Form 3160-3 FORM APPROVED OMB No. 1004-0137 (June 2015) Expires: January 31, 2018 **UNITED STATES** DEPARTMENT OF THE INTERIOR 5. Lease Serial No. NMNM027994D **BUREAU OF LAND MANAGEMENT** APPLICATION FOR PERMIT TO DRILL OR REENTER 6. If Indian, Allotee or Tribe Name 7. If Unit or CA Agreement, Name and No. **✓** DRILL REENTER 1a. Type of work: 1b. Type of Well: Oil Well ✓ Gas Well Other 8. Lease Name and Well No. 1c. Type of Completion: Hydraulic Fracturing ✓ Single Zone Multiple Zone ICEMAN 24/23 FED COM 718H 2. Name of Operator 9. API Well No. MEWBOURNE OIL COMPANY 30-015-56818 3a. Address 3b. Phone No. (include area code) 10. Field and Pool, or Exploratory PURPLE SAGE/(WOLFCAMP) GAS P O BOX 5270, HOBBS, NM 88241 (575) 393-5905 4. Location of Well (Report location clearly and in accordance with any State requirements.*) 11. Sec., T. R. M. or Blk. and Survey or Area SEC 24/T23S/R26E/NMP At surface SENE / 2020 FNL / 260 FEL / LAT 32.2918607 / LONG -104.2386698 At proposed prod. zone SWSE / 400 FSL / 2335 FEL / LAT 32.2838824 / LONG -104,262559 14. Distance in miles and direction from nearest town or post office* 12. County or Parish 13. State **EDDY** NM 10 miles 15. Distance from proposed* 16. No of acres in lease 17. Spacing Unit dedicated to this well 210 feet location to nearest property or lease line, ft. 480.0 (Also to nearest drig. unit line, if any) 18. Distance from proposed location* 19. Proposed Depth 20. BLM/BIA Bond No. in file to nearest well, drilling, completed, 20 feet 8726 feet / 16802 feet FED: NM1693 applied for, on this lease, ft. 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. Approximate date work will start* 23. Estimated duration 3222 feet 08/17/2024 60 days 24. Attachments The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable) 1. Well plat certified by a registered surveyor. 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest System Lands, the 5. Operator certification. SUPO must be filed with the appropriate Forest Service Office). 6. Such other site specific information and/or plans as may be requested by the Name (Printed/Typed) Date 25. Signature BRADLEY BISHOP / Ph: (575) 393-5905 06/17/2024 (Electronic Submission) Title Regulatory Approved by (Signature) Date Name (Printed/Typed) (Electronic Submission) CODY LAYTON / Ph: (575) 234-5959 05/08/2025 Title Office Assistant Field Manager Lands & Minerals Carlsbad Field Office Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the

applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.



General Information Phone: (505) 629-6116

Online Phone Directory Visit:

https://www.emnrd.nm.gov/ocd/contact-us/

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION

Revised July 9, 2024							
Submit Electronically							
via OCD Permitting							
X Initial Submittal							
☐ Amended Report							

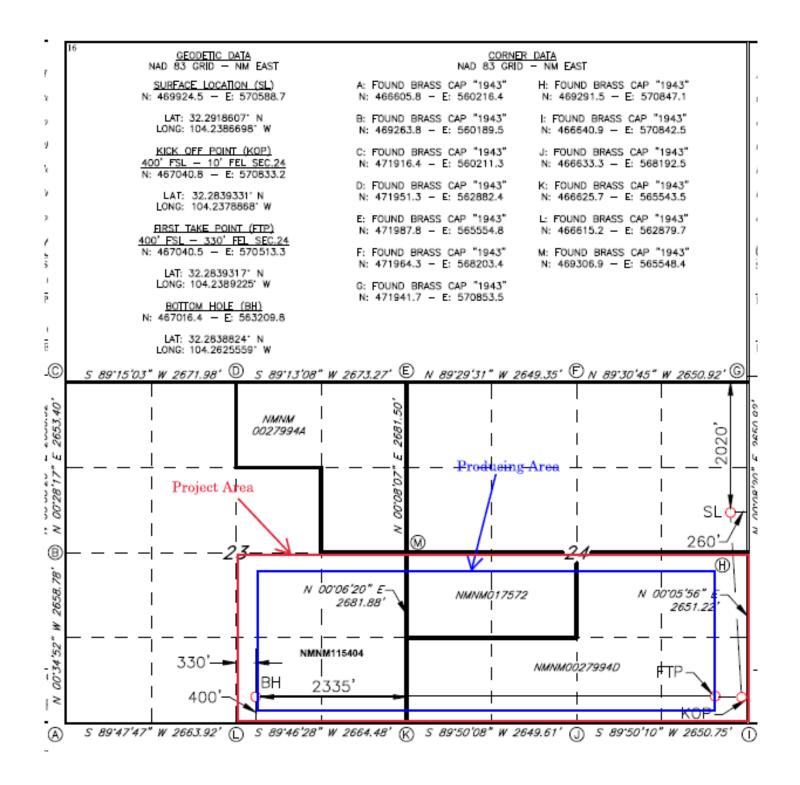
Submittal

Type:

									☐ As Drilled	1				
					WELL LOCA	ATION INFORMATION								
API Nu	mber 30-015-{	56818	Pool Code	9822	0	Pool Name PURF	PURPLE SAGE; WOLFCAMP							
Property	y Code 337348		Property Na	me IC	EMAN 24/	23 FED COM			Well Numbe	Well Number 718H				
OGRID	No. 14	744	Operator Na	ime M	EWBOUR	NE OIL COMPAN	۱Y		Ground Leve 32	el Elevation 22				
Surface	Owner: 🗆 S	tate 🗆 Fee 🗆	Tribal 🔀 Fede	eral		Mineral Owner: ☐ S	tate 🗆 Fee [□ Tribal [X Federal					
					Sur	face Location								
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County				
Н	24	23S	26E		2020 FNL	. 260 FEL	32.291	8607	-104.2386698	EDDY				
					Botto	m Hole Location								
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County				
0	23	23S	26E		400 FSL	2335 FEL	32.283	8824	-104.2625559	EDDY				
D 11 .	1.4	ren pe	. 337.11	D. C	XX 11 4 DX		rr : aran	G 1:	1 0 .1	1				
Dedicat	ed Acres	Infill or Defir	•	Defining	Well API	Overlapping Spacing	Unit (Y/N)	Consoli	dation Code	N/A				
	umbers.	DEFIIN	ing			Well setbacks are und	er Common (Ownershir	y □Ves □No	IN/A				
0140111						Well beloucks are una	Ci Common (3 WHEISHI	5. L. 1 es L. 110					
			Г	1 _	1	Off Point (KOP)	Γ							
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County				
Р	24	23	26		400 FSL	10 FEL			-104.2378868	EDDY				
First Take Point (FTP) UL Section Township Range Lot Ft. from N/S Ft. from E/W Latitude Longitude														
UL P	24	Township 23	Range 26	Lot		Ft. from E/W		1217	Longitude -104.2389225	County EDDY				
Г	24	23	20		400 FSL		32.2839	-104.2303223	EDD1					
UL	Section	Township	Range	Lot	Ft. from N/S	Ft. from E/W	Latitude		Longitude	County				
0	23	23	26		400 FSL		32.2838	8824	-104.2625590	EDDY				
					100.02	2000 : 22	02.200							
Unitized	d Area or Are	ea of Uniform I	nterest	Spacing	Unit Type [X Hor	izontal Vertical	Grou	nd Floor I	Elevation:	22				
				•										
OPERA	TOR CERTI	FICATIONS				SURVEYOR CERTIFIC	ATIONS							
I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief, and, if the well is a vertical or directional well, that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of a working interest or unleased mineral interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division. If this well is a horizontal well, I further certify that this organization has received the consent of at least one lessee or owner of a working interest or unleased mineral interest						I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision and that the same is true and correct to the best of my belief. 19680								
in each ti interval v	ract (in the tar will be located	get pool or forma or obtained a cor	tion) in which as npulsory pooling	ny part of th	e well's completed the division.		ROPERSS/O	NAL S	SP-SE					
Signature		Cdani	<u>ll</u> Date		5/12/25	Signature and Seal of Profession		0/14						
RY Printed N	AN MCI	DANIEL				Robert M. Certificate Number	Date of Surve	ett						
	ANMCD	ANIEL@	<u>MEWBO</u>	URNE	.COM	19680		,						

This grid represents a standard section. You may superimpose a non-standard section, or larger area, over this grid. Operators must outline the dedicated acreage in a red box, clearly show the well surface location and bottom hole location, if it is directionally drilled, with the dimensions from the section lines in the cardinal directions. If this is a horizontal wellbore show on this plat the location of the First Take Point and Last Take Point, and the point within the Completed interval (other than the First Take Point or Last Take Point) that is closest to any outer boundary of the tract.

Surveyors shall use the latest United States government survey or dependent resurvey. Well locations will be in reference to the New Mexico Principal Meridian. If the land is not surveyed, contact the OCD Engineering Bureau. Independent subdivision surveys will not be acceptable.



State of New Mexico Energy, Minerals and Natural Resources Department

Submit Electronically Via E-permitting

Oil Conservation Division 1220 South St. Francis Dr. Santa Fe, NM 87505

NATURAL GAS MANAGEMENT PLAN

	1 12											
This Natural Gas Management Plan must be submitted with each Application for Permit to Drill (APD) for a new or recompleted well.												
Section 1 — Plan Description <u>Effective May 25, 2021</u>												
I. Operator: Mev	vbourne C	Oil Co.	OGRID:	14744	Date:	5/2/24						
II. Type: X Original] Amendment	due to □ 19.15.27	7.9.D(6)(a) NMAC	□ 19.15.27.9.D(6)(b) NMAC □ (Other.						
If Other, please describe	.t											
III. Well(s): Provide the be recompleted from a s					wells proposed to	be drilled or proposed to						
Well Name			Anticipated Gas MCF/D	Anticipated Produced Water BBL/D								
ICEMAN 24-23 FED COM 718H		H 24 23S 26E	2020' FNL x 260' FE	L 1500	4500	5500						
				Y1:400 Y2:300 Y3:200	1: 1200 Y2: 900 Y3: 600	Y1: 1500 Y2: 1100 Y3: 700						
IV. Central Delivery Po	oint Name:	IC	EMAN 24-23 FED	COM 718H	[See 1	9.15.27.9(D)(1) NMAC]						
V. Anticipated Schedul proposed to be recompled					rell or set of wells	proposed to be drilled or						
Well Name	API	Spud Date	TD Reached Date	Completion Commencement								
ICEMAN 24-23 FED COM 718H		7/2/24	8/2/24	9/2/24	9/17/24	9/17/24						
VII. Operational Pract Subsection A through F	tices: 🛛 Attacl of 19.15.27.8 I	h a complete desc NMAC.	cription of the acti	ons Operator will	I take to comply	t to optimize gas capture. with the requirements of ices to minimize venting						

Section 2 – Enhanced Plan EFFECTIVE APRIL 1, 2022

Beginning April 1, 2022, an operator that is not in compliance with its statewide natural gas capture requirement for the applicable reporting area must complete this section.

🗴 Operator certifies that it is not required to complete this section because Operator is in compliance with its statewide natural gas capture requirement for the applicable reporting area.

IX. Anticipated Natural Gas Production:

Well	API	Anticipated Average Natural Gas Rate MCF/D	Anticipated Volume of Natural Gas for the First Year MCF								
X. Natural Gas Gathering System (NGGS):											

X. Natural Gas Gathering System (NGGS):

Operator	System	ULSTR of Tie-in	Anticipated Gathering Start Date	Available Maximum Daily Capacity of System Segment Tie-in

XI. Map. \Box Attach an accurate and legible map depicting the location of the well(s), the anticipated pipeline route(s) connecting the production operations to the existing or planned interconnect of the natural gas gathering system(s), and the maximum daily capacity of the segment or portion of the natural gas gathering system(s) to which the well(s) will be connected.

XII. Line Capacity. The natural gas gathering system [☐ will ☐ will not have capacity	to gather 100% of the	anticipated natural gas
production volume from the well prior to the date of first	production.		

XIII. Line Pressure. Operator \square does \square does not anticipate that its existing well(s) connected to the same segment,	or portion,	of the
natural gas gathering system(s) described above will continue to meet anticipated increases in line pressure caused by	the new we	ll(s).

☐ Attach Operator's plan to manage production in response to the increased line pressure.

XIV. Confidentiality: □ Operator asserts confidentiality pursuant to Section 71-2-8 NMSA 1978 for the information provided in Section 2 as provided in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and attaches a full description of the specific information for which confidentiality is asserted and the basis for such assertion.

Released to Imaging: 6/18/2025 8:15:18 AM

Section 3 - Certifications Effective May 25, 2021

Operator certifies that, after reasonable inquiry and based on the available information at the time of submittal: 🖾 Operator will be able to connect the well(s) to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system; or ☐ Operator will not be able to connect to a natural gas gathering system in the general area with sufficient capacity to transport one hundred percent of the anticipated volume of natural gas produced from the well(s) commencing on the date of first production, taking into account the current and anticipated volumes of produced natural gas from other wells connected to the pipeline gathering system. If Operator checks this box, Operator will select one of the following: Well Shut-In. ☐ Operator will shut-in and not produce the well until it submits the certification required by Paragraph (4) of Subsection D of 19.15.27.9 NMAC; or Venting and Flaring Plan.

Operator has attached a venting and flaring plan that evaluates and selects one or more of the potential alternative beneficial uses for the natural gas until a natural gas gathering system is available, including: power generation on lease; (a) (b) power generation for grid; compression on lease; (c) liquids removal on lease; (d) reinjection for underground storage; (e) reinjection for temporary storage; **(f)**

Section 4 - Notices

1. If, at any time after Operator submits this Natural Gas Management Plan and before the well is spud:

other alternative beneficial uses approved by the division.

reinjection for enhanced oil recovery;

fuel cell production; and

- (a) Operator becomes aware that the natural gas gathering system it planned to connect the well(s) to has become unavailable or will not have capacity to transport one hundred percent of the production from the well(s), no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised venting and flaring plan containing the information specified in Paragraph (5) of Subsection D of 19.15.27.9 NMAC; or
- (b) Operator becomes aware that it has, cumulatively for the year, become out of compliance with its baseline natural gas capture rate or natural gas capture requirement, no later than 20 days after becoming aware of such information, Operator shall submit for OCD's approval a new or revised Natural Gas Management Plan for each well it plans to spud during the next 90 days containing the information specified in Paragraph (2) of Subsection D of 19.15.27.9 NMAC, and shall file an update for each Natural Gas Management Plan until Operator is back in compliance with its baseline natural gas capture rate or natural gas capture requirement.
- 2. OCD may deny or conditionally approve an APD if Operator does not make a certification, fails to submit an adequate venting and flaring plan which includes alternative beneficial uses for the anticipated volume of natural gas produced, or if OCD determines that Operator will not have adequate natural gas takeaway capacity at the time a well will be spud.

(g)

(h)

I certify that, after reasonable inquiry, the statements in and attached to this Natural Gas Management Plan are true and correct to the best of my knowledge and acknowledge that a false statement may be subject to civil and criminal penalties under the Oil and Gas Act.

Signature:	Bradley Bishop
Printed Name:	BRADLEY BISHOP
Title:	REGULATORY MANAGER
E-mail Address:	BBISHOP@MEWBOURNE.COM
Date:	5/2/24
Phone:	575-393-5905
-	OIL CONSERVATION DIVISION
	(Only applicable when submitted as a standalone form)
Approved By:	
Title:	
Approval Date:	
Conditions of Ap	pproval:

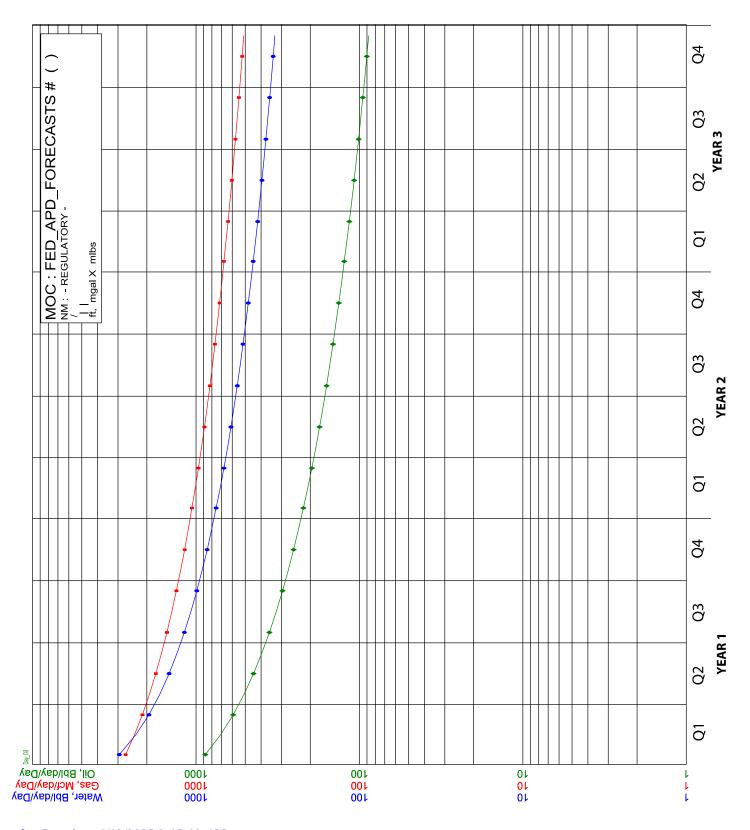
Mewbourne Oil Company

Natural Gas Management Plan – Attachment

- VI. Separation equipment will be sized by construction engineering staff based on stated manufacturer daily throughput capacities and anticipated daily production rates to ensure adequate capacity. Closed vent system piping, compression needs, and VRUs will be sized utilizing ProMax modelling software to ensure adequate capacity for anticipated production volumes and conditions.
- VII. Mewbourne Oil Company (MOC) will take following actions to comply with the regulations listed in 19.15.27.8:
 - A. MOC will maximize the recovery of natural gas by minimizing the waste, as defined by 19.15.2 NMAC, of natural gas through venting and flaring. MOC will ensure that well(s) will be connected to a natural gas gathering system with sufficient capacity to transport natural gas. If there is no adequate takeaway for the gas, well(s) will be shut in until the natural gas gathering system is available.
 - B. All drilling operations will be equipped with a rig flare located at least 100 ft from the nearest surface hole. Rig flare will be utilized to combust any natural gas that is brought to surface during normal drilling operations. In the case of emergency venting or flaring the volumes will be estimated and reported appropriately.
 - C. During completion operations any natural gas brought to surface will be flared. Immediately following the finish of completion operations, all well flow will be directed to permanent separation equipment. Produced natural gas from separation equipment will be sent to sales. It is not anticipated that gas will not meet pipeline standards. However, if natural gas does not meet gathering pipeline quality specifications, MOC will flare the natural gas for 60 days or until the natural gas meets the pipeline quality specifications, whichever is sooner. MOC will ensure that the flare is sized properly and is equipped with automatic igniter or continuous pilot. The gas sample will analyzed twice per week and the gas will be routed into a gathering system as soon as pipeline specifications are met.
 - D. Natural gas will not be flared with the exceptions and provisions listed in the 19.15.27.8 D.(1) through (4). If there is no adequate takeaway for the separator gas, well(s) will be shut in until the natural gas gathering system is available with exception of emergency or malfunction situations. Venting and/or flaring volumes will be estimated and reported appropriately.
 - E. MOC will comply with the performance standards requirements and provisions listed in 19.15.27.8 E.(1) through (8). All equipment will be designed and sized to handle maximum anticipated pressures and throughputs in order to minimize the waste. Production storage tanks constructed after May 25, 2021 will be equipped with automatic gauging system. Flares constructed after May 25, 2021 will be equipped with automatic igniter or continuous pilot. Flares will be located at least 100' from the well and storage tanks unless otherwise approved by the division. MOC will conduct AVO inspections as described in 19.15.27.8 E (5) (a) with frequencies specified in 19.15.27.8 E (5) (b) and (c). All emergencies will be resolved as quickly and safely as feasible to minimize waste.
 - F. The volume of natural gas that is vented or flared as the result of malfunction or emergency during drilling and completions operations will be estimated. The volume of natural gas that is vented, flared or beneficially used during production operations, will be measured or estimated. MOC will install equipment to measure

the volume of natural gas flared from existing process piping or a flowline piped from equipment such as high pressure separators, heater treaters, or vapor recovery units associated with a well or facility associated with a well authorized by an APD issued after May 25, 2021 that has an average daily production greater than 60 Mcf/day. If metering is not practicable due to circumstances such as low flow rate or low pressure venting and flaring, MOC will estimate the volume of vented or flared natural gas. Measuring equipment will conform to industry standards and will not be designed or equipped with a manifold that allows the diversion of natural gas around the metering element except for the sole purpose of inspecting and servicing the measurement equipment.

VIII. For maintenance activities involving production equipment and compression, venting will be limited to the depressurization of the subject equipment to ensure safe working conditions. For maintenance of production and compression equipment the associated producing wells will be shut in to eliminate venting. For maintenance of VRUs all gas normally routed to the VRU will be routed to flare to eliminate venting.





U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Drilling Plan Data Report 05/09/2025

APD ID: 10400099109 **Submission Date**: 06/17/2024

Operator Name: MEWBOURNE OIL COMPANY

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Well Type: CONVENTIONAL GAS WELL Well Work Type: Drill

Highlighted data reflects the most recent changes

Show Final Text

Section 1 - Geologic Formations

Formation			True Vertical			Mineral Resources	Producing
ID	Formation Name	Elevation		Depth	Lithologies		Formatio
15594445	UNKNOWN	3225	27	27	OTHER : Topsoil	NONE	N
15594449	TOP SALT	2650	575	575	SALT	NONE	N
15594446	BOTTOM SALT	1583	1642	1642	SALT	NONE	N
15594450	LAMAR	1355	1870	1870	DOLOMITE, LIMESTONE	NATURAL GAS, OIL	N
15594451	BELL CANYON	1275	1950	1950	SANDSTONE	NATURAL GAS, OIL	N
15594452	CHERRY CANYON	605	2620	2620	SANDSTONE	NATURAL GAS, OIL	N
15594453	MANZANITA	466	2759	2759	LIMESTONE	NATURAL GAS, OIL	N
15594454	BRUSHY CANYON	-1709	4934	4934	SANDSTONE	NATURAL GAS, OIL	N
15594444	BONE SPRING	-2078	5303	5303	LIMESTONE	NATURAL GAS, OIL	N
15594447	BONE SPRING 1ST	-3106	6331	6331	SANDSTONE	NATURAL GAS, OIL	N
15594448	BONE SPRING 2ND	-3571	6796	6796	SANDSTONE	NATURAL GAS, OIL	N
15594455	BONE SPRING 3RD	-5176	8401	8401	SANDSTONE	NATURAL GAS, OIL	N
15594456	WOLFCAMP	-5518	8743	8743	LIMESTONE, SANDSTONE, SHALE	NATURAL GAS, OIL	Y

Section 2 - Blowout Prevention

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Pressure Rating (PSI): 5M Rating Depth: 16802

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Requesting Variance? YES

Variance request: A variance is requested for the use of a variable choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

Choke Diagram Attachment:

5M BOPE Choke Diagram 20240617104342.pdf

Multi_Bowl_WH_20250131101906.pdf

Flex_Line_Specs_API_16C_20250131101906.pdf

BOP Diagram Attachment:

5M_BOPE_Schematic_20240617104459.pdf

MOC Break Testing Variance 20240617102554.pdf

MOC_Offline_Cementing_Variance_20240617102557.pdf

Section 3 - Casing

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	17.5	13.375	NEW	API	N	0	500	0	500	3222	2722	500	H-40	48	ST&C	3.44	7.74	DRY	13.4 2	DRY	22.5 4
2	INTERMED IATE	12.2 5	9.625	NEW	API	N	0	1795	0	1795	3208	1427	1795	J-55	36	LT&C	2.06	3.59	DRY	7.01	DRY	8.73
3	PRODUCTI ON	8.75	7.0	NEW	API	N	0	8851	0	8795	3208	-5573	8851	P- 110	26	LT&C	1.36	2.18	DRY	3.01	DRY	3.61
4	LINER	6.12 5	4.5	NEW	API	N	8651	16802	8595	8840	-5373	-5618	8151	P- 110	13.5	LT&C	1.93	2.25	DRY	3.07	DRY	3.83

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

	_	_	
Casing	Attac	hmei	nts

Casing ID: 1

String

SURFACE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

13.375in_48_H40_STC_Csg_20250131101658.pdf

Casing ID: 2

String

INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

9.625in_36_J55_LTC_Csg_20250131101715.pdf

Casing ID: 3

String

PRODUCTION

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

7in_26_P110_LTC_Csg_20250131101806.pdf

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Casing Attachments

Casing ID: 4

String

LINER

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

 $4.5 in_13.5_P110_LTC_Csg_20250131101820.pdf$

Section 4 - Cement

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	313	210	2.12	12.5	450	100	Class C	Salt, Gel, Extender, LCM
SURFACE	Tail	0	313	500	200	1.34	14.8	268	100	Class C	Retarder
INTERMEDIATE	Lead		0	1125	210	2.12	12.5	450	25	Class C	Salt, Gel, Extender, LCM
INTERMEDIATE	Tail		1125	1795	200	1.34	14.8	268	25	Class C	Retarder
PRODUCTION	Lead	2725	1595	2104	50	2.12	12.5	110	25	Class C	Gel, Retarder, Defoamer, Extender
PRODUCTION	Tail		2104	2725	100	1.34	14.8	134	25	Class C	Retarder FLUID LOSS DEFOAMER
PRODUCTION	Lead	2725	2725	6384	280	2.12	12.5	600	25	Class C	Gel, Retarder, Defoamer, Extender
PRODUCTION	Tail		6384	8851	400	1.18	15.6	472	25	Class H	Retarder, Fluid Loss, Defoamer
LINER	Lead		8651	1680 2	520	1.85	13.5	970	25	Class H	Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-Settling Agent

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with 43 CFR 3172:

Diagram of the equipment for the circulating system in accordance with 43 CFR 3172:

Describe what will be on location to control well or mitigate other conditions: Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.

Describe the mud monitoring system utilized: Pason/PVT/Visual Monitoring

Circulating Medium Table

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	Н	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	500	SPUD MUD	8.4	8.6		9					
500	1795	SALT SATURATED	9.5	10.2							
1795	8851	WATER-BASED MUD	8.6	10							
8851	1680 2	OIL-BASED MUD	10	11							

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures:

No logs are planned based on well control or offset log information. Offset Well: Iceman 24/23 Fed Com #712H

List of open and cased hole logs run in the well:

MEASUREMENT WHILE DRILLING, MUD LOG/GEOLOGIC LITHOLOGY LOG,

Coring operation description for the well:

None

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 5056 Anticipated Surface Pressure: 3124

Anticipated Bottom Hole Temperature(F): 165

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations

H2S_Plan_20240617093220.pdf

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

ICEMAN_24_23_FED_COM_718H_MOC_Dir_Plan_20240617104948.pdf ICEMAN_24_23_FED_COM_718H_MOC_Dir_Plot_20240617104951.pdf

Other proposed operations facets description:

: Variance is requested to perform offline cementing according to the attached procedure. R-111Q: Mewbourne is requested to perform Open Hole Cementing per R-111Q Guidelines if well is in Potash.

Other proposed operations facets attachment:

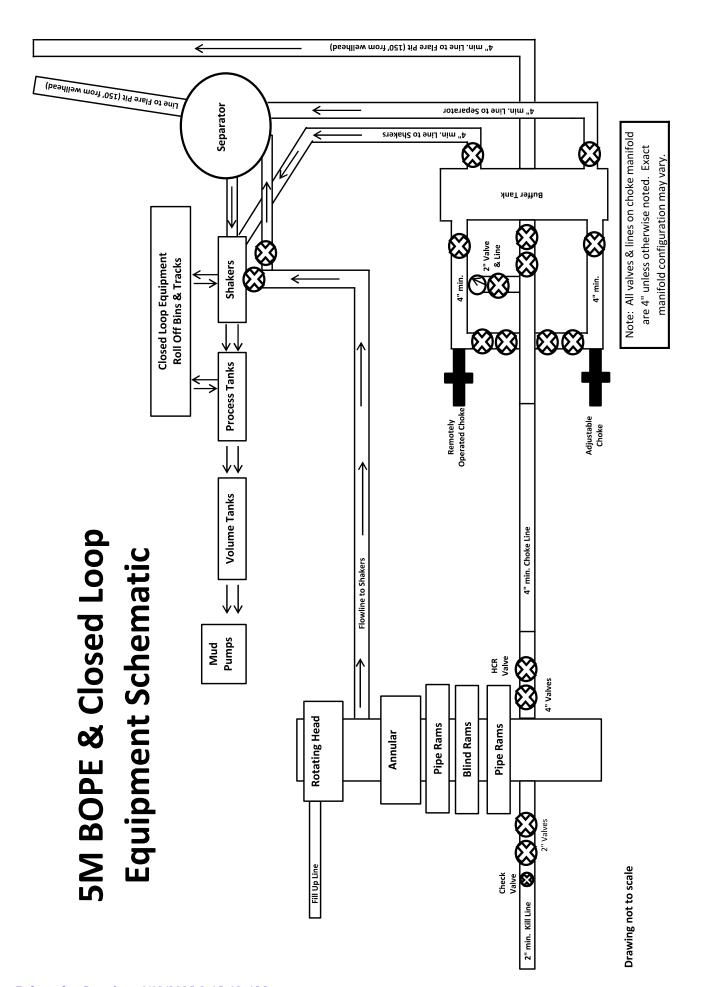
Iceman_24_23_Fed_Com_718H_AddInfo_20240617105009.pdf
Iceman_24_23_Fed_Com_718H_CsgAssumptions_20250131101943.pdf
Iceman_24_23_Fed_Com_718H_Drlg_Program_20250131101944.pdf
ICEMAN_24_23_FED_COM__718H_NGMP_20250131104126.pdf

Other Variance request(s)?:

Other Variance attachment:

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

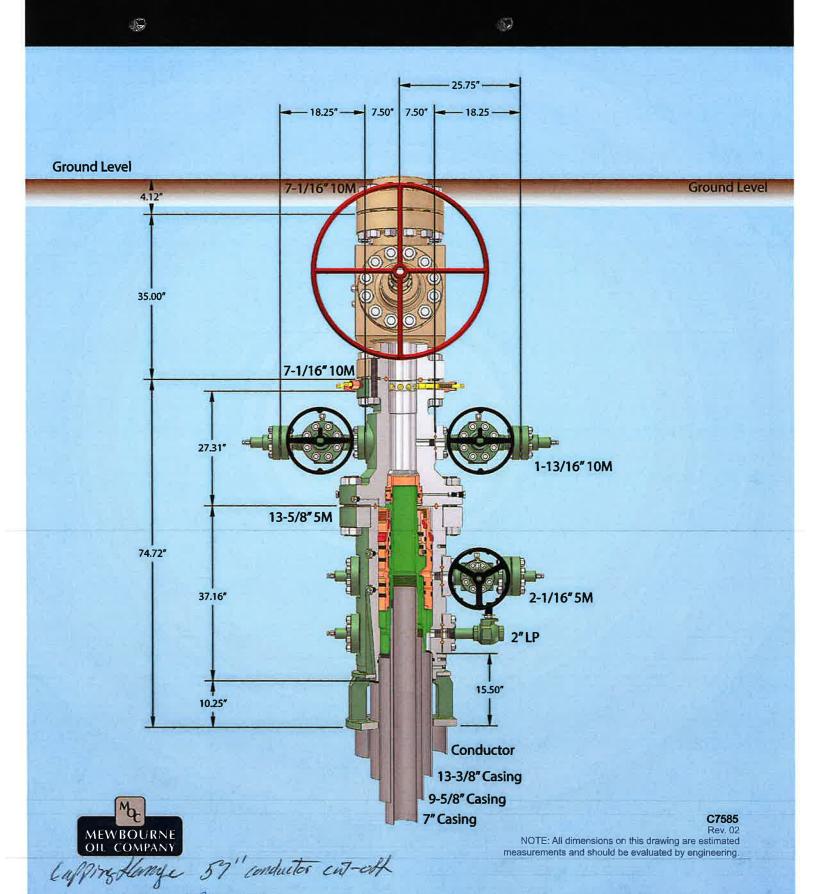
MOC_Break_Testing_Variance_20240617100912.pdf
MOC_Offline_Cementing_Variance_20240617100917.pdf



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13-5/8" MN-DS Wellhead System





LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

HYDROSTATIC TESTING REPORT

LTYY/QR-5.7.1-28

№: 230826015

Product Name	Cho	ke And Kill Hose		Standard	i Al	PI Spec 16C 3 rd edition			
Product Specification	3"×1000	0psi×60ft (18.29m	1)	Serial Num	ber	7660144			
Inspection Equipment	MTU	J-BS-1600-3200-E		Test media	um	Water			
Inspection Department	Ç	C. Department		Inspection I	Date	2023.08.26			
		Rate of le	ength change	8					
Standard requirements	At working pre	essure, the rate of le	ength change	should not n	nore than ± 2	2%			
Testing result	10000psi (69.0	10000psi (69.0MPa) ,Rate of length change 0.7%							
		Hydrosta	atic testing						
Standard requirements		orking pressure, the ssure-holding period				less than three minutes			
Testing result	15000psi (103.5MPa), 3 min for the first time, 60 min for the second time, no leakage								
Graph of pressure testing	:								
100 95 10 100 100 100 100 100 100 100 100 100			100 100						
Conclusion	प्रदेश गर्दश गर्दश गर्दश गर्द	มก พละก พมะก พมะก พละการ eted items meet stan	07 21:29:56 21:39:56	1 23:4958 23:59		1000 (1000 Medical (1000 Medic			
			1		1				



LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

CERTIFICATE OF QUALITY

LTYY/QR-5.7.1-19B

№: LT2023-126-002

Customer Name	Austin Hose						
Product Name	Choke And Kill Hose						
Product Specification	3"×10000psi×60ft (18.29m)	Quantity	2PCS				
Serial Number	7660143~7660144	FSL	FSL3				
Temperature Range	-29℃~+121℃	Standard	API Spec 16C 3 rd edition				
Inspection Department	Q.C. Department	Inspection date	2023.08.26				

	Inspection	on Items	5	Inspection results					
	Appearance (Checking	g	In accordance with API Spec 16C 3 rd edition					
	Size and L	engths		In accordance with API Spec 16C 3 rd edition					
Г	imensions and	d Tolerar	nces		In accordance with API Spec 16C 3 rd edition				
End Connections: 4-1	/16"×10000psi I	ntegral fla	ange for sour gas ser	In accordance with API Spec 6A 21st edition					
End Connections: 4-1	/16"×10000psi I	ntegral fla	ange for sour gas ser	In accordance with API Spec 17D 3 rd edition					
	Hydrostatic	Testing		In accordance with API Spec 16C 3 rd edition					
	product M	larking		In accordance with API Spec 16C 3 rd edition					
Inspection cor	nclusion	The inspected items meet standard requirements of API Spec 16C 3 rd editi					16C 3 rd edition		
Remark	S								
Approver	Jian long (Chen	Auditor	1/1	nging Dong	Inspector	Zhansheng Wang		



LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD

CERTIFICATE OF CONFORMANCE

№:LT230826016

Product Name: Choke And Kill Hose

Product Specification: 3"×10000psi×60ft (18.29m)

Serial Number: 7660143~7660144

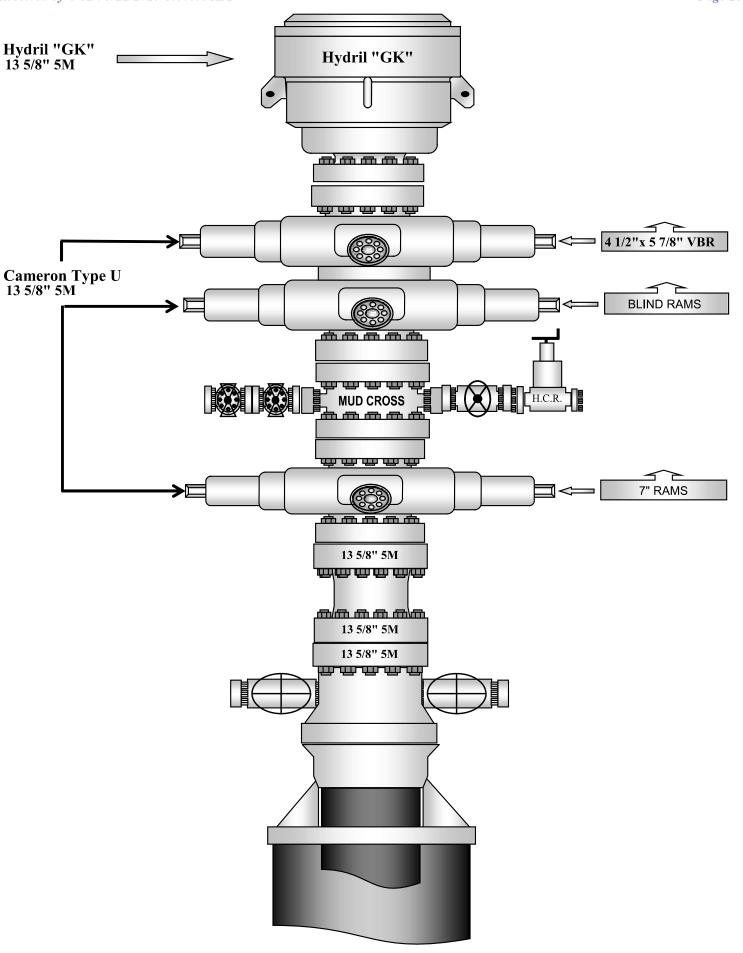
End Connections: 4-1/16"×10000psi Integral flange for sour gas service

The Choke And Kill Hose assembly was produced by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. in Aug 2023, and inspected by LUOHE LETONE HYDRAULICS TECHNOLOGY CO.,LTD. according to API Spec 16C 3rd edition on Aug 26, 2023. The overall condition is good. This is to certify that the Choke And Kill Hose complies with all current standards and specifications for API Spec 16C 3rd edition.

Jiaulong Chen

QC Manager:

Date: Aug 26, 2023





Mewbourne Oil Co.

BOP Break Testing Variance

Mewbourne Oil Company requests a variance from the minimum standards for well control equipment testing of 43 CFR 3172 to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with batch drilling & offline cementing operations. Modern rig upgrades which facilitate pad drilling allow the BOP stack to be moved between wells on a multi-well pad without breaking any BOP stack components apart. Widespread use of these technologies has led to break testing BOPE being endorsed as safe and reliable. American Petroleum Institute (API) best practices are frequently used by regulators to develop their regulations. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (5th Ed., Dec. 2018) Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component."

Procedures

- 1. Full BOPE test at first installation on the pad.
 - Full BOPE test at least every 21 days.
 - Function test BOP elements per 43 CFR 3172.
 - Contact the BLM if a well control event occurs.
- 2. After the well section is secured and the well is confirmed to be static, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad. Two breaks on the BOPE will be made (Fig. 1).
 - Connection between the flex line and the HCR valve
 - Connection between the wellhead and the BOP quick connect (Fig. 5 & 6).
- 3. A capping flange will be installed after cementing per wellhead vendor procedure & casing pressure will be monitored via wellhead valve.
- 4. The BOP will be removed and carried by a hydraulic carrier (Fig. 3 & 4).
- 5. The rig will then walk to the next well.
- 6. Confirm that the well is static and remove the capping flange.
- 7. The connection between the flex line and HCR valve and the connection between the wellhead and the BOP guick connect will be reconnected.
- 8. Install a test plug into the wellhead.
- 9. A test will then be conducted against the upper pipe rams and choke, testing both breaks (Fig. 1 & 2).
- 10. The test will be held at 250 psi low and to the high value submitted in the APD, not to exceed 5000 psi.
- 11. The annular, blind rams and lower pipe rams will then be function tested.
- 12. If a pad consists of three or more wells, steps 4 through 11 will be repeated.



13. A break test will only be conducted if the intermediate section can be drilled and cased within 21 days of the last full BOPE test.

Barriers

Before Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

After Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool and/or cement head
- Capping flange after cementing

Summary

A variance is requested to only test broken pressure seals on the BOPE when moving between wells on a multi-well pad if the following conditions are met:

- A full BOPE test is conducted on the first well on the pad. API Standard 53 requires testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater.
- If the first well on the pad is not the well with the deepest intermediate section, a full BOPE test will also be performed when moving to a deeper well.
- The hole section being drilled has a MASP under 5000 psi.
- If a well control event occurs, Mewbourne will contact BLM for permission to continue break testing.
- If significant (>50%) losses occur, full BOPE testing will be required going forward.
- Full BOPE test will be required prior to drilling the production hole.

While walking the rig, the BOP stack will be secured via hydraulic winch or hydraulic carrier. A full BOPE test will be performed at least every 21 days.



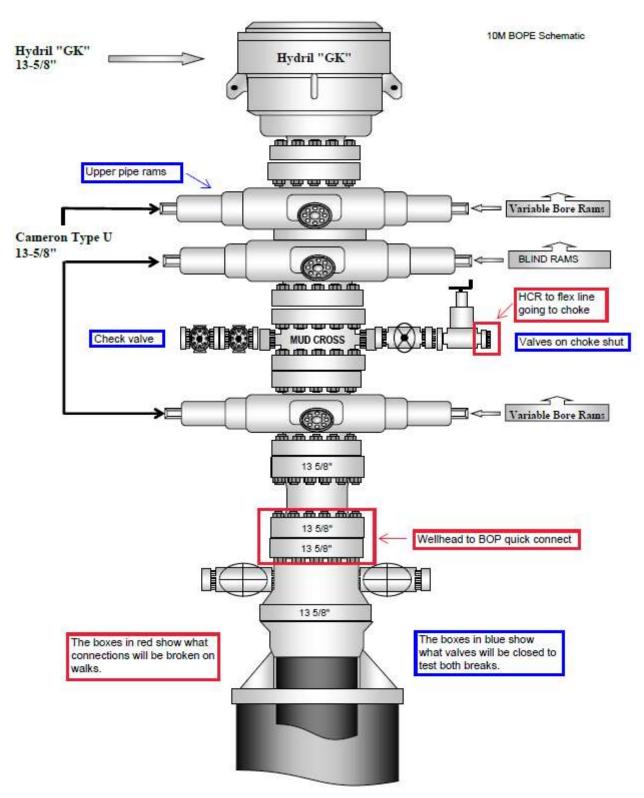


Figure 1. BOP diagram



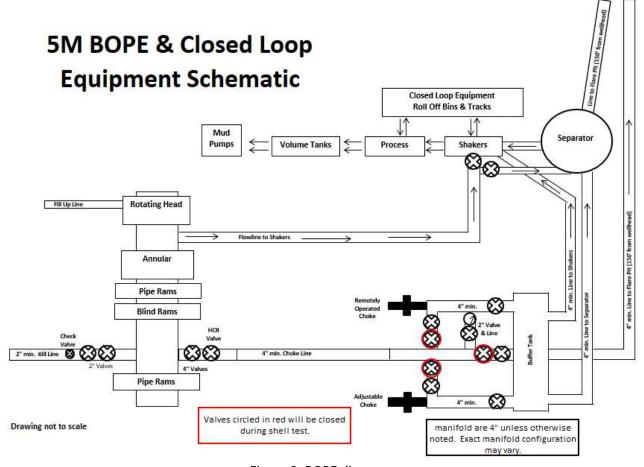


Figure 2. BOPE diagram





Figure 3. BOP handling system





Figure 4. BOP handling system



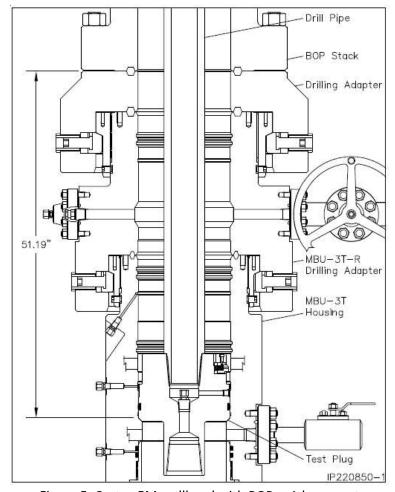


Figure 5. Cactus 5M wellhead with BOP quick connect

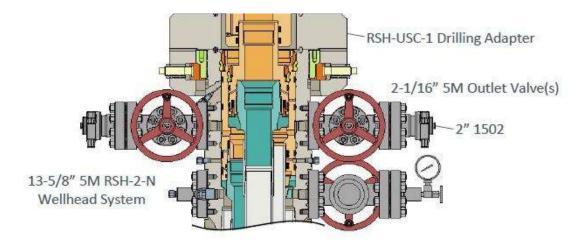


Figure 6. Vault 5M wellhead with BOP quick connect



Mewbourne Oil Co.

Surface & Intermediate Offline Cementing Variance

Mewbourne Oil Company requests a variance to perform offline cementing for surface and intermediate casing strings with the following conditions:

- Offline cementing will not be performed on production casing.
- Offline cementing will not be performed on a hole section with MASP > 5000 psi.
- Offline cementing will not be performed concurrently with offset drilling.

Surface Casing Order of Operations:

- 1. Run 13 3/8" surface casing as per normal operations (TPGS and float collar).
- 2. Perform negative pressure test to confirm integrity of float equipment while running casing.
- 3. Confirm well is static.
- 4. Make up 13 %" wellhead or wellhead landing ring assembly and land on 20" conductor.
- 5. Fill pipe, circulate casing capacity and confirm float(s) are still holding.
- 6. Confirm well is static.
- 7. Back out landing joint and pull to rig floor. Lay down landing joint.
- 8. Walk rig to next well on pad with cement crew standing by to rig up.
- 9. Make up offline cement tool with forklift per wellhead manufacturer (Fig. 1 & 2).
- 10. Make up cement head on top of offline cement tool with forklift.
- 11. Commence cement operations.
- 12. If cement circulates, confirm well is static and proceed to step 16.
- 13. If cement does not circulate, notify the appropriate BLM office, wait a minimum of six hours, and run a temperature survey to determine the top of cement.
- 14. Use 1" pipe for remedial cement job until the surface casing is cemented to surface.
- 15. Confirm well is static.
- 16. Once cement job is complete, the cement head and offline cementing tool are removed. The wellhead technician returns to cellar to install wellhead/valves.
- 17. Install wellhead capping flange.

Barriers

Before Walk:

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus



After Walk:

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Offline cementing tool tested to 5000 psi and cement head
- Capping flange after cementing

20" Surface Casing Order of Operations (4 string area):

- 1. Run 20" surface casing as per normal operations (TPGS and float collar).
- 2. Perform negative pressure test to confirm integrity of float equipment while running casing.
- 3. Fill pipe, circulate casing capacity and confirm float(s) are still holding.
- 4. Confirm well is static.
- 5. Back out landing joint and pull to rig floor. Lay down landing joint.
- 6. Make up cement head.
- 7. Walk rig to next well on pad with cement crew standing by to rig up.
- 8. Commence cement operations.
- 9. If cement circulates, confirm well is static and proceed to step 13.
- 10. If cement does not circulate, notify the appropriate BLM office, wait a minimum of six hours, and run a temperature survey to determine the top of cement.
- 11. Use 1" pipe for remedial cement job until the surface casing is cemented to surface.
- 12. Confirm well is static.
- 13. Once cement job is complete, remove cement head and install cap.

Barriers

Before Walk:

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Cement Head

After Walk:

- Float(s) in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Cement head
- Capping flange after cementing



Intermediate Casing Order of Operations:

- 1. Run casing as per normal operations (float shoe and float collar).
- 2. Perform negative pressure test to confirm integrity of float equipment while running casing.
- 3. Confirm well is static (if running SBM).
- 4. Land casing.
- 5. Fill pipe, circulate casing capacity and confirm floats are still holding.
- 6. Confirm well is static.
- 7. Back out landing joint and pull to rig floor. Lay down landing joint. Install packoff & test.
- 8. Nipple down BOP.
- 9. Walk rig to next well on pad with cement crew standing by to rig up.
- 10. Make up offline cement tool using forklift per wellhead manufacturer (Fig. 3 8).
- 11. Make up cement head on top of offline cement tool.
- 12. Commence cement operations.
- 13. If cement circulates, confirm well is static and proceed to step 16.
- 14. If cement does not circulate (when required), notify the appropriate BLM office, wait a minimum of six hours, and run a temperature survey to determine the top of cement.
- 15. Pump remedial cement job if required.
- 16. Confirm well is static.
- 17. Remove cement head and offline cementing tool.
- 18. Install wellhead capping flange and test.

Barriers

Before Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff

After Nipple Down:

- Floats in casing
- Kill weight fluid in casing
- Kill weight fluid in annulus
- Solid body mandrel and/or packoff
- Offline cementing tool tested to 5000 psi and cement head
- Capping flange after cementing



Risks:

- Pressure build up in annulus before cementing
 - o Contact BLM if a well control event occurs.
 - Rig up 3rd party pump or rig pumps to pump down casing and kill well.
 - Returns will be taken through the wellhead valves to a choke manifold (Fig 9 & 10).
 - Well could also be killed through the wellhead valves down the annulus.

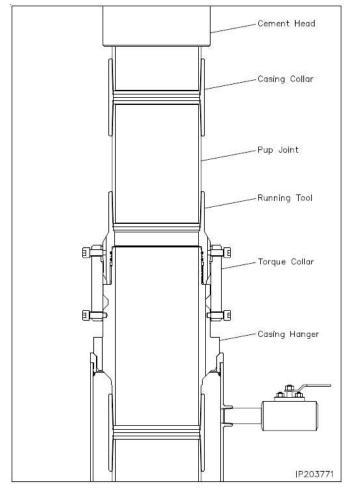


Figure 1. Cactus 13 3/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 13 3/8" pup joint and casing.



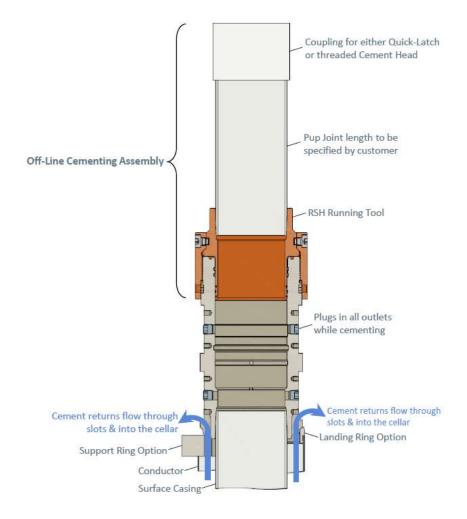


Figure 2. Vault 13 3/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 13 3/8" pup joint and casing.



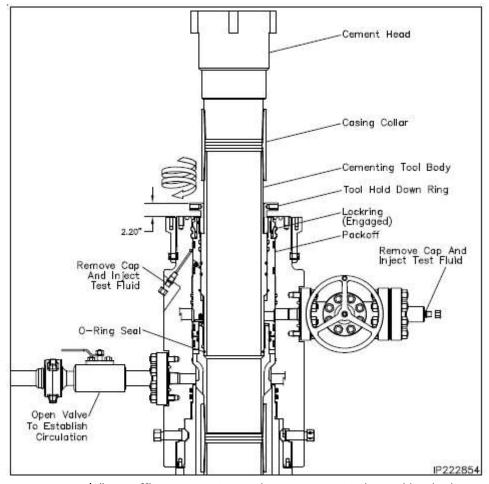


Figure 3. Cactus 9 5/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 9 5/8" pup joint and casing.



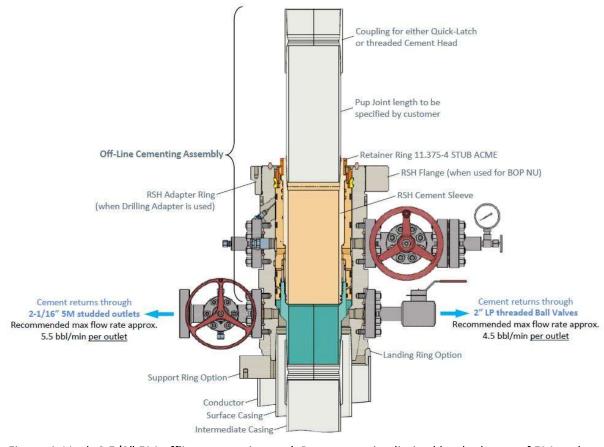


Figure 4. Vault 9 5/8" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 9 5/8" pup joint and casing.



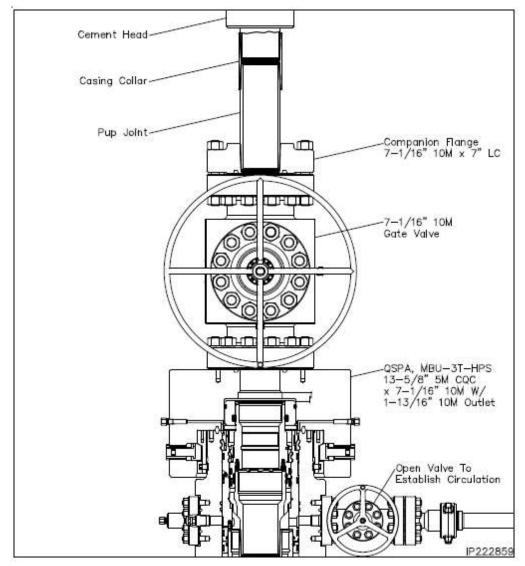


Figure 5. Cactus 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



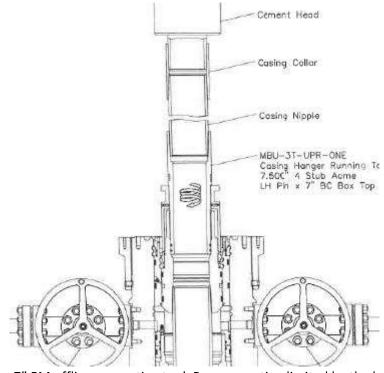


Figure 6. Cactus 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



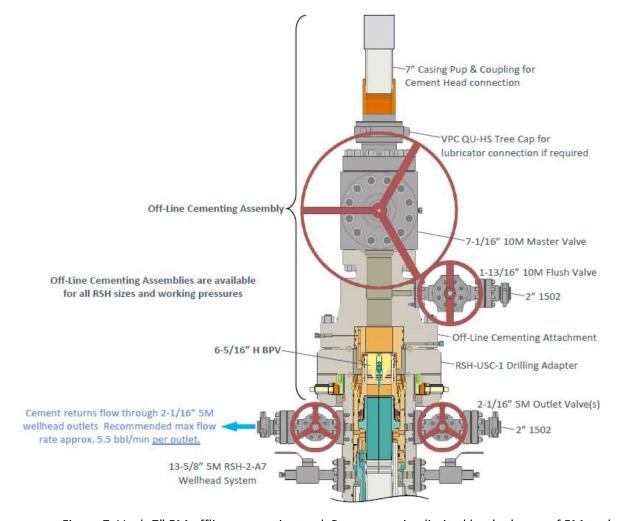


Figure 7. Vault 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



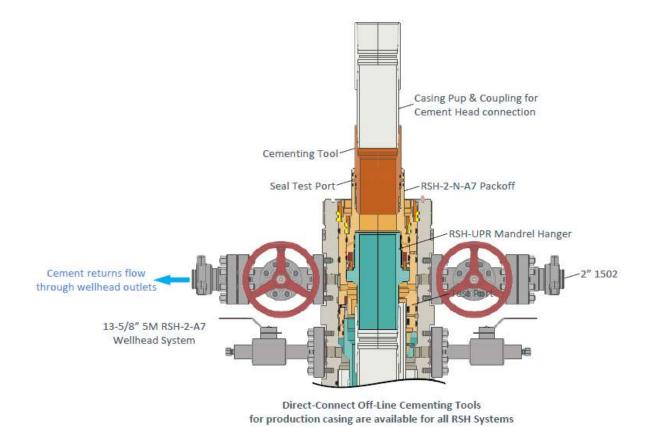


Figure 8. Vault 7" 5M offline cementing tool. Pressure rating limited by the lesser of 5M tool rating or the 7" pup joint and casing.



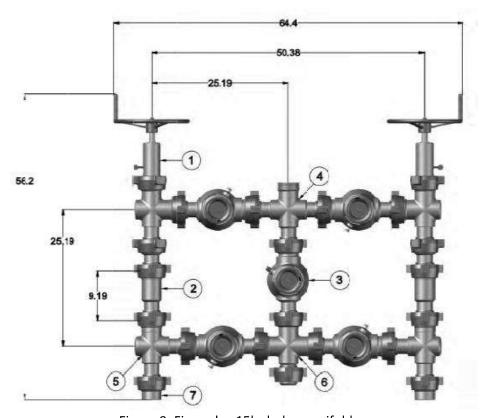


Figure 9. Five valve 15k choke manifold.

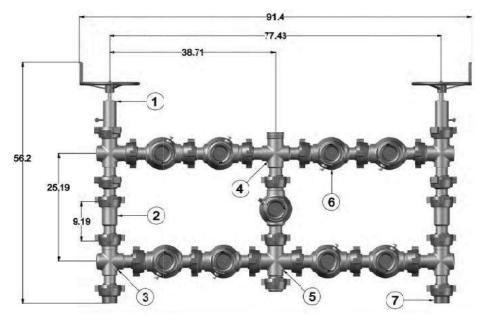


Figure 10. Nine valve 15k choke manifold.

Tenaris

API STC

Coupling	Pipe Body
Grade: H40	Grade: H40
Body: -	1st Band: Black
1st Band: Black	2nd Band: -
2nd Band: -	3rd Band: -
3rd Band: -	4th Band: -

Outside Diameter	13.375 in.	Wall Thickness	0.330 in.	Grade	H40
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

Pipe Body Data

Geometry			
Nominal OD	13,375 in.	Drift	12,559 in.
Wall Thickness	0.330 in.	Plain End Weight	46.02 lb/ft
Nominal Weight	48 lb/ft	OD Tolerance	API
Nominal ID	12.715 in.		

Performance	
SMYS	40,000 psi
Min UTS	60,000 psi
Body Yield Strength	541 x1000 lb
Min. Internal Yield Pressure	1730 psi
Collapse Pressure	740 psi
Max. Allowed Bending	14 °/100 ft

Connection Data

Hand Tight Stand Off	3.500 in.	Internal Pressure Capacity	1730 psi	Maximum Torque	4030 ft-lb
Connection OD	14.375 in.	Coupling Face Load	377 x1000 lb	Optimum Torque	3220 ft-lb
Thread per In	8	Joint Strength	322 x1000 lb	Minimum Torque	2420 ft-lb
Geometry		Performance		Make-Up Torques	

Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations.

For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations.

Couplings OD are shown according to current API 5CT 10th Edition,

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API LTC

 Coupling
 Pipe Body

 Grade: J55 (Casing)
 Grade: J55 (Casing)

 Body: Bright Green
 1st Band: Bright Green

 1st Band: White
 2nd Band:

 2nd Band: 3rd Band:

 3rd Band: 4th Band:

Outside Diameter	9.625 in.	Wall Thickness	0.352 in.	Grade	J55 (Casing)
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

Pipe Body Data

Geometry			
Nominal OD	9.625 in.	Drift	8.765 in.
Wall Thickness	0.352 in.	Plain End Weight	34.89 lb/ft
Nominal Weight	36 lb/ft	OD Tolerance	API
Nominal ID	8.921 in.		

Performance	
SMYS	55,000 psi
Min UTS	75,000 psi
Body Yield Strength	564 x1000 lb
Min. Internal Yield Pressure	3520 psi
Collapse Pressure	2020 psi
Max. Allowed Bending	26 °/100 ft

Connection Data

A.L. (
Hand Tight Stand Off	3.500 in.	Internal Pressure Capacity	3520 psi	Maximum Torque	5660 ft-lb
Connection OD	10.625 in.	Coupling Face Load	433 x1000 lb	Optimum Torque	4530 ft-lb
Thread per In	8	Joint Strength	453 x1000 lb	Minimum Torque	3400 ft-lb
Geometry		Performance		Make-Up Torques	

Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations.

For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations.

Couplings OD are shown according to current API 5CT 10th Edition.

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Coupling	Pipe Body
Grade: P110	Grade: P110
Body: White	1st Band: White
1st Band: -	2nd Band: -
2nd Band: -	3rd Band: -
3rd Band: -	4th Band: -

Outside Diameter	7.000 in.	Wall Thickness	0.362 in.	Grade	P110
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

Pipe Body Data

Geometry			
Nominal OD	7.000 in.	Drift	6.151 in.
Wall Thickness	0.362 in.	Plain End Weight	25.69 lb/ft
Nominal Weight	26 lb/ft	OD Tolerance	API
Nominal ID	6.276 in.		

Performance	
SMYS	110,000 psi
Min UTS	125,000 psi
Body Yield Strength	830 x1000 lb
Min. Internal Yield Pressure	9960 psi
Collapse Pressure	6230 psi
Max. Allowed Bending	72 °/100 ft

Connection Data

N					
Hand Tight Stand Off	3 in.	Internal Pressure Capacity	9960 psi	Maximum Torque	8660 ft-lb
Connection OD	7.875 in.	Coupling Face Load	799 x1000 lb	Optimum Torque	6930 ft-lb
Thread per In	8	Joint Strength	693 x1000 lb	Minimum Torque	5200 ft-lb
Geometry		Performance		Make-Up Torques	

Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations.

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Couplings OD are shown according to current API 5CT 10th Edition.

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Coupling	Pipe Body
Grade: P110	Grade: P110
Body: White	1st Band: White
1st Band: -	2nd Band: -
2nd Band: -	3rd Band: -
3rd Band: -	4th Band: -

Outside Diameter	4.500 in.	Wall Thickness	0.290 in.	Grade	P110
Min. Wall Thickness	87.50 %	Pipe Body Drift	API Standard	Туре	Casing
Connection OD Option	Regular				

Pipe Body Data

Geometry			
Nominal OD	4.500 in.	Drift	3.795 in.
Wall Thickness	0.290 in.	Plain End Weight	13.05 lb/ft
Nominal Weight	13.500 lb/ft	OD Tolerance	API
Nominal ID	3.920 in.		

110,000 psi
125,000 psi
422 x1000 lb
12,410 psi
10,690 psi
112 °/100 ft

Connection Data

N					
Hand Tight Stand Off	3 in.	Internal Pressure Capacity	12,410 psi	Maximum Torque	4580 ft-lb
Connection OD	5.250 in.	Coupling Face Load	473 x1000 lb	Optimum Torque	3660 ft-lb
Thread per In	8	Joint Strength	338 x1000 lb	Minimum Torque	2750 ft-lb
Geometry		Performance		Make-Up Torques	

Notes

For products according to API Standards 5CT & 5B; Performance calculated considering API Technical Report 5C3 (Sections 9 & 10) equations.

For geometrical and steel grades combinations not considered in the API Standards 5CT and/or 5B; Performance calculations indirectly derived from API Technical Report 5C3 (Sections 9 & 10) equations.

Couplings OD are shown according to current API 5CT 10th Edition,

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SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

	Casing Program Design A				BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	500'	500'	13.375" 48# H40 STC	3.44	7.74	13.42	22.54
Int	12.25"	0'	0'	1795'	1795'	9.625" 36# J55 LTC	2.12	3.70	7.01	8.73
Production	8.75"	0'	0'	8851'	8795'	7" 26# P110 LTC	1.36	2.18	3.01	3.61
Liner	6.125"	8651'	8595'	16802'	8840'	4.5" 13.5# P110 LTC	2.11	2.45	3.07	3.84

Cement Program

Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description
13,375 in	LEAD	210	12.5	2.12	0' - 313'	450	100%	Class C: Salt, Gel, Extender, LCM
13.375 III	TAIL	200	14.8	1.34	313' - 500'	268	100%	Class C: Retarder
9.625 in	LEAD	210	12.5	2.12	0' - 1125'	450	25%	Class C: Salt, Gel, Extender, LCM
9.025 III	TAIL	200	14.8	1.34	1125' - 1795'	268	23%	Class C: Retarder
1st Stg 7 in	LEAD	330	12.5	2.12	2725' - 6384'	700	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg / In	TAIL	400	15.6	1.18	6384' - 8851'	472	23%	Class H: Retarder, Fluid Loss, Defoamer
	7" DV Tool @ 2725'							
2nd Stg 7 in	LEAD	50	12.5	2.12	1595' - 2104'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Sig / III	TAIL	100	14.8	1.34	2104' - 2725'	134	2370	Class C: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	520	13.5	1.85	8651' - 16802'	970	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent

Design A - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 500'	8.4 - 8.6	Fresh Water
500' - 1795'	9.5 - 10.2	Brine
1795' - 8851'	8.6 - 10.	Cut-Brine
8851' - 16802'	10.0 - 11.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	1870'	Oil/Natural Gas
Salt Top	575'	None	Bell Canyon	1950'	Oil/Natural Gas
Salt Base	1642'	None	Cherry Canyon	2620'	Oil/Natural Gas
Yates			Manzanita Marker	2759'	Oil/Natural Gas
Seven Rivers			Basal Brushy Canyon	4934'	Oil/Natural Gas
Queen			Bone Spring	5303'	Oil/Natural Gas
Capitan			1st Bone Spring	6331'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6796'	Oil/Natural Gas
San Andres			3rd Bone Spring	8401'	Oil/Natural Gas
Glorieta			Wolfcamp	8743'	Oil/Natural Gas

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

se casing new? If used, attach certification as required in Onshore Order #1 s casing API approved? If no, attach casing specification sheet. y s casing API approved? If no, attach casing specification sheet. Noes the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). Yell the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? s well located within Capitan Reef? If yes, does production casing cement tie back a minimum of 50' above the Reef? Is well within the designated 4 string boundary. s well located in SOPA but not in R-111-Q? If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing? s well located in R-111-Q and SOPA? If yes, are the first three strings cemented to surface? Is 2 rd string set 100' to 600' below the base of salt? s an open annulus used to satisfy R-111-Q? If yes, see cement design. s an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned?		
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Does the above easing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria). Yill the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? s well located within Capitan Reef? If yes, does production casing cement tie back a minimum of 50° above the Reef? Is well within the designated 4 string boundary. s well located in SOPA but not in R-111-Q? If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing? s well located in R-111-Q and SOPA? If yes, are the first three strings cemented to surface? Is 2 rd string set 100′ to 600° below the base of salt? s an open annulus used to satisfy R-111-Q? If yes, see cement design. s an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned? s well located in high Cave/Karst? If yes, are there two strings cemented to surface? If yes, are there two strings cemented to surface? Y If yes, are there two strings cemented to surface?	Is casing API approved? If no, attach casing specification sheet.	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing? s well located within Capitan Reef? If yes, does production casing cement tie back a minimum of 50° above the Reef? Is well within the designated 4 string boundary. s well located in SOPA but not in R-111-Q? If yes, are the first 2 strings cemented to surface and 3°d string cement tied back 500° into previous casing? s well located in R-111-Q and SOPA? If yes, are the first three strings cemented to surface? Is 2°d string set 100° to 600° below the base of salt? s an open annulus used to satisfy R-111-Q? If yes, see cement design. s an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned? s well located in high Cave/Karst? If yes, are there two strings cemented to surface? Y If yes, are there two strings cemented to surface?	Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
s well located within Capitan Reef? If yes, does production casing cement tie back a minimum of 50' above the Reef? Is well within the designated 4 string boundary. Is well located in SOPA but not in R-111-Q? If yes, are the first 2 strings cemented to surface and 3" string cement tied back 500' into previous casing? If yes, are the first three strings cemented to surface? Is 2" string set 100' to 600' below the base of salt? Is an open annulus used to satisfy R-111-Q? If yes, see cement design. Is an open annulus used to satisfy R-111-Q? If yes, see cement design. If yes, are when the string temperature of the satisfy R-111-Q? If yes, see cement design. Is an open annulus used to satisfy R-111-Q? If yes, see cement design. If yes, at what depth is the weak point used to satisfy R-111-Q? If yes, are when two strings cemented to surface? If yes, are the first three two strings cemented to surface? If yes, are the first three two strings cemented to surface?	Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef? Is well within the designated 4 string boundary. 8 well located in SOPA but not in R-111-Q? If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing? 8 well located in R-111-Q and SOPA? If yes, are the first three strings cemented to surface? Is 2 rd string set 100′ to 600° below the base of salt? 8 an open annulus used to satisfy R-111-Q? If yes, see cement design. 8 an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned? 8 well located in high Cave/Karst? Y If yes, are there two strings cemented to surface?	Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
If yes, does production casing cement tie back a minimum of 50° above the Reef? Is well within the designated 4 string boundary. 8 well located in SOPA but not in R-111-Q? If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500° into previous casing? 8 well located in R-111-Q and SOPA? If yes, are the first three strings cemented to surface? Is 2 rd string set 100′ to 600° below the base of salt? 8 an open annulus used to satisfy R-111-Q? If yes, see cement design. 8 an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned? 8 well located in high Cave/Karst? Y If yes, are there two strings cemented to surface?		
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If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous easing? s well located in R-111-Q and SOPA? If yes, are the first three strings cemented to surface? Is 2 rd string set 100' to 600' below the base of salt? s an open annulus used to satisfy R-111-Q' If yes, see cement design. s an engineered weak point used to satisfy R-111-Q'? If yes, at what depth is the weak point planned? s well located in high Cave/Karst? If yes, are there two strings cemented to surface?		
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If yes, are the first three strings cemented to surface? Is 2 ⁹⁸ string set 100' to 600' below the base of salt? s an open annulus used to satisfy R-111-Q? If yes, at what depth is the weak point planned? s well located in high Cave/Karst? If yes, are there two strings cemented to surface?	If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
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s an open annulus used to satisfy R-111-Q? If yes, see cement design. s an engineered weak point used to satisfy R-111-Q? If yes, at what depth is the weak point planned? s well located in high Cave/Karst? If yes, are there two strings cemented to surface? Y	If yes, are the first three strings cemented to surface?	
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s well located in high Cave/Karst? If yes, are there two strings cemented to surface? Y	Is an engineered weak point used to satisfy R-111-Q?	
If yes, are there two strings cemented to surface?	If yes, at what depth is the weak point planned?	
If yes, are there two strings cemented to surface?		
	Is well located in high Cave/Karst?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?		Y
	(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
s well located in critical Cave/Karst?	Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	If yes, are there three strings cemented to surface?	

SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

		Casing Prog	ram Design B			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	500'	500'	13.375" 48# H40 STC	3.44	7.74	13.42	22.54
Int	12.25"	0'	0'	1795'	1795'	9.625" 36# J55 LTC	2.12	3.70	7.01	8.73
Production	8.75"	0'	0'	9760'	8840'	7" 26# P110 LTC	1.36	2.16	2.73	3.27
Liner	6.125"	8851'	8795'	16802'	8840'	4.5" 13.5# P110 LTC	2.11	2.45	3.15	3.93

Design B - Cement Program

Besign B Centent Fregran	Sign D - Centent Program											
Casing		# Sacks	Wt. lb/gal	Yield ft ³ /sack	тос/вос	Volume ft ³	% Excess	Slurry Description				
13,375 in	LEAD	210	12.5	2.12	0' - 313'	450	100%	Class C: Salt, Gel, Extender, LCM				
13.3/5 III	TAIL	200	14.8	1.34	313' - 500'	268	10078	Class C: Retarder				
9,625 in	LEAD	210	12.5	2.12	0' - 1125'	450	25%	Class C: Salt, Gel, Extender, LCM				
9.025 III	TAIL	200	14.8	1.34	1125' - 1795'	268	2370	Class C: Retarder				
1st Stg 7 in	LEAD	410	12.5	2.12	2725' - 7286'	870	25%	Class C: Salt, Gel, Extender, LCM, Defoamer				
1st Stg / III	TAIL	400	15.6	1.18	7286' - 9760'	472	2370	Class H: Retarder, Fluid Loss, Defoamer				
					7" DV	Tool @ 2725'						
2nd Stg 7 in	LEAD	50	12.5	2.12	1595' - 2104'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer				
2nd Stg / m	TAIL	100	14.8	1.34	2104' - 2725'	134	2370	Class C: Retarder, Fluid Loss, Defoamer				
4.5 in	LEAD	500 13.5		1.85	8851' - 16802'	930	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-				
		200	15.5	1.05	0051 - 10002	730	2570	settling Agent				

Design B - Mud Program

Depth	Mud Wt	Mud Type
	8.4 - 8.6	
0' - 500'	8.4 - 8.6	Fresh Water
500' - 1795'	9.5 - 10.2	Brine
1795' - 9760'	8.6 - 10.	Cut-Brine
9760' - 16802'	10.0 - 11.	OBM

Geology

Formation	Est. Top (TVD)	Mineral Resources	Formation	Est. Top (TVD)	Mineral Resources
Rustler			Yeso		
Castile			Delaware (Lamar)	1870'	Oil/Natural Gas
Salt Top	575'	None	Bell Canyon	1950'	Oil/Natural Gas
Salt Base	1642'	None	Cherry Canyon	2620'	Oil/Natural Gas
Yates			Manzanita Marker	2759'	Oil/Natural Gas
Seven Rivers			Basal Brushy Canyon	4934'	Oil/Natural Gas
Queen			Bone Spring	5303'	Oil/Natural Gas
Capitan			1st Bone Spring	6331'	Oil/Natural Gas
Grayburg			2nd Bone Spring	6796'	Oil/Natural Gas
San Andres			3rd Bone Spring	8401'	Oil/Natural Gas
Glorieta			Wolfcamp	8743'	Oil/Natural Gas

All casing strings will be tested in accordance with 43 CFR Part 3170 Subpart 3172. Must have table for contingency casing.

	V V
	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings comented to surface?	
-	

SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

Well Location GL: 3222'

Point	Calls	Leases	Aliquot	Section	Township	Range	County	Lat	Long	TVD	MD
SHL	SHL: 2020' FNL & 260' FEL (Sec 24)	Fee	SENE	24	23S	26E	Eddy	32.2918607	104.2386698	0'	0'
KOP	KOP: 400' FSL & 10' FEL (Sec 24)	NMNM0027994D	SESE	24	23S	26E	Eddy	32.2839331	104.2378868	8,267'	8,851'
FTP	FTP: 400' FSL & 330' FEL (Sec 24)	NMNM0027994D	SESE	24	23S	26E	Eddy	32.2839317	104.2389225	8,781'	9,489'
BHL	BHL: 400' FSL & 2335' FEL (Sec 23)	Fee	SWSE	23	23S	26E	Eddy	32.2838824	104.2625590	8,726'	16,802'

GEOLOGY

Formation	Est. Top (TVD)	Lithology	Mineral Resources	Formation	Est. Top (TVD)	Lithology	Mineral Resources
Rustler				Yeso			
Castile				Delaware (Lamar)	1870'	Limestone/Dolomite	Oil/Natural Gas
Salt Top	575'	Salt	None	Bell Canyon	1950'	Sandstone	Oil/Natural Gas
Salt Base	1642'	Salt	None	Cherry Canyon	2620'	Sandstone	Oil/Natural Gas
Yates				Manzanita Marker	2759'	Limestone	Oil/Natural Gas
Seven Rivers				Basal Brushy Canyon	4934'	Sandstone	Oil/Natural Gas
Queen				Bone Spring	5303'	Limestone	Oil/Natural Gas
Capitan				1st Bone Spring	6331'	Sandstone	Oil/Natural Gas
Grayburg				2nd Bone Spring	6796'	Sandstone	Oil/Natural Gas
San Andres				3rd Bone Spring	8401'	Sandstone	Oil/Natural Gas
Glorietta				Wolfcamp	8743'	Shale/Sandstone/Limestone	Oil/Natural Gas

		Casing Progra	am Design A		BLM Minimum Safety Factors	1.125	1.0	1.6 Dry 1.8 Wet	1.6 Dry 1.8 Wet	
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt Tension	SF Body Tension
Surface	17.5"	0'	0'	500'	500'	13.375" 48# H40 STC	3.44	7.74	13.42	22.54
Int	12.25"	0'	0'	1795'	1795'	9.625" 36# J55 LTC	2.12	3.70	7.01	8.73
Production	8.75"	0'	0'	8851'	8795'	7" 26# P110 LTC	1.36	2.18	3.01	3.61
Liner	6.125"	8651'	8595'	16802'	8840'	4.5" 13.5# P110 LTC	2.11	2.45	3.07	3.84

All casing strings will be tested in accordance with 43 CFR Part 3172. Must have table for contingency casing.

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
· ·	IN .
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

Design A - Cement Program

Csg. Size		# Sacks	Wt., lb/gal	Yield, ft ³ /sack	TOC/BOC	Volume, ft ³	% Excess	Slurry Description		
13,375 in	LEAD	210	12.5	2.12	0' - 313'	450	100%	Class C: Salt, Gel, Extender, LCM		
TAIL	TAIL	200	14.8	1.34	313' - 500'	268	10076	Class C: Retarder		
9,625 in	LEAD	210	12.5	2.12	0' - 1125'	450	25%	Class C: Salt, Gel, Extender, LCM		
9.025 III	TAIL	TAIL 200 14.8 1.34 1125' - 1795' 268	268	25%	Class C: Retarder					
1-4 64- 7 :	LEAD	330	12.5	2.12	2725' - 6384'	700	25%	Class C: Salt, Gel, Extender, LCM, Defoamer		
1st Stg 7 in	TAIL	400	15.6	1.18	6384' - 8851'	472	23%	Class H: Retarder, Fluid Loss, Defoamer		
7" DV Tool @ 2725'										
2nd Stg 7 in	LEAD	50	12.5	2.12	1595' - 2104'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer		
Ziiu Sig / iii	TAIL	100	14.8	1.34	2104' - 2725'	134	2376	Class C: Retarder, Fluid Loss, Defoamer		
4.5 in	LEAD	520	13.5	1.85	8651' - 16802'	970	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti- settling Agent		

Pressure Control Equipment

BOP installed and tested before drilling hole, in:	Size, in	System Rated WP	Туре			Tested to:	Rating Depth
		5M	Annular		X	2500#	16,802'
			Blind Ram		X		
12.25	13.375	5M	Pipe Ram		X	5000#	
			Double Ram			3000#	
			Other*				

^{*}Specify if additional ram is utilized.

Equipment: Annular, Pipe Rams, Blind Rams, Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Variance Request: A variance is requested for the use of a variable choke line from the BOP to the choke manifold. See attached for hydrostatic test chart. Anchors are not required by manufacturer. Variance is requested to use a multi bowl wellhead. Variance is requested to perform break testing according to attached procedure. If a breaktesting variance is approved & incorporated, API Standard 53 will be incorporated and testing annular BOP to 70% of RWP or 100% of MASP, whichever is greater, will be performed.

Testing Procedure: BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per 43 CFR Part 3172 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested. Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets.

	Y	Formation integrity test will be performed per 43 CFR Part 3172. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with 43 CFR Part 3172.
Γ	N	Mewbourne Oil Company request a variance to use a 5000 psi annular BOP with a 10,000 psi BOP stack.

Mud Program_

	Mud Wt.,	
Depth (MD)	lb/gal	Mud Type
	8.4 - 8.6	Fresh Water
0' - 500'	8.4 - 8.6	Fresh Water
500' - 1795'	9.5 - 10.2	Brine
1795' - 8851'	8.6 - 10.	Cut-Brine
8851' - 16802'	10.0 - 11.	OBM

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	tegen/DVT/Vigual Manifesting

SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

Logging and Testing Procedures

	Logging	, Coring and Testing.
	N	Will run GR/CNL from KOP (8851') to surface (horizontal well – vertical portion of hole). Stated logs run will be in the Completion Report and submitted to the BLM.
ſ	Y	No logs are planned based on well control or offset log information. Offset Well: Iceman 24/23 Fed Com #712H
ſ	N	Coring? If yes, explain:

Open & Cased Hole Logs Run In the Well

Caliper		Cement Bond Log	CNL/FDC
Compensated Densilog		Compensated Neutron Log	Computer Generated Log
Dip Meter Log	V	Directional Survey	Dual Induction/Microresistivity
Dual Lateral Log/Microspherically Focused		Electric Log	Formation Density Compensated Log
Gamma Ray Log	Ø	Measurement While Drilling	Mud Log/Geological Lithology Log
Other		Porosity-Resistivity Log	Sidewall Neutron Log
Sonic Log		Spontaneous Potential Log	Temperature Log

Drilling Conditions

Condition	Specify what type and where?
BH Pressure at deepest TVD	5056 psi
BH Temperature	165
Abnormal Temp, Pressure, or Geologic Hazards	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers in surface hole. Weighted mud for possible over-pressure in Wolfcamp formation.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

	H2S is present
Y	H2S Plan attached

SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

Other facets of operation

Mewbourne Oil Company also requests approval to implement Design B as described below. BLM will be notified of elected design.

Offline Cementing Variance: Variance is requested to perform offline cementing according to the attached procedure. R-111Q: Mewbourne is requested to perform Open Hole Cementing per R-111Q Guidelines if well is in Potash.

		Casing Progr	om Docion R			BLM Minimum Safety Factors	1.125	1.0	1.6 Dry	1.6 Dry
		Casing 1 rogi	am Design D			BEM Millimum Safety Pactors	1.123	1.0	1.8 Wet	1.8 Wet
String	Hole Size	Top MD	Top TVD	Bot MD	Bot TVD	Csg. Size	SF Collapse	SF Burst	SF Jt	SF Body
Surface	17.5"	0'	0'	500'	500'	13.375" 48# H40 STC	3.44	7.74	13.42	22.54
Int	12.25"	0'	0'	1795'	1795'	9.625" 36# J55 LTC	2.12	3.70	7.01	8.73
Production	8.75"	0'	0'	9760'	8840'	7" 26# P110 LTC	1.36	2.16	2.73	3.27
Liner	6.125"	8851'	8795'	16802'	8840'	4.5" 13.5# P110 LTC	2.11	2.45	3.15	3.93

All casing strings will be tested in accordance with 43 CFR Part 3172. Must have table for contingency casing.

An easing strings will be tested in accordance with 45 CFR 1 art 5172. Must have table for contingency easing.	
	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Is casing API approved? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	N
Is well located in SOPA but not in R-111-Q?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-Q and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 rd string set 100' to 600' below the base of salt?	
Is an open annulus used to satisfy R-111-Q? If yes, see cement design.	
Is an engineered weak point used to satisfy R-111-Q?	
If yes, at what depth is the weak point planned?	
Is well located in high Cave/Karst?	Y
If yes, are there two strings cemented to surface?	Y
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

Design B - Cement Program

	icht i rogram							
Csg. Size		# Sacks	Wt., lb/gal	Yield, ft ³ /sack	TOC/BOC	Volume, ft ³	% Excess	Slurry Description
13,375 in	LEAD	210	12.5	2.12	0' - 313'	450	100%	Class C: Salt, Gel, Extender, LCM
13.375 III	TAIL	200	14.8	1.34	313' - 500'	268	10076	Class C: Retarder
9.625 in	LEAD	210	12.5	2.12	0' - 1125'	450	25%	Class C: Salt, Gel, Extender, LCM
9.025 III	TAIL	200	14.8	1.34	1125' - 1795'	268	2376	Class C: Retarder
1st Stg 7 in	LEAD	410	12.5	2.12	2725' - 7286'	870	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
1st Stg / III	TAIL	400	15.6	1.18	7286' - 9760'	472	2376	Class H: Retarder, Fluid Loss, Defoamer
					7	"' DV Tool @ 2725'		
2nd Stg 7 in	LEAD	50	12.5	2.12	1595' - 2104'	110	25%	Class C: Salt, Gel, Extender, LCM, Defoamer
Ziiu Sig / Iii	TAIL	100	14.8	1.34	2104' - 2725'	134	2370	Class C: Retarder, Fluid Loss, Defoamer
4.5 in	LEAD	500	13.5	1.85	8851' - 16802'	930	25%	Class H: Salt, Gel, Fluid Loss, Retarder, Dispersant, Defoamer, Anti-
4.5 in LEAD		AD 300		1.00	0031 - 10802	930	23%	settling Agent

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #718H Sec 24, T23S, R26E

SHL: 2020' FNL & 260' FEL (Sec 24) BHL: 400' FSL & 2335' FEL (Sec 23)

Plan: Design #1

Standard Planning Report

13 June, 2024

Database: Hobbs

Company: Mewbourne Oil Company
Project: Eddy County, New Mexico NAD 83

Site: Iceman 24/23 Fed Com #718H

Well: Sec 24, T23S, R26E

Wellbore: BHL: 400' FSL & 2335' FEL (Sec 23)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #718H

Original Well @ 3250.0usft (Orignal Well)
Original Well @ 3250.0usft (Orignal Well)

Grid

Minimum Curvature

Project Eddy County, New Mexico NAD 83

Map System: US State Plane 1983
Geo Datum: North American Datum 1983
Map Zone: New Mexico Eastern Zone

System Datum:

Ground Level

Site Iceman 24/23 Fed Com #718H

 Site Position:
 Northing:
 469,924.50 usft
 Latitude:
 32.2918607

 From:
 Map
 Easting:
 570,588.70 usft
 Longitude:
 -104.2386699

Position Uncertainty: 0.0 usft Slot Radius: 13-3/16 "

Well Sec 24, T23S, R26E

 Well Position
 +N/-S
 0.0 usft
 Northing:
 469,924.50 usft
 Latitude:
 32.2918607

 +E/-W
 0.0 usft
 Easting:
 570,588.70 usft
 Longitude:
 -104.2386699

Position Uncertainty

0.0 usft

Wellhead Elevation:

3,250.0 usft

Ground Level:

3,222.0 usft

Grid Convergence: 0.05 °

Wellbore BHL: 400' FSL & 2335' FEL (Sec 23)

 Magnetics
 Model Name
 Sample Date
 Declination (°)
 Dip Angle (°)
 Field Strength (nT)

 IGRF2010
 12/31/2014
 7.46
 60.05
 48,206.87022632

Design Design #1

Audit Notes:

Version:Phase:PROTOTYPETie On Depth:0.0

 Vertical Section:
 Depth From (TVD) (usft)
 +N/-S (usft)
 +E/-W (usft)
 Direction (usft)

 0.0
 0.0
 0.0
 0.0
 248.49

Plan Survey Tool Program Date 6/13/2024

Depth From Depth To

(usft) (usft) Survey (Wellbore) Tool Name Remarks

1 0.0 16,802.3 Design #1 (BHL: 400' FSL & 233t

Plan Sections Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
600.0	0.00	0.00	600.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,810.2	24.20	175.15	1,774.5	-250.9	21.3	2.00	2.00	0.00	175.15	
7,640.7	24.20	175.15	7,092.5	-2,632.8	223.2	0.00	0.00	0.00	0.00	
8,850.9	0.00	0.00	8,267.0	-2,883.7	244.5	2.00	-2.00	0.00	180.00 k	OP: 400' FSL & 10
9,760.3	90.93	269.82	8,840.0	-2,885.6	-337.8	10.00	10.00	0.00	-90.18	
16,802.3	90.93	269.82	8,726.0	-2,908.1	-7,378.9	0.00	0.00	0.00	0.00 E	3HL: 400' FSL & 23

Database: Company:

Project:

Wellbore:

Site:

Hobbs

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #718H

Well: Sec 24, T23S, R26E

BHL: 400' FSL & 2335' FEL (Sec 23)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #718H Original Well @ 3250.0usft (Orignal Well) Original Well @ 3250.0usft (Orignal Well)

Grid

ed Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0		0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
	0' FNL & 260' F		400.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0 200.0		0.00 0.00	100.0 200.0	0.0 0.0	0.0 0.0	0.0 0.0	0.00 0.00	0.00 0.00	0.00 0.00
300.0		0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0		0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0		0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0		175.15	700.0	-1.7	0.1	0.5	2.00	2.00	0.00
800.0 900.0		175.15 175.15	799.8 899.5	-7.0 -15.6	0.6 1.3	2.0 4.5	2.00 2.00	2.00 2.00	0.00 0.00
1,000.0		175.15	998.7	-13.0	2.4	8.0	2.00	2.00	0.00
1,100.0		175.15	1,097.5	-27.6 -43.4	3.7	12.5	2.00	2.00	0.00
1,100.0		175.15	1,195.6	-62.4	5.3	18.0	2.00	2.00	0.00
1,300.0	14.00	175.15	1,293.1	-84.8	7.2	24.4	2.00	2.00	0.00
1,400.0	16.00	175.15	1,389.6	-110.6	9.4	31.8	2.00	2.00	0.00
1,500.0		175.15	1,485.3	-139.7	11.8	40.2	2.00	2.00	0.00
1,600.0		175.15	1,579.8	-172.2	14.6	49.5	2.00	2.00	0.00
1,700.0 1,800.0		175.15 175.15	1,673.2 1,765.2	-207.9 -246.8	17.6	59.8	2.00 2.00	2.00	0.00
1,810.2		175.15	1,765.2	-240.6 -250.9	20.9 21.3	71.0 72.2	2.00	2.00 2.00	0.00 0.00
1,900.0		175.15	1,856.4	-287.6	24.4	82.8	0.00	0.00	0.00
2,000.0		175.15	1,947.6	328.5	27.9	94.5	0.00	0.00	0.00
2,100.0		175.15	2,038.9	-369.3	31.3	106.3	0.00	0.00	0.00
2,200.0 2,300.0		175.15 175.15	2,130.1 2,221.3	-410.2 -451.0	34.8 38.2	118.0 129.8	0.00 0.00	0.00 0.00	0.00 0.00
2,400.0		175.15	2,312.5	-491.9	41.7	141.6	0.00	0.00	0.00
2,500.0		175.15	2,403.7	-532.7	45.2	153.3	0.00	0.00	0.00
2,600.0		175.15	2,494.9	-573.6	48.6	165.1	0.00	0.00	0.00
2,700.0		175.15	2,586.1	-614.4	52.1	176.8	0.00	0.00	0.00
2,800.0		175.15	2,677.3	-655.3	55.6	188.6	0.00	0.00	0.00
2,900.0		175.15	2,768.5	-696.1	59.0	200.3	0.00	0.00	0.00
3,000.0 3,100.0	24.20 24.20	175.15 175.15	2,859.7 2,950.9	-737.0 -777.8	62.5 66.0	212.1 223.8	0.00 0.00	0.00 0.00	0.00 0.00
3,200.0		175.15	3,042.2	-777.0 -818.7	69.4	235.6	0.00	0.00	0.00
3,300.0		175.15	3,133.4	-859.5	72.9	247.4	0.00	0.00	0.00
3,400.0		175.15	3,224.6	-900.4	76.3	259.1	0.00	0.00	0.00
3,500.0		175.15	3,315.8	-941.2	79.8	270.9	0.00	0.00	0.00
3,600.0		175.15	3,407.0	-982.1	83.3	282.6	0.00	0.00	0.00
3,700.0 3,800.0		175.15 175.15	3,498.2 3,589.4	-1,022.9 -1,063.8	86.7 90.2	294.4 306.1	0.00 0.00	0.00 0.00	0.00 0.00
3,900,0		175.15	3,680.6	-1,104.6	93.7	317.9	0.00	0.00	0.00
4,000.0	24.20	175.15	3,771.8	-1,145.5	97.1	329.7	0.00	0.00	0.00
4,100.0	24.20	175.15	3,863.0	-1,186.4	100.6	341.4	0.00	0.00	0.00
4,200.0 4,300.0		175.15 175.15	3,954.3	-1,227 <u>.</u> 2	104.1 107.5	353.2 364.9	0.00	0.00 0.00	0.00
			4,045.5	-1,268.1			0.00		0.00
4,400.0 4,500.0		175.15 175.15	4,136.7 4,227.9	-1,308.9 -1,349.8	111.0 114.4	376.7 388.4	0.00 0.00	0.00 0.00	0.00 0.00
4,600.0		175.15	4,319.1	-1,349.6 -1,390.6	117.9	400.2	0.00	0.00	0.00
4,700.0	24.20	175.15	4,410.3	-1,431.5	121.4	411.9	0.00	0.00	0.00
4,800.0	24.20	175.15	4,501.5	-1,472.3	124.8	423.7	0.00	0.00	0.00
4,900.0		175.15	4,592.7	-1,513.2	128.3	435.5	0.00	0.00	0.00
5,000.0 5,100.0		175.15 175.15	4,683.9 4,775.1	-1,554.0 -1,594.9	131.8 135.2	447.2 459.0	0.00 0.00	0.00 0.00	0.00 0.00

Database: Company: Project:

Site:

Hobbs

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #718H

Sec 24, T23S, R26E Well:

Wellbore: BHL: 400' FSL & 2335' FEL (Sec 23) Design:

Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #718H Original Well @ 3250.0usft (Orignal Well) Original Well @ 3250.0usft (Orignal Well)

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,200.0	24.20	175.15	4,866.3	-1,635.7	138.7	470.7	0.00	0.00	0.00
5,300.0	24.20	175.15	4,957.6	-1,676.6	142.2	482.5	0.00	0.00	0.00
5,400.0	24.20	175.15	5,048.8	-1,717.4	145.6	494.2	0.00	0.00	0.00
5,500.0	24.20	175.15	5,140.0	-1,758.3	149.1	506.0	0.00	0.00	0.00
5,600.0	24.20	175.15	5,231.2	-1,799.1	152.5	517.8	0.00	0.00	0.00
5,700.0	24.20	175.15	5,322.4	-1,840.0	156.0	529.5	0.00	0.00	0.00
5,800.0	24.20	175.15	5,413.6	-1,880.8	159.5	541.3	0.00	0.00	0.00
5,900.0	24.20	175.15	5,504.8	-1,921.7	162.9	553.0	0.00	0.00	0.00
6,000.0	24.20	175.15	5,596.0	-1,962.5	166.4	564.8	0.00	0.00	0.00
6,100.0	24.20	175.15	5,687.2	-2,003.4	169.9	576.5	0.00	0.00	0.00
6,200.0	24.20	175.15	5,778.4	-2,044.2	173.3	588.3	0.00	0.00	0.00
6,300.0	24.20	175.15	5,869.7	-2,085.1	176.8	600.0	0.00	0.00	0.00
6,400.0	24.20	175.15	5,960.9	-2,125.9	180.3	611.8	0.00	0.00	0.00
6,500.0	24.20	175.15	6,052.1	-2,166.8	183.7	623.6	0.00	0.00	0.00
6,600.0	24.20	175.15	6,143.3	-2,207.6	187.2	635.3	0.00	0.00	0.00
6,700.0	24.20	175.15	6,234.5	-2,248.5	190.6	647.1	0.00	0.00	0.00
6,800.0	24.20	175.15	6,325.7	-2,289.3	194.1	658.8	0.00	0.00	0.00
6,900.0	24.20	175.15	6,416.9	-2,330.2	197.6	670.6	0.00	0.00	0.00
7,000.0	24.20	175.15	6,508.1	-2,371.0	201.0	682.3	0.00	0.00	0.00
7,100.0	24.20	175.15	6,599.3	-2,411.9	204.5	694.1	0.00	0.00	0.00
7,200.0	24.20	175.15	6,690.5	-2,452.7	208.0	705.9	0.00	0.00	0.00
7,300.0	24.20	175.15	6,781.7	-2,493.6	211.4	717.6	0.00	0.00	0.00
7,400.0	24.20	175.15	6,873.0	-2,534.4	214.9	729.4	0.00	0.00	0.00
7,500.0	24.20	175.15	6,964.2	-2,575.3	218.4	741.1	0.00	0.00	0.00
7,600.0	24.20	175.15	7,055.4	-2,616.1	221.8	752.9	0.00	0.00	0.00
7,640.7	24.20	175.15	7,092.5	-2,632.8	223.2	757.7	0.00	0.00	0.00
7,700.0	23.02	175.15	7,146.8	-2,656.4	225.2	764.5	2.00	-2.00	0.00
7,800.0	21.02	175.15	7,239.5	-2,693.8	228.4	775.2	2.00	-2.00	0.00
7,900.0	19.02	175.15	7,333.5	-2,727.9	231.3	785.0	2.00	-2.00	0.00
8,000.0	17.02	175.15	7,428.6	-2,758.7	233.9	793.9	2.00	-2.00	0.00
8,100.0	15.02	175.15	7,524.7	-2,786.2	236.2	801.8	2.00	-2.00	0.00
8,200.0	13.02	175.15	7,621.7	-2,810.3	238.3	808.8	2.00	-2.00	0.00
8,300.0	11.02	175.15	7,719.5	-2,831.1	240.0	814.7	2.00	-2.00	0.00
8,400.0	9.02	175.15	7,818.0	-2,848.4	241.5	819.7	2.00	-2.00	0.00
8,500.0	7.02	175.15	7,917.0	-2,862.3	242.7	823.7	2.00	-2.00	0.00
8,600.0	5.02	175.15	8,016.4	-2,872.8	243.6	826.7	2.00	-2.00	0.00
8,700.0	3.02	175.15	8,116.2	-2,879.7	244.2	828.7	2.00	-2.00	0.00
8,800.0 8,850.9	1.02 0.00 FSL & 10' FEL	175.15 0.00	8,216.1 8,267.0	-2,883.2 -2,883.7	244.5 244.5	829.7 829.9	2.00 2.00	-2.00 -2.00	0.00 0.00
8,900.0 8,950.0 9,000.0	4.91 9.91 14.91	269.82 269.82 269.82 269.82	8,316.1 8,365.6 8,414.4	-2,883.7 -2,883.7 -2,883.8	242.4 235.9 225.2	831.8 837.8 847.8	10.00 10.00 10.00	10.00 10.00 10.00	0.00 0.00 0.00
9,050.0	19.91	269.82	8,462.1	-2,883.8	210.3	861.8	10.00	10.00	0.00
9,100.0	24.91	269.82	8,508.4	-2,883.9	191.2	879.5	10.00	10.00	0.00
9,150.0	29.91	269.82	8,552.7	-2,883.9	168.2	901.0	10.00	10.00	0.00
9,200.0	34.91	269.82	8,594.9	-2,884.0	141.4	925.9	10.00	10.00	0.00
9,250.0	39.90	269.82	8,634.6	-2,884.1	111.0	954.2	10.00	10.00	0.00
9,300.0	44.90	269.82	8,671.5	-2,884.2	77.3	985.6	10.00	10.00	0.00
9,350.0	49.90	269.82	8,705.4	-2,884.4	40.5	1,019.9	10.00	10.00	0.00
9,400.0	54.90	269.82	8,735.9	-2,884.5	0.9	1,056.8	10.00	10.00	0.00
9,450.0	59.90	269.82	8,762.8	-2,884.6	-41.2	1,096.0	10.00	10.00	0.00
9,488.8	63.78	269.82	8,781.1	-2,884.7	-75.4	1,127.9	10.00	10.00	0.00
FTP: 400' I	FSL & 330' FEI	L (Sec 24)							

Database: Company:

Project:

Site:

Hobbs

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #718H

Well: Sec 24, T23S, R26E

Wellbore: BHL: 400' FSL & 2335' FEL (Sec 23)

Design: Design #1

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Site Iceman 24/23 Fed Com #718H Original Well @ 3250.0usft (Orignal Well) Original Well @ 3250.0usft (Orignal Well)

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,500.0	64.90	269.82	8,786.0	-2,884.8	-85.5	1,137.2	10.00	10.00	0.00
9,550.0	69.90	269.82	8,805.2	-2,884.9	-131.6	1,180.2	10.00	10.00	0.00
9,600.0	74.90	269.82	8,820.3	-2,885.1	-179.3	1,224.6	10.00	10.00	0.00
9,650.0	79.90	269.82	8,831.2	-2,885.2	-228.0	1,270.1	10.00	10.00	0.00
9,700.0	84.90	269.82	8,837.8	-2,885.4	-277.6	1,316.2	10.00	10.00	0.00
9,750.0	89.89	269.82	8,840.1	-2,885.5	-327.5	1,362.7	10.00	10.00	0.00
9,760.3	90.92	269.82	8,840.0	-2,885.6	-337.8	1,372.3	10.00	10.00	0.00
	SL & 583' FEL								
9,800.0	90.93	269.82	8,839.4	-2,885.7	-377.5	1,409.3	0.01	0.01	0.00
9,900.0	90.93	269.82	8,837.7	-2,886.0	-477.5	1,502.4	0.00	0.00	0.00
10,000.0	90.93	269.82	8,836.1	-2,886.3	-577.5	1,595.6	0.00	0.00	0.00
10,100.0	90.93	269.82	8,834.5	-2,886.7	-677.5	1,688.7	0.00	0.00	0.00
10,200.0	90.93	269.82	8,832.9	-2,887.0	-777.5	1,781.8	0.00	0.00	0.00
10,300.0	90.93	269.82	8,831.3	-2,887.3	-877.4	1,875.0	0.00	0.00	0.00
10,400.0	90.93	269.82	8,829.6	-2,887.6	-977.4	1,968.1	0.00	0.00	0.00
10,500.0	90.93	269.82	8,828.0	-2,887.9	-1,077.4	2,061.3	0.00	0.00	0.00
10,600.0	90.93	269.82	8,826.4	-2,888.3	-1,177.4	2,154.4	0.00	0.00	0.00
10,700.0	90.93	269.82	8,824.8	-2,888.6	-1,277.4	2,247.5	0.00	0.00	0.00
10,800.0	90.93	269.82	8,823.2	-2,888.9	-1,377.4	2,340.7	0.00	0.00	0.00
10,900.0	90.93	269.82	8,821.6	-2,889.2	-1,477.4	2,433.8	0.00	0.00	0.00
11,000.0	90.93	269.82	8,819.9	-2,889.5	-1,577.3	2,527.0	0.00	0.00	0.00
11,100.0	90.93	269.82	8,818.3	-2,889.9	-1,677.3	2,620.1	0.00	0.00	0.00
11,200.0	90.93	269.82	8,816.7	-2,890.2	-1,777.3	2,713.2	0.00	0.00	0.00
11,300.0	90.93	269.82	8,815.1	-2,890.5	-1,877.3	2,806.4	0.00	0.00	0.00
11,400.0	90.93	269.82	8,813.5	-2,890.8	-1,977.3	2,899.5	0.00	0.00	0.00
11,500.0	90.93	269.82	8,811.8	-2,891.1	-2,077.3	2,992.7	0.00	0.00	0.00
11,600.0	90.93	269.82	8,810.2	-2,891.5	-2,177.3	3,085.8	0.00	0.00	0.00
11,700.0	90.93	269.82	8,808.6	-2,891.8	-2,277.2	3,179.0	0.00	0.00	0.00
11,800.0	90.93	269.82	8,807.0	-2,892.1	-2,377.2	3,272.1	0.00	0.00	0.00
11,900.0	90.93	269.82	8,805.4	-2,892.4	-2,477.2	3,365.2	0.00	0.00	0.00
12,000.0	90.93	269.82	8,803.7	-2,892.7	-2,577.2	3,458.4	0.00	0.00	0.00
12,100.0	90.93	269.82	8,802.1	-2,893.1	-2,677.2	3,551.5	0.00	0.00	0.00
12,200.0	90.93	269.82	8,800.5	-2,893.4	-2,777.2	3,644.7	0.00	0.00	0.00
12,300.0	90.93	269.82	8,798.9	-2,893.7	-2,877.2	3,737.8	0.00	0.00	0.00
12,400.0	90.93	269.82	8,797.3	-2,894.0	-2,977.2	3,830.9	0.00	0.00	0.00
12,500.0	90.93	269.82	8,795.6	-2,894.3	-3,077.1	3,924.1	0.00	0.00	0.00
12,600.0	90.93	269.82	8,794.0	-2,894.7	-3,177.1	4,017.2	0.00	0.00	0.00
12,700.0	90.93	269.82	8,792.4	-2,895.0	-3,277.1	4,110.4	0.00	0.00	0.00
12,800.0	90.93	269.82	8,790.8	-2,895.3	-3,377.1	4,203.5	0.00	0.00	0.00
12,900.0	90.93	269.82	8,789.2	-2,895.6	-3,477.1	4,296.6	0.00	0.00	0.00
13,000.0	90.93	269.82	8,787.6	-2,895.9	-3,577.1	4,389.8	0.00	0.00	0.00
13,100.0	90.93	269.82	8,785.9	-2,896.3	-3,677.1	4,482.9	0.00	0.00	0.00
13,200.0	90.93	269.82	8,784.3	-2,896.6	-3,777.0	4,576.1	0.00	0.00	0.00
13,300.0	90.93	269.82	8,782.7	-2,896.9	-3,877.0	4,669.2	0.00	0.00	0.00
13,400.0	90.93	269.82	8,781.1	-2,897.2	-3,977.0	4,762.3	0.00	0.00	0.00
13,500.0	90.93	269.82	8,779.5	-2,897.5	-4,077.0	4,855.5	0.00	0.00	0.00
13,600.0	90.93	269.82	8,777.8	-2,897.9	-4,177.0	4,948.6	0.00	0.00	0.00
13,700.0	90.93	269.82	8,776.2	-2,898.2	-4,277.0	5,041.8	0.00	0.00	0.00
13,800.0	90.93	269.82	8,774.6	-2,898.5	-4,377.0	5,134.9	0.00	0.00	0.00
13,900.0	90.93	269.82	8,773.0	-2,898.8	-4,476.9	5,228.0	0.00	0.00	0.00
14,000.0	90.93	269.82	8,771.4	-2,899.1	-4,576.9	5,321.2	0.00	0.00	0.00
14,100.0	90.93	269.82	8,769.7	-2,899.5	-4,676.9	5,414.3	0.00	0.00	0.00
14,200.0	90.93	269.82	8,768.1	-2,899.8	-4,776.9	5,507.5	0.00	0.00	0.00

Database: Company: Project:

Site:

Hobbs

Mewbourne Oil Company

Eddy County, New Mexico NAD 83 Iceman 24/23 Fed Com #718H

Well: S

Sec 24, T23S, R26E

Wellbore: BHL: 400' FSL & 2335' FEL (Sec 23)
Design: Design #1

Local Co-ordinate Reference: TVD Reference:

MD Reference:
North Reference:

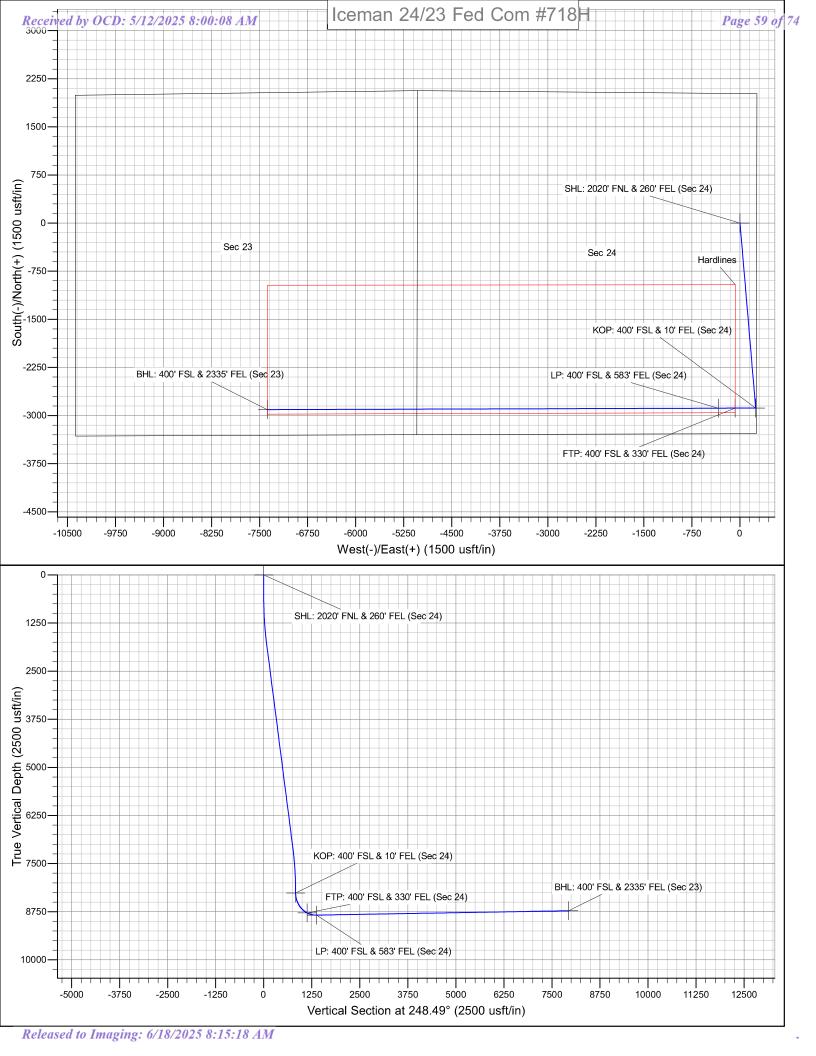
Survey Calculation Method:

Site Iceman 24/23 Fed Com #718H Original Well @ 3250.0usft (Orignal Well) Original Well @ 3250.0usft (Orignal Well)

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
14,300.0	90.93	269.82	8,766.5	-2,900.1	-4,876.9	5,600.6	0.00	0.00	0.00
14,400.0	90.93	269.82	8,764.9	-2,900.4	-4,976.9	5,693.7	0.00	0.00	0.00
14,500.0	90.93	269.82	8,763.3	-2,900.7	-5,076.9	5,786.9	0.00	0.00	0.00
14,600.0	90.93	269.82	8,761.7	-2,901.1	-5,176.9	5,880.0	0.00	0.00	0.00
14,700.0	90.93	269.82	8,760.0	-2,901.4	-5,276.8	5,973.2	0.00	0.00	0.00
14,800.0	90.93	269.82	8,758.4	-2,901.7	-5,376.8	6,066.3	0.00	0.00	0.00
14,900.0	90.93	269.82	8,756.8	-2,902.0	-5,476.8	6,159.4	0.00	0.00	0.00
15,000.0	90.93	269.82	8,755.2	-2,902.3	-5,576.8	6,252.6	0.00	0.00	0.00
15,100.0	90.93	269.82	8,753.6	-2,902.7	-5,676.8	6,345.7	0.00	0.00	0.00
15,200.0	90.93	269.82	8,751.9	-2,903.0	-5,776.8	6,438.9	0.00	0.00	0.00
15,300.0	90.93	269.82	8,750.3	-2,903.3	-5,876.8	6,532.0	0.00	0.00	0.00
15,400.0	90.93	269.82	8,748.7	-2,903.6	-5,976.7	6,625.1	0.00	0.00	0.00
15,500.0	90.93	269.82	8,747.1	-2,903.9	-6,076.7	6,718.3	0.00	0.00	0.00
15,600.0	90.93	269.82	8,745.5	-2,904.3	-6,176.7	6,811.4	0.00	0.00	0.00
15,700.0	90.93	269.82	8,743.8	-2,904.6	-6,276.7	6,904.6	0.00	0.00	0.00
15,800.0	90.93	269.82	8,742.2	-2,904.9	-6,376.7	6,997.7	0.00	0.00	0.00
15,900.0	90.93	269.82	8,740.6	-2,905.2	-6,476.7	7,090.8	0.00	0.00	0.00
16,000.0	90.93	269.82	8,739.0	-2,905.5	-6,576.7	7,184.0	0.00	0.00	0.00
16,100.0	90.93	269.82	8,737.4	-2,905.9	-6,676.6	7,277.1	0.00	0.00	0.00
16,200.0	90.93	269.82	8,735.8	-2,906.2	-6,776.6	7,370.3	0.00	0.00	0.00
16,300.0	90.93	269.82	8,734.1	-2,906.5	-6,876.6	7,463.4	0.00	0.00	0.00
16,400.0	90.93	269.82	8,732.5	-2,906.8	-6,976.6	7,556.5	0.00	0.00	0.00
16,500.0	90.93	269.82	8,730.9	-2,907.1	-7,076.6	7,649.7	0.00	0.00	0.00
16,600.0 16,700.0 16,802.3 BHL: 400'	90.93 90.93 90.93 FSL & 2335' FI	269.82 269.82 269.82 EL (Sec 23)	8,729.3 8,727.7 8,726.0	-2,907.5 -2,907.8 -2,908.1	-7,176.6 -7,276.6 -7,378.9	7,742.8 7,836.0 7,931.3	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SHL: 2020' FNL & 260 - plan hits target co - Point	0.00 enter	0.00	0.0	0.0	0.0	469,924.50	570,588.70	32.2918607	-104.2386699
KOP: 400' FSL & 10' F - plan hits target ce - Point	0.00 enter	0.00	8,267.0	-2,883.7	244.5	467,040.80	570,833.20	32.2839332	-104.2378869
BHL: 400' FSL & 2335 - plan hits target ce - Point	0.00 enter	0.00	8,726.0	-2,908.1	-7,378.9	467,016.40	563,209.80	32,2838824	-104.2625559
FTP: 400' FSL & 330' - plan hits target ce - Point	0.00 enter	0.00	8,781.1	-2,884.7	-75.4	467,039.78	570,513.30	32.2839312	-104.2389221
LP: 400' FSL & 583' F - plan hits target ce - Point	0.00 enter	0.00	8,840.0	-2,885.6	-337.8	467,038.94	570,250.90	32.2839295	-104.2397712



SHL: 2020' FNL 260' FEL (Sec 24) BHL: 400' FSL 2335' FEL (Sec 23)

Operator Name:	Property Name:	Well Number
Mewbourne Oil Company	Iceman 24/23 Fed Com	718H

Kick Off Point (KOP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
P	24	23	26	_	400'	FSL	10'	FEL	Eddy
	Latitude				Longitude				NAD
32.2839331				-104.23788	368			83	

First Take Point (FTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
P	24	23	26	-	400'	FSL	330'	FEL	Eddy
	Latitude					NAD			
32.2839317					-104.23892	225			83

Last Take Point (LTP)

UL	Section	Township	Range	Lot	Feet	From N/S	Feet	From E/W	County
О	23	23	26	-	400'	FSL	2335'	FEL	Eddy
	Latitude				Longitude				NAD
32.2838824					-104.26255	590			83

Is this well the defining well for this well an infill well?	the Horizontal Spacing Unit?	Y	
If infill is yes please provide API Spacing Unit.	if available, Operator Name as	nd well number for Defining well for Horizon	ntal
API#			
Operator Name:	Property Name:		Well Number

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: MEWBOURNE OIL COMPANY WELL NAME & NO.: ICEMAN 24/23 FED COM 718H

APD ID: 10400099109

LOCATION: Section 24, T23S, R26E. NMP
COUNTY: Eddy County, New Mexico

COA

H_2S	0	No	•	Yes
Potash /	None	Secretary	C R-111-Q	Open Annulus
WIPP				■ WIPP
Cave / Karst	C Low	Medium	• High	Critical
Wellhead	Conventional	• Multibowl	C Both	Diverter
Cementing	Primary Squeeze	Cont. Squeeze	EchoMeter	DV Tool
Special Req	Capitan Reef	Water Disposal	▼ COM	Unit
Waste Prev.	C Self-Certification	Waste Min. Plan	C APD Submitted p	prior to 06/10/2024
Additional	Flex Hose	Casing Clearance	Pilot Hole	Break Testing
Language	Four-String	Offline Cementing	Fluid-Filled	

A. HYDROGEN SULFIDE

A Hydrogen Sulfide (H₂S) Drilling Plan shall be activated **AT SPUD**. As a result, the Hydrogen Sulfide area must meet **43 CFR 3176** requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.

B. CASING DESIGN

Primary Casing Design

- 1. The 13-3/8 inch surface casing shall be set at approximately 500 ft. (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of 8

- <u>hours</u> or **500 psi compressive strength**, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 psi compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 1,795 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.

Note: Excess cement is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. Operator has proposed to set 7 in. production casing at approximately 8,851 ft. (8,267 ft. TVD). The minimum required fill of cement behind the 7 in. production casing is:
 - Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
 - **Option 2 (Two-stage):** Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.
 - a. **First stage to DV tool:** Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
 - b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
- 4. The minimum required fill of cement behind the 4-1/2 in. production liner is:
 - Cement should tie-back at least 100 feet into previous casing string. Operator shall provide method of verification.

Alternate Casing Design

- 1. The 13-3/8 inch surface casing shall be set at approximately 500 ft. (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 ft. above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic-type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>8</u> hours or 500 psi compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 psi compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The 9-5/8 inch intermediate casing shall be set in a competent bed at approximately 1,795 ft. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
 - Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.

Note: Excess cement is less than 25%, more cement is required if washout occurs. Adjust cement volume and excess based on a fluid caliper or similar method that reflects the as-drilled size of the wellbore.

- ❖ In <u>High Cave/Karst Areas</u> if cement does not circulate to surface on the first two casing strings, the cement on the 3rd casing string must come to surface.
- 3. Operator has proposed to set 7 in. production casing at approximately 9,760 ft. (8,840 ft. TVD). The minimum required fill of cement behind the 7 in. production casing is:
 - Option 1 (Single Stage): Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
 - **Option 2 (Two-stage):** Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool: Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.
- **4.** The minimum required fill of cement behind the **4-1/2 in.** production liner is:
 - Cement should tie-back at least 100 feet into previous casing string. Operator shall provide method of verification.

Offline Cementing

Operator has been (Approved) to pump the proposed cement program offline in the Surface and intermediate(s) intervals. Offline cementing should commence within 24 hours of landing the casing for the interval. Notify the BLM 4hrs prior to the commencement of any offline cementing procedure at Eddy County: 575-361-2822.

C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 5000 (5M) psi. The BOP/BOPE and annular preventer shall be pressure-tested in accordance with title 43 CFR 3172.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.
 - d. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
 - e. Whenever any seal subject to test pressure is broken, all the tests in the title 43 CFR 3172.6(b)(9) must be followed.

BOPE Break Testing Variance

• BOPE Break Testing is ONLY permitted for intervals utilizing a 5M BOPE or

less. (Annular preventer must be tested to a minimum of 70% of BOPE working pressure and shall be higher than the MASP.)

- BOPE Break Testing is NOT permitted to drilling the production hole section.
- Variance only pertains to the intermediate hole-sections and no deeper than the Bone Springs formation.
- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer (575-706-2779) prior to the commencement of any BOPE Break Testing operations.
- A full BOPE test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOPE test will be required. (200' TVD tolerance between intermediate shoes is allowable).
- The BLM is to be contacted (575-361-2822 Eddy County) 4 hours prior to BOPE
- As a minimum, a full BOPE test shall be performed at 21-day intervals.
- In the event any repairs or replacement of the BOPE is required, the BOPE shall test as per 43 CFR 3172.
- If in the event break testing is not utilized, then a full BOPE test would be conducted.

D. SPECIAL REQUIREMENT (S)

Communitization Agreement

- The operator will submit a Communitization Agreement to the Santa Fe Office, 301 Dinosaur Trail Santa Fe, New Mexico 87508, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.
- If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.
- In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

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Contact Eddy County Petroleum Engineering Inspection Staff:

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; **BLM_NM_CFO_DrillingNotifications@BLM.GOV**; (575) 361-2822.

- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - i. Notify the BLM when moving in and removing the Spudder Rig.
 - ii. Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the doghouse or stairway area.
- For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until

- both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- **4.** Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- **5.** No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- **6.** On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- **8.** Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in 43 CFR 3172.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and

- hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- **4.** If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - iii. Manufacturer representative shall install the test plug for the initial BOP test.
 - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
 - v. If the cement does not circulate and one-inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the cement plug with the casing valve open. (Only applies to single stage cement jobs, prior to the cement setting up.)
 - iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing

valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).

- iv. The test shall be run on a 5000-psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one-hour chart. A circular chart shall have a maximum 2-hour clock. If a twelve hour or twenty-four-hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low-pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per 43 CFR 3172.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crewintensive operations.

SA 05/02/2025

Hydrogen Sulfide Drilling Operations Plan Mewbourne Oil Company

1. General Requirements

Rule 118 does not apply to this well because MOC has researched this area and no high concentrations of H2S were found. MOC will have on location and working all H2S safety equipment before the Delaware formation for purposes of safety and insurance requirements.

2. Hydrogen Sulfide Training

All personnel, whether regularly assigned, contracted, or employed on an unscheduled basis, will have received training from a qualified instructor in the following areas prior to entering the drilling pad area of the well:

- 1. The hazards and characteristics of hydrogen sulfide gas.
- 2. The proper use of personal protective equipment and life support systems.
- 3. The proper use of hydrogen sulfide detectors, alarms, warning systems, briefing areas, evacuation procedures.
- 4. The proper techniques for first aid and rescue operations.

Additionally, supervisory personnel will be trained in the following areas:

- The effects of hydrogen sulfide on metal components. If high tensile tubular systems are utilized, supervisory personnel will be trained in their special maintenance requirements.
- 2 Corrective action and shut in procedures, blowout prevention, and well control procedures while drilling a well.
- The contents of the Hydrogen Sulfide Drilling Operations Plan.

There will be an initial training session prior to encountering a know hydrogen sulfide source. The initial training session shall include a review of the site specific Hydrogen Sulfide Drilling Operations Plan.

3. Hydrogen Sulfide Safety Equipment and Systems

All hydrogen sulfide safety equipment and systems will be installed, tested, and operational prior to drilling below the 9 5/8" intermediate casing.

1. Well Control Equipment

- A. Choke manifold with minimum of one adjustable choke/remote choke.
- B. Blowout preventers equipped with blind rams and pipe rams to accommodate all pipe sizes with properly sized closing unit
- C. Auxiliary equipment including annular type blowout preventer.
- 2. <u>Protective Equipment for Essential Personnel</u>

Thirty minute self contained work unit located in the dog house and at briefing areas.

Additionally: If H2S is encountered in concentrations less than 10 ppm, fans will be placed in work areas to prevent the accumulation of hazardous amounts of poisonous gas. If higher concentrations of H2S are detected the well will be shut in and a rotating head, mud/gas separator, remote choke and flare line with igniter will be installed.

3. <u>Hydrogen Sulfide Protection and Monitoring Equipment</u>

Two portable hydrogen sulfide monitors positioned on location for optimum coverage and detection. The units shall have audible sirens to notify personnel when hydrogen sulfide levels exceed 20 PPM.

4. <u>Visual Warning Systems</u>

- A. Wind direction indicators as indicated on the wellsite diagram.
- B. Caution signs shall be posted on roads providing access to location. Signs shall be painted a high visibility color with lettering of sufficient size to be readable at reasonable distances from potentially contaminated areas.

4. Mud Program

The mud program has been designed to minimize the amount of hydrogen sulfide entrained in the mud system. Proper mud weight, safe drilling practices, and the use of hydrogen sulfide scavengers will minimize hazards while drilling the well.

5. Metallurgy

All tubular systems, wellheads, blowout preventers, drilling spools, kill lines, choke manifolds, and valves shall be suitable for service in a hydrogen sulfide environment when chemically treated.

6. Communications

State & County Officials phone numbers are posted on rig floor and supervisors trailer. Communications in company vehicles and toolpushers are either two way radios or cellular phones.

7. Well Testing

Drill stem testing is not an anticipated requirement for evaluation of this well. If a drill stem test is required, it will be conducted with a minimum number of personnel in the immediate vicinity. The test will be conducted during daylight hours only.

8. Emergency Phone Numbers

Eddy County Sheriff's Office	911 or 575-887-7551
Ambulance Service	911 or 575-885-2111
Carlsbad Fire Dept	911 or 575-885-2111
Loco Hills Volunteer Fire Dept.	911 or 575-677-3266
Closest Medical Facility - Columbia Medical Cent	er of Carlsbad 575-492-5000

Mewbourne Oil Company	Hobbs District Office Fax 2 nd Fax	575-393-5905 575-397-6252 575-393-7259
District Manager	Robin Terrell	575-390-4816
Drilling Superintendent	Frosty Lathan	575-390-4103
	Bradley Bishop	575-390-6838
Drilling Foreman	Wesley Noseff	575-441-0729

Operator Name: MEWBOURNE OIL COMPANY

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Section 7 - Methods for Handling

Waste type: DRILLING

Waste content description: Drill cuttings

Amount of waste: 940 barrels

Waste disposal frequency: One Time Only

Safe containment description: Drill cuttings will be properly contained in steel tanks (20 yard roll off bins.)

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: NMOCD approved waste disposal locations are CRI or Lea Land, both facilities are located

on HWY 62/180, Sec. 27 T20S R32E.

Waste type: GARBAGE

Waste content description: Garbage & trash

Amount of waste: 1500 pounds

Waste disposal frequency : One Time Only

Safe containment description: Enclosed trash trailer

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: Waste Management facility in Carlsbad.

Waste type: SEWAGE

Waste content description: Human waste & grey water

Amount of waste: 1500 gallons

Waste disposal frequency: Weekly

Safe containment description: 2,000 gallon plastic container

Safe containment attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: City of Carlsbad Water Treatment facility

Reserve Pit

Reserve Pit being used? NO

Operator Name: MEWBOURNE OIL COMPANY

Well Name: ICEMAN 24/23 FED COM Well Number: 718H

Temporary disposal of produced water into reserve pit? NO

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.)

Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

Cuttings Area

Cuttings Area being used? NO

Are you storing cuttings on location? N

Description of cuttings location

Cuttings area length (ft.) Cuttings area width (ft.)

Cuttings area depth (ft.) Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

Cuttings area liner

Cuttings area liner specifications and installation description

Section 8 - Ancillary

Are you requesting any Ancillary Facilities?: N

Ancillary Facilities

Comments:

Section 9 - Well Site

Well Site Layout Diagram:

ICEMAN_24_23_FED_COM__718H_WellSiteLayout_20240617105134.pdf

Comments: NONE

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Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 460775

CONDITIONS

Operator:	OGRID:
MEWBOURNE OIL CO	14744
P.O. Box 5270	Action Number:
Hobbs, NM 88241	460775
	Action Type:
	[C-101] BLM - Federal/Indian Land Lease (Form 3160-3)

CONDITIONS

Created By	Condition	Condition Date
mleal	Cement is required to circulate on both surface and intermediate1 strings of casing.	5/12/2025
mleal	If cement does not circulate on any string, a Cement Bond Log (CBL) is required for that string of casing.	5/12/2025
ward.rikala	Notify the OCD 24 hours prior to casing & cement.	6/18/2025
ward.rikala	File As Drilled C-102 and a directional Survey with C-104 completion packet.	6/18/2025
ward.rikala	Once the well is spud, to prevent ground water contamination through whole or partial conduits from the surface, the operator shall drill without interruption through the fresh water zone or zones and shall immediately set in cement the water protection string.	6/18/2025
ward.rikala	Oil base muds are not to be used until fresh water zones are cased and cemented providing isolation from the oil or diesel. This includes synthetic oils. Oil based mud, drilling fluids and solids must be contained in a steel closed loop system.	6/18/2025