Form 3160-5 (June 2019)

## UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

FORM APPROVI	≛D
OMB No. 1004-01	37
Expires: October 31,	2021

5.	Lease	Serial	No

DOK	EAU OF LAND MANAGEMENT				
Do not use this t	OTICES AND REPORTS ON Worm for proposals to drill or to Use Form 3160-3 (APD) for suc	6. If Indian, Allottee or Tribe Name			
	TRIPLICATE - Other instructions on page		7. If Unit of CA/Agree	ment, Name and/or No.	
1. Type of Well	HIPLICATE - Other Instructions on pag	le 2	_	,	
Oil Well Gas W	Vell Other		8. Well Name and No.		
2. Name of Operator			9. API Well No.		
	21- DL N-	(include area code)	10. Field and Pool or E	Avaloratory Aran	
3a. Address	30. Phone No.	(inciuae area coae)	10. Field and Foot of E	xpioratory Area	
4. Location of Well (Footage, Sec., T., K	.,M., or Survey Description)		11. Country or Parish,	State	
12. CHE	CK THE APPROPRIATE BOX(ES) TO IN	DICATE NATURE OF NO	TICE, REPORT OR OTH	ER DATA	
TYPE OF SUBMISSION		TYPE OF A	CTION		
Notice of Intent	Acidize Deep	pen Pro	oduction (Start/Resume)	Water Shut-Off	
Notice of intent	Alter Casing Hydr	raulic Fracturing Re	clamation	Well Integrity	
Subsequent Report			complete	Other	
Final Abandonment Notice		=	mporarily Abandon		
	Convert to Injection Plug peration: Clearly state all pertinent details, i		nter Disposal		
14. I hereby certify that the foregoing is	true and correct. Name (Printed/Typed)				
		Title			
Signature		Date			
	THE SPACE FOR FED	ERAL OR STATE O	FICE USE		
Approved by					
		Title		Pate	
	ned. Approval of this notice does not warrar equitable title to those rights in the subject leduct operations thereon.	t or			
	3 U.S.C Section 1212, make it a crime for an ents or representations as to any matter with		illfully to make to any dep	partment or agency of the United States	

(Instructions on page 2)

#### **GENERAL INSTRUCTIONS**

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

#### **SPECIFIC INSTRUCTIONS**

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

#### **NOTICES**

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

#### **Additional Information**

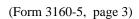
#### **Additional Remarks**

Update casing and cement program to current design.

Update HSU to 1280 acres.

Update the Pool as reflected in the C-102.

#### **Location of Well**



<u>C-102</u>					State of N	ew Mexico			Revis	ed July 9, 2024
Submit Electronic Via OCD Permitt				Energy, Minerals & Natural Resources Department					Initial Submittal	
OIL CONSERVAT						ATION DI	VISION	Submittal Type:	Amended Report	
								Type.	As Drilled	
Property Name and	Well Number				STARK 32	FED COM 7	'53H			
		W]	ELL LO	CATI	ON AND A	CREAGE	DEDICATION	N PLAT		
API Number 30-0	)15-48266	Pool Code	98220			Pool Name	PURPLE SAGE; \	VOLFCAM	IP (GAS)	
Property Code		Property N	lame		07151				Well Number	-011
OGRID No.		Operator N	Jame		STARK	32 FED CO	M		Ground Level Ele	53H
73	77	Орегают	vaine		EOG RES	OURCES, II	NC.			163'
					Surfa	ce Location				
UL or Lot No.	Section	Township	Range	Lot	Feet from the N/S	Feet from the E/W	Latitude		Longitude	County
M	32	25 S	30 E		455 FSL	1217 FWL	N 32.080299°	W 10	)3.908133°	EDDY
UL or Lot No.	Section	Township		Bottom	Hole Location	n If Different	t From Surface  Latitude		Longitude	County
OL of Lot No.	8	26 S	Range 30 E	Lot	230 FSL	2067 FEL	N 32.050485°		)3.901554°	County EDDY
					2001.02	2007 1 22	11 02.000 100	1	.0.001001	
Dedicated Acres	Infill or Defir	ning Well Defi	ning Well API			Overlapping Sp	acing Unit (Y/N)	Consolidat	ed Code	
1280	INFII	_L	30	-015-4	8598		YES			
Order Numbers	COM AGE	REEMEN	T NMNM	105810	903		Well Setback	s are under Comm	on Ownership: Yes	s No
						f Point (KOP				
UL or lot no.	Section	Township	Range	Lot		Feet from the E/W	Latitude		Longitude	County
В	5	26 S	30 E		50 FNL	2067 FEL	N 32.078934°	W 10	)3.901561°	EDDY
UL or lot no.	Section	Township	Range	Lot	First Tal	ce Point (FTI	Latitude	1	Longitude	County
В	5	26 S	30 E	Lot	330 FNL	2067 FEL	N 32.078164°	\ \ <sub>\\\\</sub> 10	)3.901558°	EDDY
					1	te Point (LTF			0.001000	LDD1
UL or lot no.	Section	Township	Range	Lot	1	Feet from the E/W	Latitude		Longitude	County
0	8	26 S	30 E		330 FSL	2067 FEL	N 32.050760°	W 10	)3.901554°	EDDY
Unitized Area or A	rea of Uniform In	terest		Spacing	Unity Type	zontal Vertical	Ground I	Floor Elevation	3188'	
				I			<b>'</b>			
OPERATO	R CERTIF	ICATION				SURVEY	ORS CERTIFICA?			
I hereby certify that the information contained herein is true and complete to the best of my knowledge and belief, and, if the well is a vertical or directional well, that this organization either owns a working interest or unleased mineral interest in the land including the proposed bottom hole location or has a right to drill this well at this location pursuant to a contract with an owner of a working interest or unleased mineral interest, or to a voluntary pooling agreement or a compulsory pooling order heretofore entered by the division.  If this well is a horizontal well, I further certify that this organization has received The consent of at least one lessee or owner of a working interest or unleased mineral interest in each tract (in the target pool or formation) in which any part of the well's completed interval will be located or obtained a compulsory pooling order from the division.					ll, st st svis 'Y	PROFITSS,	29821) 0810612024	NO HOUSE		
Kayl	a McC	onne			8/15/2024	Signature and	Seal of Professional Surveyor			
KAYLA M	CCONNE	LL	Date			I hereby ce notes of ac	rtify that the well locat tual surveys made by m correct to the best of t	ion shown on ie or under m	this plat was plotte	
Print Name KAYLA N	/CCONNE	ELL@FO	GRESOR	CES C	 OM		ELL L. MCDONAL		.L.S.	
E-mail Address						Certificate Nur	Certificate Number 29821 Date of Survey FEBRUARY 8, 2024			

Note: No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

C-102		Sta	ite of New	л Ме	exico			Revised July 9, 2024			
Submit Electronically	Energy,	Minerals	& Natura	l Re	source	es Departr	nent			Initial Submittal	
Via OCD Permitting	O]	L CONS	SERVAT	ION	N DIV	'ISION		Subm Type:	1 1 1 1	Amended Report	
								Type.		As Drilled	
Property Name and Well Number		STA	ARK 32 FE	ED C	OM 7	53H					
							1				
SURFACE LOCATION NEW MEXICO EAST NAD 1983 X=673030' Y=393209' LAT=N32.080299° LONG=W103.908133° NAD 1927 X=631845' Y=393152' LAT=N32.080174° LONG=W103.907652° 455' FSL 1217' FWL  KOP LOCATION NEW MEXICO EAST NAD 1983 X=675068' Y=392721' LAT=N32.078934° LONG=W103.901561° NAD 1927 X=633882' Y=392663' LAT=N32.078809° LONG=W103.901080° 50' FNL 2067' FEL  FIRST TAKE POINT NEW MEXICO EAST NAD 1983 X=675070' Y=392441' LAT=N32.078164° LONG=W103.901558° NAD 1927 X=633884' Y=392383' LAT=N32.078164° LONG=W103.901078° 330' FNL 2067' FEL  LOWER MOST PERF. NEW MEXICO EAST NAD 1983 X=675111' Y=382472' LAT=N32.050760° LONG=W103.901554° NAD 1927 X=633925' Y=382414' LAT=N32.050635° LONG=W103.901075° 330' FSL 2067' FEL  BOTTOM HOLE LOCATION NEW MEXICO EAST NAD 1983 X=675111' Y=382372' LAT=N32.050485° LONG=W103.901075° 330' FSL 2067' FEL  BOTTOM HOLE LOCATION NEW MEXICO EAST NAD 1983 X=675111' Y=382372' LAT=N32.050485° LONG=W103.901554° NAD 1927 X=633925' Y=382314' LAT=N32.050360° LONG=W103.901075°		SHL 1217'	ARK 32 FE  AZ = 11  2095.2'  X = 674473' Y = 392766'  X = 674531' Y = 387455'  X = 674525' Y = 382138'	330		1-E0-2642-6 	X = 6771 Y = 3927 33 2067' 2067' 1 1 4 9 9		330' STORY OF THE	X = 679795' Y = 392808' T-25-S T-26-S X = 679823' Y = 387491' X = 679846' Y = 382174'	4 9
230' FSL 2067' FEL									<b>*</b>		!
									H		



#### **Revised Permit Information 07/19/2024:**

Well Name: Stark 32 Fed Com 753H

Location: SHL: 455' FSL & 1217' FWL, Section 32, T-25-S, R-30-E, Eddy Co., N.M.

BHL: 230' FSL & 2067' FEL, Section 8, T-26-S, R-30-E, Eddy Co., N.M.

#### **CASING PROGRAM:**

Hole	Interval MD		Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
12-1/4"	0	1,320	0	1,320	9-5/8"	36#	J-55	LTC
8-3/4"	0	11,846	0	11,600	7-5/8"	29.7#	ICYP-110	MO FXL
6-3/4"	0	11,346	0	11,100	5-1/2"	20#	P110-EC	DWC/C IS MS
6-3/4"	11,346	11,846	11,100	11,600	5-1/2"	20#	P110-EC	VAM Sprint SF
6-3/4"	11,846	21,979	11,600	11,599	5-1/2"	20#	P110-EC	DWC/C IS MS

Variance is requested to waive the centralizer requirements for the 7-5/8" casing in the 8-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 8-3/4" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 5-1/2" casing in the 6-3/4" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 6-3/4" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive the annular clearance requirements for the 5-1/2" casing by 7-5/8" casing annulus to the proposed top of cement.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement from Onshore Order #2 under the following conditions:

- Annular clearance to meet or exceed 0.422" between intermediate casing ID and production casing coupling only on the first 500" overlap between both casing strings.
- Annular clearance less than 0.422" is acceptable for the production open hole section.

#### **CEMENTING PROGRAM:**

		Wt.	Yld	Clump, Description
Depth	No. Sacks	ppg	Ft3/sk	Slurry Description
1,320'	360	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-
9-5/8''				Flake (TOC @ Surface)
	80	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium
				Metasilicate (TOC @ 1,120')
11,600'	1330	14.2	1.11	1st Stage (Tail): Class C + 0.6% Halad-9 + 0.45% HR-601 + 3%
7-5/8''				Microbond (TOC @ 5,630')
	1000	14.8	1.5	2nd Stage (Bradenhead squeeze): Class C + 3% Salt + 1% PreMag-M +
				6% Bentonite Gel (TOC @ surface)
21,979'	2249	12.5	2.05	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond
5-1/2''				(TOC @ Surface)
5-1/2"	2250	13.2	1.41	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond
				(TOC @ 11,100')



Additive	Purpose						
Bentonite Gel	Lightweight/Lost circulation prevention						
Calcium Chloride	Accelerator						
Cello-flake	Lost circulation prevention						
Sodium Metasilicate	Accelerator						
MagOx	Expansive agent						
Pre-Mag-M	Expansive agent						
Sodium Chloride	Accelerator						
FL-62	Fluid loss control						
Halad-344	Fluid loss control						
Halad-9	Fluid loss control						
HR-601	Retarder						
Microbond	Expansive Agent						

EOG requests variance from minimum standards to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon (5,826') and the second stage performed as a 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of 100 sacks of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. Top will be verified by Echo-meter.

EOG will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

EOG will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

EOG requests a variance to set the intermediate casing shoe in the Bone Spring formation OR the Wolfcamp formation, depending on depletion in the area and well conditions. EOG will monitor the well and ensure the well is static before casing operations begin.

#### **MUD PROGRAM:**

<b>Measured Depth</b>	Type	Weight (ppg)	Viscosity	Water Loss
0 – 1,320'	Fresh - Gel	8.6-8.8	28-34	N/c
1,320' – 11,600'	Brine	9.0-10.5	28-34	N/c
11,600' – 11,355'	Oil Base	8.7-9.4	58-68	N/c - 6
11,355' – 21,979' Lateral	Oil Base	10.0-14.0	58-68	4 - 6



EOG requests a variance to set the intermediate casing shoe in the Bone Spring formation OR the Wolfcamp formation, depending on depletion in the area and well conditions. EOG will monitor the well and ensure the well is static before casing operations begin.

#### **TUBING REQUIREMENTS**

EOG respectively requests an exception to the following NMOCD rule:

• 19.15.16.10 Casing AND TUBING RQUIREMENTS: J (3): "The operator shall set tubing as near the bottom as practical and tubing perforations shall not be more than 250 feet above top of pay zone."

With horizontal flowing and gas lifted wells an end of tubing depth placed at or slightly above KOP is a conservative way to ensure the tubing stays clean from debris, plugging, and allows for fewer well interventions post offset completion. The deeper the tubulars are run into the curve, the higher the probability is that the tubing will become stuck in sand and or well debris as the well produces over time. An additional consideration for EOT placement during artificial lift installations is avoiding the high dog leg severity and inclinations found in the curve section of the wellbore to help improve reliability and performance. Dog leg severity and inclinations tend not to hamper gas lifted or flowing wells, but they do effect other forms of artificial lift like rod pump or ESP (electric submersible pump). Keeping the EOT above KOP is an industry best practice for those respective forms of artificial lift.



455' FSL 1217' FWL **Revised Wellbore** 

API: 30-015-48266

KB: 3188' GL: 3163'

**Section 32** 

T-25-S, R-30-E

Bit Size: 12-1/4" 9-5/8", 36#, J-55, LTC, @ 0' - 1,320' Bit Size: 8-3/4" 7-5/8", 29.7#, ICYP-110, MO FXL, @ 0' - 11,600' TOC: 10,846' MD, 10,600' TVD Lateral: 21,979' MD, 11,599' TVD Bit Size: 6-3/4" **Upper Most Perf:** 5-1/2", 20.#, P110-EC, DWC/C IS MS 330' FNL & 2067' FEL Sec. 5 @ 0' - 11,100' **Lower Most Perf:** 5-1/2", 20.#, P110-EC, VAM Sprint SF 330' FSL & 2067' FEL Sec. 8 @ 11,100' - 11,600' BH Location: 230' FSL & 2067' FEL 5-1/2", 20.#, P110-EC, DWC/C IS MS Sec. 8 @ 11,600' - 21,979' T-26-S R-30-E KOP: 11,355' MD, 11,122' TVD EOC: 12,105' MD, 11,599' TVD



## **Design B CASING PROGRAM:**

Hole	Interval MD		Interval TVD		Csg			
Size	From (ft)	To (ft)	From (ft)	To (ft)	OD	Weight	Grade	Conn
13"	0	1,320	0	1,320	10-3/4"	40.5#	J-55	STC
9-7/8"	0	11,846	0	11,600	8-3/4"	38.5#	P110-EC	VAM Sprint-SF
7-7/8"	0	11,355	0	11,122	6"	22.3#	P110-EC	DWC/C IS
6.75"	11,355	21,979	11,122	11,599	5-1/2"	20#	P110-EC	DWC/C IS MS

<sup>\*\*</sup>For highlighted rows above, variance is requested to run entire string of either 6" or 5-1/2" casing string above due to availablility.

Variance is requested to waive the centralizer requirements for the 8-3/4" casing in the 9-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 9-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive any centralizer requirements for the 6" and 5-1/2" casings in the 7-7/8" hole size. An expansion additive will be utilized, in the cement slurry, for the entire length of the 7-7/8" hole interval to maximize cement bond and zonal isolation.

Variance is also requested to waive the annular clearance requirements for the 6" and 5-1/2" casings by 8-3/4" casing annulus to the proposed top of cement.

EOG requests permission to allow deviation from the 0.422" annulus clearance requirement from Onshore Order #2 under the following conditions:

- Annular clearance to meet or exceed 0.422" between intermediate casing ID and production casing coupling only on the first 500" overlap between both casing strings.
- Annular clearance less than 0.422" is acceptable for the production open hole section.

#### **CEMENTING PROGRAM:**

		Wt.	Yld	Chamer Decemention
Depth	No. Sacks	ppg	Ft3/sk	Slurry Description
1,320'	330	13.5	1.73	Lead: Class C + 4.0% Bentonite Gel + 0.5% CaCl2 + 0.25 lb/sk Cello-Flake
10-3/4"				(TOC @ Surface)
	70	14.8	1.34	Tail: Class C + 0.6% FL-62 + 0.25 lb/sk Cello-Flake + 0.2% Sodium
				Metasilicate (TOC @ 1,120')
11,600'	1510	14.2	1.11	1st Stage (Tail): Class C + 0.6% Halad-9 + 0.45% HR-601 + 3% Microbond
8-3/4"				(TOC @ 5,626')
	1000	14.8	1.5	2nd Stage (Bradenhead squeeze): Class C + 3% Salt + 1% PreMag-M + 6%
				Bentonite Gel (TOC @ surface)
21,979'	1520	13.2	1.31	Lead: Class H + 0.4% Halad-344 + 0.35% HR-601 + 3% Microbond (TOC
6"				@ 11,100')



EOG requests variance from minimum standards to pump a two stage cement job on the 8-3/4" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon (5,826') and the second stage performed as a 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of -973 sacks of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. Top will be verified by Echo-meter.

EOG will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

EOG will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

EOG requests a variance to set the intermediate casing shoe in the Bone Spring formation OR the Wolfcamp formation, depending on depletion in the area and well conditions. EOG will monitor the well and ensure the well is static before casing operations begin.

#### **VARIANCE REQUESTS:**

EOG requests the additional variance(s) in the attached document(s):

Variances requested include (supporting documents attached):

- BOP Break Testing for 5M Intermediate Intervals (EOG BLM Variance 3a\_b)
- Offline Cementing for Surface and Intermediate Intervals (EOG BLM Variance 3a b)
- Intermediate Bradenhead Cement (EOG BLM Variance 2a)



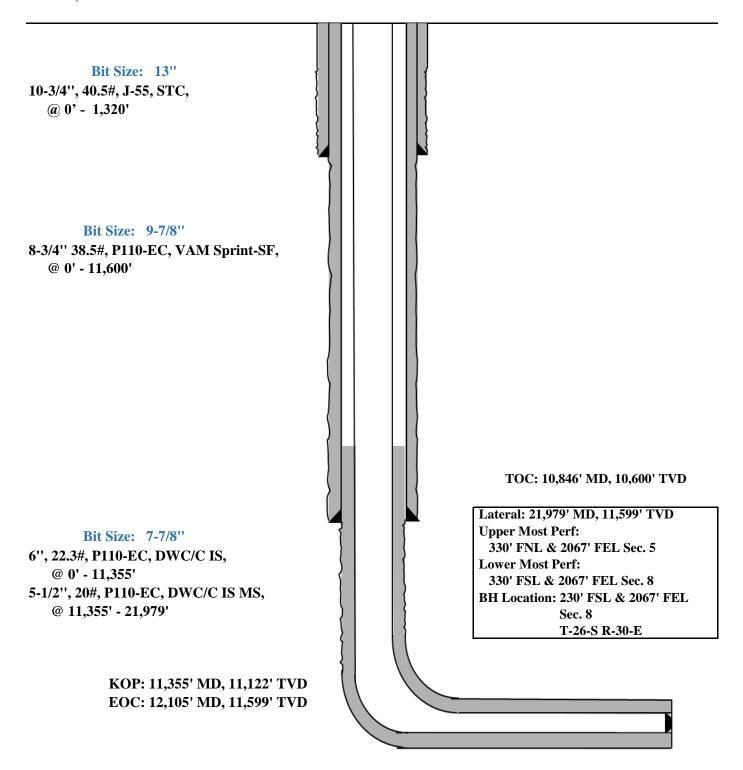
455' FSL 1217' FWL **Proposed Wellbore** 

KB: 3188' GL: 3163'

Section 32

T-25-S, R-30-E

API: 30-015-48266





#### GEOLOGIC NAME OF SURFACE FORMATION:

Permian

#### ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

Rustler	1,242'
	<i>*</i>
Tamarisk Anhydrite	1,292'
Top of Salt	1,549'
Base of Salt	3,436'
Lamar	3,634'
Bell Canyon	3,661'
Cherry Canyon	577'
Brushy Canyon	5,826'
Bone Spring Lime	7,481'
Leonard (Avalon) Shale	7,547'
1st Bone Spring Sand	8,412'
2nd Bone Spring Shale	8,685'
2nd Bone Spring Sand	9,134'
3rd Bone Spring Carb	9,615'
3rd Bone Spring Sand	10,326'
Wolfcamp	10,738'
TD	11,599'

#### ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

Upper Permian Sands	0-400'	Fresh Water
Bell Canyon	3,661'	Oil
Cherry Canyon	577'	Oil
Brushy Canyon	5,826'	Oil
Leonard (Avalon) Shale	7,547'	Oil
1st Bone Spring Sand	8,412'	Oil
2nd Bone Spring Shale	8,685'	Oil
2nd Bone Spring Sand	9.134'	Oil



### **Midland**

Eddy County, NM (NAD 83 NME) Stark 32 Fed Com #753H

OH

Plan: Plan #0.1 RT

### **Standard Planning Report**

08 August, 2024



PEDMB Database: Company: Midland

Project: Eddy County, NM (NAD 83 NME)

Site: Stark 32 Fed Com

Well: #753H Wellbore: OH Design:

Plan #0.1 RT

**Local Co-ordinate Reference:** 

**TVD Reference:** MD Reference: North Reference:

**Survey Calculation Method:** 

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid

Minimum Curvature

Project Eddy County, NM (NAD 83 NME)

US State Plane 1983 Map System: North American Datum 1983

Geo Datum: New Mexico Eastern Zone Map Zone:

System Datum: Mean Sea Level

Using geodetic scale factor

Stark 32 Fed Com Site

Northing: 393,209.00 usft Site Position: Latitude: 32° 4' 49.072 N From: Мар Easting: 673,030.00 usft Longitude: 103° 54' 29.279 W

**Position Uncertainty:** 0.0 usft Slot Radius: 13-3/16 "

Well #753H

32° 4' 49.072 N **Well Position** +N/-S 0.0 usft Northing: 393,209.00 usft Latitude: +E/-W 0.0 usft Easting: 673,030.00 usft Longitude: 103° 54' 29.279 W

**Position Uncertainty** 0.0 usft Wellhead Elevation: usft **Ground Level:** 3,163.0 usft

0.23° **Grid Convergence:** 

ОН Wellbore

Declination Magnetics **Model Name** Sample Date Dip Angle Field Strength (°) (°) (nT) 47,049.73148832 IGRF2020 8/6/2024 6.32 59.62

Plan #0.1 RT Design

Audit Notes:

PLAN Tie On Depth: 0.0 Version: Phase:

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°) 169.13 0.0 0.0 0.0

**Plan Survey Tool Program** Date

**Depth From** Depth To

(usft) (usft) Survey (Wellbore) **Tool Name** Remarks

21,978.5 Plan #0.1 RT (OH) EOG MWD+IFR1 0.0

MWD + IFR1



Database: PEDMB Company: Midland

Project: Eddy County, NM (NAD 83 NME)

Site: Stark 32 Fed Com

Well: #753H Wellbore: 0H

Design: Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

**Survey Calculation Method:** 

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid

Plan Sections										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
1,417.0	0.00	0.00	1,417.0	0.0	0.0	0.00	0.00	0.00	0.00	
2,062.1	13.03	103.47	2,056.6	-17.0	71.0	2.02	2.02	0.00	103.47	
10,710.2	13.03	103.47	10,481.9	-471.1	1,967.5	0.00	0.00	0.00	0.00	
11,355.3	0.00	0.00	11,121.5	-488.1	2,038.5	2.02	-2.02	0.00	180.00	
11,355.3	0.00	0.00	11,121.5	-488.1	2,038.5	0.00	0.00	0.00	0.00	KOP(Banjo 32 Fed Co
11,901.8	65.59	179.60	11,556.2	-768.2	2,040.5	12.00	12.00	32.87	179.60	FTP(Banjo 32 Fed Cc
12,105.2	90.00	179.77	11,598.9	-965.5	2,041.6	12.00	12.00	0.08	0.41	
21,878.5	90.00	179.77	11,599.0	-10,738.7	2,081.3	0.00	0.00	0.00	0.00	Fed LTP(Banjo 32 Fe
21,978.5	90.00	180.23	11,599.0	-10,838.7	2,081.3	0.47	0.00	0.47	89.85	PBHL(Banjo 32 Fed C



Database: PEDMB Company: Midland

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Site: Stark 32 Fed Com

 Well:
 #753H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference:

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North Reference:

Survey Calculation Method:

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid

esign:	Plan #0.1 RT								
lanned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	0.0	0.0	0.00	0.00	0.00
700.0	0.00	0.00	700.0	0.0	0.0	0.0	0.00	0.00	0.00
800.0	0.00	0.00	800.0	0.0	0.0	0.0	0.00	0.00	0.00
900.0	0.00	0.00	900.0	0.0	0.0	0.0	0.00	0.00	0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	
									0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,417.0	0.00	0.00	1,417.0	0.0	0.0	0.0	0.00	0.00	0.00
1,500.0	1.68	103.47	1,500.0	-0.3	1.2	0.5	2.02	2.02	0.00
1,600.0	3.70	103.47	1,599.9	-1.4	5.7	2.4	2.02	2.02	0.00
			,				2.02	2.02	
1,700.0 1,800.0	5.72 7.74	103.47 103.47	1,699.5 1,798.8	-3.3 -6.0	13.7 25.1	5.8 10.6	2.02	2.02	0.00 0.00
1,000.0		103.47	1,790.0			10.6			0.00
1,900.0	9.76	103.47	1,897.7	-9.6	39.9	16.9	2.02	2.02	0.00
2,000.0	11.78	103.47	1,995.9	-13.9	58.1	24.6	2.02	2.02	0.00
2,062.1	13.03	103.47	2,056.6	-17.0	71.0	30.1	2.02	2.02	0.00
2,100.0	13.03	103.47	2,093.5	-19.0	79.3	33.6	0.00	0.00	0.00
2,200.0	13.03	103.47	2,190.9	-24.3	101.3	42.9	0.00	0.00	0.00
2,200.0	13.03	103.47	2,130.3	-24.0	101.5	42.5	0.00	0.00	0.00
2,300.0	13.03	103.47	2,288.3	-29.5	123.2	52.2	0.00	0.00	0.00
2,400.0	13.03	103.47	2,385.8	-34.8	145.1	61.5	0.00	0.00	0.00
2,500.0	13.03	103.47	2,483.2	-40.0	167.1	70.8	0.00	0.00	0.00
2,600.0	13.03	103.47	2,580.6	-45.3	189.0	80.1	0.00	0.00	0.00
2,700.0	13.03	103.47	2,678.0	-50.5	210.9	89.4	0.00	0.00	0.00
2,700.0	13.03	103.47	2,070.0	-30.3		03.4	0.00	0.00	0.00
2,800.0	13.03	103.47	2,775.4	-55.8	232.9	98.7	0.00	0.00	0.00
2,900.0	13.03	103.47	2,872.9	-61.0	254.8	108.0	0.00	0.00	0.00
3,000.0	13.03	103.47	2,970.3	-66.3	276.7	117.3	0.00	0.00	0.00
3,100.0	13.03	103.47	3,067.7	-71.5	298.6	126.5	0.00	0.00	0.00
3,200.0	13.03	103.47	3,165.1	-76.8	320.6	135.8	0.00	0.00	0.00
3,300.0	13.03	103.47	3,262.6	-82.0	342.5	145.1	0.00	0.00	0.00
3,400.0	13.03	103.47	3,360.0	-87.3	364.4	154.4	0.00	0.00	0.00
3,500.0	13.03	103.47	3,457.4	-92.5	386.4	163.7	0.00	0.00	0.00
3,600.0	13.03	103.47	3.554.8	-97.8	408.3	173.0	0.00	0.00	0.00
3,700.0	13.03	103.47	3,652.3	-103.0	430.2	182.3	0.00	0.00	0.00
3,800.0	13.03	103.47	3,749.7	-108.3	452.1	191.6	0.00	0.00	0.00
3,900.0	13.03	103.47	3,847.1	-113.5	474.1	200.9	0.00	0.00	0.00
4,000.0	13.03	103.47	3,944.5	-118.8	496.0	210.2	0.00	0.00	0.00
4,100.0	13.03	103.47	4,042.0	-124.0	517.9	219.5	0.00	0.00	0.00
4,200.0	13.03	103.47	4,139.4	-129.3	539.9	228.8	0.00	0.00	0.00
4,300.0	13.03	103.47	4,236.8	-134.5	561.8	238.1	0.00	0.00	0.00
4,400.0	13.03	103.47	4,334.2	-139.8	583.7	247.3	0.00	0.00	0.00
4,500.0	13.03	103.47	4,431.7	-145.0	605.6	256.6	0.00	0.00	0.00
4,600.0	13.03	103.47	4,529.1	-150.3	627.6	265.9	0.00	0.00	0.00
4,700.0	13.03	103.47	4,626.5	-155.5	649.5	275.2	0.00	0.00	0.00
4,800.0	13.03	103.47	4,723.9	-160.8	671.4	284.5	0.00	0.00	0.00
4,900.0	13.03	103.47	4,821.4	-166.0	693.4	293.8	0.00	0.00	0.00
5,000.0	13.03	103.47	4,918.8	-171.3	715.3	303.1	0.00	0.00	0.00
5,100.0	13.03	103.47	5,016.2	-176.5	737.2	312.4	0.00	0.00	0.00



Database: PEDMB Company: Midland

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 Well:
 #753H

 Wellbore:
 OH

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 Plan #0.1 RT

Local Co-ordinate Reference:

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North Reference:

Survey Calculation Method:

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid

200.g									
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,200.0	13.03	103.47	5,113.6	-181.8	759.2	321.7	0.00	0.00	0.00
5,300.0	13.03	103.47	5,211.1	-187.0	781.1	331.0	0.00	0.00	0.00
5,400.0	13.03	103.47	5,308.5	-192.3	803.0	340.3	0.00	0.00	0.00
5,500.0	13.03	103.47	5,405.9	-197.5	824.9	349.6	0.00	0.00	0.00
5,600.0	13.03	103.47	5,503.3	-202.8	846.9	358.8	0.00	0.00	0.00
5,700.0	13.03	103.47	5,600.8	-208.0	868.8	368.1	0.00	0.00	0.00
5,800.0	13.03	103.47	5,698.2	-213.3	890.7	377.4	0.00	0.00	0.00
5,900.0	13.03	103.47	5,795.6	-218.5	912.7	386.7	0.00	0.00	0.00
6,000.0	13.03	103.47	5,893.0	-223.8	934.6	396.0	0.00	0.00	0.00
6,100.0	13.03	103.47	5,990.5	-229.0	956.5	405.3	0.00	0.00	0.00
6,200.0	13.03	103.47	6,087.9	-234.3	978.4	414.6	0.00	0.00	0.00
6,300.0	13.03	103.47	6,185.3	-239.5	1,000.4	423.9	0.00	0.00	0.00
6,400.0	13.03	103.47	6,282.7	-244.8	1,022.3	433.2	0.00	0.00	0.00
6,500.0	13.03	103.47	6,380.2	-250.0	1,044.2	442.5	0.00	0.00	0.00
6,600.0	13.03	103.47	6,477.6	-255.3	1,066.2	451.8	0.00	0.00	0.00
6,700.0	13.03	103.47	6,575.0	-260.5	1,088.1	461.1	0.00	0.00	0.00
6,800.0	13.03	103.47	6,672.4	-265.8	1,110.0	470.4	0.00	0.00	0.00
6,900.0	13.03	103.47	6,769.9	-271.0	1,131.9	479.6	0.00	0.00	0.00
7,000.0	13.03	103.47	6,867.3	-276.3	1,153.9	488.9	0.00	0.00	0.00
7,100.0	13.03	103.47	6,964.7	-281.5	1,175.8	498.2	0.00	0.00	0.00
7,200.0	13.03	103.47	7,062.1	-286.8	1,197.7	507.5	0.00	0.00	0.00
7,300.0	13.03	103.47	7,159.6	-292.0	1,219.7	516.8	0.00	0.00	0.00
7,400.0	13.03	103.47	7,257.0	-297.3	1,241.6	526.1	0.00	0.00	0.00
7,500.0	13.03	103.47	7,354.4	-302.6	1,263.5	535.4	0.00	0.00	0.00
7,600.0	13.03	103.47	7,451.8	-307.8	1,285.5	544.7	0.00	0.00	0.00
7,700.0	13.03	103.47	7,549.2	-313.1	1,307.4	554.0	0.00	0.00	0.00
7,800.0	13.03	103.47	7,646.7	-318.3	1,329.3	563.3	0.00	0.00	0.00
7,900.0	13.03	103.47	7,744.1	-323.6	1,351.2	572.6	0.00	0.00	0.00
8,000.0	13.03	103.47	7,841.5	-328.8	1,373.2	581.9	0.00	0.00	0.00
8,100.0	13.03	103.47	7,938.9	-334.1	1,395.1	591.2	0.00	0.00	0.00
8,200.0	13.03	103.47	8,036.4	-339.3	1,417.0	600.4	0.00	0.00	0.00
8,300.0	13.03	103.47	8,133.8	-344.6	1,439.0	609.7	0.00	0.00	0.00
8,400.0	13.03	103.47	8,231.2	-349.8	1,460.9	619.0	0.00	0.00	0.00
8,500.0	13.03	103.47	8,328.6	-355.1	1,482.8	628.3	0.00	0.00	0.00
8,600.0	13.03	103.47	8,426.1	-360.3	1,504.7	637.6	0.00	0.00	0.00
8,700.0	13.03	103.47	8,523.5	-365.6	1,526.7	646.9	0.00	0.00	0.00
8,800.0	13.03	103.47	8,620.9	-370.8	1,548.6	656.2	0.00	0.00	0.00
8,900.0	13.03	103.47	8,718.3	-376.1	1,570.5	665.5	0.00	0.00	0.00
9,000.0	13.03	103.47	8,815.8	-381.3	1,592.5	674.8	0.00	0.00	0.00
9,100.0	13.03	103.47	8,913.2	-386.6	1,614.4	684.1	0.00	0.00	0.00
9,200.0	13.03	103.47	9,010.6	-391.8	1,636.3	693.4	0.00	0.00	0.00
9,300.0	13.03	103.47	9,108.0	-397.1	1,658.2	702.7	0.00	0.00	0.00
9,400.0	13.03	103.47	9,205.5	-402.3	1,680.2	712.0	0.00	0.00	0.00
9,500.0	13.03	103.47	9,302.9	-407.6	1,702.1	721.2	0.00	0.00	0.00
9,600.0	13.03	103.47	9,400.3	-412.8	1,724.0	730.5	0.00	0.00	0.00
9,700.0	13.03	103.47	9,497.7	-418.1	1,746.0	739.8	0.00	0.00	0.00
9,800.0	13.03	103.47	9,595.2	-423.3	1,767.9	749.1	0.00	0.00	0.00
9,900.0	13.03	103.47	9,692.6	-428.6	1,789.8	758.4	0.00	0.00	0.00
10,000.0	13.03	103.47	9,790.0	-433.8	1,811.8	767.7	0.00	0.00	0.00
10,100.0	13.03	103.47	9,887.4	-439.1	1,833.7	777.0	0.00	0.00	0.00
10,200.0	13.03	103.47	9,984.9	-444.3	1,855.6	786.3	0.00	0.00	0.00
10,300.0	13.03	103.47	10,082.3	-449.6	1,877.5	795.6	0.00	0.00	0.00
10,400.0	13.03	103.47	10,179.7	-454.8	1,899.5	804.9	0.00	0.00	0.00
10,500.0	13.03	103.47	10,277.1	-460.1	1,921.4	814.2	0.00	0.00	0.00



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Survey Calculation Method:

Well #753H

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Grid

Design:	Plan #0.1 R1								
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
10,600.0	13.03	103.47	10,374.6	-465.3	1,943.3	823.5	0.00	0.00	0.00
10,700.0	13.03	103.47	10,472.0	-470.6	1,965.3	832.8	0.00	0.00	0.00
10,710.2	13.03	103.47	10,481.9	-471.1	1,967.5	833.7	0.00	0.00	0.00
10,800.0	11.22	103.47	10,569.7	-475.5	1,985.8	841.5	2.02	-2.02	0.00
10,900.0	9.20	103.47	10,668.1	-479.6	2,003.1	848.8	2.02	-2.02	0.00
11,000.0	7.18	103.47	10,767.1	-483.0	2,016.9	854.6	2.02	-2.02	0.00
11,100.0	5.16	103.47	10,866.5	-485.5	2,027.4	859.1	2.02	-2.02	0.00
11,200.0	3.14	103.47	10,966.3	-487.1	2,034.4	862.0	2.02	-2.02	0.00
11,300.0	1.12	103.47	11,066.2	-488.0	2,038.0	863.6	2.02	-2.02	0.00
11,355.3	0.00	0.00	11,121.5	-488.1	2,038.5	863.8	2.02	-2.02	0.00
11,375.0	2.36	179.60	11,141.2	-488.5	2,038.5	864.2	12.00	12.00	0.00
11,400.0	5.36	179.60	11,166.1	-490.2	2,038.6	865.9	12.00	12.00	0.00
11,425.0	8.36	179.60	11,190.9	-493.2	2,038.6	868.8	12.00	12.00	0.00
11,450.0	11.36	179.60	11,215.6	-497.5	2,038.6	873.0	12.00	12.00	0.00
11,475.0	14.36	179.60	11,239.9	-503.1	2,038.6	878.5	12.00	12.00	0.00
11,500.0	17.36	179.60	11,264.0	-509.9	2,038.7	885.2	12.00	12.00 12.00	0.00
11,525.0	20.36	179.60	11,287.6	-518.0	2,038.7	893.1	12.00		0.00
11,550.0	23.36	179.60	11,310.8	-527.3	2,038.8	902.3	12.00	12.00	0.00
11,575.0	26.37	179.60	11,333.5	-537.8	2,038.9	912.6	12.00	12.00	0.00
11,600.0	29.37	179.60	11,355.6	-549.5	2,039.0	924.1	12.00	12.00	0.00
11,625.0 11,650.0	32.37 35.37	179.60 179.60	11,377.1 11,397.8	-562.3 -576.2	2,039.1 2,039.2	936.7 950.4	12.00 12.00	12.00 12.00	0.00 0.00
11,675.0	38.37	179.60	11,417.8	-591.2	2,039.3	965.2	12.00	12.00	0.00
11,700.0	41.37	179.60	11,437.0	-607.2	2,039.4	980.9	12.00	12.00	0.00
11,725.0 11,750.0	44.37 47.37	179.60 179.60	11,455.3 11,472.7	-624.2 -642.2	2,039.5 2,039.6	997.7 1,015.3	12.00 12.00	12.00 12.00	0.00 0.00
11,775.0	50.37	179.60	11,489.2	-661.0	2,039.8	1,013.8	12.00	12.00	0.00
11,800.0	53.37	179.60	11,504.6	-680.7	2,039.9	1,053.2	12.00	12.00	0.00
11,825.0	56.37	179.60	11,519.0	-701.1	2,039.9	1,033.2	12.00	12.00	0.00
11,850.0	59.37	179.60	11,532.3	-722.3	2,040.2	1,094.1	12.00	12.00	0.00
11,875.0	62.37	179.60	11,544.5	-744.1	2,040.3	1,115.5	12.00	12.00	0.00
11,901.8	65.59	179.60	11,556.2	-768.2	2,040.5	1,139.2	12.00	12.00	0.00
11,925.0	68.37	179.62	11,565.3	-789.6	2,040.7	1,160.2	12.00	12.00	0.09
11,950.0	71.37	179.64	11,573.9	-813.0	2,040.8	1,183.3	12.00	12.00	0.09
11,975.0	74.37	179.66	11,581.2	-836.9	2,041.0	1,206.8	12.00	12.00	0.09
12,000.0	77.37	179.68	11,587.3	-861.2	2,041.1	1,230.6	12.00	12.00	0.08
12,025.0	80.37	179.70	11,592.2	-885.7	2,041.2	1,254.7	12.00	12.00	0.08
12,050.0	83.37	179.72	11,595.7	-910.4	2,041.4	1,279.1	12.00	12.00	0.08
12,075.0	86.37	179.74	11,597.9	-935.3	2,041.5	1,303.5	12.00	12.00	0.08
12,100.0	89.37	179.76	11,598.9	-960.3	2,041.6	1,328.1	12.00	12.00	0.08
12,105.2	90.00	179.77	11,598.9	-965.5	2,041.6	1,333.2	12.00	12.00	0.08
12,200.0	90.00	179.77	11,598.9	-1,060.3	2,042.0	1,426.4	0.00	0.00	0.00
12,300.0	90.00	179.77	11,598.9	-1,160.3	2,042.4	1,524.6	0.00	0.00	0.00
12,400.0	90.00	179.77	11,598.9	-1,260.3	2,042.8	1,622.9	0.00	0.00	0.00
12,500.0	90.00	179.77	11,598.9	-1,360.3	2,043.2	1,721.2	0.00	0.00	0.00
12,600.0 12,700.0	90.00 90.00	179.77 179.77	11,598.9 11,598.9	-1,460.3 -1,560.3	2,043.6 2,044.0	1,819.5 1,917.8	0.00 0.00	0.00 0.00	0.00 0.00
12,800.0	90.00	179.77	11,598.9	-1,660.3	2,044.4	2,016.0	0.00	0.00	0.00
12,900.0	90.00	179.77	11,598.9	-1,760.3	2,044.8	2,114.3	0.00	0.00	0.00
13,000.0 13,100.0	90.00 90.00	179.77 179.77	11,598.9 11,598.9	-1,860.3 -1,960.3	2,045.2 2,045.6	2,212.6 2,310.9	0.00 0.00	0.00 0.00	0.00 0.00
13,100.0	90.00	179.77	11,598.9	-1,960.3 -2,060.3	2,045.6 2,046.0	2,310.9	0.00	0.00	0.00
13,300.0	90.00	179.77	11,598.9	-2,160.3	2,046.5	2,507.5	0.00	0.00	0.00
13,400.0	90.00	179.77	11,598.9	-2,260.3	2,046.9	2,605.7	0.00	0.00	0.00



Database: PEDMB Company: Midland

Project: Eddy County, NM (NAD 83 NME)

Site: Stark 32 Fed Com

 Well:
 #753H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid

Design:	Plan #0.1 RT									
Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	
13,500.0	90.00	179.77	11,598.9	-2,360.3	2,047.3	2,704.0	0.00	0.00	0.00	
13,600.0	90.00	179.77	11,598.9	-2,460.3	2,047.7	2,802.3	0.00	0.00	0.00	
13,700.0	90.00	179.77	11,598.9	-2,560.3	2,048.1	2,900.6	0.00	0.00	0.00	
13,800.0	90.00	179.77	11,598.9	-2,660.3	2,048.5	2,998.9	0.00	0.00	0.00	
13,900.0	90.00	179.77	11,598.9	-2,760.3	2,048.9	3,097.1	0.00	0.00	0.00	
14,000.0	90.00	179.77	11,598.9	-2,860.3	2,049.3	3,195.4	0.00	0.00	0.00	
14,100.0	90.00	179.77	11,598.9	-2,960.3	2,049.7	3,293.7	0.00	0.00	0.00	
14,200.0	90.00	179.77	11,598.9	-3,060.3	2,050.1	3,392.0	0.00	0.00	0.00	
14,300.0	90.00	179.77	11,598.9	-3,160.3	2,050.5	3,490.3	0.00	0.00	0.00	
14,400.0	90.00	179.77	11,598.9	-3,260.3	2,050.9	3,588.6	0.00	0.00	0.00	
14,500.0	90.00	179.77	11,598.9	-3,360.3	2,051.3	3,686.8	0.00	0.00	0.00	
14,600.0	90.00	179.77	11,598.9	-3,460.3	2,051.7	3,785.1	0.00	0.00	0.00	
14,700.0	90.00	179.77	11,598.9	-3,560.3	2,052.1	3,883.4	0.00	0.00	0.00	
14,800.0	90.00	179.77	11,598.9	-3,660.3	2,052.6	3,981.7	0.00	0.00	0.00	
14,900.0	90.00	179.77	11,598.9	-3,760.3	2,053.0	4,080.0	0.00	0.00	0.00	
15,000.0	90.00	179.77	11,598.9	-3,860.3	2,053.4	4,178.2	0.00	0.00	0.00	
15,100.0	90.00	179.77	11,598.9	-3,960.3	2,053.8	4,276.5	0.00	0.00	0.00	
15,200.0	90.00	179.77	11,598.9	-4,060.3	2,054.2	4,374.8	0.00	0.00	0.00	
15,300.0	90.00	179.77	11,598.9	-4,160.3	2,054.6	4,473.1	0.00	0.00	0.00	
15,400.0	90.00	179.77	11,598.9	-4,260.3	2,055.0	4,571.4	0.00	0.00	0.00	
15,500.0	90.00 90.00	179.77	11,598.9 11,598.9	-4,360.3	2,055.4	4,669.7	0.00	0.00	0.00	
15,600.0 15,700.0	90.00	179.77 179.77	11,598.9	-4,460.3 -4,560.3	2,055.8 2,056.2	4,767.9 4,866.2	0.00 0.00	0.00 0.00	0.00 0.00	
15,800.0	90.00	179.77	11,598.9	-4,660.3	2,056.6	4,964.5	0.00	0.00	0.00	
15,900.0 16,000.0	90.00 90.00	179.77 179.77	11,598.9 11,598.9	-4,760.3 -4,860.3	2,057.0 2,057.4	5,062.8 5,161.1	0.00 0.00	0.00 0.00	0.00 0.00	
16,100.0	90.00	179.77	11,598.9	-4,960.3	2,057.4	5,259.3	0.00	0.00	0.00	
16,200.0	90.00	179.77	11,598.9	-5,060.3	2,058.2	5,357.6	0.00	0.00	0.00	
16,300.0	90.00	179.77	11,598.9	-5,160.3	2,058.7	5,455.9	0.00	0.00	0.00	
16,400.0	90.00	179.77	11,598.9	-5,160.3 -5,260.3	2,050.7	5,455.9 5,554.2	0.00	0.00	0.00	
16,500.0	90.00	179.77	11,598.9	-5,360.3	2,059.5	5,652.5	0.00	0.00	0.00	
16,600.0	90.00	179.77	11,598.9	-5,460.3	2,059.9	5,750.7	0.00	0.00	0.00	
16,700.0	90.00	179.77	11,598.9	-5,560.3	2,060.3	5,849.0	0.00	0.00	0.00	
16,800.0	90.00	179.77	11,598.9	-5,660.3	2,060.7	5,947.3	0.00	0.00	0.00	
16,900.0	90.00	179.77	11,598.9	-5,760.3	2,061.1	6,045.6	0.00	0.00	0.00	
17,000.0	90.00	179.77	11,598.9	-5,860.3	2,061.5	6,143.9	0.00	0.00	0.00	
17,100.0	90.00	179.77	11,598.9	-5,960.3	2,061.9	6,242.2	0.00	0.00	0.00	
17,200.0	90.00	179.77	11,598.9	-6,060.3	2,062.3	6,340.4	0.00	0.00	0.00	
17,300.0	90.00	179.77	11,599.0	-6,160.3	2,062.7	6,438.7	0.00	0.00	0.00	
17,400.0	90.00	179.77	11,599.0	-6,260.3	2,063.1	6,537.0	0.00	0.00	0.00	
17,500.0	90.00	179.77	11,599.0	-6,360.3	2,063.5	6,635.3	0.00	0.00	0.00	
17,600.0	90.00	179.77	11,599.0	-6,460.3	2,063.9	6,733.6	0.00	0.00	0.00	
17,700.0	90.00	179.77	11,599.0	-6,560.3	2,064.3	6,831.8	0.00	0.00	0.00	
17,800.0	90.00	179.77	11,599.0	-6,660.3	2,064.7	6,930.1	0.00	0.00	0.00	
17,900.0	90.00	179.77	11,599.0	-6,760.3	2,065.2	7,028.4	0.00	0.00	0.00	
18,000.0	90.00	179.77	11,599.0	-6,860.3	2,065.6	7,126.7	0.00	0.00	0.00	
18,100.0 18,200.0	90.00 90.00	179.77 179.77	11,599.0 11,599.0	-6,960.3 -7,060.3	2,066.0 2,066.4	7,225.0 7,323.3	0.00 0.00	0.00 0.00	0.00 0.00	
18,300.0	90.00	179.77	11,599.0	-7,160.3	2,066.8	7,421.5	0.00	0.00	0.00	
18,400.0 18,500.0	90.00 90.00	179.77 179.77	11,599.0 11,599.0	-7,260.3 -7,360.2	2,067.2 2,067.6	7,519.8 7,618.1	0.00 0.00	0.00 0.00	0.00 0.00	
18,600.0	90.00	179.77	11,599.0	-7,360.2 -7,460.2	2,067.6	7,016.1	0.00	0.00	0.00	
18,700.0	90.00	179.77	11,599.0	-7,560.2	2,068.4	7,814.7	0.00	0.00	0.00	
18,800.0	90.00	179.77	11,599.0	-7,660.2	2,068.8	7,912.9	0.00	0.00	0.00	



Database: PEDMB Company: Midland

Project: Eddy County, NM (NAD 83 NME)

Site: Stark 32 Fed Com

 Well:
 #753H

 Wellbore:
 OH

 Design:
 Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method:

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
18,900.0	90.00	179.77	11,599.0	-7,760.2	2,069.2	8,011.2	0.00	0.00	0.00
19,000.0	90.00	179.77	11,599.0	-7,860.2	2,069.6	8,109.5	0.00	0.00	0.00
19,100.0	90.00	179.77	11,599.0	-7,960.2	2,070.0	8,207.8	0.00	0.00	0.00
19,200.0	90.00	179.77	11,599.0	-8,060.2	2,070.4	8,306.1	0.00	0.00	0.00
19,300.0	90.00	179.77	11,599.0	-8,160.2	2,070.8	8,404.4	0.00	0.00	0.00
19,400.0	90.00	179.77	11,599.0	-8,260.2	2,071.3	8,502.6	0.00	0.00	0.00
19,500.0	90.00	179.77	11,599.0	-8,360.2	2,071.7	8,600.9	0.00	0.00	0.00
19,600.0	90.00	179.77	11,599.0	-8,460.2	2,072.1	8,699.2	0.00	0.00	0.00
19,700.0	90.00	179.77	11,599.0	-8,560.2	2,072.5	8,797.5	0.00	0.00	0.00
19,800.0	90.00	179.77	11,599.0	-8,660.2	2,072.9	8,895.8	0.00	0.00	0.00
19,900.0	90.00	179.77	11,599.0	-8,760.2	2,073.3	8,994.0	0.00	0.00	0.00
20,000.0	90.00	179.77	11,599.0	-8,860.2	2,073.7	9,092.3	0.00	0.00	0.00
20,100.0	90.00	179.77	11,599.0	-8,960.2	2,074.1	9,190.6	0.00	0.00	0.00
20,200.0	90.00	179.77	11,599.0	-9,060.2	2,074.5	9,288.9	0.00	0.00	0.00
20,300.0	90.00	179.77	11,599.0	-9,160.2	2,074.9	9,387.2	0.00	0.00	0.00
20,400.0	90.00	179.77	11,599.0	-9,260.2	2,075.3	9,485.4	0.00	0.00	0.00
20,500.0	90.00	179.77	11,599.0	-9,360.2	2,075.7	9,583.7	0.00	0.00	0.00
20,600.0	90.00	179.77	11,599.0	-9,460.2	2,076.1	9,682.0	0.00	0.00	0.00
20,700.0	90.00	179.77	11,599.0	-9,560.2	2,076.5	9,780.3	0.00	0.00	0.00
20,800.0	90.00	179.77	11,599.0	-9,660.2	2,076.9	9,878.6	0.00	0.00	0.00
20,900.0	90.00	179.77	11,599.0	-9,760.2	2,077.4	9,976.9	0.00	0.00	0.00
21,000.0	90.00	179.77	11,599.0	-9,860.2	2,077.8	10,075.1	0.00	0.00	0.00
21,100.0	90.00	179.77	11,599.0	-9,960.2	2,078.2	10,173.4	0.00	0.00	0.00
21,200.0	90.00	179.77	11,599.0	-10,060.2	2,078.6	10,271.7	0.00	0.00	0.00
21,300.0	90.00	179.77	11,599.0	-10,160.2	2,079.0	10,370.0	0.00	0.00	0.00
21,400.0	90.00	179.77	11,599.0	-10,260.2	2,079.4	10,468.3	0.00	0.00	0.00
21,500.0	90.00	179.77	11,599.0	-10,360.2	2,079.8	10,566.5	0.00	0.00	0.00
21,600.0	90.00	179.77	11,599.0	-10,460.2	2,080.2	10,664.8	0.00	0.00	0.00
21,700.0	90.00	179.77	11,599.0	-10,560.2	2,080.6	10,763.1	0.00	0.00	0.00
21,800.0	90.00	179.77	11,599.0	-10,660.2	2,081.0	10,861.4	0.00	0.00	0.00
21,878.5	90.00	179.77	11,599.0	-10,738.7	2,081.3	10,938.5	0.00	0.00	0.00
21,900.0	90.00	179.87	11,599.0	-10,760.2	2,081.4	10,959.7	0.47	0.00	0.47
21,978.5	90.00	180.23	11,599.0	-10,838.7	2,081.3	11,036.7	0.47	0.00	0.47

Design Targets									
Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
KOP(Banjo 32 Fed Com - plan hits target cen - Point	0.00 ter	0.00	11,121.5	-488.1	2,038.5	392,721.00	675,068.00	32° 4' 44.162 N	103° 54' 5.614 W
FTP(Banjo 32 Fed Com - plan hits target cen - Point	0.00 ter	0.00	11,556.2	-768.2	2,040.5	392,441.00	675,070.00	32° 4' 41.392 N	103° 54' 5.604 W
Fed LTP(Banjo 32 Fed C - plan hits target cen - Point		0.00	11,599.0	-10,738.7	2,081.3	382,472.00	675,111.00	32° 3′ 2.736 N	103° 54' 5.591 W
PBHL(Banjo 32 Fed Cor - plan hits target cen - Point	0.00 ter	0.00	11,599.0	-10,838.7	2,081.3	382,372.00	675,111.00	32° 3′ 1.747 N	103° 54' 5.596 W



PEDMB Database: Company: Midland

Project: Eddy County, NM (NAD 83 NME)

Stark 32 Fed Com Site:

Well: #753H Wellbore: ОН Design:

Plan #0.1 RT

Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

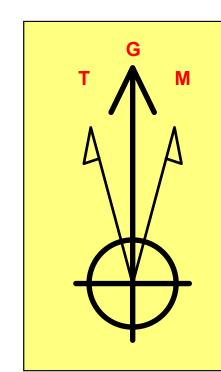
**Survey Calculation Method:** 

Well #753H

kb = 26' @ 3189.0usft kb = 26' @ 3189.0usft

Grid





1400

1750

2450

2800

3150

10150

**Azimuths to Grid North** True North: -0.23° Magnetic North: 6.09°

> **Magnetic Field** Strength: 47049.7nT Dip Angle: 59.62° Date: 8/6/2024 Model: IGRF2020

To convert a Magnetic Direction to a Grid Direction, Add 6.09° To convert a Magnetic Direction to a True Direction, Add 6.32° East To convert a True Direction to a Grid Direction, Subtract 0.23°

393209.00

# **Eddy County, NM (NAD 83 NME)**

Stark 32 Fed Com #753H

Plan #0.1 RT

## PROJECT DETAILS: Eddy County, NM (NAD 83 NME)

Geodetic System: US State Plane 1983 Datum: North American Datum 1983 Ellipsoid: GRS 1980 **Zone: New Mexico Eastern Zone** 

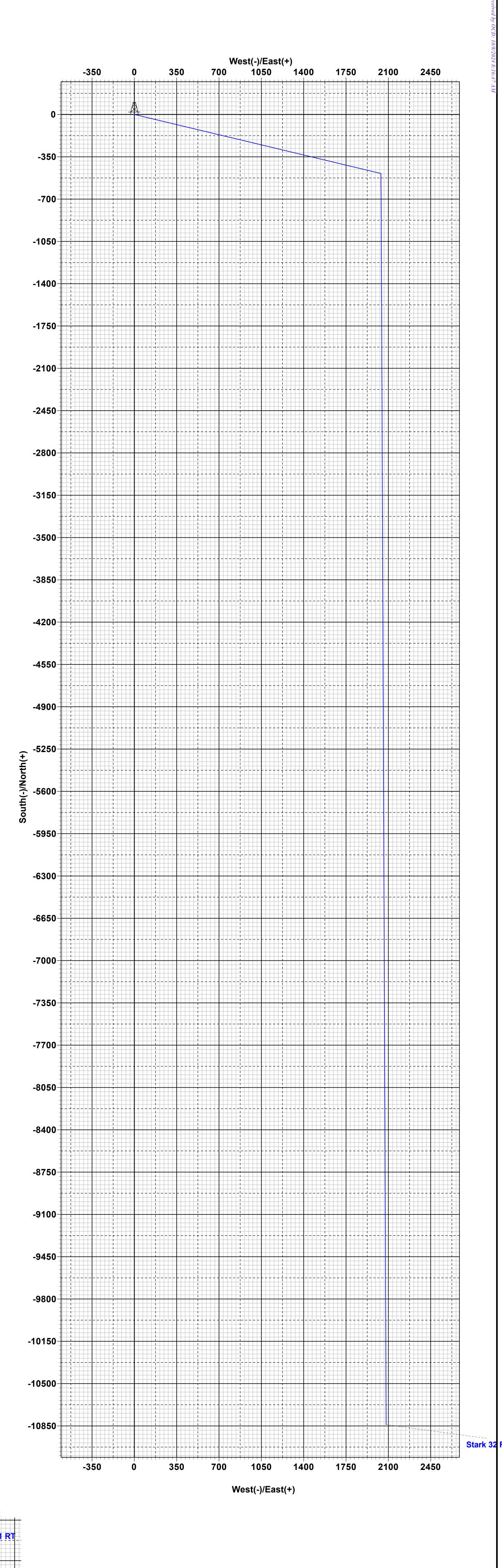
System Datum: Mean Sea Level

WELL DETAILS: #753H 3163.0 kb = 26' @ 3189.0usft **Easting 673030.00** Northing Longitude 103° 54' 29.279 W Latittude 32° 4' 49.072 N

	SECTION DETAILS									
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	1417.0	0.00	0.00	1417.0	0.0	0.0	0.00	0.00	0.0	
3	2062.1	13.03	103.47	2056.6	-17.0	71.0	2.02	103.47	30.1	
4	10710.2	13.03	103.47	10481.9	-471.1	1967.5	0.00	0.00	833.7	
5	11355.3	0.00	0.00	11121.5	-488.1	2038.5	2.02	180.00	863.8	
6	11355.3	0.00	0.00	11121.5	-488.1	2038.5	0.00	0.00	863.8	KOP(Banjo 32 Fed Com #753H)
7	11901.8	65.59	179.60	11556.2	-768.2	2040.5	12.00	179.60	1139.2	FTP(Banjo 32 Fed Com #753H)
8	12105.2	90.00	179.77	11598.9	-965.5	2041.6	12.00	0.41	1333.2	
9	21878.5	90.00	179.77	11599.0	-10738.7	2081.3	0.00	0.00	10938.5	Fed LTP(Banjo 32 Fed Com #753H)
10	21978.5	90.00	180.23	11599.0	-10838.7	2081.3	0.47	89.85	11036.7	PBHL(Banjo 32 Fed Com #753H)

CASING DETAILS No casing data is available

Name	TVD	+N/-S	+E/-W	Northing	Easting
KOP(Banjo 32 Fed Com #753H)	11121.5	-488.1	2038.5	392721.00	675068.00
FTP(Banjo 32 Fed Com #753H)	11556.2	-768.2	2040.5	392441.00	675070.00
Fed LTP(Banjo 32 Fed Com #753H)	11599.0	-10738.7	2081.3	382472.00	675111.00
PBHL(Banjo 32 Fed Com #753H)	11599.0	-10838.7	2081.3	382372.00	675111.00



Vertical Section at 169.13°

## PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

PAD: BANJO/ STARK 32/5 FED COM – DEEP TARGETS

SHL: SEC32/5 T25S R30E, EDDY COUNTY

Well Name	API#	Sur	face	Intern	nediate	Production	
vven Name	AII#	MD	TVD	MD	TVD	MD	TVD
Banjo 32 Fed Com #761H (FKA 594H)	30-015-48267	1,320	1,320	11,632	11,600	21,987	11,811
Banjo 32 Fed Com #762H (FKA 584H)	30-015-48265	1,320	1,320	11,934	11,600	22,226	11,811
Banjo 32 Fed Com #771H (FKA 504H)	30-015-48264	1,320	1,320	11,696	11,600	22,205	11,972
Banjo 5 Fed Com #751H (FKA 586H)	30-025-47901	1,320	1,320	11,617	11,600	21,761	11,599
Banjo 5 Fed Com #752H (FKA 595H)	30-015-47904	1,320	1,320	11,923	11,600	22,006	11,599
Stark 32 Fed Com #753H (FKA Banjo 32 Fed Com 593H)	30-015-48266	1,320	1,320	11,846	11,600	21,979	11,599

SUNDRY WRITTEN FOR DEEPEST WELL IN THE LIST ABOVE, BUT APPROVAL APPLIES TO ALL. ALL PREVIOUS COAS STILL APPLY

COA

H2S	• Yes	O No	
Potash	None	O Secretary	O R-111-P
Cave/Karst Potential	• Low	O Medium	O High
Cave/Karst Potential	O Critical		
Variance	O None	• Flex Hose	Other
Wellhead	Conventional	<ul><li>Multibowl</li></ul>	O Both
Wellhead Variance	O Diverter		
Other	□4 String	☐ Capitan Reef	□WIPP
Other	✓ Fluid Filled	☐ Pilot Hole	☐ Open Annulus
Cementing	☐ Contingency		Primary Cement
	Cement Squeeze		Squeeze
Special Requirements	☐ Water Disposal	<b>☑</b> COM	□ Unit
Special Requirements	☐ Batch Sundry		
Special Requirements	Break Testing	✓ Offline	✓ Casing
Variance		Cementing	Clearance

#### A. CASING

#### **Primary Casing Design:**

- 1. The **9-5/8** inch surface casing shall be set at approximately **1,320** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run

- to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The **7-5/8** inch intermediate casing shall be set at approximately **11,600 feet TVD**. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

#### Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- a. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon
- b. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified.

Operator has proposed to pump down 7-5/8" X 9-5/8" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 7-5/8" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

<u>If cement does not tie-back into the previous casing shoe, a third stage remediation</u> BH may be performed. The appropriate BLM office shall be notified.

Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be

## <u>notified prior to job with volumes and planned wellbore schematic. CBL will be</u> needed when this occurs.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

3. The **5-1/2** inch production casing shall be set at approximately **22,226** feet. The minimum required fill of cement behind the **5-1/2** inch production casing is:

#### **Option 1 (Single Stage):**

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

#### **Alternate Casing Design:**

- 1. The **10-3/4** inch surface casing shall be set at approximately **1,320** feet (a minimum of 25 feet (Lea County) into the Rustler Anhydrite, above the salt, and below usable fresh water) and cemented to the surface.
  - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - f. Wait on cement (WOC) time for a primary cement job will be a minimum of **8 hours** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
  - g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - h. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The **8-3/4** inch intermediate casing shall be set at approximately **11,600** feet TVD. The minimum required fill of cement behind the **8-3/4** inch intermediate casing is:

#### **Option 1 (Single Stage):**

• Cement to surface. If cement does not circulate see B.1.a, c-d above.

#### Option 2:

Operator has proposed to cement in two stages by conventionally cementing the first stage and performing a bradenhead squeeze on the second stage, contingent upon no returns to surface.

- c. First stage: Operator will cement with intent to reach the top of the **Brushy** Canyon
- d. Second stage:
  - Operator will perform bradenhead squeeze and top-out. Cement to surface. If cement does not reach surface, the appropriate BLM office shall be notified.

Operator has proposed to pump down 10-3/4 X 8-3/4" annulus. Operator must top out cement after the bradenhead squeeze and verify cement to surface. Operator can also check TOC with Echo-meter. CBL must be run from TD of the 8-3/4" casing to surface if confidence is lacking on the quality of the bradenhead squeeze cement job. Submit results to BLM.

If cement does not tie-back into the previous casing shoe, a third stage remediation BH may be performed. The appropriate BLM office shall be notified.

Bradenhead squeeze in the production interval is only as an edge case remediation measure and is NOT approved in this COA. If production cement job experiences losses and a bradenhead squeeze is needed for tie-back, BLM Engineering should be notified prior to job with volumes and planned wellbore schematic. CBL will be needed when this occurs.

If cement does not reach surface, the next casing string must come to surface.

Operator must use a limited flush fluid volume of 1 bbl following backside cementing procedures.

Intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

3. The **6** inch production casing shall be set at approximately **22,226** feet. The minimum required fill of cement behind the **6** inch production casing is:

#### **Option 1 (Single Stage):**

• Cement should tie-back at least **200 feet** into previous casing string. Operator shall provide method of verification.

Production casing must be kept fluid filled to meet BLM minimum collapse requirement.

# NOTE ON PRODUCTION CASING FOR ALTERNATE DESIGN: OPERATOR HAS REQUESTED TO RUN 6" OR 5.5" OR A TAPERED STRING WITH BOTH. ALL THREE OPTIONS REVIEWED AND IS OK.

#### **B. PRESSURE CONTROL**

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 10,000 (10M) psi. Variance is approved to use a 5000 (5M) Annular which shall be tested to 3500 (70% Working Pressure) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
  - e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

#### **Offline Cementing**

Offline cementing approved for surface and intermediate intervals. Contact the BLM PETs prior to the commencement of any offline cementing procedure.

#### **GENERAL REQUIREMENTS**

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

#### **Contact Eddy County Petroleum Engineering Inspection Staff:**

Email or call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220; **BLM NM CFO DrillingNotifications@BLM.GOV**; (575) 361-2822

1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.

- a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
- b. When the operator proposes to set surface casing with Spudder Rig
  - i. Notify the BLM when moving in and removing the Spudder Rig.
  - ii. Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
  - iii. BOP/BOPE test to be conducted per **43 CFR 3172** as soon as 2<sup>nd</sup> Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. For intervals in which cement to surface is required, cement to surface should be verified with a visual check and density or pH check to differentiate cement from spacer and drilling mud. The results should be documented in the driller's log and daily reports.

#### A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends of both lead and tail cement, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.

- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing integrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-Q potash area, the NMOCD requirements shall be followed.

#### **B. PRESSURE CONTROL**

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in **43 CFR 3172**.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review.

- These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - i. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - ii. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - iii. Manufacturer representative shall install the test plug for the initial BOP test.
  - iv. Whenever any seal subject to test pressure is broken, all the tests in 43 CFR 3172.6(b)(9) must be followed.
  - v. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - i. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead cement), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - ii. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the cement plug. The BOPE test can be initiated after bumping the

- cement plug with the casing valve open. (only applies to single stage cement jobs, prior to the cement setting up.)
- iii. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer and can be initiated immediately with the casing valve open. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to **43 CFR 3172** with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for 8 hours or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
- iv. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- v. The results of the test shall be reported to the appropriate BLM office.
- vi. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- vii. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- viii. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per **43 CFR 3172**.

#### C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

#### D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.)

created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area. Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

**KPI** 8/30/2024



#### Stark 32 Fed Com 753H (FKA Banjo 32 Fed Com 593H) API #: 30-015-48266 Variances

EOG respectfully requests the below variances to be applied to the above well:

- Variance is requested to waive the centralizer requirements for the intermediate casing in the intermediate hole. An expansion additive will be utilized, in the cement slurry, for the entire length of the intermediate interval to maximize cement bond and zonal isolation.
- Variance is also requested to waive the centralizer requirements for the production casing in the production hole. An expansion additive will be utilized, in the cement slurry, for the entire length of the production interval to maximize cement bond and zonal isolation.
- EOG requests a variance to set the intermediate casing shoe in the Bone Spring formation or the Wolfcamp formation, depending on depletion in the area and well conditions. EOG will monitor the well and ensure the well is static before casing operations begin.
- Variance is requested to use a co-flex line between the BOP and choke manifold (instead of using a 4" OD steel line).
  - Variance is requested to use a 5,000 psi annular BOP with the 10,000 psi BOP stack.
- EOG Resources requests the option to contract a Surface Rig to drill, set surface casing, and Cement on the subject well. After WOC 8 hours or 500 psi compressive strength (whichever is greater), the Surface Rig will move off so the wellhead can be installed. A welder will cut the casing to the proper height and weld on the wellhead (both "A" and "B" sections). The weld will be tested to 1,500 psi. All valves will be closed and a wellhead cap will be installed (diagram attached). If the timing between rigs is such that EOG Resources would not be able to preset the surface, the Primary Rig will MIRU and drill the well in its entirety per the APD.

EOG requests the additional variance(s) in the attached document(s):

- EOG BLM Variance 2a Inermediate Bradenhead Cement
- EOG BLM Variance 3a b BOP Break-test and Offline Intermediate Cement

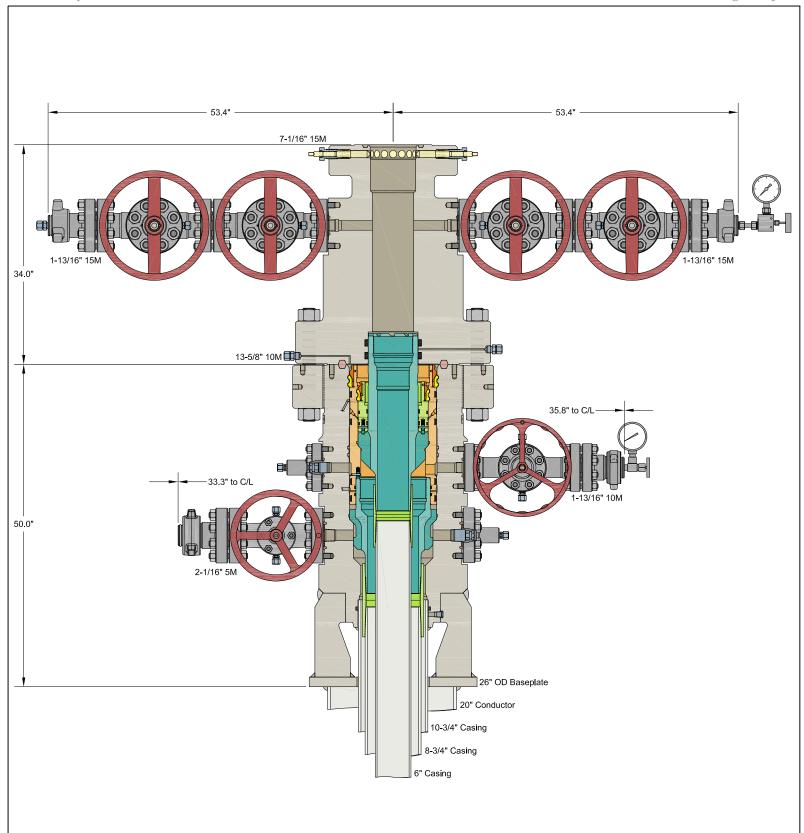


#### **Intermediate Bradenhead Cement:**

EOG requests variance from minimum standards to pump a two stage cement job on the intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brushy Canyon and the second stage performed as 1000 sack bradenhead squeeze with planned cement from the Brushy Canyon to surface. If necessary, a top out consisting of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. Top of cement will be verified by Echo-meter.

EOG will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

EOG will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.



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ALL DIMENSIONS APPROXIMATE

### CACTUS WELLHEAD LLC

10-3/4" x 8-3/4" x 6" MBU-3T-SF-SOW Wellhead System With 8-5/8" & 6" Pin Bottom Mandrel Casing Hangers And 13-5/8" 10M x 7-1/16" 15M CTH-DBLHPS Tubing Head

#### **EOG RESOURCES**

DRAWN DLE 14APR21
APPRV

DRAWING NO. SDT-3141-1

Issued on: 10 Feb. 2021 by Wesley Ott



**Connection Data Sheet** 

OD Weight (lb/ft) Wall Th. Grade API Drift: Connection

Nominal: 24.50 Plain End: 23.95

Wall Th. Grade API Drift: Connection

VAM® SPRINT-SF

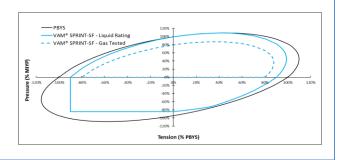
PIPE PROPERTIES		
Nominal OD	6.000	in.
Nominal ID	5.200	in.
Nominal Cross Section Area	7.037	sqin.
Grade Type	Hig	h Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi

CONNECTION PROPERTIES		
Connection Type	Integral :	Semi-Flush
Connection OD (nom):	6.277	in.
Connection ID (nom):	5.146	in.
Make-Up Loss	5.386	in.
Critical Cross Section	6.417	sqin.
Tension Efficiency	91.0	% of pipe
Compression Efficiency	91.0	% of pipe
Internal Pressure Efficiency	100	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMAN	CES	
Tensile Yield Strength	801	klb
Compression Resistance	801	klb
Internal Yield Pressure	14,580	psi
Collapse Resistance	12,500	psi
Max. Structural Bending	83	°/100ft
Max. Bending with ISO/API Sealability	30	°/100ft

TORQUE VALUES		
Min. Make-up torque	21,750	ft.lb
Opt. Make-up torque	24,250	ft.lb
Max. Make-up torque	26,750	ft.lb
Max. Torque with Sealability (MTS)	53,000	ft.lb

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.



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<sup>\* 87.5%</sup> RBW

Issued on: 09 Dec. 2020 by Wesley Ott



**Connection Data Sheet** 

 OD
 Weight (lb/ft)
 Wall Th.
 Grade
 Spec. Drift:
 Connection

 8 3/4 in.
 Nominal: 38.50 Plain End: 36.98
 0.415 in.
 P110EC
 7.875 in.
 VAM® SPRINT-SF

PIPE PROPERTIES		
Nominal OD	8.750	in.
Nominal ID	7.920	in.
Nominal Cross Section Area	10.867	sqin.
Grade Type	High	n Yield
Min. Yield Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi

CONNECTION PROPERTIES		
Connection Type	Integral :	Semi-Flush
Connection OD (nom):	9.009	in.
Connection ID (nom):	7.945	in.
Make-Up Loss	4.905	in.
Critical Cross Section	9.970	sqin.
Tension Efficiency	89.0	% of pipe
Compression Efficiency	80.0	% of pipe
Internal Pressure Efficiency	87	% of pipe
External Pressure Efficiency	100	% of pipe

CONNECTION PERFORMANCE	S	
Tensile Yield Strength	1,209	klb
Compression Resistance	1,086	klb
Internal Yield Pressure	9,030	psi
Collapse Resistance	5,210	psi
Max. Structural Bending	55	°/100ft
Max. Bending with ISO/API Sealability	30	°/100ft

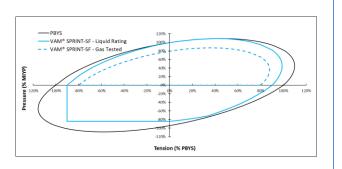
TORQUE VALUES		
Min. Make-up torque	20,750	ft.lb
Opt. Make-up torque	23,250	ft.lb
Max. Make-up torque	25,750	ft.lb
Max. Torque with Sealability (MTS)	50,000	ft.lb

VAM® SPRINT-SF is a semi-flush connection innovatively designed for extreme shale applications. Its high tension rating and ultra high torque capacity make it ideal to run a fill string length as production casing in shale wells with extended horizontal sections and tight clearance requirements.

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<sup>\* 87.5%</sup> RBW

PDF

10.750 40.50/0.350 J55

New Search »

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C Metric

	6/8/2015	10:14:05	ΑM
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Mechanical Properties	Ptpe	втс	LTC	STC	
Minimum Yield Strength	55,000	-	-	-	psi
Maximum Yield Strength	80,000	-	-	-	psi
Minimum Tensile Strength	75,000	-	-	-	psi
Dimensions	Ptpe	втс	LTC	STC	
Outside Diameter	10.750	11.750	-	11.750	in.
Wall Thickness	0.350		-		in.
Inside Diameter	10.050	10.050	-	10.050	in.
Standard Drift	9.894	9.894	-	9.894	in.
Alternate Drift	-	-	-	-	in.
Nominal Linear Weight, T&C	40.50	-	-	-	lbs/ft
Plain End Weight	38.91	-	-	-	lbs/ft
Performance	Ptpe	втс	LTC	STC	
Minimum Collapse Pressure	1,580	1,580	-	1,580	psi
Minimum Internal Yield Pressure	3,130	3,130	-	3,130	psi
Minimum Pipe Body Yield Strength	629.00	-	-	-	1000 lbs
Joint Strength	-	700	-	420	1000 lbs
Reference Length	-	11,522	-	6,915	ft
Make-Up Data	Ptpe	втс	LTC	STC	
Make-Up Loss	-	4.81	-	3.50	in.
Minimum Make-Up Torque	-	-	-	3,150	ff-lbs
Released to Imaging: 7/26/2025 8:57:36 AM  Maximum Make-Up Torque	-	-	-	5,250	ft-lbs



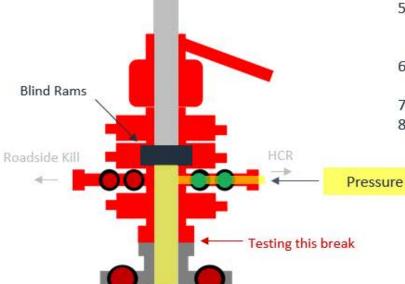
#### **Break-test BOP & Offline Cementing:**

EOG Resources Inc. (EOG) respectfully requests a variance from the minimum standards for well control equipment testing of ECFR Title 43 Part 3172.6(b)(9)(iv) to allow a testing schedule of the blow out preventer (BOP) and blow out prevention equipment (BOPE) along with Batch Drilling & Offline cement operations to include the following:

- Full BOPE test at first installation on the pad.
- Full BOPE test every 21 days.
- This test will be conducted for 5M rated hole intervals only.
- Each rig requesting the break-test variance is capable of picking up the BOP without damaging components using winches, following API Standard 53, Well Control Equipment Systems for Drilling Wells (Fifth edition, December 2018, Annex C. Table C.4) which recognizes break testing as an acceptable practice.
- Function tests will be performed on the following BOP elements:
  - Annular à during each full BOPE test
  - Upper Pipe Rams à On trip ins where FIT required
  - Blind Rams à Every trip
  - Lower Pipe Rams à during each full BOPE test
- Break testing BOP and BOPE coupled with batch drilling operations and option to offline cement and/or remediate (if needed) any surface or intermediate sections, according to attached offline cementing support documentation.
- After the well section is secured, the BOP will be disconnected from the wellhead and walked with the rig to another well on the pad.
- TA cap will also be installed per Wellhead vendor procedure and pressure inside the
  casing will be monitored via the valve on the TA cap as per standard batch drilling
  ops.

Test plug

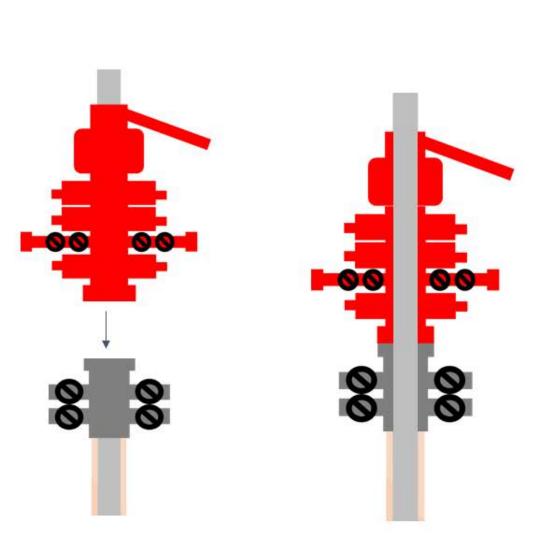
## **Break Test Diagram (HCR valve)**

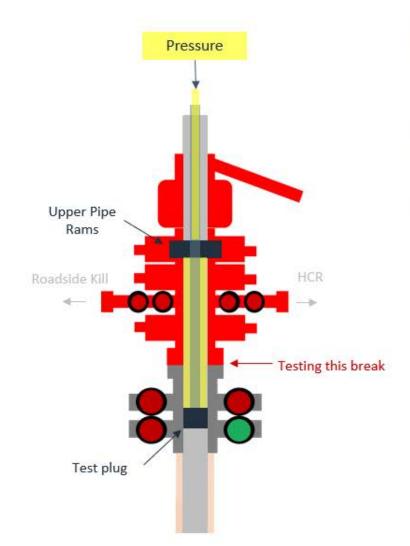


#### Steps

- 1. Set plug in wellhead (lower barrier)
- 2. Close Blind Rams (upper barrier)
- 3. Close roadside kill
- 4. Open HCR (pressure application)
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to main choke manifold crown valve
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit

## **Break Test Diagram (Test Joint)**





#### Steps

- Set plug in with test joint wellhead (lower barrier)
- 2. Close Upper Pipe Rams (upper barrier)
- 3. Close roadside kill
- Close HCR
- Open wellhead valves below test plug to ensure if leak past test plug, pressure won't be applied to wellbore
- Tie BOP testers high pressure line to top of test joint
- 7. Pressure up to test break
- Bleed test pressure from BOP testing unit



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#### **Cement Program**

1. No changes to the cement program will take place for offline cementing.

#### **Summarized Operational Procedure for Intermediate Casing**

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment back pressure valves.
  - a. Float equipment is equipped with two back pressure valves rated to a minimum of 5,000 psi.
- 2. Land production casing on mandrel hanger through BOP.
  - a. If casing is unable to be landed with a mandrel hanger, then the casing will be cemented online.
- 3. Break circulation and confirm no restrictions.
  - a. Ensure no blockage of float equipment and appropriate annular returns.
  - b. Perform flow check to confirm well is static.
- 4. Set pack-off
  - a. If utilizing a fluted/ported mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid, remove landing joint, and set annular packoff through BOP. Pressure test to 5,000 psi for 10 min.
  - b. If utilizing a solid mandrel hanger, ensure well is static on the annulus and inside the casing by filling the pipe with kill weight fluid. Pressure test seals to 5,000 psi for 10 min. Remove landing joint through BOP.
- 5. After confirmation of both annular barriers and the two casing barriers, install TA plug and pressure test to 5,000 psi for 10 min. Notify the BLM with intent to proceed with nipple down and offline cementing.
  - a. Minimum 4 hrs notice.
- 6. With the well secured and BLM notified, nipple down BOP and secure on hydraulic carrier or cradle.
  - a. Note, if any of the barriers fail to test, the BOP stack will not be nippled down until after the cement job has concluded and both lead and tail slurry have reached 500 psi.
- 7. Skid/Walk rig off current well.
- 8. Confirm well is static before removing TA Plug.
  - a. Cementing operations will not proceed until well is under control. (If well is not static, notify BLM and proceed to kill)
  - b. Casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing.
  - c. Well control plan can be seen in Section B, Well Control Procedures.
  - d. If need be, rig can be moved back over well and BOP nippled back up for any further remediation.



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- e. Diagram for rig positioning relative to offline cementing can be seen in Figure 4.
- 9. Rig up return lines to take returns from wellhead to pits and rig choke.
  - a. Test all connections and lines from wellhead to choke manifold to 5,000 psi high for 10 min.
  - If either test fails, perform corrections and retest before proceeding.
  - c. Return line schematics can be seen in Figure 3.
- 10. Remove TA Plug from the casing.
- 11. Install offline cement tool.
  - a. Current offline cement tool schematics can be seen in Figure 1 (Cameron) and Figure 2 (Cactus).
- 12. Rig up cement head and cementing lines.
  - a. Pressure test cement lines against cement head to 80% of casing burst for 10 min.
- 13. Break circulation on well to confirm no restrictions.
  - a. If gas is present on circulation, well will be shut in and returns rerouted through gas buster.
  - b. Max anticipated time before circulating with cement truck is 6 hrs.
- 14. Pump cement job as per plan.
  - a. At plug bump, test casing to 0.22 psi/ft or 1500 psi, whichever is greater.
  - b. If plug does not bump on calculated, shut down and wait 8 hrs or 500 psi compressive strength, whichever is greater before testing casing.
- 15. Confirm well is static and floats are holding after cement job.
  - a. With floats holding and backside static:
    - i. Remove cement head.
  - b. If floats are leaking:
    - i. Shut-in well and WOC (Wait on Cement) until tail slurry reaches 500 psi compressive strength and the casing is static prior to removing cement head.
  - c. If there is flow on the backside:
    - i. Shut in well and WOC until tail slurry reaches 500 psi compressive strength. Ensure that the casing is static prior to removing cement head.
- 16. Remove offline cement tool.
- 17. Install night cap with pressure gauge for monitoring.
- 18. Test night cap to 5,000 psi for 10 min.



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#### **Example Well Control Plan Content**

#### A. Well Control Component Table

The table below, which covers the cementing of the <u>5M MASP (Maximum Allowable Surface Pressure) portion of the well</u>, outlines the well control component rating in use. This table, combined with the mud program, documents that two barriers to flow can be maintained at all times, independent of the BOP nippled up to the wellhead.

Intermediate hole section, 5M requirement

Component	RWP
Pack-off	10M
Casing Wellhead Valves	10M
Annular Wellhead Valves	5M
TA Plug	10M
Float Valves	5M
2" 1502 Lo-Torque Valves	15M

#### **B.** Well Control Procedures

Well control procedures are specific to the rig equipment and the operation at the time the kick occurs. Below are the minimal high-level tasks prescribed to assure a proper shut-in while circulating and cementing through the Offline Cement Adapter.

#### **General Procedure While Circulating**

- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.

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- 6. Read and record the following:
  - a. SICP (Shut in Casing Pressure) and AP (Annular Pressure)
  - b. Pit gain
  - c. Time
  - d. Regroup and identify forward plan to continue circulating out kick via rig choke and mud/gas separator. Circulate and adjust mud density as needed to control well.

#### **General Procedure While Cementing**

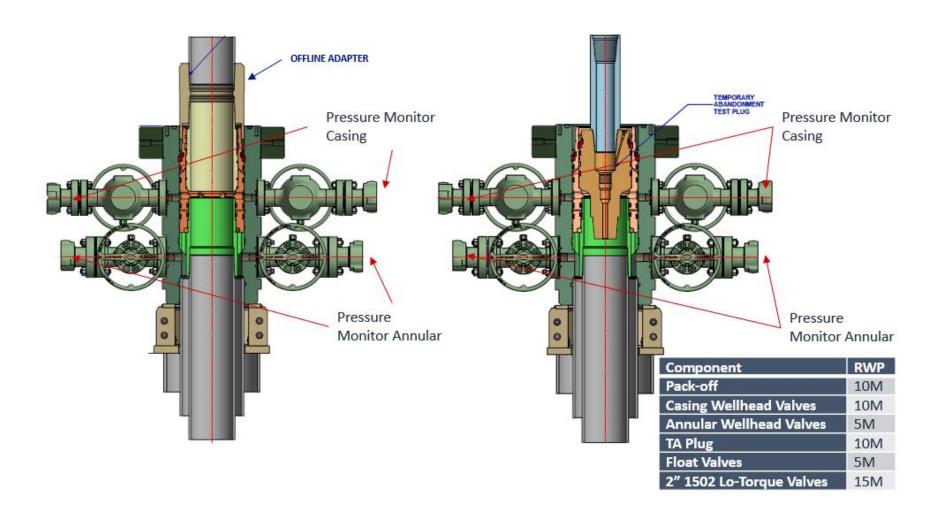
- 1. Sound alarm (alert crew).
- 2. Shut down pumps.
- 3. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 4. Confirm shut-in.
- 5. Notify tool pusher/company representative.
- 6. Open rig choke and begin pumping again taking returns through choke manifold and mud/gas separator.
- 7. Continue to place cement until plug bumps.
- 8. At plug bump close rig choke and cement head.
- 9. Read and record the following
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead

#### **General Procedure After Cementing**

- 1. Sound alarm (alert crew).
- 2. Shut-in Well (close valves to rig pits and open valve to rig choke line. Rig choke will already be in the closed position).
- 3. Confirm shut-in.
- 4. Notify tool pusher/company representative.
- 5. Read and record the following:
  - a. SICP and AP
  - b. Pit gain
  - c. Time
  - d. Shut-in annulus valves on wellhead



Figure 1: Cameron TA Plug and Offline Adapter Schematic

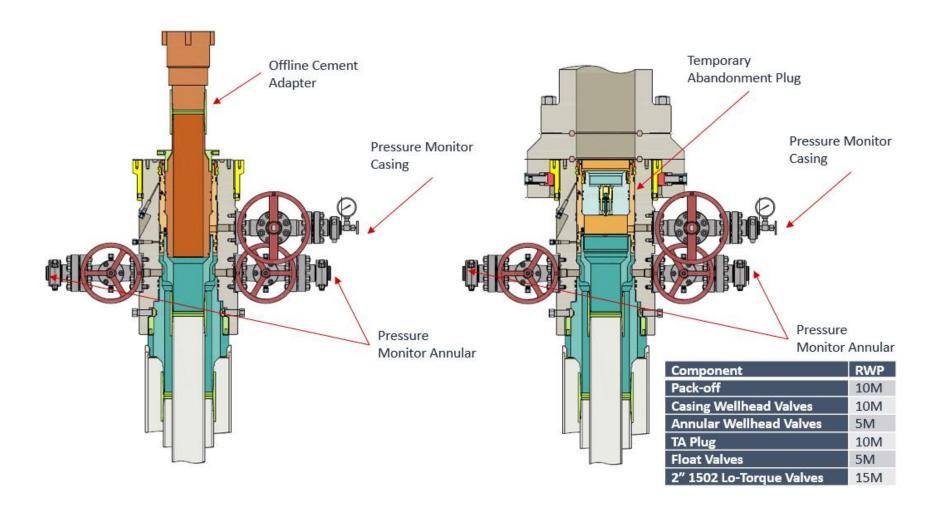


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Figure 2: Cactus TA Plug and Offline Adapter Schematic

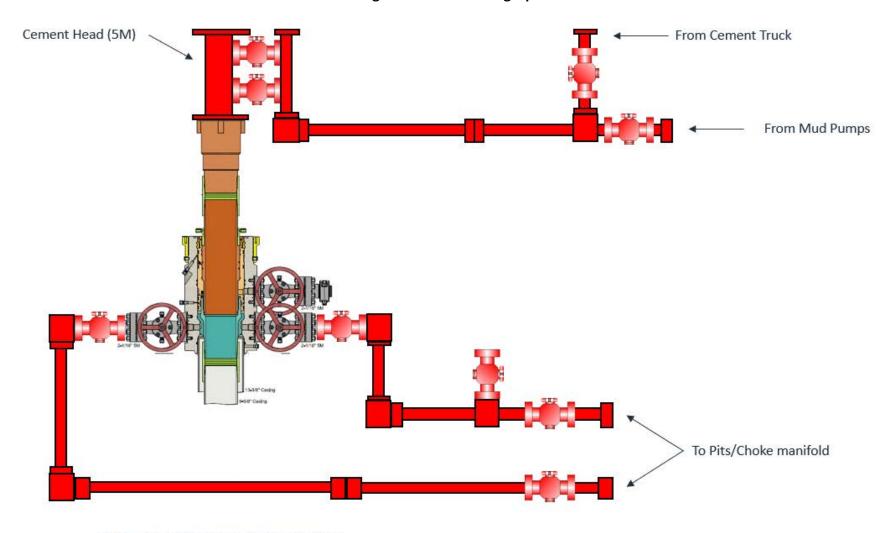


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Figure 3: Back Yard Rig Up



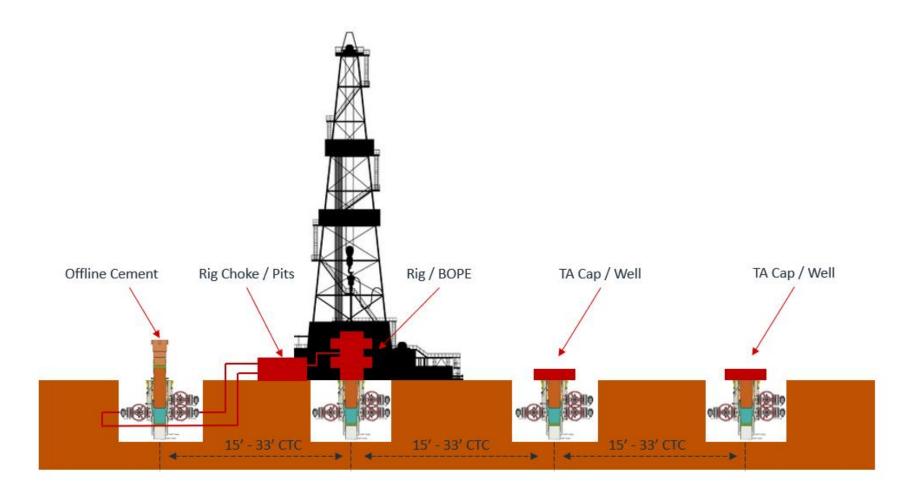
\*\*\* All Lines 10M rated working pressure

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Figure 4: Rig Placement Diagram



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### **EOG Batch Casing**

Pad Name: Banjo 32-5 Stark 32-5 Fed Com DEEP

SHL: Section 32, Township 25-S, Range 30-E, Eddy County, NM

Wall Nama	ADI# Sur		Surface		Intermediate		Production	
Well Name	API#	MD	TVD	MD	TVD	MD	TVD	
Banjo 32 Fed Com #761H (FKA 594H)	30-015-48267	1,320	1,320	11,632	11,600	21,987	11,811	
Banjo 32 Fed Com #762H (FKA 584H)	30-015-48265	1,320	1,320	11,934	11,600	22,226	11,811	
Banjo 32 Fed Com #771H (FKA 504H)	30-015-48264	1,320	1,320	11,696	11,600	22,205	11,972	
Banjo 5 Fed Com #751H (FKA 586H)	30-025-47901	1,320	1,320	11,617	11,600	21,761	11,599	
Banjo 5 Fed Com #752H (FKA 595H)	30-015-47904	1,320	1,320	11,923	11,600	22,006	11,599	
Stark 32 Fed Com #753H (FKA Banjo 32 Fed Com 593H)	30-015-48266	1,320	1,320	11,846	11,600	21,979	11,599	



### **EOG Batch Casing**

#### Variances

EOG requests the additional variance(s) in the attached document(s):

- EOG BLM Variance 2a Intermediate Bradenhead Cement
- EOG BLM Variance 3a\_b BOP Break-test and Offline Intermediate Cement



#### **EOG Batch Casing**

#### GEOLOGIC NAME OF SURFACE FORMATION:

Permian

#### ESTIMATED TOPS OF IMPORTANT GEOLOGICAL MARKERS:

Rustler	1,242'
Tamarisk Anhydrite	1,292'
Top of Salt	1,549'
Base of Salt	3,436'
Lamar	3,634'
Bell Canyon	3,661'
Cherry Canyon	577'
Brushy Canyon	5,826'
Bone Spring Lime	7,481'
Leonard (Avalon) Shale	7,547'
1st Bone Spring Sand	8,412'
2nd Bone Spring Shale	8,685'
2nd Bone Spring Sand	9,134'
3rd Bone Spring Carb	9,615'
3rd Bone Spring Sand	10,326'
Wolfcamp	10,738'

#### ESTIMATED DEPTHS OF ANTICIPATED FRESH WATER, OIL OR GAS:

Upper Permian Sands	0-400'	Fresh Water
Bell Canyon	3,661'	Oil
Cherry Canyon	577'	Oil
Brushy Canyon	5,826'	Oil
Leonard (Avalon) Shale	7,547'	Oil
1st Bone Spring Sand	8,412'	Oil
2nd Bone Spring Shale	8,685'	Oil
2nd Bone Spring Sand	9,134'	Oil

No other Formations are expected to give up oil, gas or fresh water in measurable quantities. Surface fresh water sands will be protected by setting surface casing at 1,320' and circulating cement back to surface.

Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

Online Phone Directory https://www.emnrd.nm.gov/ocd/contact-us

# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 390649

#### **CONDITIONS**

Operator:	OGRID:
EOG RESOURCES INC	7377
5509 Champions Drive	Action Number:
Midland, TX 79706	390649
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

#### CONDITIONS

Created By	Condition	Condition Date
ward.rika	Work was performed without OCD approval.	7/26/2025