Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMNM115404 **BUREAU OF LAND MANAGEMENT** APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **✓** DRILL REENTER 1a. Type of work: 1b. Type of Well: Oil Well ✓ Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing ✓ Single Zone Multiple Zone ICEMAN 24/23 FED COM 712H 2. Name of Operator 9. API Well No. 30**-0**15**-56**816 MEWBOURNE OIL COMPANY 3a. Address 3b. Phone No. (include area code) 10. Field and Pool, or Exploratory PURPLE SAGE/(WOLFCAMP) GAS P O BOX 5270, HOBBS, NM 88241 (575) 393-5905 4. Location of Well (Report location clearly and in accordance with any State requirements.*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 24/T23S/R26E/NMP At surface SENE / 1960 FNL / 260 FEL / LAT 32.2920255 / LONG -104.2386691 At proposed prod. zone NWNE / 800 FNL / 2342 FEL / LAT 32.2952617 / LONG -104.2625403 14. Distance in miles and direction from nearest town or post office* 12. County or Parish 13. State **EDDY** NM 10 miles 15. Distance from proposed* 16. No of acres in lease 17. Spacing Unit dedicated to this well 210 feet location to nearest property or lease line, ft. 480.0 (Also to nearest drig. unit line, if any) 18. Distance from proposed location* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 20 feet 8764 feet / 16350 feet FED: NM1693 applied for, on this lease, ft. 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. Approximate date work will start* 23. Estimated duration 3222 feet 08/17/2024 60 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the Name (Printed/Typed) Date 25. Signature BRADLEY BISHOP / Ph: (575) 393-5905 06/17/2024 (Electronic Submission) Title Regulatory Approved by (Signature) Date Name (Printed/Typed) (Electronic Submission) CODY LAYTON / Ph: (575) 234-5959 05/08/2025 Title Office Assistant Field Manager Lands & Minerals Carlsbad Field Office Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.



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Santa Fe Main Office

Phone: (505) 476-3441 Fax: (55) 476-3462

General Information Phone: (505) 629-6116

Online Phone Directory Visit:

https://www.emnrd.nm.gov/ocd/contact-us/

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION

Revised July 9, 2024 Submit Electronically via OCD Permitting ☑ Initial Submittal

Submittal ☐ Amended Report Type:

☐ As Drilled

WELL LOCATION INFORMATION

| API Number 30-015-56816 | Pool Code 9822 | 98220 PURPLE SAGE; WOLF | | | | |
|--------------------------------|------------------|---------------------------|---|-----------------------------|--|--|
| Property Code 337348 | Property Name | CEMAN 24/2 | 23 FED COM | Well Number 712H | | |
| OGRID No. 14744 | Operator Name | MEWBOURN | NE OIL COMPANY | Ground Level Elevation 3222 | | |
| Surface Owner: ☐ State ☐ Fee ☐ | Tribal X Federal | | Mineral Owner: □ State □ Fee □ Tribal 🔀 Federal | | | |

Surface Location

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude | Longitude | County | | |
|----|----------------------|----------|-------|-----|--------------|--------------|------------|--------------|--------|--|--|
| Н | 24 | 23S | 26E | | 1960 FNL | 260 FEL | 32.2920255 | -104.2386691 | EDDY | | |
| | Bottom Hole Location | | | | | | | | | | |
| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude | Longitude | County | | |
| В | 23 | 23S | 26E | | 800 FNL | 2342 FEL | 32.2952617 | -104.2625403 | EDDY | | |

| Dedicated Acres | Infill or Defining Well | Defining Well API | Overlapping Spacing Unit (Y/N) | Consolidation Code |
|-----------------|-------------------------|-------------------|----------------------------------|---------------------|
| 480 | DEFINING | | Υ | N/A |
| Order Numbers. | | | Well setbacks are under Common (| Ownership: □Yes □No |

Kick Off Point (KOP)

| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude | Longitude | County | | | |
|----|------------------------|----------|-------|-----|--------------|--------------|----------------------------------|--------------|--------|--|--|--|
| Α | 24 | 23 | 26 | | 800 FNL | 10 FEL | 32.2952069 | -104.2378479 | EDDY | | | |
| | First Take Point (FTP) | | | | | | | | | | | |
| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude | Longitude | County | | | |
| Α | 24 | 23 | 26 | | 800 FNL | 330 FEL | 32.2952087 | -104.2388359 | EDDY | | | |
| | | | | | Last Take | Point (LTP) | | | | | | |
| UL | Section | Township | Range | Lot | Ft. from N/S | Ft. from E/W | Latitude | Longitude | County | | | |
| В | 23 | 23 | 26 | | 800 FNL | 2342 FEL | 2342 FEL 32.2952641 -104.2625403 | | EDDY | | | |

| Unitized Area or Area of Uniform Interest | Spacing Unit Type ▼ Horizontal □ Vertical | Ground Floor Elevation: | 3222 |
|---|---|-------------------------|------|
| | | i | |

OPERATOR CERTIFICATIONS

I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief, and, if the well is a vertical or directional well, that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of a working interest or unleased mineral interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.

If this well is a horizontal well, I further certify that this organization has received the consent of at least one lessee or owner of a working interest or unleased mineral interest in each tract (in the target pool or formation) in which any part of the well's completed interval will be located or obtained a compulsory pooling order from the division.

5/12/25

RYAN MCDANIEL

RYANMCDANIEL@MEWBOURNE.COM

Email Address

SURVEYOR CERTIFICATIONS

I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision and that the same is true and correct to the best of my belief.

SIONAL

Signature and Seal of Professional Surveyor

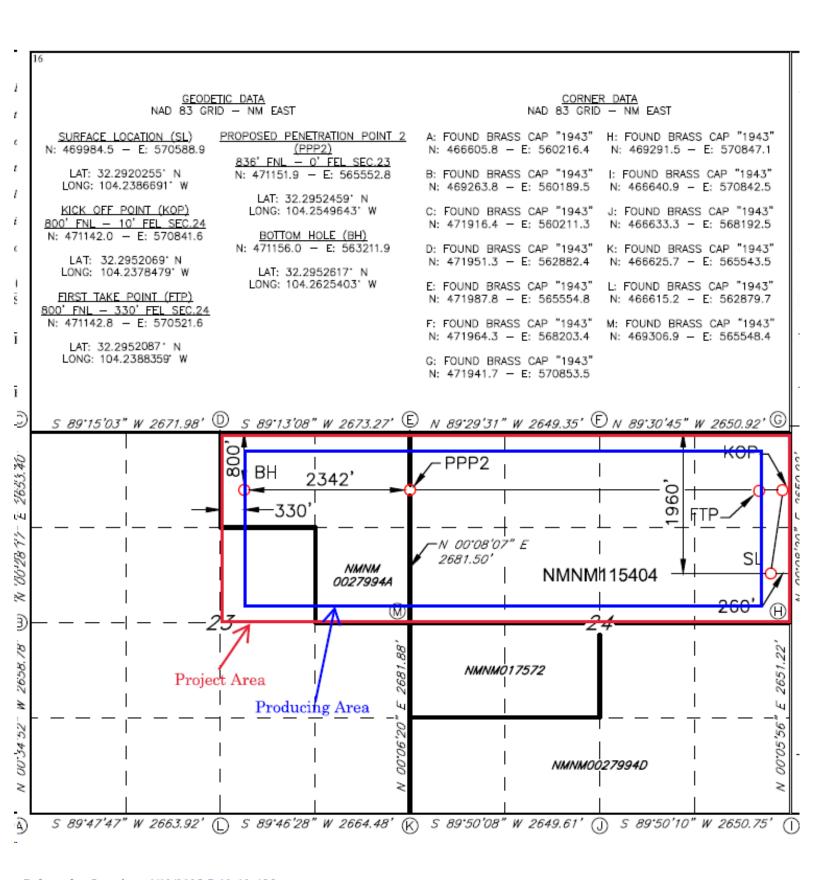
Certificate Number

Date of Survey

19680

This grid represents a standard section. You may superimpose a non-standard section, or larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is closest to any outer boundary of the tract.

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed, contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.



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State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

| | N | ATURAL G | AS MANA(| GEMENT PI | LAN | | | | | |
|--|--|--------------|---------------------|----------------------------|--------------------------|---------|---------------------------------|--|--|--|
| This Natural Gas Management Plan must be submitted with each Application for Permit to Drill (APD) for a new or recompleted well. | | | | | | | | | | |
| Section 1 – Plan Description Effective May 25, 2021 | | | | | | | | | | |
| I. Operator: Mewbourne Oil Co. OGRID: 14744 Date: 5/2/22 | | | | | | | | | | |
| II. Type: 🗶 Original | II. Type: ✓ Original □ Amendment due to □ 19.15.27.9.D(6)(a) NMAC □ 19.15.27.9.D(6)(b) NMAC □ Other. | | | | | | | | | |
| If Other, please describe | <u>.</u> | | | | | | | | | |
| III. Well(s): Provide the following information for each new or recompleted well or set of wells proposed to be drilled or proposed to be recompleted from a single well pad or connected to a central delivery point. | | | | | | | | | | |
| Well Name | API | ULSTR | Footages | Anticipated Oil BBL/D | Anticipated Gas MCF/D | Pı | Anticipated roduced Water BBL/D | | | |
| ICEMAN 24-23 FED COM 712H | | H 24 23S 26E | 1960' FNL x 260' FE | L 1500 | 5500 | | 4500 | | | |
| | | | | Y1-400 Y2-300 Y3-200 | 1500 Y2-1100 Y3-700 | | | | | |
| IV. Central Delivery P | oint Name: | IC | EMAN 24-23 FED | COM 712H | [See 1 | 9.15.2 | 7.9(D)(1) NMAC] | | | |
| V. Anticipated Schedul proposed to be recomple | | | | | rell or set of wells | s propo | sed to be drilled or | | | |
| Well Name | API | Spud Date | TD Reached Date | Completion Commencement | | | First Production Date | | | |
| ICEMAN 24-23 FED COM 712H | | 7/2/22 | 8/2/22 | 9/2/22 | 9/17/2: | 2 | 9/17/22 | | | |
| | | | | | | | | | | |
| | VI. Separation Equipment: ☐ Attach a complete description of how Operator will size separation equipment to optimize gas capture. VII. Operational Practices: ☐ Attach a complete description of the actions Operator will take to comply with the requirements of | | | | | | | | | |
| | Subsection A through F of 19.15.27.8 NMAC. | | | | | | | | | |
| VIII. Best Management during active and planned | | | ete description of | Operator's best m | nanagement pract | ices to | minimize venting | | | |
| | | | | | | | | | | |

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Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

🗴 Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

IX. Anticipated Natural Gas Production:

| Well | API | Anticipated Average Natural Gas Rate MCF/D | Anticipated Volume of Natural Gas for the First Year MCF | | | | | | |
|---|-----|---|--|--|--|--|--|--|--|
| | | | | | | | | | |
| | | | | | | | | | |
| X. Natural Gas Gathering System (NGGS): | | | | | | | | | |

| Operator | System | ULSTR of Tie-in | Anticipated Gathering Start Date | Available Maximum Daily Capacity of System Segment Tie-in | | |
|----------|--------|-----------------|-------------------------------------|---|--|--|
| | | | | | | |
| | | | | | | |

| XI. Map. \square Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the |
|---|
| production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of |
| the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected. |

| XII. Line Capacity. The natural gas gathering system \square will \square will not have capacity to gather 100% of the anticipation. | ipated natural gas |
|--|--------------------|
| production volume from the well prior to the date of first production. | |

| XIII. Line Pressure. Operator \Box does \Box does not anticipate that its existing well(s) connected to the same segment, or p | ortion, o | of the |
|--|-----------|--------|
| natural gas gathering system(s) described above will continue to meet anticipated increases in line pressure caused by the | new wel | ll(s). |

| Attach | Operator | a nlan ta | monoco | production | in | rocmonco | t-0 | tha | ingrand | lina | neoccuro |
|--------|----------|-----------|--------|------------|----|----------|-----|-----|----------|-------|----------|
| Attach | Operator | s bian u | manage | broduction | Ш | response | w | une | mereased | IIIIe | bressure |

| XIV. Confi | identiality: 🗆 | Operator asser | ts confidentiality | pursuant to | Section | 71-2-8 | NMSA | 1978 f | or the | information | provided in |
|--------------|------------------|-------------------|--------------------|--------------|----------|-----------|-----------|---------|---------|----------------|-------------|
| Section 2 as | s provided in Pa | aragraph (2) of S | Subsection D of 1 | 9.15.27.9 NN | AAC, and | d attache | es a full | descrip | tion of | f the specific | information |
| for which co | onfidentiality i | s asserted and th | e basis for such a | assertion. | | | | | | | |

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Section 3 - Certifications <u>Effective May</u> 25, 2021

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal: 🖾 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan.

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) (b) power generation for grid; compression on lease; (c) liquids removal on lease; (d)

- (e) reinjection for underground storage;
- (f) reinjection for temporary storage;
- (g) reinjection for enhanced oil recovery;
- (h) fuel cell production; and
- (i) other alternative beneficial uses approved by the division.

Section 4 - Notices

- 1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:
- (a) Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- (b) Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

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I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

| Bradley Bishop |
|---|
| BRADLEY BISHOP |
| REGULATORY MANAGER |
| BBISHOP@MEWBOURNE.COM |
| 5/2/22 |
| 575-393-5905 |
| OIL CONSERVATION DIVISION |
| (Only applicable when submitted as a standalone form) |
| |
| |
| |
| approval: |
| |

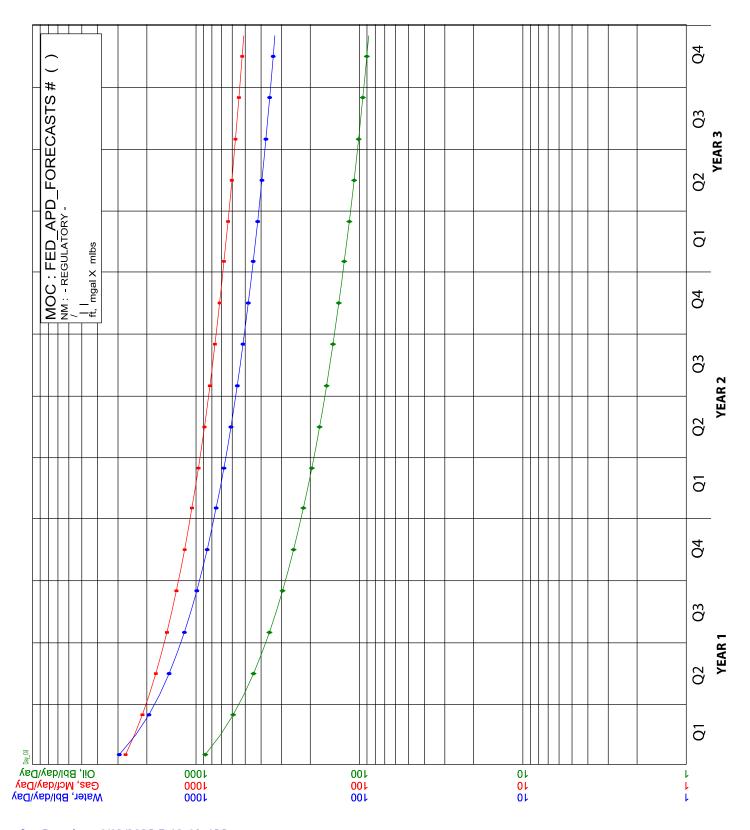
Mewbourne Oil Company

Natural Gas Management Plan – Attachment

- VI. Separation equipment will be sized by construction engineering staff based on stated manufacturer daily throughput capacities and anticipated daily production rates to ensure adequate capacity. Closed vent system piping, compression needs, and VRUs will be sized utilizing ProMax modelling software to ensure adequate capacity for anticipated production volumes and conditions.
- VII. Mewbourne Oil Company (MOC) will take following actions to comply with the regulations listed in 19.15.27.8:
 - A. MOC will maximize the recovery of natural gas by minimizing the waste, as defined by 19.15.2 NMAC, of natural gas through venting and flaring. MOC will ensure that well(s) will be connected to a natural gas gathering system with sufficient capacity to transport natural gas. If there is no adequate takeaway for the gas, well(s) will be shut in until the natural gas gathering system is available.
 - B. All drilling operations will be equipped with a rig flare located at least 100 ft from the nearest surface hole. Rig flare will be utilized to combust any natural gas that is brought to surface during normal drilling operations. In the case of emergency venting or flaring the volumes will be estimated and reported appropriately.
 - C. During completion operations any natural gas brought to surface will be flared. Immediately following the finish of completion operations, all well flow will be directed to permanent separation equipment. Produced natural gas from separation equipment will be sent to sales. It is not anticipated that gas will not meet pipeline standards. However, if natural gas does not meet gathering pipeline quality specifications, MOC will flare the natural gas for 60 days or until the natural gas meets the pipeline quality specifications, whichever is sooner. MOC will ensure that the flare is sized properly and is equipped with automatic igniter or continuous pilot. The gas sample will analyzed twice per week and the gas will be routed into a gathering system as soon as pipeline specifications are met.
 - D. Natural gas will not be flared with the exceptions and provisions listed in the 19.15.27.8 D.(1) through (4). If there is no adequate takeaway for the separator gas, well(s) will be shut in until the natural gas gathering system is available with exception of emergency or malfunction situations. Venting and/or flaring volumes will be estimated and reported appropriately.
 - E. MOC will comply with the performance standards requirements and provisions listed in 19.15.27.8 E.(1) through (8). All equipment will be designed and sized to handle maximum anticipated pressures and throughputs in order to minimize the waste. Production storage tanks constructed after May 25, 2021 will be equipped with automatic gauging system. Flares constructed after May 25, 2021 will be equipped with automatic igniter or continuous pilot. Flares will be located at least 100' from the well and storage tanks unless otherwise approved by the division. MOC will conduct AVO inspections as described in 19.15.27.8 E (5) (a) with frequencies specified in 19.15.27.8 E (5) (b) and (c). All emergencies will be resolved as quickly and safely as feasible to minimize waste.
 - F. The volume of natural gas that is vented or flared as the result of malfunction or emergency during drilling and completions operations will be estimated. The volume of natural gas that is vented, flared or beneficially used during production operations, will be measured or estimated. MOC will install equipment to measure

the volume of natural gas flared from existing process piping or a flowline piped from equipment such as high pressure separators, heater treaters, or vapor recovery units associated with a well or facility associated with a well authorized by an APD issued after May 25, 2021 that has an average daily production greater than 60 Mcf/day. If metering is not practicable due to circumstances such as low flow rate or low pressure venting and flaring, MOC will estimate the volume of vented or flared natural gas. Measuring equipment will conform to industry standards and will not be designed or equipped with a manifold that allows the diversion of natural gas around the metering element except for the sole purpose of inspecting and servicing the measurement equipment.

VIII. For maintenance activities involving production equipment and compression, venting will be limited to the depressurization of the subject equipment to ensure safe working conditions. For maintenance of production and compression equipment the associated producing wells will be shut in to eliminate venting. For maintenance of VRUs all gas normally routed to the VRU will be routed to flare to eliminate venting.





APD ID: 10400099099

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Drilling Plan Data Report 05/09/2025

Operator Name: MEWBOURNE OIL COMPANY

Well Name: ICEMAN 24/23 FED COM

Well Type: CONVENTIONAL GAS WELL

Submission Date: 06/17/2024

Well Number: 712H

Well Work Type: Drill

Highlighted data reflects the most recent changes

Show Final Text

Section 1 - Geologic Formations

| Formation ID | Formation Name | Elevation | True Vertical | Measured Depth | Lithologies | Mineral Resources | Producing Formatio |
|--------------|-----------------|-----------|---------------|-------------------|--------------------------------|-------------------|-----------------------|
| 15594419 | UNKNOWN | 3225 | 27 | 27 | OTHER : Topsoil | NONE | N |
| 15594423 | TOP SALT | 2650 | 575 | 575 | SALT | NONE | N |
| 15594420 | BOTTOM SALT | 1583 | 1642 | 1642 | SALT | NONE | N |
| 15594424 | LAMAR | 1355 | 1870 | 1870 | DOLOMITE, LIMESTONE | NATURAL GAS, OIL | N |
| 15594425 | BELL CANYON | 1275 | 1950 | 1950 | SANDSTONE | NATURAL GAS, OIL | N |
| 15594426 | CHERRY CANYON | 605 | 2620 | 2620 | SANDSTONE | NATURAL GAS, OIL | N |
| 15594427 | MANZANITA | 466 | 2759 | 2759 | LIMESTONE | NATURAL GAS, OIL | N |
| 15594428 | BRUSHY CANYON | -1709 | 4934 | 4934 | SANDSTONE | NATURAL GAS, OIL | N |
| 15594418 | BONE SPRING | -2078 | 5303 | 5303 | LIMESTONE | NATURAL GAS, OIL | N |
| 15594421 | BONE SPRING 1ST | -3106 | 6331 | 6331 | SANDSTONE | NATURAL GAS, OIL | N |
| 15594422 | BONE SPRING 2ND | -3571 | 6796 | 6796 | SANDSTONE | NATURAL GAS, OIL | N |
| 15594429 | BONE SPRING 3RD | -5176 | 8401 | 8401 | SANDSTONE | NATURAL GAS, OIL | N |
| 15594430 | WOLFCAMP | -5518 | 8743 | 8743 | LIMESTONE, SANDSTONE, SHALE | NATURAL GAS, OIL | Y |

Section 2 - Blowout Prevention

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Pressure Rating (PSI): 5M Rating Depth: 16350

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Requesting Variance? YES

Variance request: A variance is requested for the use of a variable choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

Choke Diagram Attachment:

5M_BOPE_Choke_Diagram_20240617091914.pdf Flex_Line_Specs_API_16C_20241213075354.pdf Cactus 5K WH 20241213075353.pdf

BOP Diagram Attachment:

5M_BOPE_Schematic_20240617091959.pdf

MOC_Break_Testing_Variance_20240617092027.pdf

Section 3 - Casing

| Casing ID | String Type | Hole Size | Csg Size | Condition | Standard | Tapered String | Top Set MD | Bottom Set MD | Top Set TVD | Bottom Set TVD | Top Set MSL | Bottom Set MSL | Calculated casing length MD | Grade | Weight | Joint Type | Collapse SF | Burst SF | Joint SF Type | Joint SF | Body SF Type | Body SF |
|-----------|------------------|--------------------|----------|-----------|----------|----------------|------------|---------------|-------------|----------------|-------------|----------------|-----------------------------|-----------|--------|------------|-------------|----------|---------------|-----------|--------------|-----------|
| 1 | SURFACE | 17.5 | 13.375 | NEW | API | N | 0 | 500 | 0 | 500 | 3222 | 2722 | 500 | H-40 | 48 | ST&C | 3.44 | 7.74 | DRY | 13.4 2 | DRY | 22.5 4 |
| 2 | INTERMED IATE | 12 <u>.</u> 2 5 | 9.625 | NEW | API | N | 0 | 1795 | 0 | 1795 | 3208 | 1427 | 1795 | J-55 | 36 | LT&C | 2.12 | 3.7 | DRY | 7.01 | DRY | 8.73 |
| 3 | PRODUCTI ON | 8.75 | 7.0 | NEW | API | N | 0 | 8392 | 0 | 8298 | 3208 | -5076 | 8392 | P- 110 | 26 | LT&C | 1.44 | 2.31 | DRY | 3.18 | DRY | 3.8 |
| 4 | LINER | 6.12 5 | 4.5 | NEW | API | N | 8192 | 16350 | 8131 | 8871 | -4909 | -5649 | 8158 | P- 110 | 13.5 | LT&C | 2.1 | 2.45 | DRY | 3.07 | DRY | 3.83 |

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Casing ID: 1

String

SURFACE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Iceman_24_23_Fed_Com_712H_CsgAssumptions_20241213075447.pdf

Casing ID: 2

String

INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Iceman_24_23_Fed_Com_712H_CsgAssumptions_20241213075504.pdf

Casing ID: 3

٦

String

PRODUCTION

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Iceman_24_23_Fed_Com_712H_CsgAssumptions_20241213075609.pdf

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Casing Attachments

Casing ID: 4

String

LINER

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

 $Iceman_24_23_Fed_Com_712H_CsgAssumptions_20241213075625.pdf$

Section 4 - Cement

| String Type | Lead/Tail | Stage Tool Depth | Top MD | Bottom MD | Quantity(sx) | Yield | Density | Cu Ft | Excess% | Cement type | Additives |
|--------------|-----------|---------------------|--------|-----------|--------------|-------|---------|-------|---------|-------------|---|
| SURFACE | Lead | | 0 | 313 | 210 | 2.12 | 12.5 | 450 | 100 | Class C | Salt, Gel, Extender, LCM |
| SURFACE | Tail | 0 | 313 | 500 | 200 | 1.34 | 14.8 | 268 | 100 | Class C | Retarder |
| INTERMEDIATE | Lead | | 0 | 1125 | 210 | 2.12 | 12.5 | 450 | 25 | Class C | Salt, Gel, Extender, LCM |
| INTERMEDIATE | Tail | | 1125 | 1795 | 200 | 1.34 | 14.8 | 268 | 25 | Class C | Retarder |
| PRODUCTION | Lead | 2725 | 1595 | 2104 | 50 | 2.12 | 12.5 | 110 | 25 | Class C | Gel, Retarder, Defoamer, Extender |
| PRODUCTION | Tail | | 2104 | 2725 | 100 | 1.34 | 14.8 | 134 | 25 | Class C | Retarder FLUID LOSS DEFOAMER |
| PRODUCTION | Lead | 2725 | 2725 | 5897 | 280 | 2.12 | 12.5 | 600 | 25 | Class C | Gel, Retarder, Defoamer, Extender |
| PRODUCTION | Tail | | 5897 | 8392 | 400 | 1.18 | 15.6 | 472 | 25 | Class H | Retarder, Fluid Loss, Defoamer |
| LINER | Lead | | 8192 | 1635 0 | 520 | 1.85 | 13.5 | 970 | 25 | Class H | Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-Settling Agent |

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with 43 CFR 3172:

Diagram of the equipment for the circulating system in accordance with 43 CFR 3172:

Describe what will be on location to control well or mitigate other conditions: Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.

Describe the mud monitoring system utilized: Pason/PVT/Visual Monitoring

Circulating Medium Table

| Top Depth | Bottom Depth | Mud Type | Min Weight (lbs/gal) | Max Weight (lbs/gal) | Density (lbs/cu ft) | Gel Strength (lbs/100 sqft) | Н | Viscosity (CP) | Salinity (ppm) | Filtration (cc) | Additional Characteristics |
|-----------|--------------|--------------------|----------------------|----------------------|---------------------|-----------------------------|---|----------------|----------------|-----------------|----------------------------|
| 0 | 500 | SPUD MUD | 8.4 | 8.6 | | 9 | | | | | |
| 500 | 1795 | SALT SATURATED | 9.5 | 10.2 | | | | | | | |
| 1795 | 8392 | WATER-BASED MUD | 8.6 | 10 | | | | | | | |
| 8392 | 1635 0 | OIL-BASED MUD | 10 | 11 | | | | | | | |

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures:

Will run GR/CNL from KOP (8392') to surface (horizontal well vertical portion of hole). Stated logs run will be in the Completion Report and submitted to the BLM.

List of open and cased hole logs run in the well:

COMPENSATED NEUTRON LOG,GAMMA RAY LOG,MEASUREMENT WHILE DRILLING,MUD LOG/GEOLOGIC LITHOLOGY LOG.

Coring operation description for the well:

None

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 5074 Anticipated Surface Pressure: 3135

Anticipated Bottom Hole Temperature(F): 165

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

H2S Plan 20240617093220.pdf

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

ICEMAN_24_23_FED_COM__712H_Dir_Plan_20240617093239.pdf ICEMAN_24_23_FED_COM__712H_Dir_Plot_20240617093243.pdf

Other proposed operations facets description:

: Variance is requested to perform offline cementing according to the attached procedure. R-111Q: Mewbourne is requested to perform Open Hole Cementing per R-111Q Guidelines if well is in Potash.

Other proposed operations facets attachment:

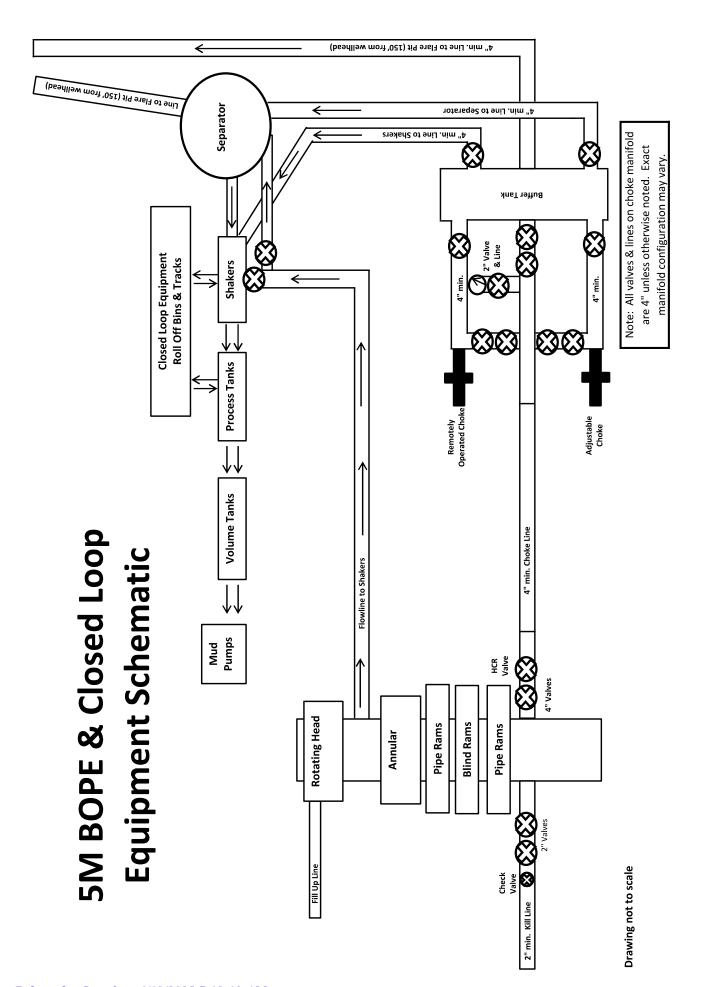
Ice_Man_24_23_Fed_Com_712H_AddInfo_20240617093337.pdf
Iceman_24_23_Fed_Com_712H_Drlg_Program_20241213075654.pdf
ICEMAN_24_23_FED_COM__712H_NGMP_1_20241213103247.pdf

Other Variance request(s)?:

Other Variance attachment:

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

MOC_Offline_Cementing_Variance_20240617093415.pdf MOC_Break_Testing_Variance_20240617093446.pdf





LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

HYDROSTATIC TESTING REPORT

LTYY/QR-5.7.1-28

№: 230826015

| - | | | | | | | | |
|--|-------------------|------------------------|--------------|-------------------|----------------------------|----------------------------------|--|--|
| Product Name | Cho | oke And Kill Hose | | Standard | API | Spec 16C 3 rd edition | | |
| Product Specificati | on 3"×1000 | 00psi×60ft(18.29m | 1) | Serial Numb | per | 7660144 | | |
| Inspection Equipme | ent MTU | J-BS-1600-3200-E | | Test mediu | m | Water | | |
| Inspection Departm | ent (| Q.C. Department | | Inspection D | ate | 2023.08.26 | | |
| | | Rate of le | ength chan | ge | 1 | | | |
| Standard requireme | nts At working pr | essure, the rate of le | ength chan | ge should not me | ore than ± 2 | 6 | | |
| Testing result | 10000psi (69.0 | OMPa) ,Rate of leng | th change | 0.7% | | | | |
| Hydrostatic testing | | | | | | | | |
| Standard requirements At 1.5 times working pressure, the initial pressure-holding period of not less than three min the second pressure-holding period of not less than one hour, no leaks. | | | | | | | | |
| Testing result | 15000psi (103 | .5MPa), 3 min for t | he first tim | ne, 60 min for th | e second time | , no leakage | | |
| raph of pressure tes | ting: | | | | | | | |
| 100 90 80 80 100 100 100 100 100 100 | | | | | | | | |
| Conclusion | The inspec | cted items meet stan | | rements of API | S (2014) SAMON (35) MARKET | 10 | | |
| Approver | Jian long Chen | | | | Inspector | Zhansheng Wa | | |



LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

CERTIFICATE OF QUALITY

LTYY/QR-5.7.1-19B

№: LT2023-126-002

| Customer Name | Austin Hose | | | | | | | | |
|-----------------------|---------------------------|-----------------|--------------------------------------|--|--|--|--|--|--|
| Product Name | Choke And Kill Hose | | | | | | | | |
| Product Specification | 3"×10000psi×60ft (18.29m) | Quantity | 2PCS | | | | | | |
| Serial Number | 7660143~7660144 | FSL | FSL3 | | | | | | |
| Temperature Range | -29℃~+121℃ | Standard | API Spec 16C 3 rd edition | | | | | | |
| Inspection Department | Q.C. Department | Inspection date | 2023.08.26 | | | | | | |

| | Inspectio | n Items | 3 | | Inspection results | | | | |
|----------------------|---------------------------------|-------------|-----------------------|------|---|-----------------------------|-----------------------------|--|--|
| | Appearance C | Checking | g | | In accorda | 16C 3 rd edition | | | |
| | Size and Le | engths | | | In accordance with API Spec 16C 3 rd edition | | | | |
| D | imensions and | Toleran | nces | | In accordance with API Spec 16C 3 rd edition | | | | |
| End Connections: 4-1 | /16"×10000psi In | ntegral fla | ange for sour gas ser | vice | In accordance with API Spec 6A 21st edition | | | | |
| End Connections: 4-1 | /16"×10000psi In | ntegral fla | ange for sour gas ser | vice | In accordance with API Spec 17D 3rd edition | | | | |
| | Hydrostatic 7 | Testing | | | In accordance with API Spec 16C 3 rd edition | | | | |
| | product Ma | arking | | | In accordance with API Spec 16C 3 rd edition | | | | |
| Inspection cor | nclusion | | The inspected ite | ms m | eet standard require | ments of API Spec | 16C 3 rd edition | | |
| Remark | s | | | | | | | | |
| Approver | Approver Jian long Chen Auditor | | | | liging Dong | Inspector | Zhansheng Wang | | |



LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

CERTIFICATE OF CONFORMANCE

№:LT230826016

Product Name: Choke And Kill Hose

Product Specification: 3"×10000psi×60ft (18.29m)

Serial Number: 7660143~7660144

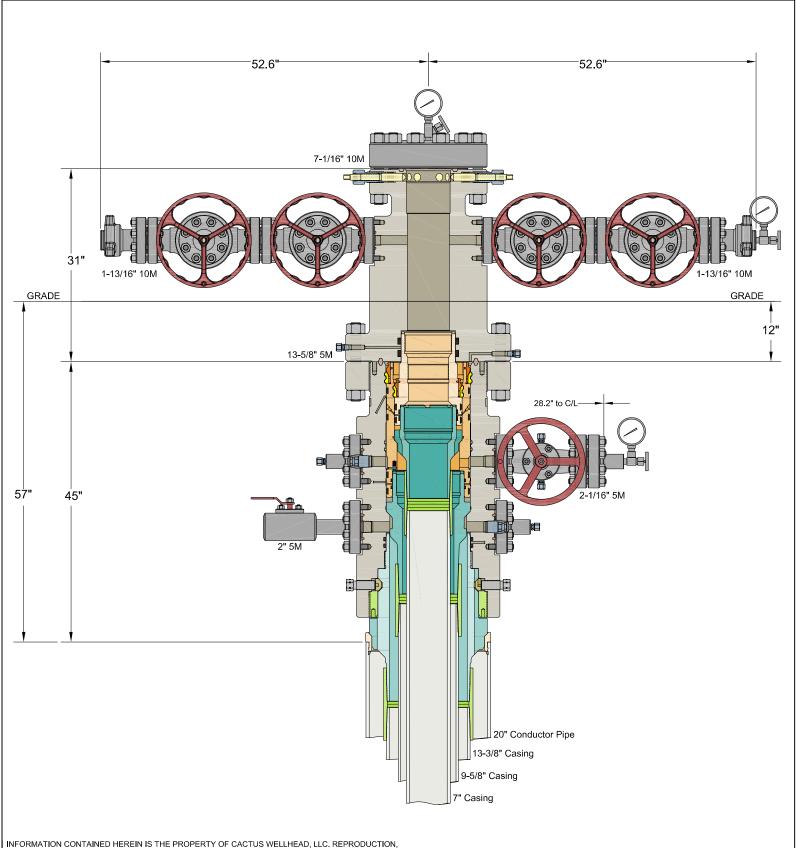
End Connections: 4-1/16"×10000psi Integral flange for sour gas service

The Choke And Kill Hose assembly was produced by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. in Aug 2023, and inspected by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. according to API Spec 16C 3rd edition on Aug 26, 2023. The overall condition is good. This is to certify that the Choke And Kill Hose complies with all current standards and specifications for API Spec 16C 3rd edition.

Jian long Chen

QC Manager:

Date: Aug 26, 2023



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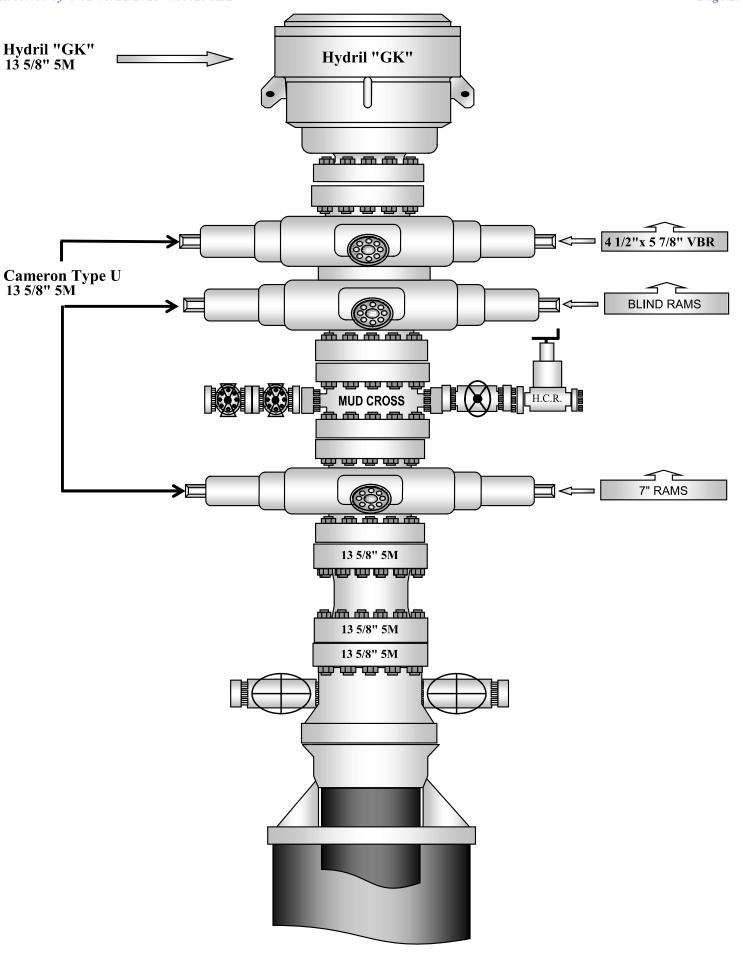
CACTUS WELLHEAD LLC

20" x 13-3/8" x 9-5/8" x 7" MBU-3T-CFL-R-DBLO Wellhead System With 9-5/8" & 7" Fluted Mandrel Casing Hangers And 13-5/8" 5M x 7-1/16" 10M CTH-DBLHPS Tubing Head

ALL DIMENSIONS APPROXIMATE MEWBOURNE OIL COMPANY

DRAWN DLE 18APR22
APPRV

DRAWING NO. HBE0000660





Mewbourne Oil Co.

BOP Break Testing Variance

Mewbourne Oil Company requests a variance from the minimum standards for well control equipment testing of 43 CFR 3172 to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with batch drilling & offline cementing operations. Modern rig upgrades which facilitate pad drilling allow the BOP stack to be moved between wells on a multi-well pad without breaking any BOP stack components apart. Widespread use of these technologies has led to break testing BOPE being endorsed as safe and reliable. American Petroleum Institute (API) best practices are frequently used by regulators to develop their regulations. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (5th Ed., Dec. 2018) Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component."

Procedures

- 1. Full BOPE test at first installation on the pad.
 - Full BOPE test at least every 21 days.
 - Function test BOP elements per 43 CFR 3172.
 - Contact the BLM if a well control event occurs.
- 2. After the well section is secured and the well is confirmed to be static, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad. Two breaks on the BOPE will be made (Fig. 1).
 - Connection between the flex line and the HCR valve
 - Connection between the wellhead and the BOP quick connect (Fig. 5 & 6).
- 3. A capping flange will be installed after cementing per wellhead vendor procedure & casing pressure will be monitored via wellhead valve.
- 4. The BOP will be removed and carried by a hydraulic carrier (Fig. 3 & 4).
- 5. The rig will then walk to the next well.
- 6. Confirm that the well is static and remove the capping flange.
- 7. The connection between the flex line and HCR valve and the connection between the wellhead and the BOP guick connect will be reconnected.
- 8. Install a test plug into the wellhead.
- 9. A test will then be conducted against the upper pipe rams and choke, testing both breaks (Fig. 1 & 2).
- 10. The test will be held at 250 psi low and to the high value submitted in the APD, not to exceed 5000 psi.
- 11. The annular, blind rams and lower pipe rams will then be function tested.
- 12. If a pad consists of three or more wells, steps 4 through 11 will be repeated.



13. A break test will only be conducted if the intermediate section can be drilled and cased within 21 days of the last full BOPE test.

Barriers

Before Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

After Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool and/or cement head
- Capping flange after cementing

Summary

A variance is requested to only test broken pressure seals on the BOPE when moving between wells on a multi-well pad if the following conditions are met:

- A full BOPE test is conducted on the first well on the pad. API Standard 53 requires testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater.
- If the first well on the pad is not the well with the deepest intermediate section, a full BOPE test will also be performed when moving to a deeper well.
- The hole section being drilled has a MASP under 5000 psi.
- If a well control event occurs, Mewbourne will contact BLM for permission to continue break testing.
- If significant (>50%) losses occur, full BOPE testing will be required going forward.
- Full BOPE test will be required prior to drilling the production hole.

While walking the rig, the BOP stack will be secured via hydraulic winch or hydraulic carrier. A full BOPE test will be performed at least every 21 days.



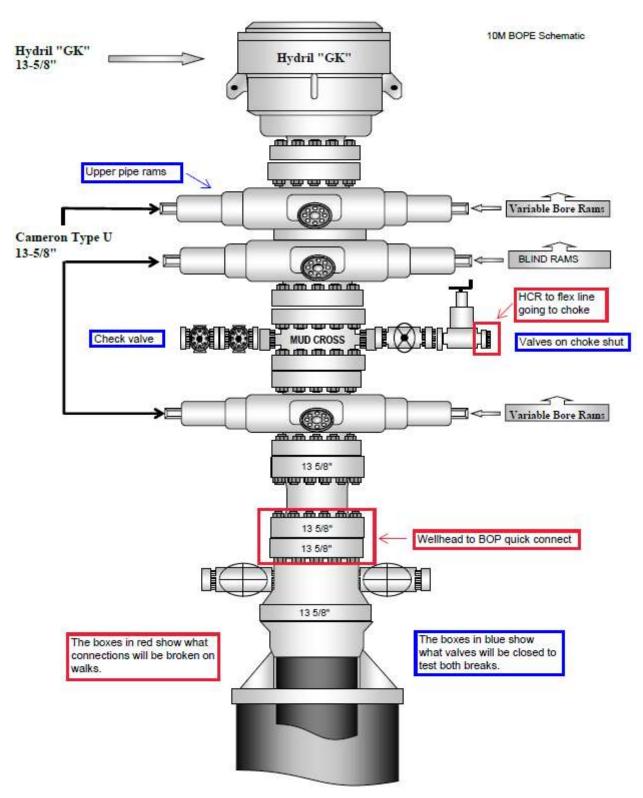


Figure 1. BOP diagram



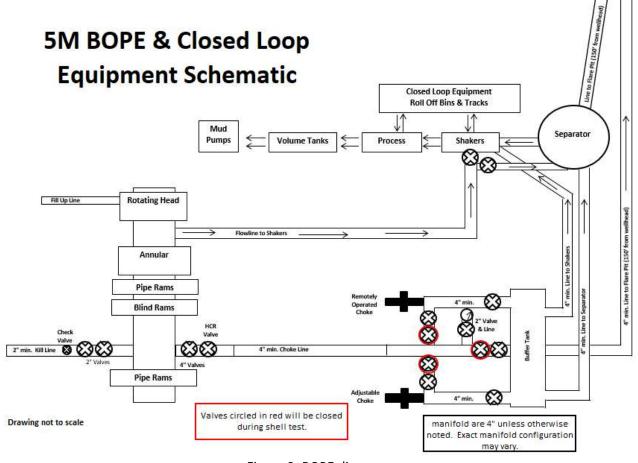


Figure 2. BOPE diagram





Figure 3. BOP handling system





Figure 4. BOP handling system



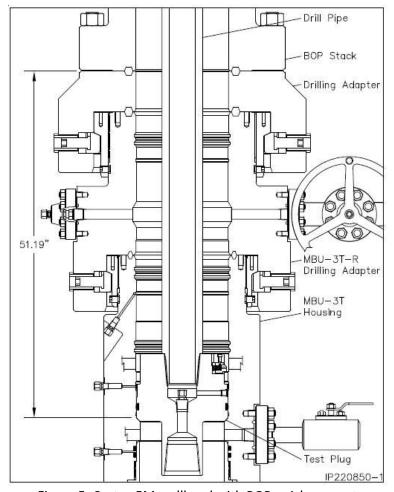


Figure 5. Cactus 5M wellhead with BOP quick connect

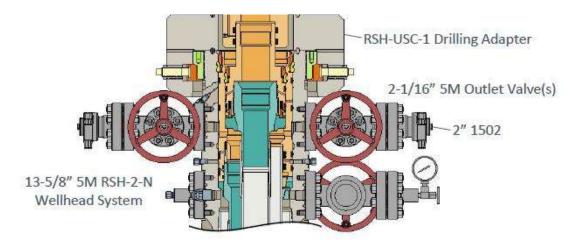


Figure 6. Vault 5M wellhead with BOP quick connect

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| | | Casing Prog | ram Design A | | | BLM Minimum Safety Factors | 1.125 | 1.0 | 1.6 Dry 1.8 Wet | 1.6 Dry 1.8 Wet |
|------------|-----------|-------------|--------------|--------|---------|-------------------------------|-------------|----------|--------------------|--------------------|
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 8392' | 8298' | 7" 26# P110 LTC | 1.44 | 2.31 | 3.18 | 3.80 |
| Liner | 6.125" | 8192' | 8131' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.07 | 3.83 |

Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description | | | |
|---------------|--------------------|---------|------------|-----------------------------|----------------|------------------------|----------|---|--|--|--|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM | | | |
| 13.575 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 10076 | Class C: Retarder | | | |
| 9.625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM | | | |
| 9.025 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2370 | Class C: Retarder | | | |
| 1st Stg 7 in | LEAD | 280 | 12.5 | 2.12 | 2725' - 5897' | 600 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| 1st Stg / III | TAIL | 400 | 15.6 | 1.18 | 5897' - 8392' | 472 | 2370 | Class H: Retarder, Fluid Loss, Defoamer | | | |
| | 7" DV Tool @ 2725' | | | | | | | | | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| 2nd Stg / in | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2370 | Class C: Retarder, Fluid Loss, Defoamer | | | |
| 4.5 in | LEAD | 520 | 13.5 | 1.85 | 8192' - 16350' | 970 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent | | | |

Design A - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 8392' | 8.6 - 10. | Cut-Brine |
| 8392' - 16350' | 10.0 - 11 | ORM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

| | Y or N | | | | | | |
|--|--------|--|--|--|--|--|--|
| Is casing new? If used, attach certification as required in Onshore Order #1 | Y | | | | | | |
| Is casing API approved? If no, attach casing specification sheet. | Y | | | | | | |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N | | | | | | |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria). | | | | | | | |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y | | | | | | |
| | | | | | | | |
| Is well located within Capitan Reef? | N | | | | | | |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | | | | | | | |
| Is well within the designated 4 string boundary. | N | | | | | | |
| | | | | | | | |
| Is well located in SOPA but not in R-111-Q? | N | | | | | | |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing? | | | | | | | |
| | | | | | | | |
| Is well located in R-111-Q and SOPA? | N | | | | | | |
| If yes, are the first three strings cemented to surface? | | | | | | | |
| Is 2 nd string set 100' to 600' below the base of salt? | | | | | | | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | | | | | | | |
| Is an engineered weak point used to satisfy R-111-Q? | | | | | | | |
| If yes, at what depth is the weak point planned? | | | | | | | |
| | | | | | | | |
| Is well located in high Cave/Karst? | Y | | | | | | |
| If yes, are there two strings cemented to surface? | Y | | | | | | |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | | | | | | | |
| | | | | | | | |
| Is well located in critical Cave/Karst? | N | | | | | | |
| If yes, are there three strings cemented to surface? | | | | | | | |

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| | | Casing Prog | ram Design B | | | BLM Minimum Safety | 1.125 | 1.0 | 1.6 Dry | 1.6 Dry |
|------------|-------------|--------------|--------------|--------|-----------|---------------------|-------------|----------|---------------|---------|
| | | Cuoning 110g | rum Design D | | | Factors | 11125 | 1.0 | 1.8 Wet | 1.8 Wet |
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body |
| ou mg | Trote Since | Top ME | I op I i D | | Dut I 1 D | Cog. Size | or compse | DI DUISI | SI OT TENSION | Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 9293' | 8871' | 7" 26# P110 LTC | 1.35 | 2.16 | 2.87 | 3.44 |
| Liner | 6.125" | 8392' | 8298' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.15 | 3.93 |

Design B - Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description |
|---------------|------|---------|------------|-----------------------------|----------------|------------------------|----------|---|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM |
| 13.575 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 10076 | Class C: Retarder |
| 9,625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM |
| 9.025 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2376 | Class C: Retarder |
| 1st Stg 7 in | LEAD | 360 | 12.5 | 2.12 | 2725' - 6797' | 770 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| 1st Stg / III | TAIL | 400 | 15.6 | 1.18 | 6797' - 9293' | 472 | 2370 | Class H: Retarder, Fluid Loss, Defoamer |
| | | | | | 7" DV | Tool @ 2725' | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| Znu Stg / III | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2376 | Class C: Retarder, Fluid Loss, Defoamer |
| 4.5 in | LEAD | 500 | 13.5 | 1.85 | 8392' - 16350' | 930 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent |

Design B - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 9293' | 8.6 - 10. | Cut-Brine |
| 9293' - 16350' | 10.0 - 11. | OBM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

| | Y or N |
|--|--------|
| Is easing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is easing API approved? If no, attach easing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above easing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, easing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |
| | |

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| Casing Program Design A | | | | | | BLM Minimum Safety Factors | 1.125 | 1.0 | 1.6 Dry 1.8 Wet | 1.6 Dry 1.8 Wet |
|-------------------------|-----------|--------|---------|--------|---------|-------------------------------|-------------|----------|--------------------|--------------------|
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 8392' | 8298' | 7" 26# P110 LTC | 1.44 | 2.31 | 3.18 | 3.80 |
| Liner | 6.125" | 8192' | 8131' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.07 | 3.83 |

Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description | | | |
|---------------|--------------------|---------|------------|-----------------------------|----------------|------------------------|----------|---|--|--|--|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM | | | |
| 13.575 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 10076 | Class C: Retarder | | | |
| 9.625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM | | | |
| 9.025 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2370 | Class C: Retarder | | | |
| 1st Stg 7 in | LEAD | 280 | 12.5 | 2.12 | 2725' - 5897' | 600 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| 1st Stg / III | TAIL | 400 | 15.6 | 1.18 | 5897' - 8392' | 472 | 2370 | Class H: Retarder, Fluid Loss, Defoamer | | | |
| | 7" DV Tool @ 2725' | | | | | | | | | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| 2 nd Stg / In | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2370 | Class C: Retarder, Fluid Loss, Defoamer | | | |
| 4.5 in | LEAD | 520 | 13.5 | 1.85 | 8192' - 16350' | 970 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent | | | |

Design A - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 8392' | 8.6 - 10. | Cut-Brine |
| 8392' - 16350' | 10.0 - 11 | ORM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

| | Y or N |
|--|--------|
| Is casing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is casing API approved? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| Casing Program Design B | | | | | BLM Minimum Safety Factors | 1.125 | 1.0 | 1.6 Dry 1.8 Wet | 1.6 Dry 1.8 Wet | |
|-------------------------|-----------|--------|---------|--------|-------------------------------|---------------------|-------------|--------------------|--------------------|--------------------|
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 9293' | 8871' | 7" 26# P110 LTC | 1.35 | 2.16 | 2.87 | 3.44 |
| Liner | 6.125" | 8392' | 8298' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.15 | 3.93 |

Design B - Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description | | | |
|----------------|--------------------|---------|------------|-----------------------------|----------------|------------------------|----------|---|--|--|--|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM | | | |
| 13.575 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 10076 | Class C: Retarder | | | |
| 9,625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM | | | |
| 9.025 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2376 | Class C: Retarder | | | |
| 1st Stg 7 in | LEAD | 360 | 12.5 | 2.12 | 2725' - 6797' | 770 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| 1st Stg / III | TAIL | 400 | 15.6 | 1.18 | 6797' - 9293' | 472 | 2376 | Class H: Retarder, Fluid Loss, Defoamer | | | |
| | 7" DV Tool @ 2725' | | | | | | | | | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| Ziid Stg / iii | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2370 | Class C: Retarder, Fluid Loss, Defoamer | | | |
| 4.5 in | LEAD | 500 | 13.5 | 1.85 | 8392' - 16350' | 930 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent | | | |

Design B - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 9293' | 8.6 - 10. | Cut-Brine |
| 9293' - 16350' | 10.0 - 11. | OBM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

| | Y or N |
|--|--------|
| Is casing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is casing API approved? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |
| | |

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| Casing Program Design A | | | | | | BLM Minimum Safety Factors | 1.125 | 1.0 | 1.6 Dry 1.8 Wet | 1.6 Dry 1.8 Wet |
|-------------------------|-----------|--------|---------|--------|---------|-------------------------------|-------------|----------|--------------------|--------------------|
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 8392' | 8298' | 7" 26# P110 LTC | 1.44 | 2.31 | 3.18 | 3.80 |
| Liner | 6.125" | 8192' | 8131' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.07 | 3.83 |

Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description | | | |
|----------------|--------------------|---------|------------|-----------------------------|----------------|------------------------|----------|---|--|--|--|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM | | | |
| 13.373 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 100% | Class C: Retarder | | | |
| 9.625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM | | | |
| 9.023 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2376 | Class C: Retarder | | | |
| 1st Stg 7 in | LEAD | 280 | 12.5 | 2.12 | 2725' - 5897' | 600 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| 1st Stg / III | TAIL | 400 | 15.6 | 1.18 | 5897' - 8392' | 472 | 2370 | Class H: Retarder, Fluid Loss, Defoamer | | | |
| | 7" DV Tool @ 2725' | | | | | | | | | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer | | | |
| Ziiu Stg / iii | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2370 | Class C: Retarder, Fluid Loss, Defoamer | | | |
| 4.5 in | LEAD | 520 | 13.5 | 1.85 | 8192' - 16350' | 970 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent | | | |

Design A - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 8392' | 8.6 - 10. | Cut-Brine |
| 8392' - 16350' | 10.0 - 11. | OBM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

| | Y or N |
|--|--------|
| Is easing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is casing API approved? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| Casing Program Design B | | | | | BLM Minimum Safety Factors | 1.125 | 1.0 | 1.6 Dry 1.8 Wet | 1.6 Dry 1.8 Wet | |
|-------------------------|-----------|--------|---------|--------|-------------------------------|---------------------|-------------|--------------------|--------------------|--------------------|
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 9293' | 8871' | 7" 26# P110 LTC | 1.35 | 2.16 | 2.87 | 3.44 |
| Liner | 6.125" | 8392' | 8298' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.15 | 3.93 |

Design B - Cement Program

| Design B - Centent i rugi ann | | | | | | | | |
|-------------------------------|------|---------|------------|-----------------------------|----------------|------------------------|----------|---|
| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description |
| 13.375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM |
| | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 100% | Class C: Retarder |
| 9.625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM |
| | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2376 | Class C: Retarder |
| 1st Stg 7 in | LEAD | 360 | 12.5 | 2.12 | 2725' - 6797' | 770 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| | TAIL | 400 | 15.6 | 1.18 | 6797' - 9293' | 472 | 2370 | Class H: Retarder, Fluid Loss, Defoamer |
| 7" DV Tool @ 2725' | | | | | | | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2570 | Class C: Retarder, Fluid Loss, Defoamer |
| 4.5 in | LEAD | 500 | 13.5 | 1.85 | 8392' - 16350' | 930 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent |

Design B - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 9293' | 8.6 - 10. | Cut-Brine |
| 9293' - 16350' | 10.0 - 11. | OBM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

| | Y or N |
|--|--------|
| Is easing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is easing API approved? If no, attach easing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50° above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |
| | |

Mewbourne Oil Company, Iceman 24/23 Fed Com 712H Sec 24, T23S, R26E

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| | | | | | | BLM Minimum Safety Factors | 1.125 | 1.0 | 1.6 Dry 1.8 Wet | 1.6 Dry 1.8 Wet |
|------------|-----------|--------|---------|--------|---------|-------------------------------|-------------|----------|--------------------|--------------------|
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 8392' | 8298' | 7" 26# P110 LTC | 1.44 | 2.31 | 3.18 | 3.80 |
| Liner | 6.125" | 8192' | 8131' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.07 | 3.83 |

Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description |
|----------------|------|---------|------------|-----------------------------|----------------|------------------------|----------|---|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM |
| 13.373 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 100% | Class C: Retarder |
| 9.625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM |
| 9.023 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2376 | Class C: Retarder |
| 1st Stg 7 in | LEAD | 280 | 12.5 | 2.12 | 2725' - 5897' | 600 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| 1st Stg / III | TAIL | 400 | 15.6 | 1.18 | 5897' - 8392' | 472 | 2370 | Class H: Retarder, Fluid Loss, Defoamer |
| | | | | | 7" DV | Tool @ 2725' | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| Ziiu Stg / iii | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2370 | Class C: Retarder, Fluid Loss, Defoamer |
| 4.5 in | LEAD | 520 | 13.5 | 1.85 | 8192' - 16350' | 970 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent |

Design A - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 8392' | 8.6 - 10. | Cut-Brine |
| 8392' - 16350' | 10.0 - 11. | OBM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | • ` ` ′ | | Yeso | • ` ` ′ | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

| | Y or N |
|--|--------|
| Is casing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is casing API approved? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |

Mewbourne Oil Company, Iceman 24/23 Fed Com 712H Sec 24, T23S, R26E

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| | | Casing Prog | ram Design B | | | BLM Minimum Safety | 1.125 | 1.0 | 1.6 Dry | 1.6 Dry |
|------------|-----------|-------------|--------------|--------|---------|---------------------|-------------|----------|---------------|---------|
| | | Cuome 110g | rum Design D | | | Factors | 11125 | 1.0 | 1.8 Wet | 1.8 Wet |
| String | Hole Size | Top MD | Top TVD | Bot MD | Bot TVD | Csg. Size | SF Collapse | SF Burst | SF Jt Tension | SF Body |
| s | | | | | | | | | | Tension |
| Surface | 17.5" | 0' | 0' | 500' | 500' | 13.375" 48# H40 STC | 3.44 | 7.74 | 13.42 | 22.54 |
| Int | 12.25" | 0' | 0' | 1795' | 1795' | 9.625" 36# J55 LTC | 2.12 | 3.70 | 7.01 | 8.73 |
| Production | 8.75" | 0' | 0' | 9293' | 8871' | 7" 26# P110 LTC | 1.35 | 2.16 | 2.87 | 3.44 |
| Liner | 6.125" | 8392' | 8298' | 16350' | 8871' | 4.5" 13.5# P110 LTC | 2.10 | 2.45 | 3.15 | 3.93 |

Design B - Cement Program

| Casing | | # Sacks | Wt. lb/gal | Yield ft ³ /sack | тос/вос | Volume ft ³ | % Excess | Slurry Description |
|---------------|------|---------|------------|-----------------------------|----------------|------------------------|----------|---|
| 13,375 in | LEAD | 210 | 12.5 | 2.12 | 0' - 313' | 450 | 100% | Class C: Salt, Gel, Extender, LCM |
| 13.573 III | TAIL | 200 | 14.8 | 1.34 | 313' - 500' | 268 | 10076 | Class C: Retarder |
| 9.625 in | LEAD | 210 | 12.5 | 2.12 | 0' - 1125' | 450 | 25% | Class C: Salt, Gel, Extender, LCM |
| 9.025 III | TAIL | 200 | 14.8 | 1.34 | 1125' - 1795' | 268 | 2370 | Class C: Retarder |
| 1st Stg 7 in | LEAD | 360 | 12.5 | 2.12 | 2725' - 6797' | 770 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| 1st Stg / iii | TAIL | 400 | 15.6 | 1.18 | 6797' - 9293' | 472 | 2376 | Class H: Retarder, Fluid Loss, Defoamer |
| | | | | | 7" DV | Tool @ 2725' | | |
| 2nd Stg 7 in | LEAD | 50 | 12.5 | 2.12 | 1595' - 2104' | 110 | 25% | Class C: Salt, Gel, Extender, LCM, Defoamer |
| 2nd Stg / m | TAIL | 100 | 14.8 | 1.34 | 2104' - 2725' | 134 | 2370 | Class C: Retarder, Fluid Loss, Defoamer |
| 4.5 in | LEAD | 500 | 13.5 | 1.85 | 8392' - 16350' | 930 | 25% | Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent |

Design B - Mud Program

| Depth | Mud Wt | Mud Type |
|----------------|------------|-------------|
| | 8.4 - 8.6 | |
| 0' - 500' | 8.4 - 8.6 | Fresh Water |
| 500' - 1795' | 9.5 - 10.2 | Brine |
| 1795' - 9293' | 8.6 - 10. | Cut-Brine |
| 9293' - 16350' | 10.0 - 11. | OBM |

Geology

| Formation | Est. Top (TVD) | Mineral Resources | Formation | Est. Top (TVD) | Mineral Resources |
|--------------|----------------|-------------------|---------------------|----------------|-------------------|
| Rustler | | | Yeso | | |
| Castile | | | Delaware (Lamar) | 1870' | Oil/Natural Gas |
| Salt Top | 575' | None | Bell Canyon | 1950' | Oil/Natural Gas |
| Salt Base | 1642' | None | Cherry Canyon | 2620' | Oil/Natural Gas |
| Yates | | | Manzanita Marker | 2759' | Oil/Natural Gas |
| Seven Rivers | | | Basal Brushy Canyon | 4934' | Oil/Natural Gas |
| Queen | | | Bone Spring | 5303' | Oil/Natural Gas |
| Capitan | | | 1st Bone Spring | 6331' | Oil/Natural Gas |
| Grayburg | | | 2nd Bone Spring | 6796' | Oil/Natural Gas |
| San Andres | | | 3rd Bone Spring | 8401' | Oil/Natural Gas |
| Glorieta | | | Wolfcamp | 8743' | Oil/Natural Gas |

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

| | Y or N |
|--|--------|
| Is easing new? If used, attach certification as required in Onshore Order #1 | Y |
| Is casing API approved? If no, attach casing specification sheet. | Y |
| Is premium or uncommon casing planned? If yes attach casing specification sheet. | N |
| Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). | Y |
| Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? | Y |
| | |
| Is well located within Capitan Reef? | N |
| If yes, does production casing cement tie back a minimum of 50' above the Reef? | |
| Is well within the designated 4 string boundary. | N |
| | |
| Is well located in SOPA but not in R-111-Q? | N |
| If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? | |
| | |
| Is well located in R-111-Q and SOPA? | N |
| If yes, are the first three strings cemented to surface? | |
| Is 2 nd string set 100' to 600' below the base of salt? | |
| Is an open annulus used to satisfy R-111-Q? If yes, see cement design. | |
| Is an engineered weak point used to satisfy R-111-Q? | |
| If yes, at what depth is the weak point planned? | |
| | |
| Is well located in high Cave/Karst? | Y |
| If yes, are there two strings cemented to surface? | Y |
| (For 2 string wells) If yes, is there a contingency casing if lost circulation occurs? | |
| | |
| Is well located in critical Cave/Karst? | N |
| If yes, are there three strings cemented to surface? | |
| | |

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #712H Sec 24, T23S, R26E

SHL: 1960' FNL & 260' FEL (Sec 24) BHL: 800' FNL & 2342' FEL (Sec 23)

Plan: Design #1

Standard Planning Report

13 June, 2024

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Iceman 24/23 Fed Com #712H

Well: Sec 24, T23S, R26E

Design: Design #1

Wellbore:

BHL: 800' FNL & 2342' FEL (Sec 23)

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #712H

Original Well @ 3250.0usft Original Well @ 3250.0usft

Grid

Minimum Curvature

Project Eddy County, New Mexico NAD 83

Map System: US State Plane 1983
Geo Datum: North American Datum 1983

Map Zone: New Mexico Eastern Zone

System Datum: Gro

Ground Level

Site Iceman 24/23 Fed Com #712H

 Site Position:
 Northing:
 469,984.50 usft
 Latitude:
 32.2920257

 From:
 Map
 Easting:
 570,588.90 usft
 Longitude:
 -104.2386691

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 "

Well Sec 24, T23S, R26E

 Well Position
 +N/-S
 0.0 usft
 Northing:
 469,984.50 usft
 Latitude:
 32.2920257

 +E/-W
 0.0 usft
 Easting:
 570,588.90 usft
 Longitude:
 -104.2386691

Position Uncertainty 0.0 usft Wellhead Elevation: 3,250.0 usft Ground Level: 3,222.0 usft

Grid Convergence: 0.05 $^{\circ}$

Wellbore BHL: 800' FNL & 2342' FEL (Sec 23)

 Magnetics
 Model Name
 Sample Date
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 IGRF2010
 12/31/2014
 7.46
 60.05
 48,206.96932161

Design #1

Audit Notes:

Version:Phase:PROTOTYPETie On Depth:0.0

 Vertical Section:
 Depth From (TVD) (usft)
 +N/-S (usft)
 +E/-W (usft)
 Direction (usft)

 0.0
 0.0
 0.0
 279.02

Plan Survey Tool Program Date 6/13/2024

Depth From Depth To

(usft) (usft) Survey (Wellbore) Tool Name Remarks

1 0.0 16,350.0 Design #1 (BHL: 800' FNL & 2342

Plan Sections Vertical Build Measured Dogleg Turn +N/-S Depth Inclination Azimuth Depth +E/-W Rate Rate Rate TFO (usft) (°) (°) (usft) (usft) (usft) (°/100usft) (°/100usft) (°/100usft) Target (°) 0.0 0.00 0.00 0.0 0.0 0.0 0.00 0.00 0.00 0.00 600.0 0.00 0.00 600.0 0.0 0.0 0.00 0.00 0.00 0.00 1,065.2 9.30 12.32 1,063.2 2.00 2.00 36.8 8.0 0.00 12 32 7,927.2 9.30 12.32 7,834.8 1,120.7 244.7 0.00 0.00 0.00 0.00 8,392.4 0.00 0.00 8,298.0 1,157.5 252.7 2.00 -2.00 0.00 180,00 KOP: 800' FNL & 10' I 9,301.2 90.87 270.11 8,871.0 1,158.6 -329.1 10.00 10.00 0.00 -89.89 16,350.0 90.87 270.11 8,764.0 1,171.5 -7,377.0 0.00 0.00 0.00 0.00 BHL: 800' FNL & 2342

Hobbs Database: Company:

Project:

Site:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83

Iceman 24/23 Fed Com #712H

Well: Sec 24, T23S, R26E Wellbore:

BHL: 800' FNL & 2342' FEL (Sec 23)

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #712H

Original Well @ 3250.0usft Original Well @ 3250.0usft

| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
|-----------------------------|--------------------|----------------|-----------------------------|-----------------|-----------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| SHL: 1960' | FNL & 260' FEL (| Sec 24) | | | | | | | |
| 100.0 | 0.00 | 0.00 | 100.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 200.0 | 0.00 | 0.00 | 200.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 300.0 | 0.00 | 0.00 | 300.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 400.0 | 0.00 | 0.00 | 400.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 500.0 | 0.00 | 0.00 | 500.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 600.0 | 0.00 | 0.00 | 600.0 | 0.0 | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 |
| 700.0 | 2.00 | 12.32 | 700.0 | 1.7 | 0.4 | -0.1 | 2.00 | 2.00 | 0.00 |
| 800.0 | 4.00 | 12.32 | 799.8 | 6.8 | 1.5 | -0.4 | 2.00 | 2.00 | 0.00 |
| 900.0 | 6.00 | 12.32 | 899.5 | 15.3 | 3.3 | -0.9 | 2.00 | 2.00 | 0.00 |
| 1,000.0 | 8.00 | 12.32 | 998.7 | 27.2 | 5.9 | -1.6 | 2.00 | 2.00 | 0.00 |
| 1,065.2 | 9.30 | 12.32 | 1,063.2 | 36.8 | 8.0 | -2.2 | 2.00 | 2.00 | 0.00 |
| 1,100.0 | 9.30 | 12.32 | 1,097.5 | 42.3 | 9.2 | -2.2 -2.5 | 0.00 | 0.00 | 0.00 |
| 1,100.0 | 9.30 | 12.32 | 1,196.2 | 58.1 | 12.7 | -2.3 -3.4 | 0.00 | 0.00 | 0.00 |
| 1,200.0 | 9.30 9.30 | 12.32 | 1,196.2 | 73.9 | 12.7 | -3.4 -4.3 | 0.00 | 0.00 | 0.00 |
| 1 400 0 | 0.20 | 40.00 | | 90.7 | 10.6 | E O | 0.00 | 0.00 | 0.00 |
| 1,400.0 | 9.30 | 12.32 | 1,393.6 | 89.7 | 19.6 | -5.3 | 0.00 | 0.00 | 0.00 |
| 1,500.0 | 9.30 | 12.32 | 1,492.2 | 105.5 | 23.0 | -6.2 | 0.00 | 0.00 | 0.00 |
| 1,600.0 | 9.30 | 12.32 | 1,590.9 | 121.3 | 26.5 | -7.1 | 0.00 | 0.00 | 0.00 |
| 1,700.0 | 9.30 | 12.32 | 1,689.6 | 137.1 | 29.9 | -8.1 | 0.00 | 0.00 | 0.00 |
| 1,800.0 | 9.30 | 12.32 | 1,788.3 | 152.9 | 33.4 | -9.0 | 0.00 | 0.00 | 0.00 |
| 1,900.0 | 9,30 | 12,32 | 1,887.0 | 168.7 | 36.8 | -9.9 | 0.00 | 0.00 | 0.00 |
| 2,000.0 | 9,30 | 12,32 | 1,985.7 | 184.5 | 40,3 | -10,8 | 0.00 | 0,00 | 0,00 |
| 2,100.0 | 9,30 | 12,32 | 2,084.3 | 200.3 | 43.7 | -11.8 | 0.00 | 0,00 | 0,00 |
| 2,200.0 | 9.30 | 12,32 | 2,183.0 | 216.1 | 47.2 | -12.7 | 0.00 | 0,00 | 0.00 |
| 2,300.0 | 9,30 | 12,32 | 2,281,7 | 231,9 | 50,6 | -13,6 | 0,00 | 0.00 | 0,00 |
| 2,400.0 | 9.30 | 12.32 | 2,380.4 | 247.7 | 54.1 | -14.6 | 0.00 | 0.00 | 0.00 |
| 2,500.0 | 9.30 | 12.32 | 2,479.1 | 263.4 | 57.5 | -15.5 | 0.00 | 0.00 | 0.00 |
| 2,600.0 | 9.30 | 12.32 | 2,577.8 | 279.2 | 61.0 | -16.4 | 0.00 | 0.00 | 0.00 |
| 2,700.0 | 9.30 | 12.32 | 2,676.5 | 295.0 | 64.4 | -17.3 | 0.00 | 0.00 | 0.00 |
| 2,800.0 | 9.30 | 12.32 | 2,775.1 | 310.8 | 67.9 | -18.3 | 0.00 | 0.00 | 0.00 |
| 2,900.0 | 9.30 | 12.32 | 2,873.8 | 326.6 | 71.3 | -19.2 | 0.00 | 0.00 | 0.00 |
| 3,000.0 | 9.30 | 12.32 | 2,972.5 | 342.4 | 74.8 | -20.1 | 0.00 | 0.00 | 0.00 |
| 3,100.0 | 9.30 | 12.32 | 3,071.2 | 358.2 | 78.2 | -21.1 | 0.00 | 0.00 | 0.00 |
| 3,200.0 | 9.30 | 12.32 | 3,169.9 | 374.0 | 81.7 | -22.0 | 0.00 | 0.00 | 0.00 |
| 3,300.0 | 9.30 | 12.32 | 3,268.6 | 389.8 | 85.1 | -22.9 | 0.00 | 0.00 | 0.00 |
| 3,400.0 | 9.30 | 12.32 | 3,367.2 | 405.6 | 88.6 | -23.8 | 0.00 | 0.00 | 0.00 |
| 3,500.0 | 9.30 | 12.32 | 3,465.9 | 421.4 | 92.0 | -24.8 | 0.00 | 0.00 | 0.00 |
| 3,600.0 | 9.30 | 12.32 | 3,564.6 | 437.2 | 95.4 | -25.7 | 0.00 | 0.00 | 0.00 |
| 3,700.0 | 9.30 | 12.32 | 3,663.3 | 453.0 | 98.9 | -26.6 | 0.00 | 0.00 | 0.00 |
| 3,800.0 | 9.30 | 12.32 | 3,762.0 | 468.8 | 102.3 | - 27.6 | 0.00 | 0.00 | 0.00 |
| 3,900.0 | 9.30 | 12.32 | 3,860.7 | 484.6 | 105.8 | -28.5 | 0.00 | 0.00 | 0.00 |
| 4,000.0 | 9.30 | 12.32 | 3,959.3 | 500.4 | 109.2 | -29.4 | 0.00 | 0.00 | 0.00 |
| 4,100.0 | 9.30 | 12.32 | 4,058.0 | 516.2 | 112.7 | -30.3 | 0.00 | 0.00 | 0.00 |
| 4,200.0 | 9.30 | 12.32 | 4,156.7 | 532.0 | 116.1 | -31.3 | 0.00 | 0.00 | 0.00 |
| 4,300.0 | 9.30 | 12.32 | 4,255.4 | 547.8 | 119.6 | -32.2 | 0.00 | 0.00 | 0.00 |
| 4,400.0 | 9.30 | 12.32 | 4,354.1 | 563.6 | 123.0 | -33.1 | 0.00 | 0.00 | 0.00 |
| 4,500.0 | 9.30 | 12.32 | 4,452.8 | 579.4 | 126.5 | -34.1 | 0.00 | 0.00 | 0.00 |
| 4,600.0 | 9.30 | 12.32 | 4,551.5 | 595.1 | 129.9 | -35.0 | 0.00 | 0.00 | 0.00 |
| 4,700.0 | 9.30 | 12.32 | 4,650.1 | 610.9 | 133.4 | -35.9 | 0.00 | 0.00 | 0.00 |
| 4,800.0 | 9.30 | 12.32 | 4,748.8 | 626.7 | 136.8 | -36.8 | 0.00 | 0.00 | 0.00 |
| 4,900.0 | 9.30 | 12.32 | 4,847.5 | 642.5 | 140.3 | -37.8 | 0.00 | 0.00 | 0.00 |
| 5,000.0 | 9.30 | 12.32 | 4,946.2 | 658.3 | 143.7 | -38.7 | 0.00 | 0.00 | 0.00 |

Database: Hobbs

Company: Mewbourne Oil Company

Project: Eddy County, New Mexico NAD 83
Site: Iceman 24/23 Fed Com #712H

Well: Sec 24, T23S, R26E

Wellbore: BHL: 800' FNL & 2342' FEL (Sec 23)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #712H

Original Well @ 3250.0usft Original Well @ 3250.0usft

Grid

| Planned Survey | | | | | | | | | |
|-----------------------------|---------------------------|------------------|-----------------------------|--------------------|-----------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 5,200.0 5,300.0 | 9.30 9.30 | 12.32 12.32 | 5,143.6 5,242.2 | 689.9 705.7 | 150.6 154.1 | -40.5 -41.5 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 |
| 5,400.0 | 9.30 | 12.32 | 5,340.9 | 721.5 | 157.5 | -42.4 | 0.00 | 0.00 | 0.00 |
| 5,500.0 | 9.30 | 12.32 | 5,439.6 | 737.3 | 161.0 | -43.3 | 0.00 | 0.00 | 0.00 |
| 5,600.0 | 9.30 | 12.32 | 5,538.3 | 753.1 | 164.4 | -44.3 | 0.00 | 0.00 | 0.00 |
| 5,700.0 5,800.0 | 9.30 9.30 | 12.32 12.32 | 5,637.0 5,735.7 | 768.9 784.7 | 167.9 171.3 | -45.2 -46.1 | 0.00 0.00 | 0.00 0.00 | 0.00 0.00 |
| 5,900.0 | 9.30 | 12.32 | 5,834.4 | 800.5 | 174.8 | -47.0 | 0.00 | 0.00 | 0.00 |
| 6,000.0 | 9.30 | 12.32 | 5,933.0 | 816.3 | 178.2 | -48.0 | 0.00 | 0.00 | 0.00 |
| 6,100.0 | 9.30 | 12.32 | 6,031.7 | 832.1 | 181.7 | -48.9 | 0.00 | 0.00 | 0.00 |
| 6,200.0 | 9.30 | 12.32 | 6,130.4 | 847.9 | 185.1 | -49.8 | 0.00 | 0.00 | 0.00 |
| 6,300.0 | 9.30 | 12.32 | 6,229.1 | 863.7 | 188.6 | -50.8 | 0.00 | 0.00 | 0.00 |
| 6,400.0 | 9.30 | 12.32 | 6,327.8 | 879.5 | 192.0 | -51.7 | 0.00 | 0.00 | 0.00 |
| 6,500.0 | 9.30 | 12.32 | 6,426.5 | 895.3 | 195.4 | -52.6 | 0.00 | 0.00 | 0.00 |
| 6,600.0 | 9.30 | 12.32 | 6,525.1 | 911.1 | 198.9 | -53.5 | 0.00 | 0.00 | 0.00 |
| 6,700.0 | 9.30 | 12.32 | 6,623.8 | 926.8 | 202.3 | -54.5 | 0.00 | 0.00 | 0.00 |
| 6,800.0 | 9.30 | 12.32 | 6,722.5 | 942.6 | 205.8 | -55.4 | 0.00 | 0.00 | 0.00 |
| 6,900.0 | 9.30 | 12.32 | 6,821.2 | 958.4 | 209.2 | -56.3 | 0.00 | 0.00 | 0.00 |
| 7,000.0 | 9.30 | 12.32 | 6,919.9 | 974.2 | 212.7 | -57.3 | 0.00 | 0.00 | 0.00 |
| 7,100.0 | 9.30 | 12.32 | 7,018.6 | 990.0 | 216.1 | -58.2 | 0.00 | 0.00 | 0.00 |
| 7,200.0 | 9.30 | 12.32 | 7,117.3 | 1,005.8 | 219.6 | -59.1 | 0.00 | 0.00 | 0.00 |
| 7,300.0 | 9.30 | 12.32 | 7,215.9 | 1,021.6 | 223.0 | -60.0 | 0.00 | 0.00 | 0.00 |
| 7,400.0 | 9.30 | 12.32 | 7,314.6 | 1,037.4 | 226.5 | -61.0 | 0.00 | 0.00 | 0.00 |
| 7,500.0 | 9.30 | 12.32 | 7,413.3 | 1,053.2 | 229.9 | -61.9 | 0.00 | 0.00 | 0.00 |
| 7,600.0 | 9.30 | 12.32 | 7,512.0 | 1,069.0 | 233.4 | -62.8 | 0.00 | 0.00 | 0.00 |
| 7,700.0 | 9.30 | 12.32 | 7,610.7 | 1,084.8 | 236.8 | -63.8 | 0.00 | 0.00 | 0.00 |
| 7,800.0 | 9.30 | 12.32 | 7,709.4 | 1,100.6 | 240.3 | -64.7 | 0.00 | 0.00 | 0.00 |
| 7,900.0 | 9.30 | 12.32 | 7,808.0 | 1,116.4 | 243.7 | -65.6 | 0.00 | 0.00 | 0.00 |
| 7,927.2 | 9.30 | 12.32 | 7,834.8 | 1,120.7 | 244.7 | -65.9 | 0.00 | 0.00 | 0.00 |
| 8,000.0 | 7.85 | 12.32 | 7,906.9 | 1,131.3 | 247.0 | -66.5 | 2.00 | -2.00 | 0.00 |
| 8,100.0 | 5.85 | 12.32 | 8,006.2 | 1,142.9 | 249.5 | - 67.2 | 2.00 | -2.00 | 0.00 |
| 8,200.0 | 3.85 | 12.32 | 8,105.8 | 1,151.2 | 251.3 | -67.7 | 2.00 | -2.00 | 0.00 |
| 8,300.0 8,392.4 | 1.85 0.00 | 12.32 0.00 | 8,205.7 8,298.0 | 1,156.0 1,157.5 | 252.4 252.7 | -67.9 -68.0 | 2.00 2.00 | -2.00 -2.00 | 0.00 0.00 |
| | NL & 10' FEL (Se | | 5,250.0 | ., | | 30.0 | 2.00 | 2.00 | 5.55 |
| 8,400.0 | 0.76 | 270.11 | 8,305.6 | 1,157.5 | 252.6 | -68.0 | 10.00 | 10.00 | 0.00 |
| 8,450.0 | 5.76 | 270.11 | 8,355.5 | 1,157.5 | 249.8 | -65.2 | 10.00 | 10.00 | 0.00 |
| 8,500.0 | 10.76 | 270.11 | 8,405.0 | 1,157.5 | 242.6 | -58.1 | 10.00 | 10.00 | 0.00 |
| 8,550.0 | 15.76 | 270.11 | 8,453.7 | 1,157.5 | 231.2 | -46.7 | 10.00 | 10.00 | 0.00 |
| 8,600.0 | 20.76 | 270.11 | 8,501.1 | 1,157.6 | 215.5 | -31.3 | 10.00 | 10.00 | 0.00 |
| 8,650.0 | 25.76 | 270.11 | 8,547.1 | 1,157.6 | 195.8 | -11.8 | 10.00 | 10.00 | 0.00 |
| 8,700.0 | 30.76 | 270.11 | 8,591.1 | 1,157.6 | 172.1 | 11.6 | 10.00 | 10.00 | 0.00 |
| 8,750.0 | 35.76 | 270.11 | 8,632.9 | 1,157.7 | 144.7 | 38.7 | 10.00 | 10.00 | 0.00 |
| 8,800.0 | 40.76 | 270.11 | 8,672.1 | 1,157.8 | 113.7 | 69.3 | 10.00 | 10.00 | 0.00 |
| 8,850.0 | 45.76 | 270.11 | 8,708.5 | 1,157.8 | 79.5 | 103.1 | 10.00 | 10.00 | 0.00 |
| 8,900.0 | 50.75 | 270.11 | 8,741.8 | 1,157.9 | 42.2 | 139.9 | 10.00 | 10.00 | 0.00 |
| 8,950.0 | 55.75 60.75 | 270.11 | 8,771.7 8,798.0 | 1,158.0 1,158.0 | 2.1 | 179.5 | 10.00 | 10.00 | 0.00 |
| 9,000.0 9,030.4 | 60.75 63.79 | 270.11 270.11 | 8,798.0 8,812.2 | 1,158.0 1,158.1 | -40.4 -67.3 | 221.5 248.1 | 10.00 10.00 | 10.00 10.00 | 0.00 0.00 |
| · · | 03.79 NL & 330' FEL (S | | 0,012.2 | 1, 130. 1 | -01.3 | ∠40. I | 10.00 | 10.00 | 0.00 |
| 9,050.0 | 65.75 | 270.11 | 8,820.5 | 1,158.1 | -85.0 | 265.6 | 10.00 | 10.00 | 0.00 |
| 9,100.0 | 70.75 | 270.11 | 8,839.0 | 1,158.2 | -131.4 | 311.5 | 10.00 | 10.00 | 0.00 |
| 9,150.0 | 75.75 | 270.11 | 8,853.4 | 1,158.3 | -179.3 | 358.8 | 10.00 | 10.00 | 0.00 |
| 9,200.0 | 80.75 | 270.11 | 8,863.6 | 1,158.4 | -228.2 | 407.1 | 10.00 | 10.00 | 0.00 |

Hobbs Database:

Company: Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Project: Iceman 24/23 Fed Com #712H Site:

Well: Sec 24, T23S, R26E BHL: 800' FNL & 2342' FEL (Sec 23)

Wellbore:

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #712H

Original Well @ 3250.0usft Original Well @ 3250.0usft

| ed Survey | | | | | | | | | |
|-----------------------------|-------------------------------------|----------------|-----------------------------|-----------------|----------------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
| 9,250.0 | 85.75 | 270.11 | 8,869.5 | 1,158.5 | -277.9 | 456.1 | 10.00 | 10.00 | 0.00 |
| 9,292.5 | 89.99 | 270.11 | 8,871.1 | 1,158.6 | -320.3 | 498.0 | 10.00 | 10.00 | 0.00 |
| LP: 800' FNL | . & 583' FEL (Se | c 24) | | | | | | | |
| 9,301.2 | 90.87 | 270.11 | 8,871.0 | 1,158.6 | -329.1 | 506.7 | 10.00 | 10.00 | 0.00 |
| 9,400.0 | 90.87 | 270.11 | 8,869.5 | 1,158.7 | -427.8 | 604.3 | 0.00 | 0.00 | 0.00 |
| 9,500.0 | 90.87 | 270.11 | 8,868.0 | 1,158.9 | -527.8 | 703.0 | 0.00 | 0.00 | 0.00 |
| 9,600.0 | 90.87 | 270.11 | 8,866.5 | 1,159.1 | -627.8 | 801.8 | 0.00 | 0.00 | 0.00 |
| 9,700.0 | 90.87 | 270.11 | 8,864.9 | 1,159.3 | -727.8 | 900.6 | 0.00 | 0.00 | 0.00 |
| 9,800.0 | 90.87 | 270.11 | 8,863.4 | 1,159.5 | -827.8 | 999.4 | 0.00 | 0.00 | 0.00 |
| 9,900.0 | 90.87 | 270.11 | 8,861.9 | 1,159.7 | -927.8 | 1,098.2 | 0.00 | 0.00 | 0.00 |
| 10,000.0 | 90.87 | 270.11 | 8,860.4 | 1,159.8 | -1,027.8 | 1,196.9 | 0.00 | 0.00 | 0.00 |
| 10,100.0 | 90.87 | 270.11 | 8,858.9 | 1,160.0 | -1,127.7 | 1,295.7 | 0.00 | 0.00 | 0.00 |
| 10,200.0 | 90.87 | 270.11 | 8,857.4 | 1,160.2 | -1,227.7 | 1,394.5 | 0.00 | 0.00 | 0.00 |
| 10,300.0 | 90.87 | 270.11 | 8,855.8 | 1,160.4 | -1,327.7 | 1,493.3 | 0.00 | 0.00 | 0.00 |
| 10,400.0 | 90.87 | 270.11 | 8,854.3 | 1,160.6 | -1,427.7 | 1,592.1 | 0.00 | 0.00 | 0.00 |
| 10,500.0 | 90.87 | 270.11 | 8,852.8 | 1,160.8 | -1,527.7 | 1,690.8 | 0.00 | 0.00 | 0.00 |
| 10.600.0 | 90.87 | 270.11 | 8,851.3 | 1,161.0 | -1,627.7 | 1,789.6 | 0.00 | 0.00 | 0.00 |
| 10,700.0 | 90.87 | 270.11 | 8,849.8 | 1,161.1 | -1,727.7 | 1,888.4 | 0.00 | 0.00 | 0.00 |
| 10,800.0 | 90.87 | 270.11 | 8,848.2 | 1,161.3 | -1,827.7 | 1,987.2 | 0.00 | 0.00 | 0.00 |
| 10,900.0 | 90.87 | 270.11 | 8,846.7 | 1,161.5 | -1,927.7 -1,927.7 | 2,086.0 | 0.00 | 0.00 | 0.00 |
| 11,000.0 | 90.87 | 270.11 | 8,845.2 | 1,161.7 | -2,027.6 | 2,184.7 | 0.00 | 0.00 | 0.00 |
| 11,100.0 | 90.87 | 270.11 | 8,843.7 | 1,161.9 | -2,127.6 | 2.283.5 | 0.00 | 0.00 | 0.00 |
| 11,100.0 | 90.87 | 270.11 | 8,842.2 | 1,162.1 | -2,127.6 -2,227.6 | 2,283.3 | 0.00 | 0.00 | 0.00 |
| 11,300.0 | 90.87 | 270.11 | 8,840.7 | 1,162.1 | -2,327.6 | 2,382.3 | 0.00 | 0.00 | 0.00 |
| 11,400.0 | 90.87 | 270.11 | 8,839.1 | 1,162.4 | -2,427.6 | 2,579.9 | 0.00 | 0.00 | 0.00 |
| 11,500.0 | 90.87 | 270.11 | 8,837.6 | 1,162.4 | -2,527.6 | 2,678.6 | 0.00 | 0.00 | 0.00 |
| 11,600.0 | 90.87 | 270.11 | 8,836.1 | 1,162.8 | -2,627.6 | 2,777.4 | 0.00 | 0.00 | 0.00 |
| 11,700.0 | 90.87 | 270.11 | 8,834.6 | 1,163.0 | -2,727.6 | 2,876.2 | 0.00 | 0.00 | 0.00 |
| 11,800.0 | 90.87 | 270.11 | 8,833.1 | 1,163.2 | -2,827.5 | 2,975.0 | 0.00 | 0.00 | 0.00 |
| 11,900.0 | 90.87 | 270.11 | 8,831.6 | 1,163.3 | -2,927.5 | 3,073.8 | 0.00 | 0.00 | 0.00 |
| 12,000.0 | 90.87 | 270.11 | 8,830.0 | 1,163.5 | -3,027.5 | 3,172.5 | 0.00 | 0.00 | 0.00 |
| 12,100.0 | 90.87 | 270.11 | 8,828.5 | 1,163.7 | -3,127.5 | 3,271.3 | 0.00 | 0.00 | 0.00 |
| 12,200.0 | 90.87 | 270.11 | 8,827.0 | 1,163.9 | -3,227.5 | 3,370.1 | 0.00 | 0.00 | 0.00 |
| 12,300.0 | 90.87 | 270.11 | 8,825.5 | 1,164.1 | -3,327.5 | 3,468.9 | 0.00 | 0.00 | 0.00 |
| 12,400.0 | 90.87 | 270.11 | 8,824.0 | 1,164.3 | -3,427.5 | 3,567.7 | 0.00 | 0.00 | 0.00 |
| 12,500.0 | 90.87 | 270.11 | 8,822.4 | 1,164.4 | -3,527.5 | 3,666.4 | 0.00 | 0.00 | 0.00 |
| 12,600.0 | 90.87 | 270.11 | 8,820.9 | 1,164.6 | -3,627.5 | 3,765.2 | 0.00 | 0.00 | 0.00 |
| 12,700.0 | 90.87 | 270.11 | 8,819.4 | 1,164.8 | -3,727.4 | 3,864.0 | 0.00 | 0.00 | 0.00 |
| 12,800.0 | 90.87 | 270.11 | 8,817.9 | 1,165.0 | -3,827.4 | 3,962.8 | 0.00 | 0.00 | 0.00 |
| 12,900.0 | 90.87 | 270.11 | 8,816.4 | 1,165.2 | -3,927.4 | 4,061.6 | 0.00 | 0.00 | 0.00 |
| 13,000.0 | 90.87 | 270.11 | 8,814.9 | 1,165.4 | -4,027.4 | 4,160.3 | 0.00 | 0.00 | 0.00 |
| 13,100.0 | 90.87 | 270.11 | 8,813.3 | 1,165,5 | -4,127.4 | 4,259.1 | 0.00 | 0.00 | 0.00 |
| 13,100.0 | 90.87 | 270.11 | 8,811.8 | 1,165.7 | -4,227.4 | 4,357.9 | 0.00 | 0.00 | 0.00 |
| 13,300.0 | 90.87 | 270.11 | 8,810.3 | 1,165.7 | -4,327.4 | 4,456.7 | 0.00 | 0.00 | 0.00 |
| 13,400.0 | 90.87 | 270.11 | 8,808.8 | 1,166.1 | -4,427.4 | 4,555.5 | 0.00 | 0.00 | 0.00 |
| 13,500.0 | 90.87 | 270.11 | 8,807.3 | 1,166.3 | -4,527.3 | 4,654.2 | 0.00 | 0.00 | 0.00 |
| 13,600.0 | 90.87 | 270.11 | 8,805.7 | 1,166.5 | -4,627.3 | 4,753.0 | 0.00 | 0.00 | 0.00 |
| 13,700.0 | 90.87 | 270.11 | 8,804.2 | 1,166.6 | -4,027.3 -4,727.3 | 4,755.0 | 0.00 | 0.00 | 0.00 |
| 13,800.0 | 90.87 | 270.11 | 8,802.7 | 1,166.8 | -4,727.3 -4,827.3 | 4,950.6 | 0.00 | 0.00 | 0.00 |
| 13,900.0 | 90.87 | 270.11 | 8,801.2 | 1,167.0 | -4,927.3 | 5,049.4 | 0.00 | 0.00 | 0.00 |
| 14,000.0 | 90.87 | 270.11 | 8,799.7 | 1,167.2 | -5,027.3 | 5,148.1 | 0.00 | 0.00 | 0.00 |
| • | | | | | | | | | |
| 14,008.8 | 90.87 NL & 0' FEL (Se | 270.11 | 8,799.5 | 1,167.2 | -5,036.1 | 5,156.8 | 0.00 | 0.00 | 0.00 |

Hobbs Database: Company:

Project:

Site:

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #712H

Well: Sec 24, T23S, R26E

BHL: 800' FNL & 2342' FEL (Sec 23) Wellbore:

Design: Design #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

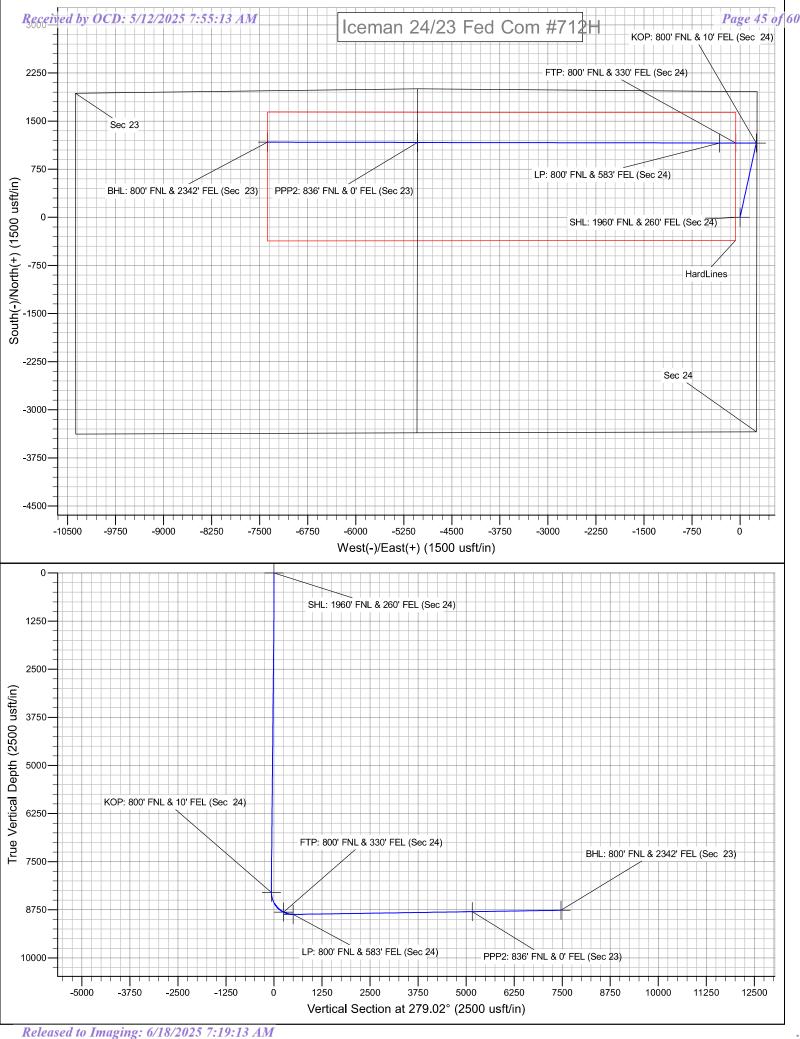
Site Iceman 24/23 Fed Com #712H

Original Well @ 3250.0usft Original Well @ 3250.0usft

Grid

| Measured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Vertical Section (usft) | Dogleg Rate (°/100usft) | Build Rate (°/100usft) | Turn Rate (°/100usft) |
|-----------------------------|--------------------|----------------|-----------------------------|-----------------|-----------------|-------------------------------|-------------------------------|------------------------------|-----------------------------|
| 14,100.0 | 90.87 | 270.11 | 8,798.2 | 1,167.4 | -5,127.3 | 5,246.9 | 0.00 | 0.00 | 0.00 |
| 14,200.0 | 90.87 | 270.11 | 8,796.6 | 1,167.6 | -5,227.3 | 5,345.7 | 0.00 | 0.00 | 0.00 |
| 14,300.0 | 90.87 | 270.11 | 8,795.1 | 1,167.7 | -5,327.3 | 5,444.5 | 0.00 | 0.00 | 0.00 |
| 14,400.0 | 90.87 | 270.11 | 8,793.6 | 1,167.9 | -5,427.2 | 5,543.3 | 0.00 | 0.00 | 0.00 |
| 14,500.0 | 90.87 | 270.11 | 8,792.1 | 1,168.1 | -5,527.2 | 5,642.0 | 0.00 | 0.00 | 0.00 |
| 14,600.0 | 90.87 | 270.11 | 8,790.6 | 1,168.3 | -5,627.2 | 5,740.8 | 0.00 | 0.00 | 0.00 |
| 14,700.0 | 90.87 | 270.11 | 8,789.0 | 1,168.5 | -5,727.2 | 5,839.6 | 0.00 | 0.00 | 0.00 |
| 14,800.0 | 90.87 | 270.11 | 8,787.5 | 1,168.7 | -5,827.2 | 5,938.4 | 0.00 | 0.00 | 0.00 |
| 14,900.0 | 90.87 | 270.11 | 8,786.0 | 1,168.8 | -5,927.2 | 6,037.2 | 0.00 | 0.00 | 0.00 |
| 15,000.0 | 90.87 | 270.11 | 8,784.5 | 1,169.0 | -6,027.2 | 6,135.9 | 0.00 | 0.00 | 0.00 |
| 15,100.0 | 90.87 | 270.11 | 8,783.0 | 1,169.2 | -6,127.2 | 6,234.7 | 0.00 | 0.00 | 0.00 |
| 15,200.0 | 90.87 | 270.11 | 8,781.5 | 1,169.4 | -6,227.1 | 6,333.5 | 0.00 | 0.00 | 0.00 |
| 15,300.0 | 90.87 | 270.11 | 8,779.9 | 1,169.6 | -6,327.1 | 6,432.3 | 0.00 | 0.00 | 0.00 |
| 15,400.0 | 90.87 | 270.11 | 8,778.4 | 1,169.8 | -6,427.1 | 6,531.0 | 0.00 | 0.00 | 0.00 |
| 15,500.0 | 90.87 | 270.11 | 8,776.9 | 1,169.9 | -6,527.1 | 6,629.8 | 0.00 | 0.00 | 0.00 |
| 15,600.0 | 90.87 | 270.11 | 8,775.4 | 1,170.1 | -6,627.1 | 6,728.6 | 0.00 | 0.00 | 0.00 |
| 15,700.0 | 90.87 | 270.11 | 8,773.9 | 1,170.3 | -6,727.1 | 6,827.4 | 0.00 | 0.00 | 0.00 |
| 15,800.0 | 90.87 | 270.11 | 8,772.3 | 1,170.5 | -6,827.1 | 6,926.2 | 0.00 | 0.00 | 0.00 |
| 15,900.0 | 90.87 | 270.11 | 8,770.8 | 1,170.7 | -6,927.1 | 7,024.9 | 0.00 | 0.00 | 0.00 |
| 16,000.0 | 90.87 | 270.11 | 8,769.3 | 1,170.9 | -7,027.1 | 7,123.7 | 0.00 | 0.00 | 0.00 |
| 16,100.0 | 90.87 | 270.11 | 8,767.8 | 1,171.0 | -7,127.0 | 7,222.5 | 0.00 | 0.00 | 0.00 |
| 16,200.0 | 90.87 | 270.11 | 8,766.3 | 1,171.2 | -7,227.0 | 7,321.3 | 0.00 | 0.00 | 0.00 |
| 16,300.0 | 90.87 | 270.11 | 8,764.8 | 1,171.4 | -7,327.0 | 7,420.1 | 0.00 | 0.00 | 0.00 |
| 16,350.0 | 90.87 | 270.11 | 8,764.0 | 1,171.5 | -7,377.0 | 7,469.4 | 0.00 | 0.00 | 0.00 |

| Design Targets | | | | | | | | | |
|---|------------------|-----------------|---------------|-----------------|-----------------|--------------------|-------------------|------------|--------------|
| Target Name - hit/miss target - Shape | Dip Angle (°) | Dip Dir. (°) | TVD (usft) | +N/-S (usft) | +E/-W (usft) | Northing (usft) | Easting (usft) | Latitude | Longitude |
| SHL: 1960' FNL & 260' F - plan hits target cent - Point | 0.00 er | 0.00 | 0.0 | 0.0 | 0.0 | 469,984.50 | 570,588.90 | 32.2920257 | -104.2386691 |
| KOP: 800' FNL & 10' FE - plan hits target cent - Point | 0.00 er | 0.00 | 8,298.0 | 1,157.5 | 252.7 | 471,142.00 | 570,841.60 | 32,2952069 | -104.2378480 |
| BHL: 800' FNL & 2342' F - plan hits target cent - Point | 0.00 er | 0.00 | 8,764.0 | 1,171.5 | -7,377.0 | 471,156.00 | 563,211.90 | 32.2952616 | -104.2625402 |
| PPP2: 836' FNL & 0' FEI - plan hits target cent - Point | 0.00 er | 0.00 | 8,799.5 | 1,167.2 | -5,036.1 | 471,151.71 | 565,552.80 | 32.2952453 | -104.2549643 |
| FTP: 800' FNL & 330' FE - plan hits target cent - Point | 0.00 er | 0.00 | 8,812.2 | 1,158.1 | -67.3 | 471,142.59 | 570,521.60 | 32.2952093 | -104.2388836 |
| LP: 800' FNL & 583' FEL - plan hits target cent - Point | 0.00 er | 0.00 | 8,871.1 | 1,158.6 | -320.3 | 471,143.05 | 570,268.60 | 32.2952112 | -104.2397024 |



Mewbourne Oil Company, Ice Man 24/23 Fed Com 712H Sec 24, T23S, R26E

SHL: 1960' FNL 260' FEL (Sec 24) BHL: 800' FNL 2342' FEL (Sec 23)

| Operator Name: | Property Name: | Well Number |
|-----------------------|-----------------------|-------------|
| Mewbourne Oil Company | Ice Man 24/23 Fed Com | 712H |

Kick Off Point (KOP)

| UL | Section | Township | Range | Lot | Feet | From N/S | Feet | From E/W | County |
|------------|----------|----------|-------|------------|------|----------|------|----------|--------|
| A | 24 | 23 | 26 | _ | 800' | FNL | 10' | FEL | Eddy |
| | Latitude | | | | NAD | | | | |
| 32.2952069 | | | | -104.23784 | 179 | | | 83 | |

First Take Point (FTP)

| UL | Section | Township | Range | Lot | Feet | From N/S | Feet | From E/W | County |
|------------|---------|----------|-------|------------|------|----------|-------|----------|--------|
| A | 24 | 23 | 26 | - | 800' | FNL | 330' | FEL | Eddy |
| | | Latitude | | | | Long | itude | | NAD |
| 32.2952087 | | | | -104.23883 | 359 | | | 83 | |

Last Take Point (LTP)

| Lust Tune I | Ome (EII | , | | | | | | | |
|-------------|----------|----------|-------|-----|------------|----------|-------|----------|--------|
| UL | Section | Township | Range | Lot | Feet | From N/S | Feet | From E/W | County |
| В | 23 | 23 | 26 | _ | 800' | FNL | 2342' | FEL | Eddy |
| | | Latitude | | | | Long | itude | | NAD |
| 32.2952641 | | | | | -104.26254 | 103 | | | 83 |

| 32.2952641 | -104.2625403 | 83 |
|--|--|-------------|
| Is this well the defining well for the Horizontal Is this well an infill well? N If infill is yes please provide API if available, C Spacing Unit. | Spacing Unit? Y Operator Name and well number for Defining well for Horizontal | |
| API# | | |
| Operator Name: | Property Name: | Well Number |
| | | |

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: MEWBOURNE OIL COMPANY **WELL NAME & NO.:** ICEMAN 24/23 FED COM 712H

APD ID: 10400099099

LOCATION: Section 24, T23S, R26E. NMP

COUNTY: Eddy County, New Mexico

COA

| H ₂ S | C | No | • | Yes |
|------------------|----------------------|-------------------|-------------------|----------------------------|
| Potash / | None | Secretary | C R-111-Q | Open Annulus |
| WIPP | | | | ☐ WIPP |
| Cave / Karst | C Low | Medium | • High | Critical |
| Wellhead | Conventional | Multibowl | Both | Diverter |
| Cementing | Primary Squeeze | Cont. Squeeze | EchoMeter | DV Tool |
| Special Req | Capitan Reef | Water Disposal | ▼ COM | Unit |
| Waste Prev. | © Self-Certification | Waste Min. Plan | C APD Submitted p | prior to 06/10/2024 |
| Additional | Flex Hose | Casing Clearance | Pilot Hole | Break Testing |
| Language | Four-String | Offline Cementing | Fluid-Filled | |

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H₂S) Drilling Plan shall be activated **AT SPUD**. As a result, the Hydrogen Sulfide area must meet **43 CFR 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING DESIGN

Primary Casing Design

- 1. The 13-3/8 inch surface casing shall be set at approximately 500 ft. (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of 8

- hours or 500 psi compressive strength, whichever is greater. (This is to include the lead cement)
- Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 psi compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 1,795 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.

Note: Excess cement is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

- ❖ In High Cave/Karst Areas if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. Operator has proposed to set 7 in. production casing at approximately 8,392 ft. (8,298) ft. TVD). The minimum required fill of cement behind the 7 in. production casing is:

Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.

Option 2 (Two-stage): Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
- 4. The minimum required fill of cement behind the 4-1/2 in. production liner is:
 - Cement should tie-back at least 100 feet into previous casing string. Operator shall provide method of verification.

Alternate Casing Design

- 1. The 13-3/8 inch surface casing shall be set at approximately 500 ft. (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> hours or 500 psi compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 psi compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 1,795 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - **Cement to surface.** If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to **cave/karst**.

Note: Excess cement is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. Operator has proposed to set 7 in. production casing at approximately 9,293 ft. (8,871 ft. TVD). The minimum required fill of cement behind the 7 in. production casing is:
 - Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
 - **Option 2 (Two-stage):** Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
- **4.** The minimum required fill of cement behind the 4-1/2 in. production liner is:
 - Cement should tie-back at least 100 feet into previous casing string. Operator shall provide method of verification.

Offline Cementing

Operator has been (**Approved**) to pump the proposed cement program offline in the **Surface and intermediate(s) intervals**. Offline cementing should commence within 24 hours of landing the casing for the interval. Notify the BLM 4hrs prior to the commencement of any offline cementing procedure at **Eddy County:** 575-361-2822.

C. PRESSURE CONTROL

- 1. Variance approved to use **flex line** from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi. The BOP/BOPE and annular preventer shall be pressure-tested in accordance with title 43 CFR 3172.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
 - e. Whenever any seal subject to test pressure is broken, all the tests in the title 43 CFR 3172.6(b)(9) must be followed.

BOPE Break Testing Variance

• BOPE Break Testing is ONLY permitted for intervals utilizing a 5M BOPE or

less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP.)

- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE tests
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

D. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

Contact Eddy County Petroleum Engineering Inspection Staff:

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; BLM NM CFO DrillingNotifications@BLM.GOV; (575) 361-2822.

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - i. Notify the BLM when moving in and removing the Spudder Rig.
 - ii. Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - iii. BOP/BOPE test to be conducted per 43 CFR 3172 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the doghouse or stairway area.
- 3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until

- both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- **4.** Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- **5.** No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- **6.** On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- **8.** Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and

- hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- **3.** 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- **4.** If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - iii. Manufacturer representative shall install the test plug for the initial BOP test.
 - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
 - v. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- **5.** The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (Only applies to single stage cement jobs, prior to the cement setting up.)
 - iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing

valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

- iv. The test shall be run on a 5000-psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one-hour chart. A circular chart shall have a maximum 2-hour clock. If a twelve hour or twenty-four-hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low-pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crewintensive operations.

SA 04/10/2025

Hydrogen Sulfide Drilling Operations Plan Mewbourne Oil Company

1. General Requirements

Rule 118 does not apply to this well because MOC has researched this area and no high concentrations of H2S were found. MOC will have on location and working all H2S safety equipment before the Delaware formation for purposes of safety and insurance requirements.

2. Hydrogen Sulfide Training

All personnel, whether regularly assigned, contracted, or employed on an unscheduled basis, will have received training from a qualified instructor in the following areas prior to entering the drilling pad area of the well:

- 1. The hazards and characteristics of hydrogen sulfide gas.
- 2. The proper use of personal protective equipment and life support systems.
- 3. The proper use of hydrogen sulfide detectors, alarms, warning systems, briefing areas, evacuation procedures.
- 4. The proper techniques for first aid and rescue operations.

Additionally, supervisory personnel will be trained in the following areas:

- The effects of hydrogen sulfide on metal components. If high tensile tubular systems are utilized, supervisory personnel will be trained in their special maintenance requirements.
- 2 Corrective action and shut in procedures, blowout prevention, and well control procedures while drilling a well.
- The contents of the Hydrogen Sulfide Drilling Operations Plan.

There will be an initial training session prior to encountering a know hydrogen sulfide source. The initial training session shall include a review of the site specific Hydrogen Sulfide Drilling Operations Plan.

3. Hydrogen Sulfide Safety Equipment and Systems

All hydrogen sulfide safety equipment and systems will be installed, tested, and operational prior to drilling below the 9 5/8" intermediate casing.

1. Well Control Equipment

- A. Choke manifold with minimum of one adjustable choke/remote choke.
- B. Blowout preventers equipped with blind rams and pipe rams to accommodate all pipe sizes with properly sized closing unit
- C. Auxiliary equipment including annular type blowout preventer.
- 2. <u>Protective Equipment for Essential Personnel</u>

Thirty minute self contained work unit located in the dog house and at briefing areas.

Additionally: If H2S is encountered in concentrations less than 10 ppm, fans will be placed in work areas to prevent the accumulation of hazardous amounts of poisonous gas. If higher concentrations of H2S are detected the well will be shut in and a rotating head, mud/gas separator, remote choke and flare line with igniter will be installed.

3. <u>Hydrogen Sulfide Protection and Monitoring Equipment</u>

Two portable hydrogen sulfide monitors positioned on location for optimum coverage and detection. The units shall have audible sirens to notify personnel when hydrogen sulfide levels exceed 20 PPM.

4. <u>Visual Warning Systems</u>

- A. Wind direction indicators as indicated on the wellsite diagram.
- B. Caution signs shall be posted on roads providing access to location. Signs shall be painted a high visibility color with lettering of sufficient size to be readable at reasonable distances from potentially contaminated areas.

4. Mud Program

The mud program has been designed to minimize the amount of hydrogen sulfide entrained in the mud system. Proper mud weight, safe drilling practices, and the use of hydrogen sulfide scavengers will minimize hazards while drilling the well.

5. Metallurgy

All tubular systems, wellheads, blowout preventers, drilling spools, kill lines, choke manifolds, and valves shall be suitable for service in a hydrogen sulfide environment when chemically treated.

6. Communications

State & County Officials phone numbers are posted on rig floor and supervisors trailer. Communications in company vehicles and toolpushers are either two way radios or cellular phones.

7. Well Testing

Drill stem testing is not an anticipated requirement for evaluation of this well. If a drill stem test is required, it will be conducted with a minimum number of personnel in the immediate vicinity. The test will be conducted during daylight hours only.

8. Emergency Phone Numbers

| Eddy County Sheriff's Office | 911 or 575-887-7551 |
|--|-----------------------------|
| Ambulance Service | 911 or 575-885-2111 |
| Carlsbad Fire Dept | 911 or 575-885-2111 |
| Loco Hills Volunteer Fire Dept. | 911 or 575-677-3266 |
| Closest Medical Facility - Columbia Medical Cent | er of Carlsbad 575-492-5000 |

| Mewbourne Oil Company | Hobbs District Office Fax 2 nd Fax | 575-393-5905 575-397-6252 575-393-7259 |
|--------------------------------|---|--|
| District Manager | Robin Terrell | 575-390-4816 |
| Drilling Superintendent | Frosty Lathan | 575-390-4103 |
| 2 | Bradley Bishop | 575-390-6838 |
| Drilling Foreman | Wesley Noseff | 575-441-0729 |

Operator Name: MEWBOURNE OIL COMPANY

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Section 7 - Methods for Handling

Waste type: SEWAGE

Waste content description: Human waste & grey water

Amount of waste: 1500 gallons

Waste disposal frequency: Weekly

Safe containment description: 2,000 gallon plastic container

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: City of Carlsbad Water Treatment facility

Waste type: GARBAGE

Waste content description: Garbage & trash

Amount of waste: 1500 pounds

Waste disposal frequency: One Time Only

Safe containment description: Enclosed trash trailer

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: Waste Management facility in Carlsbad.

Waste type: DRILLING

Waste content description: Drill cuttings

Amount of waste: 940 barrels

Waste disposal frequency : One Time Only

Safe containment description: Drill cuttings will be properly contained in steel tanks (20 yard roll off bins.)

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: NMOCD approved waste disposal locations are CRI or Lea Land, both facilities are located

on HWY 62/180, Sec. 27 T20S R32E.

Reserve Pit

Reserve Pit being used? NO

Operator Name: MEWBOURNE OIL COMPANY

Well Name: ICEMAN 24/23 FED COM Well Number: 712H

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.) Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

Cuttings Area

Cuttings Area being used? NO

Are you storing cuttings on location? N

Description of cuttings location

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

Cuttings area liner

Cuttings area liner specifications and installation description

Section 8 - Ancillary

Are you requesting any Ancillary Facilities?: N

Ancillary Facilities

Comments:

Section 9 - Well Site

Well Site Layout Diagram:

ICEMAN_24_23_FED_COM__712H_WellSiteLayout_20240617093749.pdf

Comments: NONE

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Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 460768

CONDITIONS

| Operator: | OGRID: |
|------------------|---|
| MEWBOURNE OIL CO | 14744 |
| P.O. Box 5270 | Action Number: |
| Hobbs, NM 88241 | 460768 |
| | Action Type: |
| | [C-101] BLM - Federal/Indian Land Lease (Form 3160-3) |

CONDITIONS

| Created By | Condition | Condition Date |
|-------------|---|-------------------|
| mleal | Cement is required to circulate on both surface and intermediate1 strings of casing. | 5/12/2025 |
| mleal | If cement does not circulate on any string, a Cement Bond Log (CBL) is required for that string of casing. | 5/12/2025 |
| ward.rikala | Notify the OCD 24 hours prior to casing & cement. | 6/18/2025 |
| ward.rikala | File As Drilled C-102 and a directional Survey with C-104 completion packet. | 6/18/2025 |
| ward.rikala | Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string. | 6/18/2025 |
| ward.rikala | Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system. | 6/18/2025 |