Sundry	Print Report 28
	01/20/2025

Well Name	Well Number	US Well Number	Lease Number	Case Number	Operator
STEEL GUITAR	443H	3001555941	NMNM19609	NMNM19609	WPX ENERGY
STEEL GUITAR	444H	3001555942	NMNM41646	NMNM41646	WPX ENERGY

Notice of Intent

Sundry ID: 2828321

Type of Submission: Notice of Intent

Date Sundry Submitted: 12/19/2024

Date proposed operation will begin: 12/19/2024

Type of Action: APD Change

Time Sundry Submitted: 09:32

Procedure Description: Devon Energy Production Co., L.P. (Devon) respectfully requests to change the drilling plan with casing changes and slim hole design for the Steel Guitar 35-26 Fed Com 443H (API ID 10400095628) and Steel Guitar 35-26 Fed Com 444H (API ID 10400095624). Please see attachments. Batch sundry to only include attachments by pad for the drilling plan for the deepest well (TVD).

NOI Attachments

Procedure Description

9.625_40lb_J55_SeAH_20241219091751.pdf

5.5_20lb_P110HP_TALON_RD_20241219091704.pdf

7.625_29.7lb_P110_HP_Talon_SFC_20241219091641.pdf

STEEL_GUITAR_35_26_FED_COM_443H_REV_20241219091317.pdf

Conditions of Approval

Specialist Review

26_26_29_A_Sundry_ID_2828321_Steel_Guitar_35_26_Fed_Com_443H_alt.pdf_20250129104554.pdf 26_26_29_A_Sundry_ID_2828321_Steel_Guitar_35_26_Fed_Com_443H_20250129104555.pdf Steel_Guitar_35_26_Fed_Com__Dr_COA_Sundry_ID_2828321_20250129104554.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Name: WPX ENERGY PERMIAN LLC Title: Regulatory Professional Street Address: 333 WEST SHERIDAN AVENUE City: OKLAHOMA CITY State: OK Phone: (405) 552-6137 Email address: AMY.BROWN@DVN.COM

Field

Representative Name: Street Address: City: State: Z Phone: Email address:

BLM Point of Contact

BLM POC Name: LONG VO BLM POC Phone: 5759885402 Disposition: Approved Signature: Long Vo

BLM POC Title: Petroleum Engineer BLM POC Email Address: LVO@BLM.GOV Disposition Date: 01/29/2025

Signed on: JAN 22, 2025 09:25 AM

Zip:

SěAH 9.625" 40# .395" J-55

Dimensions (Nominal)

Outside Diameter	9.625	in.
Wall	0.395	in.
Inside Diameter	8.835	in.
Drift	8.750	in.
Weight, T&C	40.000	lbs./ft.
Weight, PE	38.970	lbs./ft.

Performance Properties

Collapse, PE	2570	psi
Internal Yield Pressure at Minimum Yield		
PE	3950	psi
LTC	3950	psi
BTC	3950	psi
Yield Strength, Pipe Body	630	1000 lbs.
Joint Strength		
STC	452	1000 lbs.
LTC	520	1000 lbs.
втс	714	1000 lbs.

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

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U. S. Steel Tubular Products 5.500" 20.00lb/ft (0.361" Wall) P110 HP

IP	USS-TALON HTQ™	RD

IECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		-
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		-
Critical Area	5.828	5.828	sq. in.	-
Joint Efficiency		100.0	%	[]
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		-
Minimum Collapse Pressure	13,150	13,150	psi	-
Minimum Internal Yield Pressure	14,360	14,360	psi	
Minimum Pipe Body Yield Strength	729,000		lb	-
Joint Strength		729,000	lb	-
Compression Rating		729,000	lb	-
Reference Length		24,300	ft	[{
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	[;
IAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		-
Make-Up Loss		5.58	in.	-
Minimum Make-Up Torque		18,400	ft-lb	[4
Maximum Make-Up Torque		21,400	ft-lb	[4
Maximum Operating Torque		44,400	ft-lb	[4

Notes

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.

3. Uniaxial bend rating shown is structural only.

- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

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U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall)

P110 HP	USS-TALON SFC™

		the second		
MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		[6
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	
Joint Efficiency		85.8	%	I
PERFORMANCE	Pipe	USS-TALON SFC™		
Minimum Collapse Pressure	7,260	7,260	psi	-
Minimum Internal Yield Pressure	10,750	10,750	psi	
Minimum Pipe Body Yield Strength	1,068,000		lb	
Joint Strength		916,000	lb	
Compression Rating		916,000	lb	
Reference Length		20,560	ft	
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	
MAKE-UP DATA	Pipe	USS-TALON SFC™		
Make-Up Loss		5.08	in.	
Minimum Make-Up Torque		30,000	ft-lb	I
Maximum Make-Up Torque		33,000	ft-lb	
Maximum Operating Torque		80,500	ft-lb	

Notes

1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).

2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.

3. Uniaxial bend rating shown is structural only.

4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).

- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

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1. Geologic Formations

TVD of target	10675	Pilot hole depth	N/A
MD at TD:	17557	Deepest expected fresh water	

Basin

Dusin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	386		
Salt	1261		
Base of Salt	2967		
Delaware	2967		
Cherry Canyon	3981		
Brushy Canyon	5070		
1st Bone Spring Lime	6701		
Bone Spring 1st	7627		
Bone Spring 2nd	8224		
3rd Bone Spring Lime	8687		
Bone Spring 3rd	9527		
Wolfcamp	9839		

*H2S, water flows, loss of circulation, abnormal pressures, etc.

		Wt			Casing Interval		Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
13 1/2	9 5/8	40	J-55	BTC	0	411	0	411
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	10060	0	10060
6 3/4	5 1/2	20	P110HP	TALON RD	0	17557	0	10675

2. Casing Program (Primary Design)

• All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 IILB.1.h Must have table for contingency casing.

3. Cementing Program (Primary Design)

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	228	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	200	Surf	9	3.27	Lead: Class C Cement + additives
Int I	460	5070	13.2	1.44	Tail: Class H / C + additives
Int 1	454	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Intermediate	200	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	460	5070	13.2	1.44	Tail: Class H / C + additives
Production	62	8160	9	3.27	Lead: Class H /C + additives
Production	472	10160	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Sec	cone	dary	⁷ Design	
-	-		_	

2. Casing Program

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45 1/2	J-55	BTC	0	411	0	411
9 7/8	8 5/8	32	P110	Sprint FJ	0	10129	0	10129
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	17557	0	10675

•All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

Secondary Design

3. Cementing Program

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	262	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	252	Surf	9	3.27	Lead: Class C Cement + additives
Int I	586	5070	13.2	1.44	Tail: Class H / C + additives
Int 1	572	Surf	13.2	1.44	Squeeze Lead: Class C Cement + additives
Int 1 Intermediate	252	Surf	9	3.27	Lead: Class C Cement + additives
Squeeze	586	5070	13.2	1.44	Tail: Class H / C + additives
Production	117	8160	9	3.27	Lead: Class H /C + additives
Production	979	10160	13.2	1.44	Tail: Class H / C + additives

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Intermediate 1 (Two Stage)	25%
Prod	10%

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Ty	уре	~	Tested to:
				nular	Х	50% of rated working pressure
Int 1	13-5/8"	5M		d Ram	X	
int i	15 5/0	5101	1	Ram		5M
				le Ram	Х	5111
			Other*			
			Annul	ar (5M)	Х	50% of rated working pressure
Production	13-5/8"	5M	Blind Ram Pipe Ram Double Ram		Х	
Tioduction						5M
					X	
			Other*			
			Annul	ar (5M)		
			Blinc	d Ram		
			Pipe Ram			
			Doub	le Ram		
			Other*			
N A variance is requested for	the use of a	a diverter or	n the surface	e casing. See	attached for	schematic.
Y A variance is requested to r	ed to run a 5 M annular on a 10M system					

4. Pressure Control Equipment (Three String Design)

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid? PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, Co	oring and Testing
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the
Х	Completion Rpeort and sbumitted to the BLM.
	No logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain.
	Coring? If yes, explain.

Additiona	l logs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
Х	CBL	Production casing
Х	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	5829
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

Ν	H2S is present
Y	H2S plan attached.

8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

Will be pre-setting casing? Potentially

1 Spudder rig will move in and batch drill surface hole.

- a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).

³ The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.

- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
 - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments

X Directional Plan

Other, describe

Steel Guitar 35-26 Fed Com 443H

10 3/4	sur	face csg in a	14 3/4	inch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	45.50		j 55	btc	38.25	10.88	0.65	411	20	1.09	20.54	18,701
"B"			,	btc				0	20			0
	w/8.4#	/g mud, 30min Sfc Csg Test	t psig: 1.500	Tail Cmt	does not	circ to sfc.	Totals:	411				18,701
omparison o		inimum Required Cem										,
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
14 3/4	0.5563	262	377	229	65	9.00	3297	5M				1.50
lurst Frac Grac	lient(s) for Segme	ent(s) A, B = , b All > 0.	.70, ОК.									
												
8 5/8		ng inside the	10 3/4			Design				Int 1		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	32.00		p 110	vam sprint fj	2.30	0.72	1.23	10,129	1	2.06	1.21	. ,
"B"								0				0
	w/8.4#	/g mud, 30min Sfc Csg Test					Totals:	10,129				324,12
				ded to achieve a top of	0	ft from su		411				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
9 7/8	0.1261	838	1668	1281	30	10.50	3474	5M				0.61
D V Tool(s):			5070				sum of sx	<u>Σ CuFt</u>				Σ%exces
oy stage % :		161	28				1410	2492				95
lass 'C' tail cm	nt yld > 1.35											
Tail cmt 5 1/2		ng inside the	8 5/8			Design Fa	<u>ctors</u>			Prod 1		
Tail cmt 5 1/2 Segment	casi #/ft	ng inside the Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	
Tail cmt 5 1/2 Segment "A"	casi		85/8 p 110	Coupling dwc/c is+	Joint 3.41	-		17,557	B@s 2		a-C 3.48	351,14
Tail cmt 5 1/2 Segment "A" "B"	casi #/ft					Collapse	Burst	17,557 0	<u> </u>	a-B		351,14 0
Tail cmt 5 1/2 Segment "A" "B" "C"	casi #/ft					Collapse	Burst	17,557 0 0	<u> </u>	a-B		351,140 0 0
Tail cmt 5 1/2 Segment "A" "B"	casi #/ft 20.00	Grade	p 110			Collapse	Burst 2.47	17,557 0 0 0	<u> </u>	a-B		351,140 0 0 0
Tail cmt 5 1/2 Segment "A" "B" "C"	casi #/ft 20.00	Grade /g mud, 30min Sfc Csg Tesl	p 110 t psig: 2,349	dwc/c is+	3.41	Collapse 2.08	Burst 2.47 Totals:	17,557 0 0 0 17,557	<u> </u>	a-B	3.48	351,14 0 0 0 351,14
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	casi #/ft 20.00 w/8.4#	Grade /g mud, 30min Sfc Csg Test The cement	p 110 t psig: 2,349 volume(s) are intend	dwc/c is+	3.41 9929	Collapse 2.08 ft from su	Burst 2.47 Totals: Irface or a	17,557 0 0 17,557 200	<u> </u>	a-B	3.48	351,140 0 0 351,140 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole	casi #/ft 20.00 w/8.4# Annular	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage	p 110 t psig: 2,349 volume(s) are intend 1 Stage	dwc/c is+ ded to achieve a top of Min	3.41 9929 1 Stage	Collapse 2.08 ft from su Drilling	Burst 2.47 Totals: Inface or a Calc	17,557 0 0 17,557 200 Req'd	<u> </u>	a-B	3.48	0 0 351,140 overlap. Min Dist
Tail cmt 5 1/2 Segment "A" "C" "D" Hole Size	casi #/ft 20.00 w/8.4# Annular Volume	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft	3.41 9929 1 Stage % Excess	Collapse 2.08 ft from su Drilling Mud Wt	Burst 2.47 Totals: Irface or a	17,557 0 0 17,557 200	<u> </u>	a-B	3.48	351,140 0 0 351,140 overlap. Min Dist Hole-Cpl
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole	casi #/ft 20.00 w/8.4# Annular Volume 0.1733	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage	p 110 t psig: 2,349 volume(s) are intend 1 Stage	dwc/c is+ ded to achieve a top of Min	3.41 9929 1 Stage	Collapse 2.08 ft from su Drilling	Burst 2.47 Totals: Inface or a Calc	17,557 0 0 17,557 200 Req'd	<u> </u>	a-B	3.48	351,140 0 0 351,140 overlap.
Tail cmt Tail cmt 51/2 Segment "A" "C" "C" "D" Hole Size 7 7/8 Class 'C' tail cm	casi #/ft 20.00 w/8.4# Annular Volume 0.1733	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft	3.41 9929 1 Stage % Excess	Collapse 2.08 ft from su Drilling Mud Wt	Burst 2.47 Totals: Inface or a Calc	17,557 0 0 17,557 200 Req'd	<u> </u>	a-B	3.48	351,140 0 0 351,140 overlap. Min Dis Hole-Cpl
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm #N/A	casi #/ft 20.00 w/8.4# Annular Volume 0.1733	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792	dwc/c is+ ded to achieve a top of Min Cu Ft	3.41 9929 1 Stage % Excess	Collapse 2.08 ft from su Drilling Mud Wt 10.50	Burst 2.47 Totals: urface or a Calc MASP	17,557 0 0 17,557 200 Req'd	2	a-B 4.13	3.48	351,140 0 0 351,140 overlap. Min Dis Hole-Cpl
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm	casi #/ft 20.00 w/8.4# Annular Volume 0.1733 tt yld > 1.35	Grade /g mud, 30min Sfc Csg Test The cement 1 1 Stage Cmt Sx 1096	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft 1322	3.41 9929 1 Stage % Excess 36	Collapse 2.08 ft from su Drilling Mud Wt 10.50 Design	Burst 2.47 Totals: urface or a Calc MASP Factors	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.48 ng>	351,140 0 0 351,140 overlap. Min Dis Hole-Cpl 0.79
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment	casi #/ft 20.00 w/8.4# Annular Volume 0.1733	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling	3.41 9929 1 Stage % Excess	Collapse 2.08 ft from su Drilling Mud Wt 10.50	Burst 2.47 Totals: urface or a Calc MASP	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13	3.48	351,140 0 0 351,140 overlap. Min Dis Hole-Cpl 0.79 Weigh
Tail cmt Tail cmt 5 1/2 Segment "A" "D" Hole Size 7 7/8 Cass 'C' tail cm #N/A 0 Segment "A"	casi #/ft 20.00 w/8.4# Annular Volume 0.1733 tt yld > 1.35	Grade /g mud, 30min Sfc Csg Test The cement 1 1 Stage Cmt Sx 1096	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling 0.00	3.41 9929 1 Stage % Excess 36	Collapse 2.08 ft from su Drilling Mud Wt 10.50 Design	Burst 2.47 Totals: urface or a Calc MASP Factors	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.48 ng>	351,140 0 0 351,140 overlap. Min Dis Hole-Cpl 0.79 Weigh 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Iass 'C' tail cm #N/A 0 Segment	casi #/ft 20.00 w/8.4# Annular Volume 0.1733 it yld > 1.35 #/ft	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1096 Grade	p 110 t psig: 2,349 volume(s) are intenc 1 Stage CuFt Cmt 1792 5 1/2	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling	3.41 9929 1 Stage % Excess 36	Collapse 2.08 ft from su Drilling Mud Wt 10.50 Design	Burst 2.47 Totals: Inface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.48 ng>	351,14 0 0 351,14 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Jass 'C' tail cm #IV/A 0 Segment "A"	casi #/ft 20.00 w/8.4# Annular Volume 0.1733 it yld > 1.35 #/ft	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1096 Grade /g mud, 30min Sfc Csg Test	p 110 t psig: 2,349 volume(s) are intenc 1 Stage CuFt Cmt 1792 5 1/2	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling 0.00 0.00	3.41 9929 1 Stage % Excess 36 #N/A	Collapse 2.08 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.47 Totals: Inface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.48 ng> a-C	351,14 0 0 351,14 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0
Tail emt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 Class 'C' tail em #N/A 0 Segment "A" "B"	casi #/ft 20.00 w/8.4# Annular Volume 0.1733 at yld > 1.35 #/ft w/8.4#	Grade /g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 1096 Grade /g mud, 30min Sfc Csg Test Cmt vol c:	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792 5 1/2 t psig: alc below includes t	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling 0.00 0.00 his csg, TOC intended	3.41 9929 1 Stage % Excess 36 #N/A	Collapse 2.08 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.47 Totals: Inface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 wN/A	2	a-B 4.13 hoose Casi	3.48 ng> a-C	351,14 0 0 351,14 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment "A" "B" Hole	ccasi #/ft 20.00 w/8.4# Annular 0.1733 tryld > 1.35 #/ft w/8.4# Annular	Grade /g mud, 30min Sfc Csg Test The cement 1 1 Stage Cmt Sx 1096 Grade /g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792 5 1/2 t psig: alc below includes t 1 Stage	dwc/c is+	3.41 9929 1 Stage % Excess 36 #N/A 1 Stage	Collapse 2.08 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	Burst 2.47 Totals: Inface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 WN/A Req'd	2	a-B 4.13 hoose Casi	3.48 ng> a-C	351,14 0 0 351,14 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0 overlap. Min Dis
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	casi #/ft 20.00 w/8.4# Annular Volume 0.1733 at yld > 1.35 #/ft w/8.4#	Grade /g mud, 30min Sfc Csg Test The cement 1 1 Stage Cmt Sx 1096 Grade /g mud, 30min Sfc Csg Test Cmt vol c: 1 Stage Cmt Sx	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792 5 1/2 t psig: alc below includes t 1 Stage CuFt Cmt	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling 0.00 0.00 0.00 his csg, TOC intended Min Cu Ft	3.41 9929 1 Stage % Excess 36 #N/A #N/A 1 Stage % Excess	Collapse 2.08 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse	Burst 2.47 Totals: Inface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 wN/A	2	a-B 4.13 hoose Casi	3.48 ng> a-C	351,14 0 0 351,14 overlap. Min Dis Hole-Cpi 0.79 Weigh 0 0 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 7 7/8 class 'C' tail cm #N/A 0 Segment "A" "B" Hole	ccasi #/ft 20.00 w/8.4# Annular 0.1733 tryld > 1.35 #/ft w/8.4# Annular	Grade /g mud, 30min Sfc Csg Test The cement 1 1 Stage Cmt Sx 1096 Grade /g mud, 30min Sfc Csg Test Cmt vol c 1 Stage	p 110 t psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 1792 5 1/2 t psig: alc below includes t 1 Stage	dwc/c is+ ded to achieve a top of Min Cu Ft 1322 Coupling 0.00 0.00 his csg, TOC intended Min Cu Ft 0	3.41 9929 1 Stage % Excess 36 #N/A 1 Stage	Collapse 2.08 ft from su Drilling Mud Wt 10.50 <u>Design</u> Collapse ft from su Drilling	Burst 2.47 Totals: Inface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 WN/A Req'd	2	a-B 4.13 hoose Casi	3.48 ng> a-C	351,14 0 0 351,14 overlap. Min Dis Hole-Cp 0.79 Weigh 0 0 0 overlap. Min Dis

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Steel Guitar 35-26 Fed Com 443H

	:	surface csg in a	13 1/2	inch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	40.00		j 55	btc	38.32	13.37	0.72	411	22	1.21	25.26	16,440
"B"			,	btc				0				0
	w/s	8.4#/g mud, 30min Sfc Csg Test	t psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	411				16,440
Comparison o	f Proposed t	o Minimum Required Cem	ent Volumes									
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
13 1/2	0.4887	228	328	201	63	9.00	3274	5M				1.44
Burst Frac Grad	ient(s) for Se	gment(s) A, B = , b All > 0.	70, OK.									
7.5./0						Design				Int 1		
7 5/8 Segment	c #/ft	asing inside the Grade	9 5/8	Coupling	loint	Design		Longth	B@c	a-B	a-C	Woight
Segment "A"	#/ft 29.70	Grade	p 110	Coupling talon sfc	Joint 3.07	Collapse 1.32	Burst 1.85	Length 10,060	B@s 2	а-в 3.09		Weight 298,782
"B"	29.70		P I IU	Laion Sic	3.07	1.52	1.00	10,060 0	2	3.09	2.22	298,782
В		8.4#/g mud, 30min Sfc Csg Test	nsig: 2 213				Totals:	10,060				U 298,782
	w/			led to achieve a top of	0	ft from su		411				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Rea'd				Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cpl
8 3/4	0.1005	660	1316	1014	30	10.50	3474	5M				0.43
D V Tool(s):			5070				sum of sx	<u>Σ CuFt</u>				Σ%exces
by stage % :		163	27				1114	1970				94
	t yld > 1.35											
Tail cmt 5 1/2	C	asing inside the	7 5/8			Design Fa				Prod 1		
Tail cmt 5 1/2 Segment	c: #/ft	asing inside the Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	•
Tail cmt 5 1/2 Segment "A"	C	•	7 5/8 p 110	Coupling talon rd	Joint 3.41			17,557	B@s 2		a-C 3.79	351,140
Tail cmt 5 1/2 Segment "A" "B"	c: #/ft	•				Collapse	Burst	17,557 0	<u> </u>	a-B	-	351,140 0
Tail cmt 5 1/2 Segment "A" "B" "C"	c: #/ft	•				Collapse	Burst	17,557 0 0	<u> </u>	a-B	-	351,140 0
Tail cmt 5 1/2 Segment "A" "B"	c: #/ft 20.00	Grade	p 110			Collapse	Burst 2.47	17,557 0 0 0	<u> </u>	a-B	-	351,140 0 0
Tail cmt 5 1/2 Segment "A" "B" "C"	c: #/ft 20.00	Grade 8.4#/g mud, 30min Sfc Csg Test	p 110 : psig: 2,349	talon rd	3.41	Collapse 2.26	Burst 2.47 Totals:	17,557 0 0 0 17,557	<u> </u>	a-B	3.79	351,140 0 0 351,140
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	c #/ft 20.00 w/	Grade 8.4#/g mud, 30min Sfc Csg Test The cement	p 110 p 110 p pig: 2,349 volume(s) are intend	talon rd	3.41 9860	Collapse 2.26 ft from su	Burst 2.47 Totals: rface or a	17,557 0 0 17,557 200	<u> </u>	a-B	3.79	351,140 0 0 351,140 overlap.
5 1/2 Segment "A" "B" "C" "D" Hole	c: #/ft 20.00 w/: Annular	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage	p 110 : psig: 2,349 volume(s) are intend 1 Stage	talon rd led to achieve a top of Min	3.41 9860 1 Stage	Collapse 2.26 ft from su Drilling	Burst 2.47 Totals: rface or a Calc	17,557 0 0 17,557 200 Req'd	<u> </u>	a-B	3.79	351,140 0 0 351,140 overlap. Min Dist
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size	c: #/ft 20.00 w/: Annular Volume	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt	talon rd ded to achieve a top of Min Cu Ft	3.41 9860 1 Stage % Excess	Collapse 2.26 ft from su Drilling Mud Wt	Burst 2.47 Totals: rface or a	17,557 0 0 17,557 200	<u> </u>	a-B	3.79	0 0 351,140 overlap. Min Dist Hole-Cplg
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole	c: #/ft 20.00 w/: Annular Volume 0.0835	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage	p 110 : psig: 2,349 volume(s) are intend 1 Stage	talon rd led to achieve a top of Min	3.41 9860 1 Stage	Collapse 2.26 ft from su Drilling	Burst 2.47 Totals: rface or a Calc	17,557 0 0 17,557 200 Req'd	<u> </u>	a-B	3.79	351,140 0 0 351,140 overlap. Min Dist
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4	c: #/ft 20.00 w/: Annular Volume 0.0835	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt	talon rd ded to achieve a top of Min Cu Ft	3.41 9860 1 Stage % Excess	Collapse 2.26 ft from su Drilling Mud Wt	Burst 2.47 Totals: rface or a Calc	17,557 0 0 17,557 200 Req'd	<u> </u>	a-B	3.79	351,140 0 0 351,140 overlap. Min Dist Hole-Cpl
Tail cmt 5 1/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 Class 'C' tail cm	c: #/ft 20.00 w/: Annular Volume 0.0835	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt	talon rd ded to achieve a top of Min Cu Ft	3.41 9860 1 Stage % Excess	Collapse 2.26 ft from su Drilling Mud Wt	Burst 2.47 Totals: rface or a Calc MASP	17,557 0 0 17,557 200 Req'd	2	a-B	3.79	351,140 0 0 351,140 overlap. Min Dist Hole-Cplg
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 class 'C' tail cm #N/A 0 Segment	c: #/ft 20.00 w/: Annular Volume 0.0835	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 882	talon rd ded to achieve a top of Min Cu Ft 644 Coupling	3.41 9860 1 Stage % Excess	Collapse 2.26 ft from su Drilling Mud Wt 10.50	Burst 2.47 Totals: rface or a Calc MASP	17,557 0 0 17,557 200 Req'd	2	a-B 4.13	3.79	351,140 0 0 351,140 overlap. Min Dist Hole-Cpli 0.43
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 Cass 'C' tail cm #N/A 0 Segment "A"	c: #/ft 20.00 w/: Annular Volume 0.0835 tyld ≥ 1.35	Grade 8.4#/g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 534	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 882	talon rd ded to achieve a top of Min Cu Ft 644 Coupling 0.00	3.41 9860 1 Stage % Excess 37	Collapse 2.26 ft from su Drilling Mud Wt 10.50 Design	Burst 2.47 Totals: rface or a Calc MASP Factors	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.79 ng>	351,14(0 0 351,14(overlap. Min Dist Hole-Cpl 0.43 Weight 0
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 class 'C' tail cm #N/A 0 Segment	C: #/ft 20.00 w/: Annular Volume 0.0835 t yld > 1.35 #/ft	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 534 Grade	p 110 p 110 p sig: 2,349 volume(s) are intent 1 Stage CuFt Cmt 882 5 1/2	talon rd ded to achieve a top of Min Cu Ft 644 Coupling	3.41 9860 1 Stage % Excess 37	Collapse 2.26 ft from su Drilling Mud Wt 10.50 Design	Burst 2.47 Totals: rface or a Calc MASP Factors Burst	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.79 ng>	351,14(0 0 351,14(overlap. Min Dist Hole-Cpl 0.43 Weight 0 0
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 Cass 'C' tail cm #N/A 0 Segment "A"	C: #/ft 20.00 w/: Annular Volume 0.0835 t yld > 1.35 #/ft	Grade 8.4#/g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 534 Grade 8.4#/g mud, 30min Sfc Csg Test	p 110 : psig: 2,349 volume(s) are intenc 1 Stage CuFt Cmt 882 5 1/2	taion rd ded to achieve a top of Min Cu Ft 644 Coupling 0.00 0.00	3.41 9860 1 Stage % Excess 37 #N/A	Collapse 2.26 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse	Burst 2.47 Totals: rface or a Calc MASP Factors Burst Totals:	17,557 0 0 17,557 200 Req'd BOPE	2	a-B 4.13 hoose Casi	3.79 ng> a-C	351,14(0 0 351,14(overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0
Tail cmt 5 1/2 Segment "A" "D" Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B"	C: #/ft 20.00 w/: Annular Volume 0.0835 tyld ≥ 1.35 tyld ≥ 1.35 #/ft	Grade 8.4#/g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 534 Grade 8.4#/g mud, 30min Sfc Csg Test Cmt vol ca	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 882 5 1/2 : psig: alc below includes t	taion rd ded to achieve a top of Min Cu Ft 644 Coupling 0.00 0.00 his csg, TOC intended	3.41 9860 1 Stage % Excess 37 #N/A	Collapse 2.26 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	Burst 2.47 Totals: rface or a Calc MASP Factors Burst Totals: rface or a	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 0 #N/A	2	a-B 4.13 hoose Casi	3.79 ng> a-C	351,14(0 0 351,14(overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 class 'C' tail cm #N/A 0 Segment "A" "B" Hole	د: #/ft 20.00 «/‹ Annular Volume 0.0835 tyld > 1.35 #/ft #/ft «/› Annular	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 534 Grade 8.4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 882 5 1/2 : psig: alc below includes t 1 Stage	talon rd ded to achieve a top of Min Cu Ft 644 Coupling 0.00 0.00 his csg, TOC intended Min	3.41 9860 1 Stage % Excess 37 #N/A #N/A 1 Stage	Collapse 2.26 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su Drilling	Burst 2.47 Totals: rface or a Calc MASP Factors Burst Totals: rface or a Calc	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 4.13 hoose Casi	3.79 ng> a-C	351,140 0 0 351,140 overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0 0 overlap. Min Dist
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 63/4 Class 'C' tail cm #N/A 0 Segment "A" "B" Hole Size	C: #/ft 20.00 w/: Annular Volume 0.0835 tyld ≥ 1.35 tyld ≥ 1.35 #/ft	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 534 Grade 8.4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage Cmt Sx	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 882 5 1/2 : psig: alc below includes t 1 Stage CuFt Cmt	talon rd ded to achieve a top of Min Cu Ft 644 Coupling 0.00 0.00 his csg, TOC intended Min Cu Ft	3.41 9860 1 Stage % Excess 37 #N/A #N/A 1 Stage % Excess	Collapse 2.26 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su	Burst 2.47 Totals: rface or a Calc MASP Factors Burst Totals: rface or a	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 0 #N/A	2	a-B 4.13 hoose Casi	3.79 ng> a-C	351,140 0 0 351,140 overlap. Min Dist Hole-Cplg 0.43 Weight 0 0 0
Tail cmt 51/2 Segment "A" "B" "C" "D" Hole Size 6 3/4 class 'C' tail cm #N/A 0 Segment "A" "B" Hole	د: #/ft 20.00 «/‹ Annular Volume 0.0835 tyld > 1.35 #/ft #/ft «/› Annular	Grade 8.4#/g mud, 30min Sfc Csg Test The cement v 1 Stage Cmt Sx 534 Grade 8.4#/g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	p 110 : psig: 2,349 volume(s) are intend 1 Stage CuFt Cmt 882 5 1/2 : psig: alc below includes t 1 Stage	talon rd ded to achieve a top of Min Cu Ft 644 Coupling 0.00 0.00 0.00 his csg, TOC intended Min Cu Ft 0	3.41 9860 1 Stage % Excess 37 #N/A #N/A 1 Stage	Collapse 2.26 ft from su Drilling Mud Wt 10.50 <u>Design I</u> Collapse ft from su Drilling	Burst 2.47 Totals: rface or a Calc MASP Factors Burst Totals: rface or a Calc	17,557 0 0 17,557 200 Req'd BOPE Length 0 0 0 #N/A Req'd	2	a-B 4.13 hoose Casi	3.79 ng> a-C	351,140 0 0 351,140 overlap. Min Dist Hole-Cpl 0.43 Weight 0 0 0 0 overlap. Min Dist

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PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	WPX Energy Permian LLC -
LOCATION:	Section 26, T.26 S., R.29 E., NMPM
COUNTY:	Eddy County, New Mexico
WELL NAME & NO.:	Steel Guitar 35-26 Fed Com 443H
ATS/API ID:	3001555941
APD ID:	10400095628
Sundry ID:	2828321
WELL NAME & NO.:	Steel Guitar 35-26 Fed Com 444H
ATS/API ID:	3001555942
APD ID:	10400095624
Sundry ID:	2828321

COA

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Primary Desig	<u></u>		-
H2S	Yes		
Potash	None 🔻	None	
Cave/Karst Potential	High		
Cave/Karst Potential	Critical		
Variance	C None	🖸 Flex Hose	C Other
Wellhead	Conventional and Multibov	vl 🔫	
Other	□ 4 String □ 5 String	Capitan Reef None	□WIPP
Other	Pilot Hole None	C Open Annulus	
Cementing	Contingency Squeeze	Echo-Meter Int 1	Primary Cement Squeeze None
Special Requirements	□ Water Disposal/Injection	COM	🗖 Unit
Special Requirements	Batch Sundry	Waste Prevention None	
Special Requirements Variance	□ Break Testing	Cementing	Casing Clearance

Primary Design:

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Alternate Desi	ign:		
Potash	None	None	
Cave/Karst Potential	High		
Cave/Karst Potential	Critical		
Other	□ 4 String □ 5 String	Capitan Reef None	WIPP
Other	Pilot Hole None	C Open Annulus	
Cementing	Contingency Squeeze	Echo-Meter Int 1	Primary Cement Squeeze None

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. As a result, the Hydrogen Sulfide area must meet **43 CFR part 3170 Subpart 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

Primary Design

B. CASING

- 1. The 9-5/8 inch surface casing shall be set at approximately 411 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 13 1/2 inch in diameter.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

Option 1 (Single Stage):

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 5070'.
- b. Second stage:
 - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 454 sxs Class C)
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down **9-5/8**" X **7-5/8**" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the **7-5/8**" casing to surface after the second stage <u>BH to verify TOC.</u></u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Alternate Design

C. CASING

- 4. The 10-3/4 inch surface casing shall be set at approximately 411 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 14 3/4 inch in diameter.
 - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature

survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- f. Wait on cement (WOC) time for a primary cement job will be a minimum of $\underline{8}$ <u>hours</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- h. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

5. The minimum required fill of cement behind the 8-5/8 inch intermediate casing is:

Option 1 (Single Stage):

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- c. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 5070'.
- d. Second stage:
 - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 572 sxs Class C)
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down **10-3/4**" X **8-5/8**" annulus after primary cementing stage. <u>Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the **8-5/8**" casing to surface after the second stage <u>BH to verify TOC.</u></u>

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 6. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

D. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2.

Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **8-5/8** inch intermediate casing shoe shall be **5000 (5M)** psi.

Option 2:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **9-5/8** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.

a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.

- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

Option 3:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the **10-3/4** inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
 - e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

E. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171

- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be on the sign.</u>

Batch Sundry:

- Approval shall be for wells with surface, intermediate, and production section within 200' TVD tolerance between shoes above the deepest well shoe(s) set depth.
- Approval shall be for wells with same drill plan design. (Casing depth may vary and cement volumes may vary per Condition of Approval.)
- Approval shall be for wells within the same drill pad.
- Cement excess shall be a minimum of 25%, adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Eddy County
 EMAIL or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,
 BLM NM CFO DrillingNotifications@BLM.GOV

(575) 361-2822

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or

if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

- Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.

- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
 - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been

done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

Long Vo (LVO) 1/29/2025

Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Operator:	OGRID:
WPX Energy Permian, LLC	246289
Devon Energy - Regulatory	Action Number:
Oklahoma City, OK 73102	426223
	Action Type:
	[C-103] NOI Change of Plans (C-103A)
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CONDITIONS

Created By	Condition	Condition Date
ward.rikala	Any previous COA's not addressed within the updated COA's still apply.	2/7/2025

CONDITIONS

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Action 426223