Grade  //8.4#/g mud, 30min Sfc Csg Te Cmt vol of	7 5/8 p 110 st psig: 2,349 volume(s) are intended 1 Stage CuFt Cmt 881	talon rd  ed to achieve a top of Min Cu Ft 642  Coupling 0.00 0.00  his csg, TOC intended	9827 1 Stage % Excess 37 #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Totals: Totals: Totals: Totals:	Length 17,508 0 0 17,508 200 Req'd BOPE  Length 0 0 4N/A	2	a-B 4.13	3.79	Weigh 350,16 0 0 350,16 overlap. Min Dis Hole-Cp 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B"	#/ft 20.00  Annular Volume 0.0835 tyld > 1.35  #/ft	casing inside the Grade  //8.4#/g mud, 30min Sfc Csg Te The cement 1 Stage Cmt Sx 533  Grade  //8.4#/g mud, 30min Sfc Csg Te Cmt vol 0 1 Stage	7 5/8 p 110 st psig: 2,349 volume(s) are intended. 1 Stage CuFt Cmt 881 5 1/2 st psig: calc below includes th	talon rd  ed to achieve a top of Min Cu Ft 642  Coupling 0.00 0.00  his csg, TOC intended Min	9827 1 Stage % Excess 37 #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Totals: rfactors Burst  Totals: rface or a Calc	Length 17,508 0 0 17,508 200 Req'd BOPE  Length 0 0 #N/A Req'd	2	a-B 4.13	3.79	Weigi 350,10 0 0 350,10 overlap. Min Di Hole-C  0.43 Weigi 0 0 overlap. Min Di

Carlsbad Field Office 2/5/2025 12 1/4

r D V Tool(s):

0.3132

0.81

Σ%excess

27

#### Steel Guitar 35-26 Fed Com

13 3/8	sur	face csg in a	17 1/2	inch hole.		Design I	Factors -			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	54.50		j 55	btc	38.09	5.88	1.61	411	15	2.71	11.11	22,400
"B"				btc				0				0
	w/8.4#/	g mud, 30min Sfc Csg Test	t psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	411				22,400
Comparison o	of Proposed to Mi	nimum Required Cem	ent Volumes									
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cplg
17 1/2	0.6946	335	482	285	69	9.00	1009	2M				1.56
					Site plat (pip	e racks S or E) a	is per O.O.1.I	II.D.4.i. not fo				
05/8	ensir	og incida tha	12 2 /0		Site plat (pip			II.D.4.i. not fo		Int 1		
95/8 Segment		ng inside the	13 3/8	Coupling		<u>Design I</u>	Factors			Int 1		Weight
Segment	#/ft	ng inside the Grade	,	Coupling	Body	<u>Design I</u> Collapse	Factors Burst	Length	B@s	а-В	a-C	Weight
9 5/8 Segment "A" "B"			13 3/8 j 55	Coupling btc		<u>Design I</u>	Factors	<b>Length</b> 3,100				<b>Weight</b> 124,000
Segment "A"	<b>#/ft</b> 40.00	Grade	j 55		Body	<u>Design I</u> Collapse	Factors Burst 0.72	Length 3,100	B@s	а-В	a-C	Weight 124,000 0
Segment "A"	<b>#/ft</b> 40.00	<b>Grade</b> /g mud, 30min Sfc Csg Test	j 55 t psig: 1,412	btc	Body	Design I Collapse 1.52	Factors Burst 0.72 Totals:	Length 3,100 0 3,100	B@s	а-В	<b>a-C</b> 2.55	Weight 124,000 0 124,000
Segment "A"	<b>#/ft</b> 40.00	Grade /g mud, 30min Sfc Csg Test The cement v	j 55 t psig: 1,412 volume(s) are inter		<b>Body</b> 5.08	Design I Collapse 1.52  ft from su	Factors Burst 0.72  Totals: rface or a	Length 3,100 0 3,100 411	B@s	а-В	<b>a-C</b> 2.55	Weight 124,000 0 124,000 overlap.
Segment "A" "B"	#/ft 40.00 w/8.4#/	<b>Grade</b> /g mud, 30min Sfc Csg Test	j 55 t psig: 1,412	btc	<b>Body</b> 5.08	Design I Collapse 1.52	Factors Burst 0.72 Totals:	Length 3,100 0 3,100	B@s	а-В	<b>a-C</b> 2.55	Weight 124,000 0 124,000

27

991

1262

5M

Σ CuFt

1262

3296

sum of sx

472

10.50

**#VALUE!** #VALUE! t by stage %: Class 'C' tail cmt yld > 1.35 Burst Frac Gradient(s) for Segment(s): A, B, C, D = 1.27, b, c, d All > 0.70, OK.

472

7 5/8	casi	ing inside the	9 5/8			<u>Design Factors</u>					Int 2		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight	
"A"	29.70	р	110	talon sfc	3.05	1.31	1.85	10,127	2	3.09	2.20	300,772	
"B"								0				0	
"C"								0				0	
"D"								0				0	
	w/8.4i	#/g mud, 30min Sfc Csg Test psig:	2,228				Totals:	10,127				300,772	
		The cement volun	ne(s) are inten	ded to achieve a top of	0	ft from su	ırface or a	3100				overlap.	
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dist	
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cplg	
8 3/4	0.1005	631	1211	1043	16	10.50	3474	5M				0.43	
	Se	tting Depths for D V Tool(s):	5070				sum of sx	Σ CuFt				<u>Σ%excess</u>	
% exces	ss cmt by stage:	138	1				1006	1751				68	
Class 'C' tail cm	nt yld > 1.35												

Tail cmt 5 1/2	cas	ing inside the	7 5/8			Design F	Factors			Prod 1		
Segment	#/ft	Grade	, 5, 5	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	20.00		p 110	talon rd	3.41	2.26	2.47	17,508	2	4.13	3.79	350,160
"B"								0				0
	w/8.4	#/g mud, 30min Sfc Csg Test ps	ig: 2,349				Totals:	17,508				350,160
		The cement vo	lume(s) are intend	ded to achieve a top of	9927	ft from su	rface or a	200				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cplg
6 3/4	0.0835	533	881	634	39	10.50						0.43
Class 'H' tail cm	nt yld > 1.20		Capitan Reef es	t top XXXX.								

Carlsbad Field Office 2/5/2025 Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 428775

#### **CONDITIONS**

Operator:	OGRID:
WPX Energy Permian, LLC	246289
Devon Energy - Regulatory	Action Number:
Oklahoma City, OK 73102	428775
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rikala	Any previous COA's not addressed within the updated COA's still apply.	2/7/2025