

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Sundry Print Reports
01/27/2025

Well Name: MORGAN 25-13 FED COM Well Location: T25S / R31E / SEC 25 / County or Parish/State: EDDY /

SWNE / 32.101855 / -103.728479

NM

Well Number: 837H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMLC062300 Unit or CA Name: Unit or CA Number:

US Well Number: 3001555871 **Operator:** DEVON ENERGY

PRODUCTION COMPANY LP

Notice of Intent

Sundry ID: 2831341

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/13/2025 Time Sundry Submitted: 09:48

Date proposed operation will begin: 01/14/2025

Procedure Description: Devon Energy Production Co., L.P. (Devon) respectfully requests to move BHL on the subject well. We also request a change to the drilling plan with casing changes and slim hole design. Please see attached revised C102, Drill plan, and directional plan. Permitted BHL: NWNE, 20 FNL, 1650 FEL, 13-25S-31E Proposed BHL: NENW, 20 FNL, 2310 FWL, 13-25S-31E

NOI Attachments

Procedure Description

5.5_20lb_P110HP_TALON_RD_20250113093413.pdf

7.625_29.7lb_P110_HP_Talon_SFC_20250113093347.pdf

10.75_45.5lb_J55_SEAH_20250113093334.pdf

MORGAN_25_13_FED_COM_837H_Directional_Plan_11_21_24_20250113093258.pdf

MORGAN_25_13_FED_COM_837H_Rev1_20250113093237.pdf

WA022390597_MORGAN_25_13_FED_COM_837H_WL_R1_SIGNED_20250113093222.pdf

well Name: MORGAN 25-13 FED COM Well Location: T25S / R31E / SEC 25 / County or Parish/State: EDBY 7 of

SWNE / 32.101855 / -103.728479

Well Number: 837H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMLC062300 Unit or CA Name: Unit or CA Number:

US Well Number: 3001555871 **Operator:** DEVON ENERGY

PRODUCTION COMPANY LP

Conditions of Approval

Specialist Review

Morgan_25_13_Fed_Com_837H_Sundry_ID_2831341_20250124081826.pdf

Operator

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Signed on: JAN 13, 2025 09:34 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Professional

Street Address: 333 WEST SHERIDAN AVENUE

City: OKLAHOMA CITY State: OK

Phone: (405) 552-6137

Email address: AMY.BROWN@DVN.COM

Field

Representative Name:

Street Address:

City: State: Zip:

Phone:

Email address:

BLM Point of Contact

BLM POC Name: LONG VO BLM POC Title: Petroleum Engineer

BLM POC Phone: 5759885402 **BLM POC Email Address:** LVO@BLM.GOV

Disposition: Approved **Disposition Date:** 01/24/2025

Signature: Long Vo

Form 3160-5 (June 2019)

UNITED STATES DEPARTMENT OF THE INTERIOR DEPARTMENT OF TAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

BURI	EAU OF LAND MANAGEMENT	5. Lease Serial No.		
Do not use this f	OTICES AND REPORTS ON Worm for proposals to drill or to Use Form 3160-3 (APD) for suc	6. If Indian, Allottee or Tribe	Name	
SUBMIT IN 1	TRIPLICATE - Other instructions on pag	7. If Unit of CA/Agreement, N	Name and/or No.	
1. Type of Well Oil Well Gas W	/ell Other		8. Well Name and No.	
2. Name of Operator			9. API Well No.	
3a. Address	3b. Phone No.	(include area code)	10. Field and Pool or Explora	tory Area
4. Location of Well (Footage, Sec., T.,R	.,M., or Survey Description)		11. Country or Parish, State	
12. CHE	CK THE APPROPRIATE BOX(ES) TO IN	DICATE NATURE (DF NOTICE, REPORT OR OTI	HER DATA
TYPE OF SUBMISSION		TYPI	E OF ACTION	
Notice of Intent	Acidize Deep Alter Casing Hydr	oen raulic Fracturing	Production (Start/Resume) Reclamation	Water Shut-Off Well Integrity
Subsequent Report		Construction and Abandon	Recomplete Temporarily Abandon	Other
Final Abandonment Notice		Back	Water Disposal	
is ready for final inspection.)				
14. I hereby certify that the foregoing is	true and correct. Name (Printed/Typed)	TOTAL STATE OF THE		
		Title		
Signature				
	THE SPACE FOR FED	ERAL OR STA	TE OFICE USE	
Approved by				
		Title		Date
	ned. Approval of this notice does not warrar equitable title to those rights in the subject led duct operations thereon.			
	3 U.S.C Section 1212, make it a crime for a ents or representations as to any matter with		and willfully to make to any do	epartment or agency of the United States

(Instructions on page 2)

GENERAL INSTRUCTIONS

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

SPECIFIC INSTRUCTIONS

Item 4 - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

(Form 3160-5, page 2)

Additional Information

Location of Well

0. SHL: SWNE / 2433 FNL / 1680 FEL / TWSP: 25S / RANGE: 31E / SECTION: 25 / LAT: 32.101855 / LONG: -103.728479 (TVD: 0 feet, MD: 0 feet) PPP: SWNE / 2538 FNL / 1650 FEL / TWSP: 25S / RANGE: 31E / SECTION: 25 / LAT: 32.101567 / LONG: -103.728383 (TVD: 11645 feet, MD: 11656 feet) PPP: SWSE / 192 FSL / 1647 FEL / TWSP: 25S / RANGE: 31E / SECTION: 13 / LAT: 32.1235811 / LONG: -103.7283535 (TVD: 12679 feet, MD: 20600 feet) PPP: SWNE / 2508 FNL / 1648 FEL / TWSP: 25S / RANGE: 31E / SECTION: 24 / LAT: 32.11616 / LONG: -103.7283628 (TVD: 12717 feet, MD: 17900 feet) PPP: SWSE / 171 FSL / 1650 FEL / TWSP: 25S / RANGE: 31E / SECTION: 24 / LAT: 32.1090137 / LONG: -103.7283718 (TVD: 12753 feet, MD: 15300 feet) BHL: NWNE / 20 FNL / 1650 FEL / TWSP: 25S / RANGE: 31E / SECTION: 13 / LAT: 32.137524 / LONG: -103.728336 (TVD: 12609 feet, MD: 25673 feet)

U. S. Steel Tubular Products 5.500" 20.00lb/ft (0.361" Wall)

P110 HP USS-TALON HTQ™ RD

2/21/2024 7:48:59 AM

MECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		
Critical Area	5.828	5.828	sq. in.	
Joint Efficiency		100.0	%	[2]
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		
Minimum Collapse Pressure	13,150	13,150	psi	
Minimum Internal Yield Pressure	14,360	14,360	psi	
Minimum Pipe Body Yield Strength	729,000		lb	
Joint Strength		729,000	lb	
Compression Rating		729,000	lb	
Reference Length		24,300	ft	[5]
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		
Make-Up Loss		5.58	in.	
Minimum Make-Up Torque		18,400	ft-lb	[4]
Maximum Make-Up Torque		21,400	ft-lb	[4]
Maximum Operating Torque		44,400	ft-lb	[4]

Notes

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3. Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- Coupling must meet minimum mechanical properties of the pipe.

Legal Notice

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com

[4]

U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall)

5/15/2024 6:31:14 PM

P110 HP USS-TALON SFC™

	~~~~		-	
MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	
Joint Efficiency		85.8	%	
PERFORMANCE	Pipe	USS-TALON SFC™		
Minimum Collapse Pressure	7,260	7,260	psi	
Minimum Internal Yield Pressure	10,750	10,750	psi	
Minimum Pipe Body Yield Strength	1,068,000		lb	
Joint Strength		916,000	lb	
Compression Rating		916,000	lb	
Reference Length		20,560	ft	
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	
MAKE-UP DATA	Pipe	USS-TALON SFC™		
Make-Up Loss		5.08	in.	
Minimum Make-Up Torque		30,000	ft-lb	
Maximum Make-Up Torque		33,000	ft-lb	

### **Notes**

1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).

80,500

- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- Uniaxial bend rating shown is structural only.

Maximum Operating Torque

- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

### **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com

ft-lb



# <u>10-3/4"</u> <u>45.50#</u> <u>0.400"</u> <u>J-55</u>

in.

in.

1000 lbs

1000 lbs

493

796

10.750

0.400

### **Dimensions (Nominal)**

**Outside Diameter** 

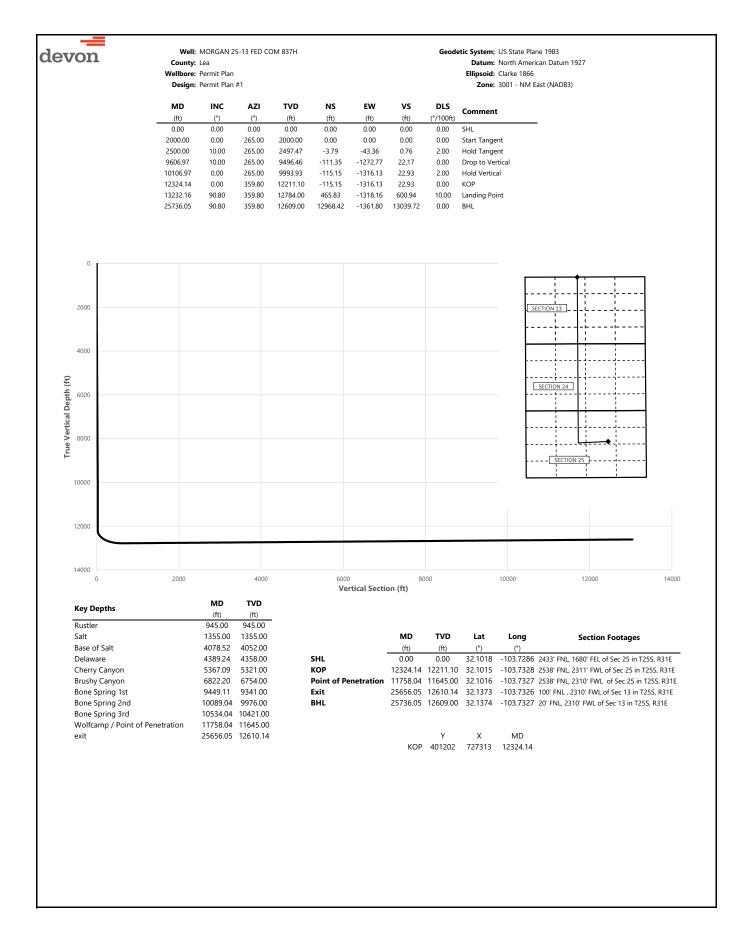
Wall

Inside Diameter	9.950	in.
Drift	9.875	in.
Weight TSC	45.500	lbs/ft
Weight, T&C		lbs/ft
Weight, PE	44.260	lbs/ft
Internal Yield Pressure at Minimum Yield		
Collapse	2090	psi
Internal Yields Pressure		
PE	3580	psi
STC	3580	psi
ВТС	3580	psi
Yield Strength, Pipe Body	715	1000 lbs
Joint Strength, STC		

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

STC

**BTC** 





Well: MORGAN 25-13 FED COM 837H

County: Lea

Datum: North American Datum 1927

Vellbore: Permit Plan

Ellipsoid: Clarke 1866

Wellbore: Permit Plan
Design: Permit Plan #1

Zone: 3001 - NM East (NAD83) MD TVD vs INC AZI NS EW DLS Comment (°/100ft) (ft) (ft) (°) (°) (ft) (ft) (ft) SHL 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 100.00 0.00 265.00 100.00 0.00 0.00 0.00 0.00 200.00 0.00 265.00 200.00 0.00 0.00 0.00 0.00 300.00 0.00 265.00 300.00 0.00 0.00 0.00 0.00 400.00 0.00 265.00 400.00 0.00 0.00 0.00 0.00 500.00 0.00 265.00 500.00 0.00 0.00 0.00 0.00 600.00 0.00 265.00 600.00 0.00 0.00 0.00 0.00 700.00 0.00 265.00 700.00 0.00 0.00 0.00 0.00 800.00 0.00 265.00 800.00 0.00 0.00 0.00 0.00 900.00 0.00 265.00 900.00 0.00 0.00 0.00 0.00 945.00 265.00 945.00 0.00 0.00 0.00 0.00 0.00 Rustle 1000.00 0.00 265.00 1000.00 0.00 0.00 0.00 0.00 1100.00 0.00 265.00 1100.00 0.00 0.00 0.00 0.00 1200.00 0.00 265.00 1200.00 0.00 0.00 0.00 1300.00 0.00 265.00 1300.00 0.00 0.00 0.00 0.00 1355.00 0.00 265.00 1355.00 0.00 0.00 0.00 0.00 Salt 1400.00 265.00 1400.00 0.00 0.00 0.00 0.00 0.00 1500.00 0.00 265.00 1500.00 0.00 0.00 0.00 0.00 1600.00 0.00 265.00 1600.00 0.00 0.00 0.00 0.00 1700.00 0.00 265.00 1700.00 0.00 0.00 0.00 0.00 1800.00 0.00 265.00 1800.00 0.00 0.00 0.00 0.00 1900.00 0.00 265.00 1900.00 0.00 0.00 0.00 0.00 2000.00 0.00 265.00 2000 00 0.00 0.00 0.00 0.00 Start Tangent 2100.00 2.00 265.00 2099.98 -0.15 -1.74 0.03 2.00 2200.00 4.00 265.00 2199.84 -0.61 -6.95 0.12 2.00 2300.00 6.00 265.00 2299.45 -1.37 -15.63 0.27 2.00 2400.00 8.00 265.00 2398.70 -243 -27 77 0.48 2.00 2500.00 10.00 265.00 2497.47 -3.79 -43.36 0.76 Hold Tangent 2.00 2600.00 10.00 265.00 2595.95 -5.31 -60.66 1.06 0.00 2700.00 10.00 265.00 2694.43 -6.82 -77.95 0.00 1.36 2800.00 10.00 265.00 2792.91 -8.33 -95.25 1.66 0.00 2900.00 10.00 2891.39 -9.85 -112.55 1.96 0.00 265.00 3000.00 2989.87 -11.36 -129.85 0.00 10.00 265.00 2.26 3088.35 3100.00 10.00 265.00 -12.87-147.152.56 0.00 3200.00 10.00 265.00 3186.83 -14.39 -164.45 2.87 0.00 3300.00 10.00 265.00 3285.31 -15.90 -181.75 3.17 0.00 3400.00 10.00 265.00 3383.79 -17.41 -199.05 0.00 3.47 3500.00 10.00 265.00 3482.27 -18.93 -216.34 3.77 0.00 3600.00 10.00 265.00 3580.75 -20.44 -233.64 4.07 0.00 3700.00 265.00 3679.23 -21.96 -250.94 4.37 0.00 10.00 3800.00 10.00 265.00 3777.72 -23.47-268.24 4.67 0.00 3900.00 10.00 265.00 3876.20 -24.98 -285.54 4 97 0.00 4000.00 10.00 265.00 3974.68 -26.50 -302.84 5.28 0.00 4052.00 -27.68 4078.52 10.00 265.00 -316.42 0.00 Base of Salt 5.51 4100.00 10.00 265.00 4073.16 -28.01 -320.145.58 0.00 4200.00 10.00 265.00 4171.64 -29.52 -337.44 5.88 0.00 4300.00 10.00 265.00 4270.12 -31.04 -354.73 6.18 0.00 4389.24 265.00 4358.00 0.00 10.00 -32.39 -370.176.45 Delaware 4400.00 10.00 265.00 4368.60 -32.55 -372.03 6.48 0.00 4500.00 10.00 265.00 4467.08 -34.06 -389.33 6.78 0.00 4600.00 10.00 265.00 4565.56 -35.58 -406.63 7.08 0.00 4700.00 10.00 265.00 4664.04 -37.09-423.93 0.00 7.39

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5944.29

6042 77

6141.25

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-475.82

-493 12

-510.42

-527.72

-539.33

-545.02

-562.32

-579.62

-596 92

-614.21

-631.51

-648.81

-666.11

-683.41

-700.71

-718.01

7.69

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Cherry Canyon



Well: MORGAN 25-13 FED COM 837H

County: Lea Wellbore: Permit Plan Design: Permit Plan #1 Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

**Zone:** 3001 - NM East (NAD83)

	Design.	remitria						Zone. 3001 - Mili Edst (MA
MD	INC	AZI	TVD	NS	EW	vs	DLS	_
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
500.00	10.00	265.00	6436.70	-64.33	-735.31	12.81	0.00	
600.00	10.00	265.00	6535.18	-65.85	-752.60	13.11	0.00	
700.00	10.00	265.00	6633.66	-67.36	-769.90	13.41	0.00	
5800.00	10.00	265.00	6732.14	-68.87	-787.20	13.71	0.00	
								Prushu Canuan
6822.20	10.00	265.00	6754.00	-69.21	-791.04	13.78	0.00	Brushy Canyon
6900.00	10.00	265.00	6830.62	-70.39	-804.50	14.02	0.00	
7000.00	10.00	265.00	6929.10	-71.90	-821.80	14.32	0.00	
7100.00	10.00	265.00	7027.58	-73.41	-839.10	14.62	0.00	
7200.00	10.00	265.00	7126.06	-74.93	-856.40	14.92	0.00	
7300.00	10.00	265.00	7224.54	-76.44	-873.70	15.22	0.00	
7400.00	10.00	265.00	7323.02	-77.96	-890.99	15.52	0.00	
7500.00	10.00	265.00	7421.50	-79.47	-908.29	15.82	0.00	
7600.00	10.00	265.00	7519.99	-80.98	-925.59	16.13	0.00	
7700.00	10.00	265.00	7618.47	-82.50	-942.89	16.43	0.00	
'800.00	10.00	265.00	7716.95	-84.01	-960.19	16.73	0.00	
900.00	10.00	265.00	7815.43	-85.52	-977.49	17.03	0.00	
8000.00	10.00	265.00	7913.91	-87.04	-994.79	17.33	0.00	
3100.00	10.00	265.00	8012.39	-88.55	-1012.09	17.63	0.00	
200.00	10.00	265.00	8110.87	-90.06	-1029.38	17.93	0.00	
3300.00	10.00	265.00	8209.35	-91.58	-1046.68	18.24	0.00	
8400.00	10.00	265.00	8307.83	-93.09	-1063.98	18.54	0.00	
3500.00	10.00	265.00	8406.31	-94.60	-1003.30	18.84	0.00	
3600.00	10.00	265.00		-94.60 -96.12	-1081.28		0.00	
			8504.79			19.14		
3700.00	10.00	265.00	8603.27	-97.63	-1115.88	19.44	0.00	
800.00	10.00	265.00	8701.75	-99.14	-1133.18	19.74	0.00	
3900.00	10.00	265.00	8800.24	-100.66	-1150.47	20.04	0.00	
9000.00	10.00	265.00	8898.72	-102.17	-1167.77	20.34	0.00	
9100.00	10.00	265.00	8997.20	-103.68	-1185.07	20.65	0.00	
9200.00	10.00	265.00	9095.68	-105.20	-1202.37	20.95	0.00	
9300.00	10.00	265.00	9194.16	-106.71	-1219.67	21.25	0.00	
9400.00	10.00	265.00	9292.64	-108.23	-1236.97	21.55	0.00	
9449.11	10.00	265.00	9341.00	-108.97	-1245.46	21.70	0.00	Bone Spring 1st
9500.00	10.00	265.00	9391.12	-109.74	-1254.27	21.85	0.00	
9600.00	10.00	265.00	9489.60	-111.25	-1271.57	22.15	0.00	
9606.97	10.00	265.00	9496.46	-111.35	-1272.77	22.17	0.00	Drop to Vertical
9700.00	8.14	265.00	9588.33	-112.63	-1287.38	22.43	2.00	
9800.00	6.14	265.00	9687.55	-113.71	-1299.76	22.65	2.00	
9900.00	4.14	265.00	9787.14	-114.50	-1308.69	22.80	2.00	
10000.00	2.14	265.00	9886.98	-114.97	-1314.14	22.90	2.00	
0089.04	0.36	265.00	9976.00	-115.14	-1316.07	22.93	2.00	Bone Spring 2nd
10069.04	0.14	265.00	9986.96	-115.14	-1316.07	22.93	2.00	Done Spring Life
10106.00		265.00	9993.93			22.93		Hold Vertical
	0.00			-115.15	-1316.13		2.00	Hold Vertical
10200.00	0.00	359.80	10086.96	-115.15	-1316.13	22.93	0.00	
10300.00	0.00	359.80	10186.96	-115.15	-1316.13	22.93	0.00	
10400.00	0.00	359.80	10286.96	-115.15	-1316.13	22.93	0.00	
10500.00	0.00	359.80	10386.96	-115.15	-1316.13	22.93	0.00	
10534.04	0.00	359.80	10421.00	-115.15	-1316.13	22.93	0.00	Bone Spring 3rd
10600.00	0.00	359.80	10486.96	-115.15	-1316.13	22.93	0.00	
0700.00	0.00	359.80	10586.96	-115.15	-1316.13	22.93	0.00	
10800.00	0.00	359.80	10686.96	-115.15	-1316.13	22.93	0.00	
0900.00	0.00	359.80	10786.96	-115.15	-1316.13	22.93	0.00	
1000.00	0.00	359.80	10886.96	-115.15	-1316.13	22.93	0.00	
11100.00	0.00	359.80	10986.96	-115.15	-1316.13	22.93	0.00	
11200.00	0.00	359.80	11086.96	-115.15	-1316.13	22.93	0.00	
11300.00	0.00	359.80	11186.96	-115.15	-1316.13	22.93	0.00	
11400.00	0.00	359.80	11186.96	-115.15	-1316.13	22.93	0.00	
11500.00	0.00	359.80	11386.96	-115.15	-1316.13	22.93	0.00	
11600.00	0.00	359.80	11486.96	-115.15	-1316.13	22.93	0.00	
11700.00	0.00	359.80	11586.96	-115.15	-1316.13	22.93	0.00	
11758.04	0.00	359.80	11645.00	-115.15	-1316.13	22.93	0.00	Wolfcamp / Point of Penetration
11800.00	0.00	359.80	11686.96	-115.15	-1316.13	22.93	0.00	
11900.00	0.00	359.80	11786.96	-115.15	-1316.13	22.93	0.00	
12000.00	0.00	359.80	11886.96	-115.15	-1316.13	22.93	0.00	
12100.00	0.00	359.80	11986.96	-115.15	-1316.13	22.93	0.00	
12200.00	0.00	359.80	12086.96	-115.15	-1316.13	22.93	0.00	
	0.00	359.80	12186.96	-115.15	-1316.13	22.93	0.00	
12300.00			12211.10	-115.15	-1316.13	22.93	0.00	KOP
12300.00 12324.14	0.00					//	0.00	****
12324.14	0.00 7.59	359.80 359.80			-1316 15	27 92	10.00	
12324.14 12400.00	7.59	359.80	12286.74	-110.13	-1316.15 -1316.22	27.92 49.58	10.00	
12324.14					-1316.15 -1316.22 -1316.36	27.92 49.58 87.74	10.00 10.00 10.00	



Well: MORGAN 25-13 FED COM 837H

County: Lea
Wellbore: Permit Plan
Design: Permit Plan #1

Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

	Design:	Permit Plan	n #1	<b>Zone:</b> 3001 - NM East (NAD83)				
MD (ft)	INC (°)	<b>AZI</b> (°)	TVD (ft)	NS (ft)	<b>EW</b> (ft)	VS (ft)	<b>DLS</b> (°/100ft)	Comment
12700.00	37.59	359.80	12560.58	3.78	-1316.55	141.25	10.00	
12800.00	47.59	359.80	12634.11	71.36	-1316.78	208.49	10.00	
12900.00	57.59	359.80	12694.79	150.69	-1317.06	287.41	10.00	
13000.00	67.59	359.80	12740.77	239.34	-1317.37	375.62	10.00	
13100.00	77.59	359.80	12770.66	334.64	-1317.70	470.42	10.00	
13200.00	87.59	359.80	12783.55	433.68	-1318.05	568.96	10.00	Landing Point
13232.16 13300.00	90.80 90.80	359.80 359.80	12784.00 12783.05	465.83 533.66	-1318.16 -1318.39	600.94 668.43	10.00 0.00	Landing Point
13400.00	90.80	359.80	12781.65	633.65	-1318.74	767.91	0.00	
13500.00	90.80	359.80	12780.25	733.64	-1319.09	867.39	0.00	
13600.00	90.80	359.80	12778.85	833.63	-1319.44	966.87	0.00	
13700.00	90.80	359.80	12777.45	933.62	-1319.79	1066.35	0.00	
13800.00	90.80	359.80	12776.05	1033.61	-1320.14	1165.83	0.00	
13900.00	90.80	359.80	12774.65	1133.60	-1320.49	1265.31	0.00	
14000.00	90.80	359.80	12773.25	1233.59	-1320.84	1364.79	0.00	
14100.00	90.80	359.80	12771.86	1333.58	-1321.19	1464.27	0.00	
14200.00	90.80	359.80	12770.46	1433.57	-1321.54	1563.75	0.00	
14300.00 14400.00	90.80 90.80	359.80 359.80	12769.06 12767.66	1533.56 1633.55	-1321.89 -1322.24	1663.23 1762.70	0.00	
14500.00	90.80	359.80	12767.66	1733.54	-1322.24	1862.18	0.00	
14600.00	90.80	359.80	12764.86	1833.53	-1322.94	1961.66	0.00	
14700.00	90.80	359.80	12763.46	1933.52	-1323.29	2061.14	0.00	
14800.00	90.80	359.80	12762.06	2033.51	-1323.64	2160.62	0.00	
14900.00	90.80	359.80	12760.66	2133.50	-1323.99	2260.10	0.00	
15000.00	90.80	359.80	12759.26	2233.49	-1324.34	2359.58	0.00	
15100.00	90.80	359.80	12757.86	2333.48	-1324.69	2459.06	0.00	
15200.00 15300.00	90.80	359.80	12756.46	2433.46	-1325.04	2558.54	0.00	
15400.00	90.80 90.80	359.80 359.80	12755.06 12753.66	2533.45 2633.44	-1325.39 -1325.74	2658.02 2757.50	0.00	
15500.00	90.80	359.80	12752.26	2733.43	-1325.74	2856.98	0.00	
15600.00	90.80	359.80	12750.86	2833.42	-1326.43	2956.46	0.00	
15700.00	90.80	359.80	12749.46	2933.41	-1326.78	3055.94	0.00	
15800.00	90.80	359.80	12748.07	3033.40	-1327.13	3155.41	0.00	
15900.00	90.80	359.80	12746.67	3133.39	-1327.48	3254.89	0.00	
16000.00	90.80	359.80	12745.27	3233.38	-1327.83	3354.37	0.00	
16100.00	90.80	359.80	12743.87	3333.37	-1328.18	3453.85	0.00	
16200.00	90.80	359.80	12742.47	3433.36	-1328.53	3553.33	0.00	
16300.00 16400.00	90.80 90.80	359.80 359.80	12741.07 12739.67	3533.35 3633.34	-1328.88 -1329.23	3652.81 3752.29	0.00	
16500.00	90.80	359.80	12738.27	3733.33	-1329.58	3851.77	0.00	
16600.00	90.80	359.80	12736.87	3833.32	-1329.93	3951.25	0.00	
16700.00	90.80	359.80	12735.47	3933.31	-1330.28	4050.73	0.00	
16800.00	90.80	359.80	12734.07	4033.30	-1330.63	4150.21	0.00	
16900.00	90.80	359.80	12732.67	4133.29	-1330.98	4249.69	0.00	
17000.00	90.80	359.80	12731.27	4233.28	-1331.33	4349.17	0.00	
17100.00	90.80	359.80	12729.87	4333.27	-1331.68	4448.65	0.00	
17200.00 17300.00	90.80 90.80	359.80 359.80	12728.47 12727.07	4433.26 4533.25	-1332.03 -1332.38	4548.13 4647.60	0.00	
17300.00	90.80	359.80	12727.07	4533.25	-1332.36	4747.08	0.00	
17500.00	90.80	359.80	12724.27	4733.23	-1332.73	4846.56	0.00	
17600.00	90.80	359.80	12722.88	4833.22	-1333.43	4946.04	0.00	
17700.00	90.80	359.80	12721.48	4933.20	-1333.78	5045.52	0.00	
17800.00	90.80	359.80	12720.08	5033.19	-1334.12	5145.00	0.00	
17900.00	90.80	359.80	12718.68	5133.18	-1334.47	5244.48	0.00	
18000.00	90.80	359.80	12717.28	5233.17	-1334.82	5343.96	0.00	
18100.00	90.80	359.80	12715.88	5333.16	-1335.17	5443.44	0.00	
18200.00 18300.00	90.80 90.80	359.80 359.80	12714.48 12713.08	5433.15 5533.14	-1335.52 -1335.87	5542.92 5642.40	0.00	
18400.00	90.80	359.80	12713.08	5533.14 5633.13	-1335.87 -1336.22	5642.40 5741.88	0.00	
18500.00	90.80	359.80	12711.08	5733.12	-1336.57	5841.36	0.00	
18600.00	90.80	359.80	12708.88	5833.11	-1336.92	5940.84	0.00	
18700.00	90.80	359.80	12707.48	5933.10	-1337.27	6040.32	0.00	
18800.00	90.80	359.80	12706.08	6033.09	-1337.62	6139.79	0.00	
18900.00	90.80	359.80	12704.68	6133.08	-1337.97	6239.27	0.00	
19000.00	90.80	359.80	12703.28	6233.07	-1338.32	6338.75	0.00	
19100.00	90.80	359.80	12701.88	6333.06	-1338.67	6438.23	0.00	
19200.00	90.80	359.80	12700.48	6433.05	-1339.02	6537.71	0.00	
19300.00 19400.00	90.80 90.80	359.80 359.80	12699.09 12697.69	6533.04 6633.03	-1339.37 -1339.72	6637.19 6736.67	0.00	
19500.00	90.80	359.80	12696.29	6733.02	-1339.72	6836.15	0.00	



Well: MORGAN 25-13 FED COM 837H

County: Lea Wellbore: Permit Plan Design: Permit Plan #1 Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

Zone: 3001 - NM East (NAD83)

MD	INC	AZI	TVD	NS	EW	VS	DLS	Comment
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	
9600.00 9700.00	90.80 90.80	359.80 359.80	12694.89 12693.49	6833.01 6933.00	-1340.42 -1340.77	6935.63 7035.11	0.00	
9800.00	90.80	359.80	12692.09	7032.99	-1340.77	7134.59	0.00	
19900.00	90.80	359.80	12690.69	7132.98	-1341.47	7234.07	0.00	
20000.00	90.80	359.80	12689.29	7232.97	-1341.82	7333.55	0.00	
20100.00	90.80	359.80	12687.89	7332.95	-1342.16	7433.03	0.00	
20200.00	90.80	359.80	12686.49	7432.94	-1342.51	7532.51	0.00	
0300.00	90.80	359.80	12685.09	7532.93	-1342.86	7631.98	0.00	
20400.00	90.80	359.80	12683.69	7632.92	-1343.21	7731.46	0.00	
20500.00	90.80	359.80	12682.29	7732.91	-1343.56	7830.94	0.00	
20600.00	90.80	359.80	12680.89	7832.90	-1343.91	7930.42	0.00	
20700.00	90.80	359.80	12679.49	7932.89	-1344.26	8029.90	0.00	
00.0080	90.80	359.80	12678.09	8032.88	-1344.61	8129.38	0.00	
20900.00	90.80	359.80	12676.69	8132.87	-1344.96	8228.86	0.00	
21000.00	90.80	359.80	12675.29	8232.86	-1345.31	8328.34	0.00	
21100.00 21200.00	90.80 90.80	359.80 359.80	12673.90 12672.50	8332.85 8432.84	-1345.66 -1346.01	8427.82 8527.30	0.00	
1200.00	90.80	359.80	12672.30	8532.83	-1346.36	8626.78	0.00	
1400.00	90.80	359.80	12669.70	8632.82	-1346.71	8726.26	0.00	
21500.00	90.80	359.80	12668.30	8732.81	-1347.06	8825.74	0.00	
21600.00	90.80	359.80	12666.90	8832.80	-1347.41	8925.22	0.00	
21700.00	90.80	359.80	12665.50	8932.79	-1347.76	9024.69	0.00	
21800.00	90.80	359.80	12664.10	9032.78	-1348.11	9124.17	0.00	
21900.00	90.80	359.80	12662.70	9132.77	-1348.46	9223.65	0.00	
22000.00	90.80	359.80	12661.30	9232.76	-1348.81	9323.13	0.00	
22100.00	90.80	359.80	12659.90	9332.75	-1349.16	9422.61	0.00	
22200.00	90.80	359.80	12658.50	9432.74	-1349.51	9522.09	0.00	
22300.00	90.80	359.80	12657.10	9532.73	-1349.86	9621.57	0.00	
22400.00	90.80	359.80	12655.70	9632.72	-1350.20	9721.05	0.00	
22500.00 22600.00	90.80	359.80	12654.30	9732.71	-1350.55	9820.53	0.00	
22700.00	90.80 90.80	359.80 359.80	12652.90 12651.50	9832.69 9932.68	-1350.90 -1351.25	9920.01 10019.49	0.00	
22800.00	90.80	359.80	12650.10	10032.67	-1351.23	10019.49	0.00	
22900.00	90.80	359.80	12648.71	10132.66	-1351.95	10218.45	0.00	
23000.00	90.80	359.80	12647.31	10232.65	-1352.30	10317.93	0.00	
23100.00	90.80	359.80	12645.91	10332.64	-1352.65	10417.41	0.00	
23200.00	90.80	359.80	12644.51	10432.63	-1353.00	10516.88	0.00	
23300.00	90.80	359.80	12643.11	10532.62	-1353.35	10616.36	0.00	
23400.00	90.80	359.80	12641.71	10632.61	-1353.70	10715.84	0.00	
23500.00	90.80	359.80	12640.31	10732.60	-1354.05	10815.32	0.00	
23600.00	90.80	359.80	12638.91	10832.59	-1354.40	10914.80	0.00	
23700.00	90.80	359.80	12637.51	10932.58	-1354.75	11014.28	0.00	
23800.00	90.80	359.80	12636.11	11032.57	-1355.10	11113.76	0.00	
23900.00	90.80	359.80		11132.56		11213.24	0.00	
24000.00	90.80	359.80	12633.31	11232.55	-1355.80	11312.72	0.00	
24100.00	90.80	359.80		11332.54	-1356.15	11412.20	0.00	
24200.00	90.80	359.80 359.80	12630.51	11432.53 11532.52	-1356.50 -1356.85	11511.68 11611.16	0.00	
24300.00 24400.00	90.80 90.80	359.80 359.80		11632.52			0.00	
24400.00 24500.00	90.80	359.80		11732.50			0.00	
24600.00	90.80	359.80		11832.49			0.00	
24700.00	90.80	359.80		11932.48			0.00	
24800.00	90.80	359.80		12032.47			0.00	
24900.00	90.80	359.80		12132.46			0.00	
25000.00	90.80	359.80		12232.45		12307.51	0.00	
25100.00	90.80	359.80	12617.92	12332.43	-1359.64	12406.99	0.00	
25200.00	90.80	359.80		12432.42		12506.47	0.00	
25300.00	90.80	359.80	12615.12	12532.41	-1360.34	12605.95	0.00	
25400.00	90.80	359.80	12613.72	12632.40	-1360.69	12705.43	0.00	
25500.00	90.80	359.80		12732.39		12804.91	0.00	
25600.00	90.80	359.80		12832.38		12904.39	0.00	
25656.05	90.80	359.80		12888.43		12960.15	0.00	exit
25700.00	90.80	359.80		12932.37		13003.87	0.00	D. II
	90.80	359.80	12609.00	12968.42	-1361.80	13039.72	0.00	BHL
25736.05								

### MORGAN 25-13 FED COM 837H

### 1. Geologic Formations

TVD of target	12610	Pilot hole depth	N/A
MD at TD:	25673	Deepest expected fresh water	

### Basin

Dasin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	945		
Salt	1355		
Base of Salt	4052		
Delaware	4358		
Cherry Canyon	5321		
Brushy Canyon	6754		
Bone Spring 1st	9341		
Bone Spring 2nd	9976		
Bone Spring 3rd	10421		
Wolfcamp	11645		

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

		Wt			Casing Interval		Casing Interval		
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)	
13 1/2	9 5/8	40	J-55	BTC	0	970	0	970	
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	11921	0	11921	
6 3/4	5 1/2	20	P110HP	TALON RD	0	25673	0	12610	

[•]All casing strings will be tested in accordance with 43 CFR 3172.

### 3. Cementing Program (Primary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	512	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	375	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
	475	6764	13.2	1.44	Tail: Class H / C + additives
Production	61	10222	9	3.27	Lead: Class H /C + additives
Production	858	12222	13.2	1.44	Tail: Class H / C + additives

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

2. Casing Program (Secondary Design)

		Wt			Casing	Interval	Casing	Interval
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
14 3/4	10 3/4	45 1/2	J-55	ВТС	0	970	0	970
9 7/8	8 5/8	32	P110	Sprint FJ	0	11921	0	11921
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	25673	0	12610

[•]All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

### 3. Cementing Program (Secondary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	TOC	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	586	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	474	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
III I	597	6764	13.2	1.44	Tail: Class H / C + additives
Production	117	10222	9	3.27	Lead: Class H /C + additives
Froduction	1780	12222	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

4. Pressure Control Equipment (Three String Design)

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Ty	ype	<b>√</b>	Tested to:																																
			Anı	nular	X	50% of rated working pressure																																
Int 1	13-5/8"	5M	Bline	d Ram	X																																	
IIIt I	13-3/6	3101	Pipe	Ram		5M																																
			Doub	le Ram	X	JIVI																																
			Other*																																			
	13-5/8"		Annul	ar (5M)	X	100% of rated working pressure																																
Dun dunation		101/1	Bline	d Ram	X																																	
Production		13-5/8" 10M	Pipe	Ram		10M																																
																															,				Doub	le Ram	X	TOW
			Other*																																			
			Annular (5M)																																			
			Blind Ram																																			
			Pipe Ram																																			
			Double Ram																																			
			Other*																																			
N A variance is requested for	the use of a diverter on the surface casing. See attached for schematic.																																					
Y A variance is requested to a	A variance is requested to run a 5 M annular on a 10M system																																					

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, C	Coring and Testing
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the
X	Completion Report and sbumitted to the BLM.
	No logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain.
	Coring? If yes, explain.

Additional l	ogs planned	Interval
	Resistivity	Int. shoe to KOP
	Density	Int. shoe to KOP
X	CBL	Production casing
X	Mud log	Intermediate shoe to TD
	PEX	

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6885
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

measured va	alues and formations will be provided to the BEW.
N	H2S is present
Y	H2S plan attached.

#### MORGAN 25-13 FED COM 837H

### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

### Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).
- 3  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachments	
X	Directional Plan
	Other, describe

<u>C-102</u>			Energy,	Minera	State of ls & Natura	New Mexico Il Resources Department		Revised July, 2024		
Submit E	lectronically		OIL	CON	SERVAT	TION DIVISION				
Via OCD Permitting								Submittal	✓ Initial Submittal	
								Type:	☐ Amended Repor	t
									☐ As Drilled	
						ION INFORMATIO	N			
	umber		Pool Cod			Pool Name PURPLE SAGE; WOLFCAMP (GAS)				
30-015-55871 98220 Property Code Property Name					PURPLE SA	FCAMP (	(GAS)   Well Number			
				MORGAN	25-13 FED COM			837H		
OGRID No. Operator Name 6137 DEVON				ENERGY PRODUCTION COMPANY, L.P.				Ground Level	Elevation	
Surface Owner: $\Box$ State $\Box$ Fe			 						3328.9'	
Suriac	e Owner:	state _	ree uirii	oai ⊔ree	uerai	Mineral Owner: □State □Fee □Tribal □Federal				
					Suri	face Location				
UL	Section	Township	Range	Lot	Ft. from N,	/S Ft. from E/W	Latitude		Longitude	County
G	25	25-S	31-E		2433' N	1680' E	32.101	855	103.728479	EDDY
					Botto	m Hole Location				
UL	Section	Township	Range	Lot	Ft. from N,	/S Ft. from E/W	Latitude		Longitude	County
C	13	25-S	31-E		20' N	2310' W	32.137	524	103.732644	EDDY
Dedicate	ed Acres	Infill or Def	ining Well	Defining	Well API Over	clapping Spacing Uni	t (Y/N)	Consolid	lation Code	
800.0	0	INFILL		30-015-	55637					
Order 1	Numbers	PENDING 1	NSL		Well setbacks are under Common Ownership: □Yes □No					
										,
UL	Section	Township	Danas	Lot	Ft. from N	f Point (KOP) /S Ft. from E/W	Latitude		Longitude	Country
	Section	-	Range	Lot	·	·			Longitude	County
F	25	25-S	31-E		2538' N	2311' W	32.1015		-103.7328	EDDY
		m 1.		T		ake Point (FTP)			· · · ·	
UL F	Section 25	Township 25-S	Range 31-E	Lot	Ft. from N, 2538' N	/S Ft. from E/W 2310' W	Latitude	550	Longitude 103.732734	County EDDY
Г	20	20-5	21-F		2000 N	2310 W	32.101	556	103.732734	EDDI
	I					ake Point (LTP)				
UL	Section	Township	Range	Lot	Ft. from N		Latitude	004	Longitude	County
С	13	25-S	31-E		100' N	2310' W	32.137	304	103.732644	EDDY
Spacing						Unit Type Horizontal Vertical		cal	Ground Floor Elevation:	
1		FICATIONS				SURVEYOR CERTIFICATIONS				
					omplete to the best onal well, that this	I hereby certify that the we	I hereby certify that the well location shown on this plat was plotted from field notes			
of my knowledge and belief, and, if the well is a vertical or directional well, that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of a working interest or unleased mineral interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.					of actual surveys made by me or under supervision, and that the same is true and correct to the best of my belief. $R \cdot D_{EA}$					
									DEHO	
					correct to the best of my belief.  R. DEMOLOGO  WEXT COST  23261			MEX O		
·								(%\"\		
If this well is a horizontal well, I further certify that this organization has received the consent of at least one lessee or owner of a working interest or unleased mineral								)		
interest in each tract (in the target pool or formation) in which any part of the well's completed interval will be located or obtained a compulsory pooling order from the								1 2 /2		
division										
Amy A. Brown 01/08/2025						Signature and Soci	of Profes	ssional G	Surveyor	<u> </u>
Signature Date						Signature and Seal of Professional Surveyor ONAL				
Amy A. Brown										
Printed Name						Certificate Number	Date of	Survey		
amy.brown@dvn.com Email Address						23261	10/20	24		
MARANA ARAMA COO						~5~01	10, 20	- 1		

#### ACREAGE DEDICATION PLATS

This grid represents a standard section. You may superimpose a non-standard section, or larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is closest to any outer boundary of the tract.

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.

SURFACE HOLE LOCATION
GEODETIC CODRDINATES NAD 83
NMSP EAST SURFACE LOCATION
2433' FNL 1680' FEL SECTION 25
EL: 3329.5'
N:401316.80/E:728628.98
LAT:32.101855/LON:103.728479

KICK DFF PDINT
CALLS: 2538' FNL, 2311' FWL
N:401202 _ /E:727313 _
LAT: 32.1015_/LON:_103.7328

FIRST TAKE PDINT
2538' FNL 2310' FWL SECTION 25
N:401201.46/E:727312.09
LAT:32.101558/LON:103.732734

LAST TAKE PDINT
100' FNL 2310' FWL SECTION 13
N:414205.22/E:727267.55
LAT:32.137304/LON:103.732644

BOTTOM HOLE LOCATION
20' FNL 2310' FWL SECTION 13
N:414285.22/E:727267.18
LAT:32.137524/LON:103.732644

PPP 2
0' FNL 2310' FWL SECTION 25
N:386656.07/E:729055.59

PPP 3
2641' FSL 2305' FWL SECTION 24
N:388569.38/E:729049.04
LAT:32.066808/LDN:103.727354

PPP 4 0' FSL 2306' FWL SECTION 13 N:390486.38/E:729042.47 LAT:32.072078/LDN:103.727341

B N 89*44'46" E 2652.37' N 89°26'06" E 2641.11' 837H BHL 10 837H LTP 00"15'47" 13 T25S + R31E0061862 ñ W 2639.14 S 89°45'23" E0061869 24 MT25S-R31E 125634 2638.63 S 89*35'52" W 00"13"39" LC 0062300 837H SHL 00'18'12" NM 019619 25  $T25S^{\perp}R31E$ .80 2657.17 S 89*45'03" W S 89°15'58"

A= N:414282.44 E:724957.17 B= N:414308.48 E:727598.15 C= N:414320.23 E:730250.50 D= N:411680.59 E:730261.56 E= N:409040.49 E:730271.65 F= N:406401.43 E:730284.99 G= N:403762.83 E:730299.28 H= N:401125.54 E:730309.76 I= N:398487.77 E:730323.72 J= N:398453.76 E:727668.80 K= N:398442.20 E:725011.65 L= N:403723.61 F:724993.33 M= N:406364.11 E:724989.78 E:724979.03 N= N:409003.32 □= N:411638.94 E:724969.31 E:727618.04 P= N:409029.21 Q= N:403742.23 E:727645.07



# U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Sundry Print Reports
01/24/2025

Well Name: MORGAN 25-13 FED COM Well Location: T25S / R31E / SEC 25 / County or Parish/State: EDDY /

SWNE / 32.101855 / -103.728479

Well Number: 837H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMLC062300 Unit or CA Name: Unit or CA Number:

**US Well Number:** 3001555871 **Operator:** DEVON ENERGY

PRODUCTION COMPANY LP

### **Notice of Intent**

**Sundry ID: 2831341** 

Type of Submission: Notice of Intent

Type of Action: APD Change

Date Sundry Submitted: 01/13/2025 Time Sundry Submitted: 09:48

Date proposed operation will begin: 01/14/2025

**Procedure Description:** Devon Energy Production Co., L.P. (Devon) respectfully requests to move BHL on the subject well. We also request a change to the drilling plan with casing changes and slim hole design. Please see attached revised C102, Drill plan, and directional plan. Permitted BHL: NWNE, 20 FNL, 1650 FEL, 13-25S-31E Proposed BHL: NENW, 20 FNL, 2310 FWL, 13-25S-31E

### **NOI Attachments**

### **Procedure Description**

5.5_20lb_P110HP_TALON_RD_20250113093413.pdf

7.625_29.7lb_P110_HP_Talon_SFC_20250113093347.pdf

10.75_45.5lb_J55_SEAH_20250113093334.pdf

MORGAN_25_13_FED_COM_837H_Directional_Plan_11_21_24_20250113093258.pdf

MORGAN_25_13_FED_COM_837H_Rev1_20250113093237.pdf

WA022390597_MORGAN_25_13_FED_COM_837H_WL_R1_SIGNED_20250113093222.pdf

Well Name: MORGAN 25-13 FED COM Well Location: T25S / R31E / SEC 25 / County or Parish/State: EDDY / of

SWNE / 32.101855 / -103.728479

Well Number: 837H Type of Well: OIL WELL Allottee or Tribe Name:

Lease Number: NMLC062300 Unit or CA Name: Unit or CA Number:

**US Well Number:** 3001555871 **Operator:** DEVON ENERGY

PRODUCTION COMPANY LP

### **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: AMY BROWN Signed on: JAN 13, 2025 09:34 AM

Name: DEVON ENERGY PRODUCTION COMPANY LP

Title: Regulatory Professional

Street Address: 333 WEST SHERIDAN AVENUE

City: OKLAHOMA CITY State: OK

Phone: (405) 552-6137

Email address: AMY.BROWN@DVN.COM

### **Field**

**Representative Name:** 

**Street Address:** 

City: State: Zip:

Phone:

**Email address:** 

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:

LOCATION:
COUNTY:

Devon Energy Production Company LP

Section 25, T.25 S., R.31 E., NMPM

Eddy County, New Mexico

WELL NAME & NO.: Morgan 25-13 Fed Com 837H

ATS/API ID: 3001555871

APD ID: 10400097853

Sundry ID: 2831341

COA

**Primary Design:** 

	<b>3</b>		
H2S	No 🔽		
Potash	None	None	
Cave/Karst Potential	Medium 🔽		
Cave/Karst Potential	☐ Critical		
Variance	None	Flex Hose	C Other
Wellhead	Conventional and Multibov	vl 🔻	
Other	□ 4 String □ 5 String	Capitan Reef None	□WIPP
Other	Pilot Hole  None	☐ Open Annulus	
Cementing	Contingency Squeeze  None	Echo-Meter Int 1	Primary Cement Squeeze None
Special Requirements	☐ Water Disposal/Injection	<b>☑</b> COM	Unit
Special Requirements	☐ Batch Sundry	Waste Prevention None	
Special Requirements Variance	☐ Break Testing	☐ Offline Cementing	☐ Casing Clearance

Alternate Design:

Potash	None	None	
Cave/Karst Potential	Medium <u>▼</u>		
Cave/Karst Potential	Critical		
Other	□4 String □5 String	Capitan Reef None	□WIPP
Other	Pilot Hole  None	□ Open Annulus	
Cementing	Contingency Squeeze  None	Echo-Meter Int 1	Primary Cement Squeeze None

#### A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet **43 CFR part 3170 Subpart 3176**, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

### PRIMARY DESIGN

### B. CASING

- 1. The 9-5/8 inch surface casing shall be set at approximately 970 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 13 1/2 inch in diameter.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

2. The minimum required fill of cement behind the 7-5/8 inch intermediate casing is:

### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

### Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6754'.
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 378 sxs Class C)
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down 9-5/8" X 7-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 7-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- ❖ In Medium Cave/Karst Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 200 feet into previous casing string.
     Operator shall provide method of verification.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
     Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

### ALTERNATE DESIGN

### C. CASING

- 4. The 10-3/4 inch surface casing shall be set at approximately 970 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt when present, and below usable fresh water) and cemented to the surface. The surface hole shall be 14 3/4 inch in diameter.
  - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - f. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - h. If cement falls back, remedial cementing will be done prior to drilling out that string.

# Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

5. The minimum required fill of cement behind the 8-5/8 inch intermediate casing is:

### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

### **Option 2:**

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

c. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon at 6754'.

### d. Second stage:

Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified. (Squeeze 478 sxs Class C)
 Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed to pump down 10-3/4" X 8-5/8" annulus after primary cementing stage. Operator must run Echo-meter to verify Cement Slurry/Fluid top in the annulus Or operator shall run a CBL from TD of the 8-5/8" casing to surface after the second stage BH to verify TOC.

Submit results to the BLM. No displacement fluid/wash out shall be utilized at the top of the cement slurry between second stage BH and top out. Operator must run one CBL per Well Pad. Operator may conduct a negative and positive pressure test during completion to remediate sustained casing pressure.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

- ❖ In Medium Cave/Karst Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 6. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 200 feet into previous casing string.
     Operator shall provide method of verification.
     Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
     Cement excess is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

### D. PRESSURE CONTROL

1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'

2.

### Option 1:

- a. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.
- b. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 8-5/8 inch intermediate casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

### **Option 2:**

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 9-5/8 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

### Option 3:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 10-3/4 inch surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 5000 (5M) psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.

- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.

### E. SPECIAL REQUIREMENT (S)

### **Communitization Agreement**

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- The operator will submit an as-drilled survey well plat of the well completion, but are not limited to, those specified in 43 CFR part 3170 Subpart 3171
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

### **☑** Eddy County

**EMAIL** or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220,

**BLM_NM_CFO_DrillingNotifications@BLM.GOV** (575) 361-2822

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per **43** CFR part **3170** Subpart **3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

### A. CASING

1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or

- if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- B. PRESSURE CONTROL
- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR part 3170 Subpart 3172 and API STD 53 Sec. 5.3.

- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been

done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)

- c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to 43 CFR part 3170 Subpart 3172 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- e. The results of the test shall be reported to the appropriate BLM office.
- f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR part 3170 Subpart 3172.

### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

Long Vo (LVO) 1/24/2025

Form 3160-5 (June 2019)

## UNITED STATES DEPARTMENT OF THE INTERIOR

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

BURI	EAU OF LAND MANAGEMENT	Lease Serial No.     If Indian, Allottee or Tribe Name			
Do not use this t	IOTICES AND REPORTS ON \ form for proposals to drill or t Use Form 3160-3 (APD) for su				
SUBMIT IN T	TRIPLICATE - Other instructions on pa	ge 2	7. If Unit of CA/Agreement, N	Jame and/or No.	
1. Type of Well Gas W	Vell Other		8. Well Name and No.		
2. Name of Operator			9. API Well No.		
3a. Address	3b. Phone No	. (include area code)	10. Field and Pool or Explorat	ory Area	
4. Location of Well (Footage, Sec., T.,R	R.,M., or Survey Description)		11. Country or Parish, State		
12. CHE	CK THE APPROPRIATE BOX(ES) TO IN	DICATE NATURE (	OF NOTICE, REPORT OR OTH	HER DATA	
TYPE OF SUBMISSION		TYPI	E OF ACTION		
Notice of Intent	Acidize Dee	-	Production (Start/Resume)	Water Shut-Off	
		Iraulic Fracturing	Reclamation	Well Integrity	
Subsequent Report		v Construction	Recomplete	Other	
		g and Abandon	Temporarily Abandon		
Final Abandonment Notice	Convert to Injection Plus	g Back	Water Disposal		
completed. Final Abandonment Notice is ready for final inspection.)	ons. If the operation results in a multiple co tices must be filed only after all requiremen				
4. I hereby certify that the foregoing is	true and correct. Name (Printed/Typed)				
		Title			
Signature		Date			
	THE SPACE FOR FED	ERAL OR STA	TE OFICE USE		
Approved by					
		Title	1	Date	
	hed. Approval of this notice does not warra equitable title to those rights in the subject liduct operations thereon.				
Fitle 18 U.S.C Section 1001 and Title 4.	3 U.S.C Section 1212, make it a crime for a	ny person knowingly	and willfully to make to any de	epartment or agency of the United States	

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United State any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

#### **GENERAL INSTRUCTIONS**

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

#### SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

#### **NOTICES**

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-3, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

(Form 3160-5, page 2)

#### **Additional Information**

#### **Location of Well**

0. SHL: SWNE / 2433 FNL / 1680 FEL / TWSP: 25S / RANGE: 31E / SECTION: 25 / LAT: 32.101855 / LONG: -103.728479 ( TVD: 0 feet, MD: 0 feet ) PPP: SWNE / 2538 FNL / 1650 FEL / TWSP: 25S / RANGE: 31E / SECTION: 25 / LAT: 32.101567 / LONG: -103.728383 ( TVD: 11645 feet, MD: 11656 feet ) PPP: SWSE / 192 FSL / 1647 FEL / TWSP: 25S / RANGE: 31E / SECTION: 13 / LAT: 32.1235811 / LONG: -103.7283535 ( TVD: 12679 feet, MD: 20600 feet ) PPP: SWNE / 2508 FNL / 1648 FEL / TWSP: 25S / RANGE: 31E / SECTION: 24 / LAT: 32.11616 / LONG: -103.7283628 ( TVD: 12717 feet, MD: 17900 feet ) PPP: SWSE / 171 FSL / 1650 FEL / TWSP: 25S / RANGE: 31E / SECTION: 24 / LAT: 32.1090137 / LONG: -103.7283718 ( TVD: 12753 feet, MD: 15300 feet ) BHL: NWNE / 20 FNL / 1650 FEL / TWSP: 25S / RANGE: 31E / SECTION: 13 / LAT: 32.137524 / LONG: -103.728336 ( TVD: 12609 feet, MD: 25673 feet )

2/21/2024 7:48:59 AM

## U. S. Steel Tubular Products 5.500" 20.00lb/ft (0.361" Wall)

## P110 HP USS-TALON HTQ™ RD

MECHANICAL PROPERTIES	Pipe	USS-TALON HTQ™ RD		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON HTQ™ RD		
Outside Diameter	5.500	5.900	in.	
Wall Thickness	0.361		in.	
Inside Diameter	4.778	4.778	in.	
Standard Drift	4.653	4.653	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	20.00		lb/ft	
Plain End Weight	19.83		lb/ft	
SECTION AREA	Pipe	USS-TALON HTQ™ RD		-
Critical Area	5.828	5.828	sq. in.	
Joint Efficiency		100.0	%	[2]
PERFORMANCE	Pipe	USS-TALON HTQ™ RD		
Minimum Collapse Pressure	13,150	13,150	psi	
Minimum Internal Yield Pressure	14,360	14,360	psi	
Minimum Pipe Body Yield Strength	729,000		lb	
Joint Strength		729,000	lb	
Compression Rating		729,000	lb	
Reference Length		24,300	ft	[5]
Maximum Uniaxial Bend Rating		104.2	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON HTQ™ RD		
Make-Up Loss		5.58	in.	
Minimum Make-Up Torque		18,400	ft-lb	[4]
Maximum Make-Up Torque		21,400	ft-lb	[4]
Maximum Operating Torque		44,400	ft-lb	[4]

#### **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- 3. Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- 5. Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

#### **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com

5/15/2024 6:31:14 PM

## U. S. Steel Tubular Products 7.625" 29.70lb/ft (0.375" Wall)

## P110 HP USS-TALON SFC™

MECHANICAL PROPERTIES	Pipe	USS-TALON SFC™		[6]
Minimum Yield Strength	125,000		psi	
Maximum Yield Strength	140,000		psi	
Minimum Tensile Strength	130,000		psi	
DIMENSIONS	Pipe	USS-TALON SFC™		
Outside Diameter	7.625	7.900	in.	
Wall Thickness	0.375		in.	
Inside Diameter	6.875	6.815	in.	
Standard Drift	6.750	6.750	in.	
Alternate Drift			in.	
Nominal Linear Weight, T&C	29.70		lb/ft	
Plain End Weight	29.06		lb/ft	
SECTION AREA	Pipe	USS-TALON SFC™		
Critical Area	8.541	7.331	sq. in.	
Joint Efficiency		85.8	%	[2]
PERFORMANCE	Pipe	USS-TALON SFC™		
Minimum Collapse Pressure	7,260	7,260	psi	
Minimum Internal Yield Pressure	10,750	10,750	psi	
Minimum Pipe Body Yield Strength	1,068,000		lb	
Joint Strength		916,000	lb	
Compression Rating		916,000	lb	
Reference Length		20,560	ft	[5]
Maximum Uniaxial Bend Rating		64.4	deg/100 ft	[3]
MAKE-UP DATA	Pipe	USS-TALON SFC™		
Make-Up Loss		5.08	in.	
Minimum Make-Up Torque		30,000	ft-lb	[4]
Maximum Make-Up Torque		33,000	ft-lb	[4]
Maximum Operating Torque		80,500	ft-lb	[4]

#### **Notes**

- 1. Other than proprietary collapse and connection values, performance properties have been calculated using standard equations defined by API 5C3 and do not incorporate any additional design or safety factors. Calculations assume nominal pipe OD, nominal wall thickness, and Specified Minimum Yield Strength (SMYS).
- 2. Joint efficiencies are calculated by dividing the connection critical area by the pipe body area.
- Uniaxial bend rating shown is structural only.
- 4. Torques have been calculated assuming a thread compound friction factor of 1.0 and are recommended only. Field make-up torques may require adjustment based on actual field conditions (e.g. make-up speed, temperature, thread compound, etc.).
- Reference length is calculated by Joint Strength divided by Nominal Linear Weight, T&C with a 1.5 Safety factor.
- 6. Coupling must meet minimum mechanical properties of the pipe.

#### **Legal Notice**

All material contained in this publication is for general information only. This material should not therefore be used or relied upon for any specific application without independent competent professional examination and verification of accuracy, suitability and applicability. Anyone making use of this material does so at their own risk and assumes any and all liability resulting from such use. U. S. Steel disclaims any and all expressed or implied warranties of fitness for any general or particular application.

U. S. Steel Tubular Products 460 Wildwood Forest Drive, Suite 300S Spring, Texas 77380 1-877-893-9461 connections@uss.com www.usstubular.com



## <u>10-3/4"</u> <u>45.50#</u> <u>0.400"</u> <u>J-55</u>

in.

in.

10.750

0.400

### **Dimensions (Nominal)**

**Outside Diameter** 

Wall

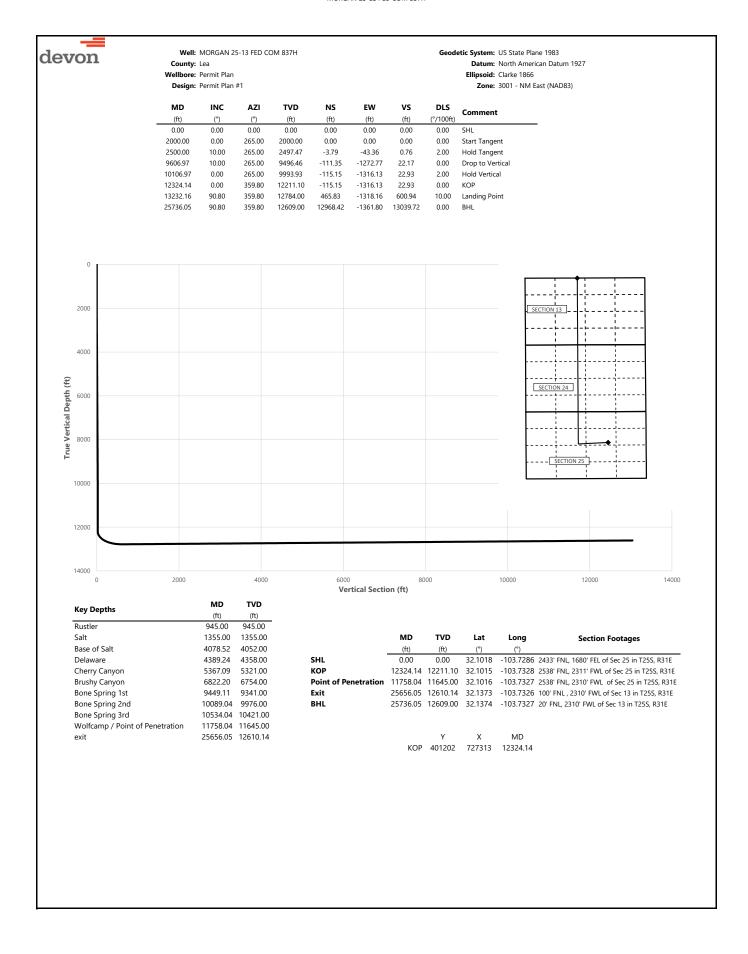
•••	0.400	
Inside Diameter	9.950	in.
Drift	9.875	in.
Weight, T&C	45.500	lbs/ft
Weight, PE	44.260	lbs/ft
Internal Yield Pressure at Minimum Yield		
Collapse	2090	psi
Internal Yields Pressure		
PE	3580	psi
STC	3580	psi
ВТС	3580	psi
Yield Strength, Pipe Body	715	1000 lbs
Joint Strength, STC		
STC	493	1000 lbs

Note: SeAH Steel has produced this specification sheet for general information only. SeAH does not assume liability or responsibility for any loss or injury resulting from the use of information or data contained herein. All applications for the material described are at the customer's own risk and responsibility.

796

1000 lbs

**BTC** 





Well: MORGAN 25-13 FED COM 837H Geodetic System: US State Plane 1983
County: Lea Datum: North American Datu

Wellbore: Permit Plan

Design: Permit Plan #

Datum: North American Datum 1927 Ellipsoid: Clarke 1866 Zone: 3001 - NM East (NAD83)

		Permit Plan	#1					Zone: 3001 - NM East (NAD83)
	Design.	T CITILE T Idi						Zone. 3001 1444 Edit (14AB03)
MD	INC	AZI	TVD	NS	EW	vs	DLS	Comment
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	SHL
100.00	0.00	265.00	100.00	0.00	0.00	0.00	0.00	
200.00	0.00	265.00	200.00	0.00	0.00	0.00	0.00	
300.00	0.00	265.00	300.00	0.00	0.00	0.00	0.00	
400.00	0.00	265.00	400.00	0.00	0.00	0.00	0.00	
500.00	0.00	265.00	500.00	0.00	0.00	0.00	0.00	
600.00	0.00	265.00	600.00	0.00	0.00	0.00	0.00	
700.00	0.00	265.00	700.00	0.00	0.00	0.00	0.00	
800.00	0.00	265.00	800.00	0.00	0.00	0.00	0.00	
900.00	0.00	265.00	900.00	0.00	0.00	0.00	0.00	
945.00	0.00	265.00	945.00	0.00	0.00	0.00	0.00	Rustler
1000.00	0.00	265.00	1000.00	0.00	0.00	0.00	0.00	
1100.00	0.00	265.00	1100.00	0.00	0.00	0.00	0.00	
1200.00	0.00	265.00	1200.00	0.00	0.00	0.00	0.00	
1300.00	0.00	265.00	1300.00	0.00	0.00	0.00	0.00	C-IL
1355.00	0.00	265.00	1355.00	0.00	0.00	0.00	0.00	Salt
1400.00 1500.00	0.00	265.00 265.00	1400.00 1500.00	0.00	0.00	0.00	0.00	
1600.00	0.00	265.00	1600.00	0.00	0.00	0.00	0.00	
1700.00	0.00	265.00	1700.00	0.00	0.00	0.00	0.00	
1800.00	0.00	265.00	1800.00	0.00	0.00	0.00	0.00	
1900.00	0.00	265.00	1900.00	0.00	0.00	0.00	0.00	
2000.00	0.00	265.00	2000.00	0.00	0.00	0.00	0.00	Start Tangent
2100.00	2.00	265.00	2099.98	-0.15	-1.74	0.03	2.00	Start rangent
2200.00	4.00	265.00	2199.84	-0.61	-6.95	0.12	2.00	
2300.00	6.00	265.00	2299.45	-1.37	-15.63	0.27	2.00	
2400.00	8.00	265.00	2398.70	-2.43	-27.77	0.48	2.00	
2500.00	10.00	265.00	2497.47	-3.79	-43.36	0.76	2.00	Hold Tangent
2600.00	10.00	265.00	2595.95	-5.31	-60.66	1.06	0.00	-
2700.00	10.00	265.00	2694.43	-6.82	-77.95	1.36	0.00	
2800.00	10.00	265.00	2792.91	-8.33	-95.25	1.66	0.00	
2900.00	10.00	265.00	2891.39	-9.85	-112.55	1.96	0.00	
3000.00	10.00	265.00	2989.87	-11.36	-129.85	2.26	0.00	
3100.00	10.00	265.00	3088.35	-12.87	-147.15	2.56	0.00	
3200.00	10.00	265.00	3186.83	-14.39	-164.45	2.87	0.00	
3300.00	10.00	265.00	3285.31	-15.90	-181.75	3.17	0.00	
3400.00	10.00	265.00	3383.79	-17.41	-199.05	3.47	0.00	
3500.00	10.00	265.00	3482.27	-18.93	-216.34	3.77	0.00	
3600.00	10.00	265.00	3580.75	-20.44	-233.64	4.07	0.00	
3700.00	10.00	265.00	3679.23	-21.96	-250.94	4.37	0.00	
3800.00	10.00	265.00	3777.72	-23.47	-268.24	4.67	0.00	
3900.00	10.00	265.00	3876.20	-24.98	-285.54	4.97	0.00	
4000.00	10.00	265.00	3974.68	-26.50	-302.84	5.28	0.00	D (C)
4078.52	10.00	265.00	4052.00	-27.68	-316.42	5.51	0.00	Base of Salt
4100.00	10.00	265.00	4073.16	-28.01	-320.14	5.58	0.00	
4200.00	10.00	265.00	4171.64	-29.52 -31.04	-337.44	5.88	0.00	
4300.00	10.00	265.00	4270.12		-354.73	6.18	0.00	Dolawara
4389.24 4400.00	10.00	265.00	4358.00	-32.39	-370.17	6.45	0.00	Delaware
4500.00	10.00 10.00	265.00 265.00	4368.60 4467.08	-32.55 -34.06	-372.03 -389.33	6.48 6.78	0.00	
4600.00	10.00	265.00	4565.56	-34.06	-309.55 -406.63	7.08	0.00	
4700.00	10.00	265.00	4664.04	-37.09	-423.93	7.39	0.00	
4800.00	10.00	265.00	4762.52	-38.60	-441.23	7.69	0.00	
4900.00	10.00	265.00	4861.00	-40.12	-458.53	7.99	0.00	
5000.00	10.00	265.00	4959.48	-41.63	-475.82	8.29	0.00	
5100.00	10.00	265.00	5057.97	-43.14	-493.12	8.59	0.00	
5200.00	10.00	265.00	5156.45	-44.66	-510.42	8.89	0.00	
5300.00	10.00	265.00	5254.93	-46.17	-527.72	9.19	0.00	
5367.09	10.00	265.00	5321.00	-47.19	-539.33	9.40	0.00	Cherry Canyon
5400.00	10.00	265.00	5353.41	-47.69	-545.02	9.50	0.00	
5500.00	10.00	265.00	5451.89	-49.20	-562.32	9.80	0.00	
5600.00	10.00	265.00	5550.37	-50.71	-579.62	10.10	0.00	
5700.00	10.00	265.00	5648.85	-52.23	-596.92	10.40	0.00	
5800.00	10.00	265.00	5747.33	-53.74	-614.21	10.70	0.00	
5900.00	10.00	265.00	5845.81	-55.25	-631.51	11.00	0.00	
6000.00	10.00	265.00	5944.29	-56.77	-648.81	11.30	0.00	
6100.00	10.00	265.00	6042.77	-58.28	-666.11	11.61	0.00	
6200.00	10.00	265.00	6141.25	-59.79	-683.41	11.91	0.00	
6300.00	10.00	265.00	6239.73	-61.31	-700.71	12.21	0.00	
6400.00	10.00	265.00	6338.22	-62.82	-718.01	12.51	0.00	



Well: MORGAN 25-13 FED COM 837H

County: Lea
Wellbore: Permit Plan
Design: Permit Plan #1

Geodetic System: US State Plane 1983

Datum: North American Datum 1927 Ellipsoid: Clarke 1866

**Zone:** 3001 - NM East (NAD83)

	Design:	Permit Plan	n #1					<b>Zone:</b> 3001 - NM East (NAD83)
MD	INC	AZI	TVD	NS	EW	vs	DLS	
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
6500.00	10.00	265.00	6436.70	-64.33	-735.31	12.81	0.00	
6600.00	10.00	265.00	6535.18	-65.85	-752.60	13.11	0.00	
6700.00	10.00	265.00	6633.66	-67.36	-769.90	13.41	0.00	
6800.00	10.00	265.00	6732.14	-68.87	-787.20	13.71	0.00	
6822.20	10.00	265.00	6754.00	-69.21	-791.04	13.78	0.00	Brushy Canyon
6900.00	10.00	265.00	6830.62	-70.39	-804.50	14.02	0.00	bidsity Carlyon
7000.00	10.00	265.00	6929.10	-71.90	-821.80	14.32	0.00	
7100.00	10.00	265.00	7027.58	-73.41	-839.10	14.62	0.00	
7200.00	10.00	265.00	7126.06	-74.93	-856.40	14.92	0.00	
7300.00	10.00	265.00	7224.54	-76.44	-873.70	15.22	0.00	
7400.00	10.00	265.00	7323.02	-77.96	-890.99	15.52	0.00	
7500.00	10.00	265.00	7421.50	-79.47	-908.29	15.82	0.00	
7600.00	10.00	265.00	7519.99	-80.98	-925.59	16.13	0.00	
7700.00	10.00	265.00	7618.47	-82.50	-942.89	16.43	0.00	
7800.00	10.00	265.00	7716.95	-84.01	-960.19	16.73	0.00	
7900.00	10.00	265.00	7815.43	-85.52	-977.49	17.03	0.00	
8000.00	10.00	265.00	7913.91	-87.04	-994.79	17.33	0.00	
8100.00	10.00	265.00	8012.39	-88.55	-1012.09	17.63	0.00	
8200.00	10.00	265.00	8110.87	-90.06	-1029.38	17.93	0.00	
8300.00	10.00	265.00	8209.35	-91.58	-1046.68	18.24	0.00	
8400.00	10.00	265.00	8307.83	-93.09	-1063.98	18.54	0.00	
8500.00	10.00	265.00	8406.31	-94.60	-1081.28	18.84	0.00	
8600.00	10.00	265.00	8504.79	-96.12	-1098.58	19.14	0.00	
8700.00	10.00	265.00	8603.27	-97.63	-1115.88	19.44	0.00	
8800.00	10.00	265.00	8701.75	-99.14	-1133.18	19.74	0.00	
8900.00	10.00	265.00	8800.24	-100.66	-1150.47	20.04	0.00	
9000.00	10.00	265.00	8898.72	-102.17	-1167.77	20.34	0.00	
9100.00	10.00	265.00	8997.20	-103.68	-1185.07	20.65	0.00	
9200.00	10.00	265.00	9095.68	-105.20	-1202.37	20.95	0.00	
9300.00	10.00	265.00	9194.16	-105.20	-1219.67	21.25	0.00	
9400.00			9292.64	-108.23				
	10.00	265.00			-1236.97	21.55	0.00	Dana Carina 1st
9449.11	10.00	265.00	9341.00	-108.97	-1245.46	21.70	0.00	Bone Spring 1st
9500.00	10.00	265.00	9391.12	-109.74	-1254.27	21.85	0.00	
9600.00	10.00	265.00	9489.60	-111.25	-1271.57	22.15	0.00	
9606.97	10.00	265.00	9496.46	-111.35	-1272.77	22.17	0.00	Drop to Vertical
9700.00	8.14	265.00	9588.33	-112.63	-1287.38	22.43	2.00	
9800.00	6.14	265.00	9687.55	-113.71	-1299.76	22.65	2.00	
9900.00	4.14	265.00	9787.14	-114.50	-1308.69	22.80	2.00	
10000.00	2.14	265.00	9886.98	-114.97	-1314.14	22.90	2.00	
10089.04	0.36	265.00	9976.00	-115.14	-1316.07	22.93	2.00	Bone Spring 2nd
10100.00	0.14	265.00	9986.96	-115.15	-1316.12	22.93	2.00	
10106.97	0.00	265.00	9993.93	-115.15	-1316.13	22.93	2.00	Hold Vertical
10200.00	0.00	359.80	10086.96	-115.15	-1316.13	22.93	0.00	
10300.00	0.00	359.80	10186.96	-115.15	-1316.13	22.93	0.00	
10400.00	0.00	359.80	10286.96	-115.15	-1316.13	22.93	0.00	
10500.00	0.00	359.80	10386.96	-115.15	-1316.13	22.93	0.00	
10534.04	0.00	359.80	10421.00	-115.15	-1316.13	22.93	0.00	Bone Spring 3rd
10600.00	0.00	359.80	10486.96	-115.15	-1316.13	22.93	0.00	. 5
10700.00	0.00	359.80	10586.96	-115.15	-1316.13	22.93	0.00	
10800.00	0.00	359.80	10686.96	-115.15	-1316.13	22.93	0.00	
10900.00	0.00	359.80	10786.96	-115.15	-1316.13	22.93	0.00	
11000.00	0.00	359.80	10886.96	-115.15	-1316.13	22.93	0.00	
11100.00	0.00	359.80	10986.96	-115.15	-1316.13	22.93	0.00	
11200.00	0.00	359.80	11086.96	-115.15	-1316.13	22.93	0.00	
11300.00	0.00	359.80	11186.96	-115.15	-1316.13	22.93	0.00	
11400.00	0.00	359.80	11286.96	-115.15	-1316.13	22.93	0.00	
11500.00	0.00	359.80	11386.96	-115.15	-1316.13	22.93	0.00	
11600.00	0.00	359.80	11486.96	-115.15	-1316.13	22.93	0.00	
11700.00	0.00	359.80	11586.96	-115.15	-1316.13	22.93	0.00	
11758.04	0.00	359.80	11645.00	-115.15	-1316.13	22.93	0.00	Wolfcamp / Point of Penetration
11800.00	0.00	359.80	11686.96	-115.15	-1316.13	22.93	0.00	
11900.00	0.00	359.80	11786.96	-115.15	-1316.13	22.93	0.00	
12000.00	0.00	359.80	11886.96	-115.15	-1316.13	22.93	0.00	
12100.00	0.00	359.80	11986.96	-115.15	-1316.13	22.93	0.00	
12200.00	0.00	359.80	12086.96	-115.15	-1316.13	22.93	0.00	
12300.00	0.00	359.80	12186.96	-115.15	-1316.13	22.93	0.00	
12324.14	0.00	359.80	12211.10	-115.15	-1316.13	22.93	0.00	KOP
12400.00	7.59	359.80	12286.74	-110.13	-1316.15	27.92	10.00	
	17.59	359.80	12384.21	-88.37	-1316.22	49.58	10.00	
12500.00								
12500.00 12600.00	27.59	359.80	12476.42	-50.01	-1316.36	87.74	10.00	



Well: MORGAN 25-13 FED COM 837H

County: Lea
Wellbore: Permit Plan
Design: Permit Plan #1

Geodetic System: US State Plane 1983

Datum: North American Datum 1927 Ellipsoid: Clarke 1866

Zone: 3001 - NM East (NAD83)

	Design:	Permit Plan	n #1		Zone: 3001 - NM East (NAD				
MD	INC	AZI	TVD	NS	EW	vs	DLS		
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment	
2700.00	37.59	359.80	12560.58	3.78	-1316.55	141.25	10.00		
2800.00	47.59	359.80	12634.11	71.36	-1316.78	208.49	10.00		
2900.00	57.59	359.80	12694.79	150.69	-1317.06	287.41	10.00		
3000.00	67.59	359.80	12740.77	239.34	-1317.37	375.62	10.00		
3100.00	77.59	359.80	12770.66	334.64	-1317.70	470.42	10.00		
3200.00	87.59	359.80	12783.55	433.68	-1318.05	568.96	10.00		
3232.16	90.80	359.80	12784.00	465.83	-1318.16	600.94	10.00	Landing Point	
3300.00	90.80	359.80	12783.05	533.66	-1318.39	668.43	0.00		
3400.00	90.80	359.80	12781.65	633.65	-1318.74	767.91	0.00		
3500.00	90.80	359.80	12780.25	733.64	-1319.09	867.39	0.00		
3600.00	90.80	359.80	12778.85	833.63	-1319.44	966.87	0.00		
3700.00	90.80	359.80	12777.45	933.62	-1319.79	1066.35	0.00		
3800.00	90.80	359.80	12776.05	1033.61	-1320.14	1165.83	0.00		
3900.00	90.80	359.80	12774.65	1133.60	-1320.49	1265.31	0.00		
4000.00	90.80	359.80	12773.25	1233.59	-1320.84	1364.79	0.00		
4100.00	90.80	359.80	12771.86	1333.58	-1321.19	1464.27	0.00		
4200.00	90.80	359.80	12770.46	1433.57	-1321.54	1563.75	0.00		
4300.00	90.80	359.80	12769.06	1533.56	-1321.89	1663.23	0.00		
4400.00	90.80	359.80	12767.66	1633.55	-1322.24	1762.70	0.00		
4500.00 4600.00	90.80	359.80 359.80	12766.26	1733.54	-1322.59 -1322.94	1862.18 1961.66	0.00		
4600.00 4700.00	90.80 90.80	359.80 359.80	12764.86 12763.46	1833.53 1933.52	-1322.94 -1323.29	2061.14	0.00		
4800.00	90.80	359.80	12763.46	2033.52	-1323.29	2160.62	0.00		
4900.00	90.80	359.80	12762.06	2133.50	-1323.04	2260.10	0.00		
5000.00	90.80	359.80	12759.26	2233.49	-1323.99	2359.58	0.00		
5100.00	90.80	359.80	12757.86	2333.48	-1324.54	2459.06	0.00		
5200.00	90.80	359.80	12756.46	2433.46	-1325.04	2558.54	0.00		
5300.00	90.80	359.80	12755.06	2533.45	-1325.39	2658.02	0.00		
5400.00	90.80	359.80	12753.66	2633.44	-1325.74	2757.50	0.00		
5500.00	90.80	359.80	12752.26	2733.43	-1326.09	2856.98	0.00		
5600.00	90.80	359.80	12750.86	2833.42	-1326.43	2956.46	0.00		
5700.00	90.80	359.80	12749.46	2933.41	-1326.78	3055.94	0.00		
5800.00	90.80	359.80	12748.07	3033.40	-1327.13	3155.41	0.00		
5900.00	90.80	359.80	12746.67	3133.39	-1327.48	3254.89	0.00		
6000.00	90.80	359.80	12745.27	3233.38	-1327.83	3354.37	0.00		
6100.00	90.80	359.80	12743.87	3333.37	-1328.18	3453.85	0.00		
6200.00	90.80	359.80	12742.47	3433.36	-1328.53	3553.33	0.00		
6300.00	90.80	359.80	12741.07	3533.35	-1328.88	3652.81	0.00		
6400.00	90.80	359.80	12739.67	3633.34	-1329.23	3752.29	0.00		
6500.00	90.80	359.80	12738.27	3733.33	-1329.58	3851.77	0.00		
6600.00	90.80	359.80	12736.87	3833.32	-1329.93	3951.25	0.00		
6700.00	90.80	359.80	12735.47	3933.31	-1330.28	4050.73	0.00		
6800.00	90.80	359.80	12734.07	4033.30	-1330.63	4150.21	0.00		
6900.00	90.80	359.80	12732.67	4133.29	-1330.98	4249.69	0.00		
7000.00	90.80	359.80	12731.27	4233.28	-1331.33	4349.17	0.00		
7100.00	90.80	359.80	12729.87	4333.27	-1331.68	4448.65	0.00		
7200.00	90.80	359.80	12728.47	4433.26	-1332.03	4548.13	0.00		
7300.00 7400.00	90.80	359.80 359.80	12727.07	4533.25 4633.24	-1332.38 -1332.73	4647.60 4747.08	0.00		
7500.00	90.80 90.80	359.80	12725.67 12724.27	4633.24 4733.23	-1332.73	4846.56	0.00		
7600.00	90.80	359.80	12724.27	4833.22	-1333.43	4946.04	0.00		
7700.00	90.80	359.80	12722.66	4933.20	-1333.78	5045.52	0.00		
7800.00	90.80	359.80	12721.48	5033.19	-1333.76	5145.00	0.00		
7900.00	90.80	359.80	12720.08	5133.18	-1334.12	5244.48	0.00		
8000.00	90.80	359.80	12717.28	5233.17	-1334.82	5343.96	0.00		
8100.00	90.80	359.80	12715.88	5333.16	-1335.17	5443.44	0.00		
8200.00	90.80	359.80	12714.48	5433.15	-1335.52	5542.92	0.00		
8300.00	90.80	359.80	12713.08	5533.14	-1335.87	5642.40	0.00		
8400.00	90.80	359.80	12711.68	5633.13	-1336.22	5741.88	0.00		
8500.00	90.80	359.80	12710.28	5733.12	-1336.57	5841.36	0.00		
8600.00	90.80	359.80	12708.88	5833.11	-1336.92	5940.84	0.00		
8700.00	90.80	359.80	12707.48	5933.10	-1337.27	6040.32	0.00		
00.0088	90.80	359.80	12706.08	6033.09	-1337.62	6139.79	0.00		
0000 00	90.80	359.80	12704.68	6133.08	-1337.97	6239.27	0.00		
8900.00		359.80	12703.28	6233.07	-1338.32	6338.75	0.00		
9000.00	90.80	555.00		c222.0c	-1338.67	6438.23	0.00		
	90.80 90.80	359.80	12701.88	6333.06	1550.01				
9000.00 9100.00 9200.00	90.80 90.80		12700.48	6433.05	-1339.02	6537.71	0.00		
9000.00 9100.00 9200.00 9300.00	90.80 90.80 90.80	359.80 359.80 359.80	12700.48 12699.09	6433.05 6533.04	-1339.02 -1339.37	6537.71 6637.19	0.00		
9000.00 9100.00 9200.00	90.80 90.80	359.80 359.80	12700.48	6433.05	-1339.02	6537.71			



Well: MORGAN 25-13 FED COM 837H

County: Lea Wellbore: Permit Plan Design: Permit Plan #1 Geodetic System: US State Plane 1983

**Datum:** North American Datum 1927 **Ellipsoid:** Clarke 1866

**Zone:** 3001 - NM East (NAD83)

MD	INC	AZI	TVD	NS	EW	VS	DLS	Comment
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	Comment
19600.00	90.80	359.80	12694.89	6833.01	-1340.42	6935.63	0.00	
19700.00	90.80	359.80	12693.49	6933.00	-1340.77	7035.11	0.00	
19800.00	90.80	359.80	12692.09	7032.99	-1341.12	7134.59	0.00	
19900.00	90.80	359.80	12690.69	7132.98	-1341.47	7234.07	0.00	
20000.00	90.80	359.80	12689.29	7232.97	-1341.82	7333.55	0.00	
20100.00	90.80	359.80	12687.89	7332.95	-1342.16	7433.03	0.00	
20200.00 20300.00	90.80 90.80	359.80 359.80	12686.49 12685.09	7432.94 7532.93	-1342.51 -1342.86	7532.51 7631.98	0.00	
20400.00	90.80	359.80	12683.69	7632.92	-1342.00	7731.46	0.00	
20500.00	90.80	359.80	12682.29	7732.91	-1343.56	7830.94	0.00	
20600.00	90.80	359.80	12680.89	7832.90	-1343.91	7930.42	0.00	
20700.00	90.80	359.80	12679.49	7932.89	-1344.26	8029.90	0.00	
20800.00	90.80	359.80	12678.09	8032.88	-1344.61	8129.38	0.00	
20900.00	90.80	359.80	12676.69	8132.87	-1344.96	8228.86	0.00	
21000.00	90.80	359.80	12675.29	8232.86	-1345.31	8328.34	0.00	
21100.00	90.80	359.80	12673.90	8332.85	-1345.66	8427.82	0.00	
21200.00	90.80	359.80	12672.50	8432.84	-1346.01	8527.30	0.00	
21300.00	90.80	359.80	12671.10	8532.83	-1346.36	8626.78	0.00	
21400.00	90.80	359.80	12669.70	8632.82	-1346.71	8726.26	0.00	
21500.00	90.80	359.80	12668.30	8732.81	-1347.06	8825.74	0.00	
21600.00	90.80	359.80	12666.90	8832.80	-1347.41	8925.22	0.00	
21700.00	90.80	359.80	12665.50	8932.79	-1347.76	9024.69	0.00	
21800.00	90.80	359.80	12664.10	9032.78	-1348.11	9124.17	0.00	
21900.00	90.80	359.80	12662.70	9132.77	-1348.46	9223.65	0.00	
22000.00 22100.00	90.80	359.80 359.80	12661.30	9232.76	-1348.81	9323.13	0.00	
22200.00	90.80 90.80	359.80	12659.90 12658.50	9332.75 9432.74	-1349.16 -1349.51	9422.61 9522.09	0.00	
22300.00	90.80	359.80	12657.10	9532.73	-1349.86	9621.57	0.00	
22400.00	90.80	359.80	12655.70	9632.72	-1350.20	9721.05	0.00	
22500.00	90.80	359.80	12654.30	9732.71	-1350.55	9820.53	0.00	
22600.00	90.80	359.80	12652.90	9832.69	-1350.90	9920.01	0.00	
22700.00	90.80	359.80	12651.50	9932.68	-1351.25	10019.49	0.00	
22800.00	90.80	359.80	12650.10	10032.67	-1351.60	10118.97	0.00	
22900.00	90.80	359.80	12648.71	10132.66	-1351.95	10218.45	0.00	
23000.00	90.80	359.80	12647.31	10232.65	-1352.30	10317.93	0.00	
23100.00	90.80	359.80	12645.91	10332.64	-1352.65	10417.41	0.00	
23200.00	90.80	359.80	12644.51	10432.63	-1353.00	10516.88	0.00	
23300.00	90.80	359.80	12643.11	10532.62	-1353.35	10616.36	0.00	
23400.00	90.80	359.80	12641.71	10632.61	-1353.70	10715.84	0.00	
23500.00	90.80	359.80	12640.31	10732.60	-1354.05	10815.32	0.00	
23600.00 23700.00	90.80 90.80	359.80	12638.91	10832.59	-1354.40 -1354.75	10914.80 11014.28	0.00	
23800.00	90.80	359.80 359.80	12637.51 12636.11	10932.58 11032.57	-1355.10	11113.76	0.00	
23900.00	90.80	359.80	12634.71	11132.56	-1355.45	11213.24	0.00	
24000.00	90.80	359.80	12633.31	11232.55	-1355.80	11312.72	0.00	
24100.00	90.80	359.80		11332.54	-1356.15	11412.20	0.00	
24200.00	90.80	359.80	12630.51	11432.53	-1356.50	11511.68	0.00	
24300.00	90.80	359.80	12629.11	11532.52	-1356.85	11611.16	0.00	
24400.00	90.80	359.80	12627.71	11632.51	-1357.20	11710.64	0.00	
24500.00	90.80	359.80	12626.31	11732.50		11810.12	0.00	
24600.00	90.80	359.80	12624.92	11832.49	-1357.90	11909.60	0.00	
24700.00	90.80	359.80	12623.52	11932.48	-1358.24	12009.07	0.00	
24800.00	90.80	359.80	12622.12	12032.47	-1358.59	12108.55	0.00	
24900.00	90.80	359.80		12132.46		12208.03	0.00	
25000.00	90.80	359.80		12232.45		12307.51	0.00	
25100.00	90.80	359.80		12332.43		12406.99	0.00	
25200.00	90.80	359.80		12432.42		12506.47	0.00	
25300.00	90.80	359.80		12532.41		12605.95	0.00	
25400.00	90.80	359.80		12632.40		12705.43 12804.91	0.00	
25500.00 25600.00	90.80	359.80		12732.39			0.00	
	90.80 90.80	359.80 359.80		12832.38 12888.43		12904.39 12960.15	0.00	exit
25656.05		359.80		12932.37		13003.87	0.00	CAIL
25656.05 25700.00	90.80						0.00	
25656.05 25700.00 25736.05	90.80 90.80	359.80		12968.42		13039.72	0.00	BHL

#### MORGAN 25-13 FED COM 837H

#### 1. Geologic Formations

TVD of target	12610	Pilot hole depth	N/A
MD at TD:	25673	Deepest expected fresh water	

#### Basin

Dasin			
	Depth	Water/Mineral	
Formation	(TVD)	Bearing/Target	Hazards*
	from KB	Zone?	
Rustler	945		
Salt	1355		
Base of Salt	4052		
Delaware	4358		
Cherry Canyon	5321		
Brushy Canyon	6754		
Bone Spring 1st	9341		
Bone Spring 2nd	9976		
Bone Spring 3rd	10421		
Wolfcamp	11645		

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program (Primary Design)

		Wt			Casing	Interval	Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)
13 1/2	9 5/8	40	J-55	BTC	0	970	0	970
8 3/4	7 5/8	29.7	P110HP	TALON SFC	0	11921	0	11921
6 3/4	5 1/2	20	P110HP	TALON RD	0	25673	0	12610

[•]All casing strings will be tested in accordance with 43 CFR 3172.

#### 3. Cementing Program (Primary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures

Casing	# Sks	тос	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	512	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	375	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int 1	475	6764	13.2	1.44	Tail: Class H / C + additives
Production	61	10222	9	3.27	Lead: Class H /C + additives
Production	858	12222	13.2	1.44	Tail: Class H / C + additives

Devon Energy requests to offline cement on intermediate strings that are set in formations shallower than the Wolfcamp. Prior to commencing offline cementing operations, the well will be monitored for any abnormal pressures and confirmed to be static. A dual manifold system (equipped with chokes) for the returns will also be utilized as a redundancy. All equipment used for offline cementing will have a minimum 5M rating to match intermediate sections' 5M BOPE requirements

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

2. Casing Program (Secondary Design)

		Wt			Casing	Casing Interval		Casing Interval	
Hole Size	Csg. Size	(PPF)	Grade	Conn	From (MD)	To (MD)	From (TVD)	To (TVD)	
14 3/4	10 3/4	45 1/2	J-55	ВТС	0	970	0	970	
9 7/8	8 5/8	32	P110	Sprint FJ	0	11921	0	11921	
7 7/8	5 1/2	20	P110	DWC / C-IS+	0	25673	0	12610	

[•]All casing strings will be tested in accordance with 43 CFR 3172. Must have table for contingency casing.

#### 3. Cementing Program (Secondary Design)

Assuming no returns are established while drilling, Devon requests to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. The final cement top will be verified by Echo-meter. Devon will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program. Devon will report to the BLM the volume of fluid (limited to 1 bbls) used to flush intermediate casing valves following backside cementing procedures.

Casing	# Sks	TOC	Wt. ppg	Yld (ft3/sack)	Slurry Description
Surface	586	Surf	13.2	1.44	Lead: Class C Cement + additives
Int 1	474	Surf	13.0	2.3	2nd State: Bradenhead Squeeze - Lead: Class C Cement + additives
Int I	597	6764	13.2	1.44	Tail: Class H / C + additives
Production	117	10222	9	3.27	Lead: Class H /C + additives
Froduction	1780	12222	13.2	1.44	Tail: Class H / C + additives

Casing String	% Excess
Surface	50%
Intermediate 1	30%
Prod	10%

**4. Pressure Control Equipment (Three String Design)** 

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Ty	ype	<b>√</b>	Tested to:
				nular	X	50% of rated working pressure
Int 1	13-5/8"	5M	Blind	d Ram	X	
IIIL I	13-3/6	JIVI	Pipe	Ram		5M
			Doub	le Ram	X	5M
			Other*			
	13-5/8"		Annular (5M)		X	100% of rated working pressure
Due due et i e e		101/1	Blind Ram		X	10M
Production		10M	Pipe Ram			
			Double Ram		X	
			Other*			
			Annul	ar (5M)		
	Blind Ram					
			Pipe Ram			
			Doub	le Ram		
			Other*			
N A variance is requested for	the use of a	diverter or	the surface	casing. See	attached for s	chematic.
Y A variance is requested to 1	A variance is requested to run a 5 M annular on a 10M system					

5. Mud Program (Three String Design)

Section	Туре	Weight (ppg)
Surface	FW Gel	8.5-9
Intermediate	DBE / Cut Brine	10-10.5
Production	OBM	10-10.5

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring

6. Logging and Testing Procedures

Logging, C	Logging, Coring and Testing				
	Will run GR/CNL from TD to surface (horizontal well - vertical portion of hole). Stated logs run will be in the				
X	Completion Report and sbumitted to the BLM.				
	No logs are planned based on well control or offset log information.				
	Drill stem test? If yes, explain.				
	Coring? If yes, explain.				

Additional l	ogs planned	Interval	
	Resistivity	Int. shoe to KOP	
	Density	Int. shoe to KOP	
X	CBL	Production casing	
X	Mud log	Intermediate shoe to TD	
	PEX		

7. Drilling Conditions

Condition	Specfiy what type and where?
BH pressure at deepest TVD	6885
Abnormal temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogren Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of 43 CFR 3176. If Hydrogen Sulfide is encountered measured values and formations will be provided to the BLM.

measured v	measured values and formations will be provided to the BLM.		
N	H2S is present		
Y	H2S plan attached.		

#### MORGAN 25-13 FED COM 837H

#### 8. Other facets of operation

Is this a walking operation? Potentially

- 1 If operator elects, drilling rig will batch drill the surface holes and run/cement surface casing; walking the rig to next wells on the pad.
- 2 The drilling rig will then batch drill the intermediate sections and run/cement intermediate casing; the wellbore will be isolated with a blind flange and pressure gauge installed for monitoring the well before walking to the next well.
- 3 The drilling rig will then batch drill the production hole sections on the wells with OBM, run/cement production casing, and install TA caps or tubing heads for completions.

NOTE: During batch operations the drilling rig will be moved from well to well however, it will not be removed from the pad until all wells have production casing run/cemented.

#### Will be pre-setting casing? Potentially

- 1 Spudder rig will move in and batch drill surface hole.
  - a. Rig will utilize fresh water based mud to drill surface hole to TD. Solids control will be handled entirely on a closed loop basis.,
- 2 After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (43 CFR 3172, all COAs and NMOCD regulations).
- 3  The wellhead will be installed and tested once the surface casing is cut off and the WOC time has been reached.
- 4 A blind flange with the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with a pressure gauge installed on the wellhead.
- 5 Spudder rig operations is expected to take 4-5 days per well on a multi-well pa.
- 6 The NMOCD will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 7 Drilling operations will be performed with drilling rig. A that time an approved BOP stack will be nippled up and tested on the wellhead before drilling operations commences on each well.
  - a. The NMOCD will be contacted / notified 24 hours before the drilling rig moves back on to the pad with the pre-set surface casing.

Attachment	ts
X	Directional Plan
	Other, describe

<u>C-10</u>	02		Energy,	Minera	State of ls & Natura	New Mexico al Resources Depa	rtment		Rev	vised July, 2024
Submit E	lectronically		OIL	CON	NSERVAT	TION DIVISI	ON			
Via OCD	Permitting							Submittal	✓ Initial Submittal	
								Type:	☐ Amended Repor	t
							☐ As Drilled			
						ION INFORMATIO	N			
	umber		Pool Cod			Pool Name	CE. WOLL	ECAMD (		
	15-55871 rty Code		Property	220 Name		PURPLE SA	GE; WOLI	FCAMP (	(GAS)   Well Number	
_	v				MORGAN	25-13 FED COM			837H	
OGRID	No. 6137		Operator		I PNPDCV D	RODUCTION COMPA	NNV I D		Ground Level	Elevation
G			 						3328.9'	
Surfac	e Owner:	□State □	ree Lirii	oai ⊔ree	deral	Mineral Owner:	⊔State	⊔ree ⊔	Tribal   Federal	
					Sur	face Location				
UL	Section	Township	Range	Lot	Ft. from N,	/S Ft. from E/W	Latitude		Longitude	County
G	25	25-S	31-E		2433' N	1680'E	32.101	855	103.728479	EDDY
					Botto	m Hole Location				
UL	Section	Township	Range	Lot	Ft. from N	/S Ft. from E/W	Latitude		Longitude	County
C	13	25-S	31-E		20' N	2310' W	32.137	524	103.732644	EDDY
Dedicate	ed Acres	Infill or Def	ining Well	Defining	Well API Over	clapping Spacing Uni	t (Y/N)	Consolid	lation Code	
800.0	0	INFILL		30-015-	55637					
Order 1	Numbers	PENDING 1	NSL			setbacks are under	Common	Ownersh	nip: □Yes □No	
			_			f Point (KOP)				
UL	Section	Township	Range	Lot	Ft. from N	/S Ft. from E/W	Latitude		Longitude	County
F	25	25-S	31-E		2538' N	2311' W	32.1015		-103.7328	EDDY
	1	T				ake Point (FTP)	ı			
UL	Section	Township	Range	Lot	Ft. from N,	. '	Latitude		Longitude	County
F	25	25-S	31-E		2538' N	2310' W	558	103.732734	EDDY	
		1				ake Point (LTP)				
UL	Section	Township	Range	Lot	Ft. from N,		Latitude		Longitude	County
C	13	25-S	31-E		100' N	2310' W	32.137	304	103.732644	EDDY
					Spacing	Unit Type Horizon	tal Verti	cal	Ground Floor Ele	vation:
					1					
1		FICATIONS				SURVEYOR CERTIFIC	ATIONS			
					omplete to the best onal well, that this	I hereby certify that the we				
organizat	ion either ow	ns a working inte	rest or unlease	d mineral in	terest in the land	of actual surveys made by correct to the best of my be		upervision,		
location p	oursuant to a	bottom hole loc contract with an o	owner of a wor	king interest	t or unleased	Í			RT R. C	DEHOLOS
	nterest, or to a e entered by t		ng agreement o	or a compuls	ory pooling order				N MEX	10/2
	-				1				A FM	(%\"\
consent o	f at least one	lessee or owner	of a working in	terest or unl					(23261	
					part of the well's ng order from the				PR DOCL	1 / 2 /
division			•						SYNDE	V. /
Simo	y XY.	Brown	Date	2025		Signature and Seal	of Profes	ssional S	Surveyor	<u> </u>
Signa	yure		Date			biginature and Sear	. or rrore:	ssional i	Surveyor / ONAL	/
_	A. Brown	l								
Printe	ed Name					Certificate Number	Date of	Survey		
	brown@d Address	vn.com				23261	10/20	24		
Linaii	.1441 033					~5~01	10, 20	- 1		

#### ACREAGE DEDICATION PLATS

This grid represents a standard section. You may superimpose a non-standard section, or larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is closest to any outer boundary of the

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.

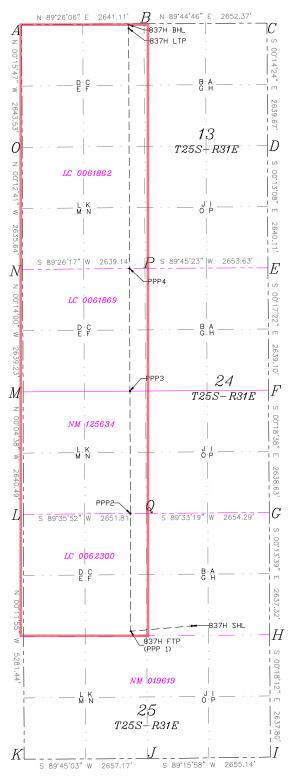
SURFACE HOLE LOCATION
GEODETIC COORDINATES NAD 83
NMSP EAST SURFACE LOCATION
2433' FNL 1680' FEL SECTION 25
EL: 329.5'
N:401316.80/E:728628.98
LAT:32.101855/LON:103.728479 FIRST TAKE POINT FNL 2310' FWL SECTION 25 N:401201.46/E:727312.09 LAT:32.101558/LDN:103.732734 LAST TAKE POINT 100' FNL 2310' FWL SECTION 13 N:414205.22/E:727267.55 LAT:32.137304/LDN:103.732644 BOTTOM HOLE LOCATION 20' FNL 2310' FWL SECTION 13 N:414285.22/E:727267.18 LAT:32.137524/LDN:103.732644 <u>PPP 2</u> FNL 2310' FWL SECTION 25 N:386656.07/E:729055.59

LAT:32.061549/LDN:103.727368 2641' FSL 2305' FWL SECTION 24 N:388569.38/E:729049.04

LAT:32.066808/LDN:103.727354 FSL 2306' FWL SECTION 13

N:390486.38/E:729042.47 LAT:32.072078/LDN:103.727341

A= N:414282.44 E:724957.17 B= N:414308.48 E:727598.15 C= N:414320.23 E:730250.50 D= N:411680.59 E:730261.56 E= N:409040.49 E:730271.65 F= N:406401.43 E:730284.99 G= N:403762.83 E:730299.28 H= N:401125.54 E:730309.76 I= N:398487.77 E:730323.72 J= N:398453.76 E:727668.80 K= N:398442.20 E:725011.65 L= N:403723.61 F:724993.33 M= N:406364.11 E:724989.78 E:724979.03 N= N:409003.32 □= N:411638.94 E:724969.31 E:727618.04 P= N:409029.21 Q= N:403742.23 E:727645.07



#### Morgan 25-13 Fed Com 837H

9 5/8	surf	face csg in a	13 1/2 i	nch hole.		Design	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A" <b>"B"</b>	40.00		j 55	btc btc	16.24	5.67	0.61	970 <b>0</b>	9	1.02	10.70	38,80 <b>0</b>
		g mud, 30min Sfc Csg Test		Tail Cmt	does not	circ to sfc.	Totals:	970				38,80
		nimum Required Cem										
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Di
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-C
13 1/2	0.4887	512	737	474	56	9.00	3880	5M				1.44
urst Frac Grac	lient(s) for Segmer	nt(s) A, B = , b All > 0.	.70, OK.		Site plat (pip	e racks S or E) a	is per O.O.1.II	I.D.4.i. not fo				
7 5/8	casin	ng inside the	9 5/8			Design	Factors			Int 1		
Segment	#/ft	Grade	,	Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigl
"A"	29.70	2.000	p 110	talon sfc	2.59	1.12	1.56	11,921	2	2.62	1.87	354,05
"B"								Ô				0
	w/8.4#/	g mud, 30min Sfc Csg Test	t psig: 2,623				Totals:	11,921				354,05
				ed to achieve a top of	0	ft from su	rface or a	970				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Di
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-C
8 3/4	0.1005	475	684	1206	-43	10.50	4104	5M				0.43
D V Tool(s):			6754				sum of sx	Σ CuFt				Σ%exce
(-)-												
, ,	t yld > 1.35	32	26				850	1547				28
Class 'C' tail cm			26					1547				28
Tail cmt 5 1/2	casin	g inside the	7 5/8	····		Design Fac	ctors			Prod 1		
Tail cmt 5 1/2 Segment	casin #/ft		7 5/8	Coupling	Joint	Collapse	ctors Burst	Length	B@s	a-B	a-C	Weigl
Tail cmt 5 1/2 Segment "A"	casin	g inside the		Coupling talon rd	Joint 2.89		ctors	<b>Length</b> 25,673	<b>B@s</b> 2			<b>Weig</b> l 513,46
Tail cmt 5 1/2 Segment "A" "B"	casin #/ft	g inside the	7 5/8	, ,		Collapse	ctors Burst	Length 25,673		a-B		Weigl 513,46
Tail cmt 5 1/2 Segment "A" "B" "C"	casin #/ft	g inside the	7 5/8	, ,		Collapse	ctors Burst	Length 25,673 0		a-B		Weigl 513,46 0
Tail cmt 5 1/2 Segment "A" "B"	casin #/ft 20.00	g inside the Grade	<b>75/8</b> p 110	, ,		Collapse	ctors Burst 2.09	Length 25,673 0 0		a-B		Weigl 513,46 0 0
Tail cmt 5 1/2 Segment "A" "B" "C"	casin #/ft 20.00	ng inside the Grade	<b>7 5/8</b> p 110 t psig: 2,774	talon rd	2.89	Collapse 1.91	Ctors Burst 2.09	Length 25,673 0 0 0 25,673		a-B	3.20	Weigl 513,46 0 0 0 513,46
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	casin #/ft 20.00	ng inside the Grade (g mud, 30min Sfc Csg Test The cement	7 5/8 p 110 t psig: 2,774 volume(s) are intende	talon rd	2.89	Collapse 1.91  ft from su	Ctors Burst 2.09  Totals:	Length 25,673 0 0 0 25,673 200		a-B	3.20	Weigl 513,44 0 0 513,44 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	casin #/ft 20.00 w/8.4#//	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement 1 Stage	7 5/8 p 110 t psig: 2,774 volume(s) are intended 1 Stage	talon rd ed to achieve a top of	2.89 11721 1 Stage	ft from su Drilling	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 25,673 200 Req'd		a-B	3.20	Weigl 513,46 0 0 0 513,46 overlap.
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size	casin #/ft 20.00 w/8.4#// Annular Volume	ng inside the Grade (g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	7 5/8 p 110 t psig: 2,774 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.09  Totals:	Length 25,673 0 0 0 25,673 200		a-B	3.20	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt 51/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835	ng inside the Grade 'g mud, 30min Sfc Csg Test The cement 1 Stage	7 5/8 p 110 t psig: 2,774 volume(s) are intended 1 Stage	talon rd ed to achieve a top of	2.89 11721 1 Stage	ft from su Drilling	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 25,673 200 Req'd		a-B	3.20	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt 51/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835	ng inside the Grade (g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	7 5/8 p 110 t psig: 2,774 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 25,673 200 Req'd		a-B	3.20	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt 51/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835	ng inside the Grade (g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	7 5/8 p 110 t psig: 2,774 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 25,673 200 Req'd		a-B	3.20	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 class 'C' tail cm	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835	ng inside the Grade (g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	7 5/8 p 110 t psig: 2,774 volume(s) are intende 1 Stage CuFt Cmt	talon rd  ed to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Totals: rface or a Calc MASP	Length 25,673 0 0 25,673 200 Req'd	2	a-B	3.20	Weigl 513,46 0 0 0 513,46
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 llass 'C' tail cm	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835	ng inside the Grade (g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435	ed to achieve a top of Min Cu Ft 1166	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	<b>a-B</b> 3.50	3.20	Weigl 513,46 0 0 513,46 overlap. Min Di Hole-Cl 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 lass 'C' tail cm	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835 tyld > 1.35	ng inside the Grade Grade I'g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 919	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435	talon rd  ed to achieve a top of  Min  Cu Ft	2.89  11721 1 Stage % Excess 23	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 25,673 200 Req'd	2	a-B 3.50	3.20	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 class 'C' tail cm  #N/A 0 Segment	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835 tyld > 1.35	ng inside the Grade Grade I'g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 919	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435	ed to achieve a top of Min Cu Ft 1166	2.89  11721 1 Stage % Excess 23	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	3.20	Weigl 513,44 0 0 513,44 overlap. Min Di Hole-C 0.43
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 lass 'C' tail cm  #N/A 0 Segment "A"	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835 tyld > 1.35	ng inside the Grade (g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 919	7 5/8 p 110  t psig: 2,774 volume(s) are intende 1 Stage CuFt Cmt 1435	ed to achieve a top of Min Cu Ft 1166  Coupling 0.00	2.89  11721 1 Stage % Excess 23	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	3.20	Weigl 513,44 0 0 513,44 overlap. Min Di Hole-C ₁ 0.43
Tail cmt 51/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 llass 'C' tail cm	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835 tyld > 1.35	ig mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 919  Grade	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435  5 1/2	ed to achieve a top of Min Cu Ft 1166  Coupling 0.00 0.00	2.89  11721 1 Stage % Excess 23	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP  Factors Burst Totals:	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	3.20 ing> a-C	Weig 513,44 0 0 513,44 overlap. Min Di Hole-C 0.43 Weig 0 0 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 class 'C' tail cm  #N/A 0 Segment "A"	casin #/ft 20.00 w/8.4#// Annular Volume 0.0835 tyld > 1.35	ng inside the Grade  Grade  g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 919  Grade  Grade	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435  5 1/2	talon rd  ed to achieve a top of Min Cu Ft 1166  Coupling 0.00 0.00  dis csg, TOC intended	2.89  11721 1 Stage % Excess 23  #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a	Length 25,673 0 0 0 25,673 200 Req'd BOPE  Length 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2	a-B 3.50	3.20 ing> a-C	Weigi 513,44 0 0 513,44 overlap. Min Di Hole-Ci 0.43 Weigi 0 0 0 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 class 'C' tail cm #N/A 0 Segment "A" "B"	casin #/ft 20.00  w/8.4#// Annular Volume 0.0835 tyld > 1.35  #/ft  w/8.4#// Annular	og inside the Grade  Grade  I'g mud, 30min Sfc Csg Test The cement 1 Stage Cmt Sx 919  Grade  I'g mud, 30min Sfc Csg Test Cmt vol ca 1 Stage	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435  5 1/2  t psig: alc below includes th 1 Stage	talon rd  ed to achieve a top of Min Cu Ft 1166  Coupling 0.00 0.00  dis csg, TOC intended Min	2.89  11721 1 Stage % Excess 23  #N/A  #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse  ft from su Drilling	Totals: rface or a Calc MASP  Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	3.20 ing> a-C	Weigl 513,46 0 0 513,46 overlap. Min Di Hole-C  0.43  Weigl 0 0 overlap. Min Di
5 1/2 Segment "A" "B" "C" "D"  Hole Size 6 3/4 Class 'C' tail cm #N/A 0 Segment "A" "B"	Casin #/ft 20.00  w/8.4#// Annular Volume 0.0835 tyld > 1.35	ng inside the Grade  Grade  g mud, 30min Sfc Csg Test The cement of 1 Stage Cmt Sx 919  Grade  Grade	7 5/8 p 110  t psig: 2,774 volume(s) are intended 1 Stage CuFt Cmt 1435  5 1/2	talon rd  ed to achieve a top of Min Cu Ft 1166  Coupling 0.00 0.00  dis csg, TOC intended	2.89  11721 1 Stage % Excess 23  #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Factors Burst  Totals: rface or a	Length 25,673 0 0 0 25,673 200 Req'd BOPE  Length 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2	a-B 3.50	3.20 ing> a-C	Weig 513,4 0 0 513,4 0verlap. Min Di Hole-C 0.43  Weig 0 0 0 0verlap.

Carlsbad Field Office 1/24/2025

#### Morgan 25-13 Fed Com 837H

10 3/4	sur	face csg in a	14 3/4 i	inch hole.		<u>Design</u>	Factors			Surface		
Segment	#/ft	Grade		Coupling	Body	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	45.50		j 55	btc	16.21	4.61	0.55	970	8	0.92	8.70	44,13
"B"				btc				0				0
	w/8.4#/	g mud, 30min Sfc Csg Tes	t psig: 1,500	Tail Cmt	does not	circ to sfc.	Totals:	970				44,13
omparison o		nimum Required Cem										
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Di
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-C
14 3/4	0.5563	586	844	540	56	9.00	3880	5M				1.50
urst Frac Grac	dient(s) for Segme	nt(s) A, B = , b All > 0	.70, OK.									
8 5/8		ng inside the	10 3/4			<u>Design</u>				Int 1	_	
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigl
"A" <b>"B"</b>	32.00		p 110	vam sprint fj	1.95	0.62	1.04	11,921 <b>0</b>	1	1.74	1.03	381,47 <b>0</b>
	w/8.4#/	/g mud, 30min Sfc Csg Tes	t psig: -197				Totals:	11,921				381,47
				led to achieve a top of	0	ft from su		970				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Di
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-C
9 7/8	0.1261	597	860	1511	-43	10.50	4104	5M				0.61
O V Tool(s):	0.1201	001	6754	1011	10	10.00	sum of sx	Σ CuFt				Σ%exce
J V 1001(3).							Julii Ol JX					
	nt yld > 1.35	32	27				1071	1950				29
Class 'C' tail cm	nt yld > 1.35	32	27				1071	1950				
		32	27 8 5/8			Design Fac		1950		Prod 1		29
Tail cmt				Coupling	Joint	Design Fac		1950	B@s	Prod 1 a-B	a-C	
Tail cmt	casii	ng inside the	8 5/8	Coupling dwc/c is+	<b>Joint</b> 2.89		ctors	Length	<b>B@s</b> 2		-	Weigl
Tail cmt 5 1/2 Segment	casiı #/ft	ng inside the				Collapse	ctors Burst		_	а-В	-	Weigl
Tail cmt 5 1/2 Segment "A"	casiı #/ft	ng inside the	8 5/8			Collapse	ctors Burst	Length 25,673	_	а-В	-	<b>Weig</b> l 513,46
Tail cmt 5 1/2 Segment "A" "B"	casiı #/ft	ng inside the	8 5/8			Collapse	ctors Burst	Length 25,673 0	_	а-В	-	Weigl 513,46 0
Tail cmt 51/2 Segment "A" "B" "C"	casin #/ft 20.00	ng inside the Grade	85/8 p 110			Collapse	ctors Burst	Length 25,673 0 0	_	а-В	-	Weigl 513,46 0 0
Tail cmt 51/2 Segment "A" "B" "C"	casin #/ft 20.00	ng inside the Grade	8 5/8 p 110 t psig: 2,774	dwc/c is+	2.89	Collapse 1.76	Ctors Burst 2.09	Length 25,673 0 0 0 25,673	_	а-В	-	Weigl 513,46 0 0 0 513,46
Tail cmt 51/2 Segment "A" "B" "C"	casin #/ft 20.00	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement	8 5/8 p 110 t psig: 2,774 volume(s) are intend		2.89	1.76	Ctors Burst 2.09	Length 25,673 0 0 0 25,673 200	_	а-В	-	Weigl 513,46 0 0 0 513,46 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"	casii #/ft 20.00 w/8.4#/	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement 1 Stage	8 5/8 p 110 t psig: 2,774 volume(s) are intend 1 Stage	dwc/c is+	2.89 11721 1 Stage	1.76  ft from su	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 0 25,673 200 Req'd	_	а-В	-	Weigl 513,46 0 0 0 513,46 overlap.
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size	casir #/ft 20.00 w/8.4#,/ Annular Volume	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+  led to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.09  Totals:	Length 25,673 0 0 0 25,673 200	_	а-В	-	Weigl 513,46 0 0 513,46 overlap. Min Di: Hole-C;
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8	casir #/ft 20.00 w/8.4#,/ Annular Volume 0.1733	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement 1 Stage	8 5/8 p 110 t psig: 2,774 volume(s) are intend 1 Stage	dwc/c is+	2.89 11721 1 Stage	1.76  ft from su	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 0 25,673 200 Req'd	_	а-В	-	Weigl 513,46 0 0 0 513,46 overlap. Min Di
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 class 'C' tail cm	casir #/ft 20.00 w/8.4#,/ Annular Volume 0.1733	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+  led to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 0 25,673 200 Req'd	_	а-В	-	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 Class 'C' tail cm	casir #/ft 20.00 w/8.4#,/ Annular Volume 0.1733	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+  led to achieve a top of  Min  Cu Ft	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt	Ctors Burst 2.09  Totals: rface or a Calc	Length 25,673 0 0 0 25,673 200 Req'd	_	а-В	-	Weigl 513,46 0 0 513,46 overlap. Min Di
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 lass 'C' tail cm	casin #/ft 20.00 w/8.4#/ Annular Volume 0.1733 at yld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 1897	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt	dwc/c is+	2.89  11721 1 Stage % Excess 22	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd	2	а-В	2.95	Weigl 513,46 0 0 513,46 overlap. Min Di Hole-Cl 0.79
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 llass 'C' tail cm	casir #/ft 20.00 w/8.4#,/ Annular Volume 0.1733	ng inside the Grade /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946	dwc/c is+	2.89 11721 1 Stage % Excess	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	<b>a-B</b> 3.50	2.95	Weigi 513,44 0 0 513,44 0 overlap. Min Di Hole-C  0.79
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 lass 'C' tail cm	casin #/ft 20.00 w/8.4#/ Annular Volume 0.1733 at yld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 1897	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946	dwc/c is+  led to achieve a top of  Min  Cu Ft  2418  Coupling  0.00	2.89  11721 1 Stage % Excess 22	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weigl 513,44 0 0 513,44 0 overlap. Min Di Hole-C 0.79
Tail cmt  5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 llass 'C' tail cm	casin #/ft 20.00 w/8.4#/ Annular Volume 0.1733 at yld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 1897	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946	dwc/c is+	2.89  11721 1 Stage % Excess 22	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weig 513,44 0 0 513,44 overlap. Min Di Hole-C 0.79 Weig 0 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 class 'C' tail cm	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733 htyld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 1897	p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946	dwc/c is+  led to achieve a top of  Min  Cu Ft  2418  Coupling  0.00	2.89  11721 1 Stage % Excess 22	ft from su Drilling Mud Wt 10.50	Totals: rface or a Calc MASP	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weig 513,44 0 0 513,44 overlap. Min Di Hole-C 0.79
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 Class 'C' tail cm	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733 htyld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes: The cement 1 Stage Cmt Sx 1897  Grade	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946  5 1/2	dwc/c is+  led to achieve a top of  Min  Cu Ft  2418  Coupling  0.00	2.89  11721 1 Stage % Excess 22	ft from su Drilling Mud Wt 10.50	Totals:  Totals:  rface or a  Calc MASP  Factors Burst  Totals:	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weig 513,44 0 0 513,44 overlap. Min Di Hole-C 0.79 Weig 0 0
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 Class 'C' tail cm	casir #/ft 20.00 w/8.4#// Annular Volume 0.1733 htyld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes: The cement 1 Stage Cmt Sx 1897  Grade	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946  5 1/2	dwc/c is+  led to achieve a top of  Min  Cu Ft  2418  Coupling  0.00  0.00	2.89  11721 1 Stage % Excess 22  #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals:  Totals:  rface or a  Calc MASP  Factors Burst  Totals:	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weig 513,4 0 0 513,4 0verlap. Min Di Hole-C 0.79 Weig 0 0 overlap.
Tail cmt 5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 Class 'C' tail cm  #N/A 0 Segment "A" "B"	casin #/ft 20.00 w/8.4#, Annular Volume 0.1733 at yld > 1.35	ng inside the Grade  /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 1897  Grade  /g mud, 30min Sfc Csg Tes Cmt vol c	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946  5 1/2	dwc/c is+  led to achieve a top of Min Cu Ft 2418  Coupling 0.00 0.00 his csg, TOC intended	2.89  11721 1 Stage % Excess 22  #N/A	ft from su Drilling Mud Wt 10.50  Design Collapse	Totals: rface or a Calc MASP  Totals: Totals: rfactors Burst	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weigi 513,44 0 0 513,44 0verlap. Min Di Hole-C  0.79  Weigi 0 0 0verlap. Min Di
5 1/2 Segment "A" "B" "C" "D"  Hole Size 7 7/8 Class 'C' tail cm #N/A 0 Segment "A" "B"	casin #/ft 20.00  w/8.4#/ Annular Volume 0.1733 at yld > 1.35  #/ft  w/8.4#/ Annular	ng inside the Grade  /g mud, 30min Sfc Csg Tes The cement 1 Stage Cmt Sx 1897  Grade  /g mud, 30min Sfc Csg Tes Cmt vol c 1 Stage	8 5/8 p 110  t psig: 2,774 volume(s) are intend 1 Stage CuFt Cmt 2946  5 1/2  t psig: alc below includes th 1 Stage	dwc/c is+  led to achieve a top of  Min  Cu Ft  2418  Coupling  0.00  0.00  his csg, TOC intended  Min	2.89  11721 1 Stage % Excess 22  #N/A  #N/A  1 Stage	ft from su Drilling Mud Wt 10.50  Design Collapse  ft from su Drilling	Totals: rface or a Calc MASP  Totals: rfactors Burst  Totals: rface or a Calc	Length 25,673 0 0 0 25,673 200 Req'd BOPE	2	a-B 3.50	2.95	Weig 513,4 0 0 513,4 0verlap. Min Di Hole-C 0.79 Weig 0 0 overlap.

Carlsbad Field Office 1/24/2025 Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 425043

#### **CONDITIONS**

Operator:	OGRID:
DEVON ENERGY PRODUCTION COMPANY, LP	6137
333 West Sheridan Ave.	Action Number:
Oklahoma City, OK 73102	425043
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rikala	Any previous COA's not addressed within the updated COA's still apply.	4/2/2025