

**BUREAU OF LAND MANAGEMENT** 

# U.S. Department of the Interior

Sundry Print Report

Well Name: BRUSHY DRAW 30

**FEDERAL** 

Well Location: T25S / R30E / SEC 30 /

SWSW / 32.094511 / -103.925502

County or Parish/State: EDDY /

Well Number: 102H Type of Well: CONVENTIONAL GAS

WELL

Allottee or Tribe Name:

Lease Number: NMNM014785,

NMNM14785

**Unit or CA Name:** 

**Unit or CA Number:** 

**US Well Number: 3001545186** 

**Operator: XTO PERMIAN OPERATING** 

LLC

# **Notice of Intent**

**Sundry ID: 2662750** 

Type of Submission: Notice of Intent

Date Sundry Submitted: 03/18/2022

Type of Action: Other

Time Sundry Submitted: 07:10

Date proposed operation will begin: 04/19/2022

Procedure Description: \*\*Formation Change, Pool Change, Spacing, Casing/Cement, Drilling Variance Changes XTO Permian Operating, LLC requests permission to make the following changes to the original APD: No Additional Surface Disturbance Change formation from Wolfcamp to Bone Spring Change Pool fr/Purple Sage; Wolfcamp (98220) to Corral Canyon; Bone Spring, South (13354) Change BHL fr/2440'FNL & 990'FWL to 2460'FNL & 1870'FWL Casing/Cement design per the attached drilling program. Batch & Spudder Rig Attachments: C102 Drilling Program Directional Plan Multibowl Diagram Spudder Rig Request Offline Cement Variance (Surface & Intermediate Only) Request BOP Breaktest Variance

# **Surface Disturbance**

Is any additional surface disturbance proposed?: No

# **NOI Attachments**

# **Procedure Description**

BD\_30\_Fed\_102H\_Attachments\_20220421133450.pdf

Page 1 of 2

eived by OCD: 6/27/2025 11:15:56 AM Well Name: BRUSHY DRAW 30

**FEDERAL** 

Well Location: T25S / R30E / SEC 30 / SWSW / 32.094511 / -103.925502

County or Parish/State: Page 2 of

NM

Well Number: 102H

Type of Well: CONVENTIONAL GAS WELL

**Allottee or Tribe Name:** 

Lease Number: NMNM014785,

NMNM14785

**Unit or CA Name:** 

**Unit or CA Number:** 

**US Well Number: 3001545186** 

**Operator: XTO PERMIAN OPERATING** 

# **Conditions of Approval**

# **Additional**

Sec\_30\_25S\_30E\_NMP\_Sundry\_2662750\_Brushy\_Draw\_31\_Federal\_102H\_Eddy\_NMNM14785\_XTO\_13\_22\_44673\_ Allison\_Morency\_20220422102753.pdf

Sec\_30\_25S\_30E\_NMP\_Sundry\_2662750\_Brushy\_Draw\_31\_Federal\_102H\_Eddy\_NMNM14785\_XTO\_COAs\_202204 22102752.pdf

Sec\_30\_25S\_30E\_NMP\_Sundry\_2662750\_Brushy\_Draw\_31\_Federal\_102H\_Eddy\_NMNM14785\_XTO\_Break\_Testing COAs 20220422102752.pdf

# **Operator**

I certify that the foregoing is true and correct. Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction. Electronic submission of Sundry Notices through this system satisfies regulations requiring a

Operator Electronic Signature: STEPHANIE RABADUE Signed on: APR 21, 2022 01:34 PM

Name: XTO PERMIAN OPERATING LLC

Title: Regulatory Coordinator

Street Address: 500 W. Illinois St. Ste 100

City: Midland State: TX

Phone: (432) 620-6714

Email address: STEPHANIE.RABADUE@EXXONMOBIL.COM

# **Field**

**Representative Name:** 

**Street Address:** 

State: City: Zip:

Phone:

**Fmail address:** 

# **BLM Point of Contact**

**BLM POC Name: CHRISTOPHER WALLS BLM POC Title:** Petroleum Engineer

**BLM POC Phone:** 5752342234 BLM POC Email Address: cwalls@blm.gov

**Disposition:** Approved Disposition Date: 04/22/2022

Signature: Chris Walls

Page 2 of 2

Form 3160-5 (June 2019)

# **UNITED STATES** DEPARTMENT OF THE INTERIOR

FORM APPROVED
OMB No. 1004-0137
Expires: October 31, 202

BURI	EAU OF LAND MANA		5. Lease Serial No.			
Do not use this t	IOTICES AND REPO form for proposals to Use Form 3160-3 (Al	o drill or to re-	enter an	6. If Indian, Allottee or Trib	e Name	
SUBMIT IN T	TRIPLICATE - Other instru	ctions on page 2		7. If Unit of CA/Agreement	, Name an	d/or No.
1. Type of Well  Oil Well  Gas W	Vell Other			8. Well Name and No.		
2. Name of Operator				9. API Well No.		
3a. Address		3b. Phone No. (inclu	de area code)	10. Field and Pool or Explor	ratory Are	a
4. Location of Well (Footage, Sec., T.,R	R.,M., or Survey Description)			11. Country or Parish, State		
12. CHE	CK THE APPROPRIATE BO	OX(ES) TO INDICAT	ΓΕ NATURE	OF NOTICE, REPORT OR O	THER DA	TA.
TYPE OF SUBMISSION		TYP	E OF ACTION			
Notice of Intent	Acidize Alter Casing	Deepen Hydraulic 1	Fracturing	Production (Start/Resume	_	Water Shut-Off Well Integrity
Subsequent Report	Casing Repair	New Const	_	Recomplete	_	Other
Subsequent Report	Change Plans	Plug and A	bandon	Temporarily Abandon		
Final Abandonment Notice	Convert to Injection	Plug Back		Water Disposal		
is ready for final inspection.)	true and correct. Name (Drie	tod/Timed)				
14. I hereby certify that the foregoing is	true and correct. Name (Prin	nted/Typed)   Title				
		TILLE	,			
Signature		Date	;			
	THE SPACE	FOR FEDERA	L OR STA	ATE OFICE USE		
Approved by			Title		Date	
Conditions of approval, if any, are attacl certify that the applicant holds legal or ewhich would entitle the applicant to con	equitable title to those rights i		Office		2000	
Title 18 U.S.C Section 1001 and Title 4.	3 U.S.C Section 1212, make i	t a crime for any pers	son knowingl	y and willfully to make to any	departme	nt or agency of the United States

any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

## **GENERAL INSTRUCTIONS**

This form is designed for submitting proposals to perform certain well operations and reports of such operations when completed as indicated on Federal and Indian lands pursuant to applicable Federal law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local area or regional procedures and practices, are either shown below, will be issued by or may be obtained from the local Federal office.

# SPECIFIC INSTRUCTIONS

*Item 4* - Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult the local Federal office for specific instructions.

Item 13: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by the local Federal office. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to the top of any tubing left in the hole; method of closing top of well and date well site conditioned for final inspection looking for approval of the abandonment. If the proposal will involve **hydraulic fracturing operations**, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

# **NOTICES**

The privacy Act of 1974 and the regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 351 et seq., 25 U.S.C. 396; 43 CFR 3160.

PRINCIPAL PURPOSE: The information is used to: (1) Evaluate, when appropriate, approve applications, and report completion of subsequent well operations, on a Federal or Indian lease; and (2) document for administrative use, information for the management, disposal and use of National Resource lands and resources, such as: (a) evaluating the equipment and procedures to be used during a proposed subsequent well operation and reviewing the completed well operations for compliance with the approved plan; (b) requesting and granting approval to perform those actions covered by 43 CFR 3162.3-2, 3162.3-3, and 3162.3-4; (c) reporting the beginning or resumption of production, as required by 43 CFR 3162.4-1(c)and (d) analyzing future applications to drill or modify operations in light of data obtained and methods used.

ROUTINE USES: Information from the record and/or the record will be transferred to appropriate Federal, State, local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecutions in connection with congressional inquiries or to consumer reporting agencies to facilitate collection of debts owed the Government.

EFFECT OF NOT PROVIDING THE INFORMATION: Filing of this notice and report and disclosure of the information is mandatory for those subsequent well operations specified in 43 CFR 3162.3-2, 3162.3-4.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to evaluate proposed and/or completed subsequent well operations on Federal or Indian oil and gas leases.

Response to this request is mandatory.

The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

**BURDEN HOURS STATEMENT:** Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C St., N.W., Mail Stop 401 LS, Washington, D.C. 20240

(Form 3160-5, page 2)

# **Additional Information**

# **Additional Remarks**

Attachments:

C102

Drilling Program

Directional Plan

Multibowl Diagram

Spudder Rig Request

Offline Cement Variance (Surface & Intermediate Only) Request

**BOP** Breaktest Variance

# **Location of Well**

 $0. \ SHL: SWSW / 330 \ FSL / 1175 \ FWL / TWSP: 25S / RANGE: 30E / SECTION: 30 / LAT: 32.094511 / LONG: -103.925502 ( \ TVD: 0 \ feet, \ MD: 0 \ feet ) \\ PPP: \ NWNW / 330 \ FNL / 990 \ FWL / TWSP: 25S / RANGE: 30E / SECTION: 31 / LAT: 32.092695 / LONG: -103.926093 ( \ TVD: 10633 \ feet, \ MD: 11064 \ feet ) \\ BHL: \ SWNW / 2440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet, \ MD: 23802 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -103.926035 ( \ TVD: 10700 \ feet ) \\ \ NWNW / 3440 \ FNL / 990 \ FWL / TWSP: 26S / RANGE: 30E / SECTION: 7 / LAT: 32.05768 / LONG: -$ 

Sec 30-25S-30E-NMP Sundry 2662750 Brushy Draw 31 Federal 102H Eddy NMNM14785 XTO 13-22 44673 Allison Morency

## Brushy Draw 31 Federal 102H

95/8	surface	csg in a	12 1/4	inch hole.		Design	Factors			Surfac	e	
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weight
"A"	40.00	J	55	STC	15.27	7.27	0.87	740	12	1.49	13.47	29,600
"B"				STC				0				0
	g mud, 30min Sf			Tail Cmt	does not	circ to sfc.	Totals:	740	-			29,600
Comparison o	of Proposed to	Minimum R	equired Ceme	nt Volumes								
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Reg'd				Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE				Hole-Cp
12 1/4	0.3132	270	437	232	89	9.20	2647	3M				0.81
Burst Frac Grac	dient(s) for Seg	ment(s) A, B	= , b All > 0.7	70, OK.								
7 5/8	casing in		9 5/8			Design				Int 1		
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	B@s	a-B	a-C	Weigh
"A"	29.70	RY P		Flush Joint	2.17	2.52	2.14	4,000	2	3.97	4.32	118,800
"B"	29.70	HCL	80	Flush Joint	2.93	1.28	1.56	4,670	2	2.88	2.18	138,69
	g mud, 30min Sf						Totals:	8,670				257,49
		· ,		chieve a top of	0	ft from su		740				overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd				Min Dis
					U/ Evaces	Mud M/+	MASP	DADE				Hole-Cp
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt		BOPE				
Size 8 3/4 Class 'H' tail cm	0.1005	560	1239	877	41	10.20	2386	3M				0.56
8 3/4	0.1005	560					2386			Prod	1	
8 3/4 Class 'H' tail cm	0.1005 nt yld > 1.20	560	1239			10.20	2386	3M	B@s	Prod a-B	1 a-C	0.56
8 3/4 Class 'H' tail cm Tail cmt 5 1/2	0.1005 nt yld > 1.20 casing ins	560	1239 <b>7</b> 5/8	877	41	10.20  Design Fa	2386		<b>B@s</b> 3		a-C	0.56 Weigh
8 3/4 Class 'H' tail cm Tail cmt 5 1/2 Segment	0.1005 nt yld > 1.20  casing ine	560 side the Grade	1239 <b>7</b> 5/8	877 Coupling	41 Joint	10.20  Design Fa Collapse	2386  ctors  Burst	3M Length	_	a-B	a-C	0.56 Weigh 171,40
8 3/4 Class 'H' tail cm Tail cmt 5 1/2 Segment "A" "B"	0.1005 nt yld > 1.20  casing ins #/ft 20.00	560 side the Grade RY P RY P	1239 <b>7 5/8</b> 110 <b>110</b>	877  Coupling Semi-Premiur	Joint 3.46	Design Fa Collapse 2.71	2386  ctors  Burst 2.86	3M Length 8,570	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	0.56  Weigh 171,40 276,40
8 3/4 Class 'H' tail cm  Tail cmt 5 1/2 Segment "A" "B"  w/8.4#/	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf	side the Grade RY P RY P c CSg Test psig:	7 5/8 110 110 1,885	877  Coupling Semi-Premiur	Joint 3.46	Design Fa Collapse 2.71	2386 <u>ctors</u> Burst 2.86 2.86 Totals:	3M Length 8,570 13,820	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	0.56  Weigh 171,40 276,40
8 3/4 Class 'H' tail cm  Tail cmt 5 1/2 Segment "A" "B"  w/8.4#/	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf	side the Grade RY P RY P c CSg Test psig:	7 5/8 110 110 1,885	Coupling Semi-Premiur Semi-Flush	Joint 3.46 47.13	Design Fa Collapse 2.71 2.51	2386 <u>ctors</u> Burst 2.86 2.86 Totals:	Length 8,570 13,820 22,390	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	0.56  Weigh 171,40 276,40 447,80 overlap.
8 3/4 Class 'H' tail cm  Tail cmt 5 1/2 Segment "A" "B"  w/8.4#/	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo	side the Grade RY P RY P c Csg Test psig: olume(s) are	7 5/8 110 110 1,885 intended to a	Coupling Semi-Premiur Semi-Flush	Joint 3.46 47.13 8950	Design Fa Collapse 2.71 2.51 ft from su	2386  Cotors  Burst 2.86 2.86 Totals: urface or a	3M Length 8,570 13,820 22,390 -280	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	Weigh 171,40 276,40 447,80 overlap. Min Dis
8 3/4 Class 'H' tail cmt 5 1/2 Segment "A" "B" w/8.4#/	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo	side the Grade RY P RY P c Csg Test psig: blume(s) are 1 Stage	7 5/8 110 110 1,885 intended to a 1 Stage	Coupling Semi-Premiur Semi-Flush chieve a top of Min	Joint 3.46 47.13 8950 1 Stage	Design Fa Collapse 2.71 2.51 ft from su Drilling	2386  Cotors  Burst 2.86 2.86 Totals: Inface or a Calc	22,390 -280 Req'd	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	Weigh 171,40 276,40 447,80 overlap. Min Dis
8 3/4 Class 'H' tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835	side the Grade RY P RY P c Csg Test psig: blume(s) are 1 Stage Cmt Sx	7 5/8 110 110 1,885 intended to a 1 Stage CuFt Cmt	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft	Joint 3.46 47.13 8950 1 Stage % Excess	Design Far Collapse 2.71 2.51 ft from su Drilling Mud Wt	2386  Cotors  Burst 2.86 2.86 Totals: Inface or a Calc	22,390 -280 Req'd	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	Weigh 171,400 276,400 447,800 overlap. Min Dis Hole-Cpl
8 3/4 Class 'H' tail cm  Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835	side the Grade RY P RY P c Csg Test psig: blume(s) are 1 Stage Cmt Sx	7 5/8 110 110 1,885 intended to a 1 Stage CuFt Cmt	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft	Joint 3.46 47.13 8950 1 Stage % Excess	Design Far Collapse 2.71 2.51 ft from su Drilling Mud Wt	2386  Cotors  Burst 2.86 2.86 Totals: Inface or a Calc	22,390 -280 Req'd	3	<b>a-B</b> 5.30	<b>a-C</b> 5.02	Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cpl
Tail cmt 5 1/2 Segment "A" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835	side the Grade RY P RY P c Csg Test psig: blume(s) are 1 Stage Cmt Sx	7 5/8 110 110 1,885 intended to a 1 Stage CuFt Cmt	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft	Joint 3.46 47.13 8950 1 Stage % Excess	Design Far Collapse 2.71 2.51 ft from sur Drilling Mud Wt	2386  ctors  Burst 2.86 2.86 Totals: urface or a Calc MASP	22,390 -280 Req'd	3 3	<b>a-B</b> 5.30	<b>a-C</b> 5.02 4.65	Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cpi
Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm	0.1005 nt yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835	side the Grade RY P RY P c Csg Test psig: blume(s) are 1 Stage Cmt Sx	75/8  110 1,885 intended to a 1 Stage CuFt Cmt 1507	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft 1122	Joint 3.46 47.13 8950 1 Stage % Excess 34	Design Fa Collapse 2.71 2.51 ft from su Drilling Mud Wt 9.20	2386  ctors  Burst 2.86 2.86 Totals: urface or a Calc MASP	Length 8,570 13,820 22,390 -280 Req'd BOPE	3 3	<b>a-B</b> 5.30 <b>5.30 5.30</b>	<b>a-C</b> 5.02 4.65	0.56  Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23
Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4 class 'C' tail cm	0.1005 at yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835	side the Grade RY P c Csg Test psig: blume(s) are 1 Stage Cmt Sx 990	75/8  110 1,885 intended to a 1 Stage CuFt Cmt 1507	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft	Joint 3.46 47.13 8950 1 Stage % Excess	Design Fa Collapse 2.71 2.51 ft from su Drilling Mud Wt 9.20	2386  ctors  Burst 2.86 2.86 Totals: urface or a Calc MASP	22,390 -280 Req'd	3 3	<b>a-B</b> 5.30 <b>5.30 5.30</b>	<b>a-C</b> 5.02 4.65	0.56  Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23
Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm	0.1005 at yld > 1.20  casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835	side the Grade RY P c Csg Test psig: blume(s) are 1 Stage Cmt Sx 990	75/8  110 1,885 intended to a 1 Stage CuFt Cmt 1507	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft 1122 Coupling	Joint 3.46 47.13 8950 1 Stage % Excess 34	Design Fa Collapse 2.71 2.51 ft from su Drilling Mud Wt 9.20	2386  ctors  Burst 2.86 2.86 Totals: urface or a Calc MASP	Length 8,570 13,820 22,390 -280 Req'd BOPE	3 3	<b>a-B</b> 5.30 <b>5.30 Choose C</b>	<b>a-C</b> 5.02 4.65	0.56  Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23
Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm  #N/A 0 Segment "A" "B"	0.1005 Int yld > 1.20  Casing ins #/ft 20.00 20.00 //g mud, 30min Sf The cement vo Annular Volume 0.0835 Int yld > 1.35  #/ft  //g mud, 30min Sf	side the Grade RY P RY P c Csg Test psig: olume(s) are 1 Stage Cmt Sx 990  Grade	1239  7 5/8  110 110 1,885 intended to a 1 Stage CuFt Cmt 1507	Coupling Semi-Premiur Semi-Flush chieve a top of Min Cu Ft 1122  Coupling 0.00 0.00	Joint 3.46 47.13 8950 1 Stage % Excess 34 #N/A	Design Factorial Collapse 2.71 2.51  If from surprilling Mud Wt 9.20  Design Collapse	2386  ctors Burst 2.86 2.86 Totals: urface or a Calc MASP  Factors Burst  Totals:	Length 8,570 13,820 22,390 -280 Req'd BOPE  Length 0 0	3 3	<b>a-B</b> 5.30 <b>5.30 Choose C</b>	<b>a-C</b> 5.02 4.65	0.56  Weight 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23  Weight 0 0
Tail cmt 5 1/2  Segment "A" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm  #N/A  O  Segment "A" "B" w/8.4#/	Casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835 bt yld > 1.35  #/ft /g mud, 30min Sf Cmt vol cal	side the Grade RY P RY P c Csg Test psig: Dlume(s) are 1 Stage Cmt Sx 990  Grade	7 5/8  110 110 1,885 intended to a 1 Stage CuFt Cmt 1507  5 1/2	Coupling Semi-Premiur Semi-Flush Chieve a top of Min Cu Ft 1122  Coupling 0.00 0.00 TOC intended	Joint 3.46 47.13 8950 1 Stage % Excess 34 #N/A	Design Factorial Collapse 2.71 2.51  ft from su Drilling Mud Wt 9.20  Design Collapse	2386  ctors Burst 2.86 2.86 Totals: urface or a Calc MASP  Factors Burst  Totals: urface or a	Length 8,570 13,820 22,390 -280 Req'd BOPE  Length 0 0 #N/A	3 3	<b>a-B</b> 5.30 <b>5.30 Choose C</b>	<b>a-C</b> 5.02 4.65	Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23 Weigh 0 overlap.
8 3/4 Class 'H' tail cm  Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm  #N/A 0 Segment "A" "B" w/8.4#/ Hole	casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835 at yld > 1.35  #/ft /g mud, 30min Sf Cmt vol cal Annular	side the Grade RY P RY P c Csg Test psig: clume(s) are 1 Stage Cmt Sx 990  Grade  c Csg Test psig:	75/8  110 110 1,885 intended to a 1 Stage CuFt Cmt 1507  51/2  udes this csg. 1 Stage	Coupling Semi-Premiur Semi-Flush Chieve a top of Min Cu Ft 1122  Coupling 0.00 0.00 TOC intended Min	Joint 3.46 47.13 8950 1 Stage % Excess 34 #N/A	Design Factorial Collapse 2.71 2.51  ft from su Drilling Mud Wt 9.20  Design Collapse  ft from su Drilling	2386  ctors Burst 2.86 2.86 Totals: urface or a Calc MASP  Factors Burst  Totals: urface or a Calc	Length 8,570 13,820 22,390 -280 Req'd BOPE  Length 0 0 #N/A Req'd	3 3	<b>a-B</b> 5.30 <b>5.30 Choose C</b>	<b>a-C</b> 5.02 4.65	Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23  Weigh 0 overlap. Min Dis
Tail cmt 5 1/2 Segment "A" "B" w/8.4#/ Hole Size 6 3/4 Class 'C' tail cm  #N/A 0 Segment "A" "B" w/8.4#/	Casing ins #/ft 20.00 20.00 /g mud, 30min Sf The cement vo Annular Volume 0.0835 bt yld > 1.35  #/ft /g mud, 30min Sf Cmt vol cal	side the Grade RY P RY P c Csg Test psig: Dlume(s) are 1 Stage Cmt Sx 990  Grade	7 5/8  110 110 1,885 intended to a 1 Stage CuFt Cmt 1507  5 1/2	Coupling Semi-Premiur Semi-Flush Chieve a top of Min Cu Ft 1122  Coupling 0.00 0.00 TOC intended	Joint 3.46 47.13 8950 1 Stage % Excess 34 #N/A	Design Factorial Collapse 2.71 2.51  ft from su Drilling Mud Wt 9.20  Design Collapse	2386  ctors Burst 2.86 2.86 Totals: urface or a Calc MASP  Factors Burst  Totals: urface or a	Length 8,570 13,820 22,390 -280 Req'd BOPE  Length 0 0 #N/A	3 3	<b>a-B</b> 5.30 <b>5.30 Choose C</b>	<b>a-C</b> 5.02 4.65	Weigh 171,40 276,40 447,80 overlap. Min Dis Hole-Cp 0.23 Weigh 0 overlap.

Carlsbad Field Office 4/22/2022

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

Updated COAs per Sundry 2662750 approved through engineering on 04/22/2022. Includes approval for an updated casing plan, to use a bradenhead squeeze to get the second stage cement to surface, to utilize a spudder rig, offline cementing for the surface and intermediate casing, and additional COAs for break / shell testing the BOP.

OPERATOR'S NAME: XTO Permian Operating
WELL NAME & NO.: Brushy Draw 30 Federal 102H
LOCATION: Sec 30-25S-30E-NMP
COUNTY: Eddy County, New Mexico

COA

H2S	O Yes	• No	
Potash	None	Secretary	© R-111-P
Cave/Karst Potential	• Low	Medium	O High
Cave/Karst Potential	Critical		
Variance	O None	Flex Hose	Other
Wellhead	Conventional	• Multibowl	O Both
Other	☐4 String Area	☐ Capitan Reef	□WIPP
Other	☐ Fluid Filled		☐ Pilot Hole
Special Requirements	☐ Water Disposal	□ СОМ	□ Unit

# A. HYDROGEN SULFIDE

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

# **B. CASING**

- 1. The **9-5/8** inch surface casing shall be set at approximately 740 feet (a minimum of 70 feet (Eddy County) into the Rustler Anhydrite and above the salt) and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

- b. Wait on cement (WOC) time for a primary cement job will be a minimum of **8** hours or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the **7-5/8** inch intermediate casing is:

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:
  - Cement to surface. If cement does not circulate, contact the appropriate BLM office.

# Operator has proposed to pump down 9-5/8" X 7-5/8" annulus. <u>Operator must run</u> a CBL from TD of the 7-5/8" casing to surface. Submit results to BLM.

- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Casing does not meet 0.422" clearance requirement so cement should tie-back at least **300 feet** into previous casing string. Operator shall provide method of verification.

# C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).'
- 2. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **3000** (**3M**) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.

- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.

# GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
  - Eddy County
     Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
  - ✓ Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)689-5981
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
  - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
  - b. When the operator proposes to set surface casing with Spudder Rig
    - Notify the BLM when moving in and removing the Spudder Rig.
    - Notify the BLM when moving in the 2<sup>nd</sup> Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
    - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.
- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area

immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.

3. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

# A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the

- formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.

# B. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time, except the casing pressure test can be initiated immediately after bumping the plug (only applies to single stage cement jobs).
  - c. The tests shall be done by an independent service company utilizing a test plug not a cup or J-packer. The operator also has the option of utilizing an independent tester to test without a plug (i.e. against the casing) pursuant to Onshore Order 2 with the pressure not to exceed 70% of the burst rating for the casing. Any test against the casing must meet the WOC time for water basin (8 hours) or potash (24 hours) or 500 pounds compressive strength, whichever is greater, prior to initiating the test (see casing segment as lead cement may be critical item).
  - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
  - e. The results of the test shall be reported to the appropriate BLM office.
  - f. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
  - g. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to

the test at full stack pressure.

h. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

# C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

# D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

# Conditions of Approval Brushy Draw 30 Federal 102H

**BOP Break Testing Variance** (Note: Shell testing is not approved for any portion of the hole with a MASP of 5000 psi or greater)

- While in transfer between wells, the BOPE shall be secured by the hydraulic carrier or cradle.
- Any well control event while drilling require notification to the BLM Petroleum Engineer prior to the commencement of any BOP Break Testing operations.

A full BOP test is required prior to drilling the first deep intermediate hole section. If any subsequent hole interval is deeper than the first, a full BOP test will be required.

District I 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720

1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV

District III

1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

# State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Francis Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

☐ AMENDED REPORT

# WELL LOCATION AND ACREAGE DEDICATION PLAT

<sup>1</sup> API Number 30 - 0 15 - 451		<sup>3</sup> Pool Name Corral Canyon; Bone Spring, South	
<sup>4</sup> Property Code 322241		<sup>5</sup> Property Name Y DRAW 30 FEDERAL	<sup>6</sup> Well Number 102H
7 OGRID No.		8 Operator Name	9 Elevation
373075	XTO PER	3,091'	

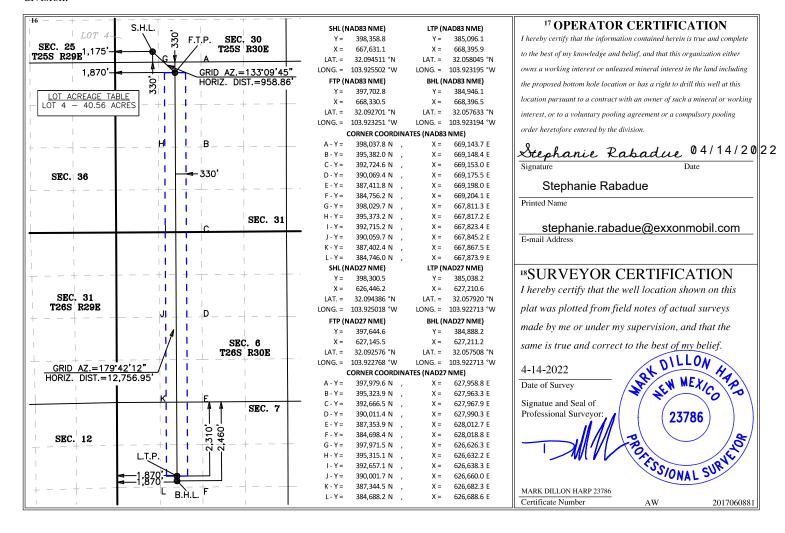
# <sup>10</sup> Surface Location

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
4	30	25 S	30 E		330	SOUTH	1,175	WEST	EDDY

# <sup>11</sup> Bottom Hole Location If Different From Surface

UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County
F	7	26 S	30 E		2,460	NORTH	1,870	WEST	EDDY
12 Dedicated Acres	13 Joint or	· Infill 14 C	onsolidation	Code 15 Or	der No.			-	
400									

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.



DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. Brushy Draw 30 Federal 102H Projected TD: 22390' MD / 9250' TVD Eddy County, NM

# 1. Geologic Name of Surface Formation

A. Quaternary

# 2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation	Well Depth (TVD)	Water/Oil/Gas
Rustler	640'	Water
Top of Salt	1040'	Water
Base of Salt	3260'	Water
Delaware	3470'	Water
Brushy Canyon	6260'	Water/Oil/Gas
Bone Spring	7287'	Water
1st Bone Spring Ss	8190'	Water/Oil/Gas
2nd Bone Spring Ss	8790'	Water/Oil/Gas
Target/Land Curve	9280'	Water/Oil/Gas

<sup>\*\*\*</sup> Hydrocarbons @ Brushy Canyon

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 9.625 inch casing @ 740' (300' above the salt) and circulating cement back to surface. The intermediate will isolate from the top of salt down to the next casing seat by setting 7.625 inch casing at 8670' and cemented to surface. A 6.75 inch curve and 6.75 inch lateral hole will be drilled to 22390 MD/TD and 5.5 inch production casing will be set at TD and cemented back up in the intermediate shoe (estimated TOC 8370 feet).

# 3. Casing Design

Hole Size	TVD	Measured Depth	OD Csg	Weight	Grade	Collar	New/Used	SF Burst	SF Collapse	SF Tension
12.25	740'	0' – 740'	9.625	40	J-55	втс	New	1.60	7.68	21.28
8.75	3982'	0' – 4000'	7.625	29.7	RY P-110	Flush Joint	New	4.40	2.65	2.17
8.75	8541'	4000' – 8670'	7.625	29.7	HC L-80	Flush Joint	New	3.20	2.31	2.93
6.75	8441'	0' – 8570'	5.5	20	RY P-110	Semi-Premium	New	1.05	2.86	2.27
6.75	9250'	8570' - 22390'	5.5	20	RY P-110	Semi-Flush	New	1.05	2.65	5.80

- · Production casing meets the clearance requiremenets as tapered string crosses over before encountering the intermediate shoe, per Onshore Order 2.3.B.1
- · XTO requests the option to utilize a spudder rig (Atlas Copco RD20 or Equivalent) to set and cement surface casing per this Sundry
- · XTO requests to not utilize centralizers in the curve and lateral
- 7.625 Collapse analyzed using 50% evacuation based on regional experience.
- 5.5 Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35
- · Test on Casing will be limited to 70% burst of the casing or 1500 psi, whichever is less
- $\cdot$  XTO requests the option to use 5" BTC Float equipment for the the production casing

# Wellhead:

Permanent Wellhead - Multibowl System

- A. Starting Head: 11" 10M top flange x 9-5/8" bottom
- B. Tubing Head: 11" 10M bottom flange x 7-1/16" 15M top flange
  - · Wellhead will be installed by manufacturer's representatives.
  - · Manufacturer will monitor welding process to ensure appropriate temperature of seal.
  - Operator will test the 7-5/8" casing per BLM Onshore Order 2
  - $\cdot \ \text{Wellhead Manufacturer representative will not be present for BOP test plug installation}$

<sup>\*\*\*</sup> Groundwater depth 40' (per NM State Engineers Office).

#### 4. Cement Program

#### Surface Casing: 9.625, 40 New BTC, J-55 casing to be set at +/- 740'

Lead: 140 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)
Tail: 130 sxs Class C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Top of Cement: Surface

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

#### 2nd Intermediate Casing: 7.625, 29.7 New casing to be set at +/- 8670'

1st Stage

Optional Lead: 340 sxs Class C (mixed at 10.5 ppg, 2.77 ft3/sx, 15.59 gal/sx water)

TOC: Surface

Tail: 220 sxs Class C (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

TOC: Brushy Canyon @ 6260

Compressives: 12-hr = 900 psi 24 hr = 1150 psi

## 2nd Stage

Lead: 0 sxs Class C (mixed at 12.9 ppg, 2.16 ft3/sx, 9.61 gal/sx water) Tail: 700 sxs Class C (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Top of Cement: 0

Compressives: 12-hr = 900 psi 24 hr = 1150 psi

XTO requests to pump a two stage cement job on the 7-5/8" intermediate casing string with the first stage being pumped conventionally with the calculated top of cement at the Brush Canyon (6260') and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface. If cement is not visually confirmed to circulate to surface, the final cement top after the second stage job will be verified by Echo-meter. If necessary, a top out consisting of 1,500 sack of Class C cement + 3% Salt + 1% PreMag-M + 6% Bentonite Gel (2.30 yld, 12.91 ppg) will be executed as a contingency. If cement is still unable to circulate to surface, another Echo-meter run will be performed for cement top verification.

XTO will include the Echo-meter verified fluid top and the volume of displacement fluid above the cement slurry in the annulus in all post-drill sundries on wells utilizing this cement program.

XTO will report to the BLM the volume of fluid (limited to 5 bbls) used to flush intermediate casing valves following backside cementing procedures.

XTO requests to pump an Optional Lead if well conditions dictate in an attempt to bring cement inside the first intermediate casing. If cement reaches the desired height, the BLM will be notified and the second stage bradenhead squeeze and subsequent TOC verification will be negated.

XTO requests the option to conduct the bradenhead squeeze and TOC verification offline as per standard approval from BLM when unplanned remediation is needed and batch drilling is approved. In the event the bradenhead is conducted, we will ensure the first stage cement job is cemented properly and the well is static with floats holding and no pressure on the csg annulus as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops.

#### Production Casing: 5.5, 20 New Semi-Flush, RY P-110 casing to be set at +/- 22390'

 Lead: 10 sxs NeoCem (mixed at 11.5 ppg, 2.69 ft3/sx, 15.00 gal/sx water) Top of Cement:
 8370 feet

 Tail: 980 sxs VersaCem (mixed at 13.2 ppg, 1.51 ft3/sx, 8.38 gal/sx water) Top of Cement:
 8736 feet

 Compressives:
 12-hr =
 800 psi
 24 hr = 1500 psi

XTO requests the option to offline cement and remediate (if needed) surface and intermediate casing strings where batch drilling is approved and if unplanned remediation is needed. XTO will ensure well is static with no pressure on the csg annulus, as with all other casing strings where batch drilling operations occur before moving off the rig. The TA cap will also be installed when applicable per Cactus procedure and pressure inside the casing will be monitored via the valve on the TA cap as per standard batch drilling ops. Offline cement operations will then be conducted after the rig is moved off the current well to the next well in the batch sequence.

## 5. Pressure Control Equipment

Once the permanent WH is installed on the 9.625 casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 3M Hydril and a 13-5/8" minimum 3M Double Ram BOP. MASP should not exceed 2150 psi. In any instance where 10M BOP is required by BLM, XTO requests a variance to utilize 5M annular with 10M ram preventers (a common BOP configuration, which allows use of 10M rams in unlikely event that pressures exceed 5M).

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nippling up on the 9.625, 3M bradenhead and flange, the BOP test will be limited to 3000 psi. When nippling up on the 7.625, the BOP will be tested to a minimum of 3000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 3M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

XTO requests a variance to be able to batch drill this well if necessary. In doing so, XTO will set casing and ensure that the well is cemented properly (unless approval is given for offline cementing) and the well is static. With floats holding, no pressure on the csg annulus, and the installation of a 10K TA cap as per Cactus recommendations, XTO will contact the BLM to skid the rig to drill the remaining wells on the pad. Once surface and both intermediate strings are all completed, XTO will begin drilling the production hole on each of the wells.

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken. Based on discussions with the BLM on February 27th 2020, we will request permission to **ONLY** retest broken pressure seals if the following conditions are met: 1. After a full BOP test is conducted on the first well on the pad 2. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.

## 6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW	Viscosity	Fluid Loss
INTERVAL	Tible Size	widd Type	(ppg)	(sec/qt)	(cc)
0' - 740'	12.25	FW/Native	8.7-9.2	35-40	NC
740' - 8670'	8.75	FW / Cut Brine / Direct Emulsion	9.7-10.2	30-32	NC
8670' - 22390'	6.75	ОВМ	8.7-9.2	50-60	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 9-5/8" surface casing with brine solution. A 9.7 ppg - 10.2 ppg cut brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

#### 7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 9.625 casing.

## 8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

## 9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 160 to 180 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 4185 psi.

## 10. Anticipated Starting Date and Duration of Operations

Anticipated spud date will be after BLM approval. Move in operations and drilling is expected to take 40 days.

9250.00 ft

TVB RKB:

Catographic New Mexico Reference

East - NAD 27

System:

Northing: 398301.28 ft

Easting: 626455.19 ft

3170.00 ft RKB:

Ground Level:

3140.00 ft

North Reference:

Grid

Convergence

Angle:

0.22 Deg

Site:

BD 30 Pad B

Slot:

0

**Brushy Draw** 30 Fed 102H

Plan Sections **Brushy Draw** 30 Fed 102H Measured Inclination Azin Depth (ft) (Deg)

0

0

0

	TVD			Build	Turn	Dogleg	
muth	RKB	Y Offset	X Offset	Rate	Rate	Rate	
(Deg)	(ft)	(ft)	(ft)	(Deg/100ft)	(Deg/100ft)	(Deg/100ft) Target	

0

0

0

0

0

0	0	2500	0	0	0	0	0
9.98	96.73	2996.24	-5.07	43.01	2	0	2
9.98	96.73	6503.76	-77.33	655.66	0	0	0
0	0	7000	-82.41	698.67	-2	0	2
0	0	8677	-82.41	698.67	0	0	0
90	179.7	9249.96	-655.36	701.67	10	0	10
90	179.7	9250	-13409.3	762.07	0	0	0 BHL 1
	9.98 9.98 0 0	9.98 96.73 9.98 96.73 0 0 0 0 90 179.7	9.98     96.73     2996.24       9.98     96.73     6503.76       0     0     7000       0     0     8677       90     179.7     9249.96	9.98     96.73     2996.24     -5.07       9.98     96.73     6503.76     -77.33       0     0     7000     -82.41       0     0     8677     -82.41       90     179.7     9249.96     -655.36	9.98     96.73     2996.24     -5.07     43.01       9.98     96.73     6503.76     -77.33     655.66       0     0     7000     -82.41     698.67       0     0     8677     -82.41     698.67       90     179.7     9249.96     -655.36     701.67	9.98       96.73       2996.24       -5.07       43.01       2         9.98       96.73       6503.76       -77.33       655.66       0         0       0       7000       -82.41       698.67       -2         0       0       8677       -82.41       698.67       0         90       179.7       9249.96       -655.36       701.67       10	9.98     96.73     2996.24     -5.07     43.01     2     0       9.98     96.73     6503.76     -77.33     655.66     0     0       0     0     7000     -82.41     698.67     -2     0       0     0     8677     -82.41     698.67     0     0       90     179.7     9249.96     -655.36     701.67     10     0

Position Brushy Draw 30 Fed 102H

easured			TVD	Highside		Lateral		Vertical	1	Magnitude	Semi-major	Semi-minor	Semi-minor Tool
Depth	Inclination	Azimuth	RKB	Error	Bias	Error	Bias	Error	Bias	of Bias	Error	Error	Azimuth Used
(ft)	(°)	(°)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(°)
0	0	0	0	0	0	0	0	2.297	0	0	0	0	OWSG 0 MWD+IFR1+ MS
100	0	0	100	0.358	0	0.358	0	2.299	0	0	0.358	0.358	OWSG 0 MWD+IFR1+ MS OWSG
200	0	0	200	0.717	0	0.717	0	2.307	0	0	0.717	0.717	0 MWD+IFR1+ MS OWSG
300	0	0	300	1.075	0	1.075	0	2.321	0	0	1.075	1.075	0 MWD+IFR1+ MS OWSG
400	0	0	400	1.434	0	1.434	0	2.34	0	0	1.434	1.434	0 MWD+IFR1+ MS OWSG
500	0	0	500	1.792	0	1.792	0	2.364	0	0	1.792	1.792	0 MWD+IFR1+ MS OWSG
600	0	0	600	2.151	0	2.151	0	2.393	0	0	2.151	2.151	0 MWD+IFR1+ MS OWSG
700	0	0	700	2.509	0	2.509	0	2.428	0	0	2.509	2.509	0 MWD+IFR1+ MS OWSG
800	0	0	800	2.868	0	2.868	0	2.467	0	0	2.868	2.868	0 MWD+IFR1+ MS OWSG
900	0	0	900	3.225	0	3.225	0	2.511	0	0	3.225	3.225	0 MWD+IFR1+S MS

Received by OCD: 6/27/2025 11:15:56 AM

														OWSG
Re	1000	0	0	1000	3.585	0	3.585	0	2.559	0	0	3.585	3.585	0 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM														MS
sed	1100	0	0	1100	3.942	0	3.942	0	2.613	0	0	3.942	3.942	OWSG 0 MWD+IFR1+
0	1100	0	0	1100	3.942	0	3.342	U	2.015	U	0	5.942	3.342	MS MS
Im														owsg 🖁
ıgi	1200	0	0	1200	4.301	0	4.301	0	2.67	0	0	4.301	4.301	0 MWD+IFR1+
30:														MS 👔
10/	1200	•		4200	4.650	•	4.650	•	2 724	•	•	4.650	4.650	OWSG
23/	1300	0	0	1300	4.659	0	4.659	0	2.731	0	0	4.659	4.659	0 MWD+IFR1+ MS
202														OWSG
5 1	1400	0	0	1400	5.018	0	5.018	0	2.797	0	0	5.018	5.018	0 MWD+IFR1+
1:2														MS 🐇
4:0										•				OWSG
1 A	1500	0	0	1500	5.377	0	5.377	0	2.866	0	0	5.377	5.377	0 MWD+IFR1+ MS
X														OWSG
	1600	0	0	1600	5.735	0	5.735	0	2.939	0	0	5.735	5.735	0 MWD+IFR1+
														MS
						_				_				OWSG
	1700	0	0	1700	6.093	0	6.093	0	3.015	0	0	6.093	6.093	0 MWD+IFR1+ MS
														OWSG
	1800	0	0	1800	6.452	0	6.452	0	3.095	0	0	6.452	6.452	0 MWD+IFR1+
														MS
										•				OWSG
	1900	0	0	1900	6.81	0	6.81	0	3.178	0	0	6.81	6.81	0 MWD+IFR1+ MS
														OWSG
	2000	0	0	2000	7.169	0	7.169	0	3.265	0	0	7.169	7.169	0 MWD+IFR1+
														MS
	2400	•	•	2400	7.507		7.507	•	2 25 4	•	•	7.527	7.507	OWSG
	2100	0	0	2100	7.527	0	7.527	0	3.354	0	0	7.527	7.527	0 MWD+IFR1+ MS
														OWSG
	2200	0	0	2200	7.886	0	7.886	0	3.447	0	0	7.886	7.886	0 MWD+IFR1+
														MS
	2200	0	0	2200	0.244	0	0.244	0	2 5 4 4	0	0	0.244	0.244	OWSG
	2300	0	0	2300	8.244	0	8.244	0	3.544	0	0	8.244	8.244	0 MWD+IFR1+ MS
														OWSG
	2400	0	0	2400	8.603	0	8.603	0	3.643	0	0	8.603	8.603	0 MWD+IFR1+
														MS
	3500	0	0	2500	0.063	0	0.002	0	2 744	0	0	0.003	0.002	OWSG
	2500	0	0	2500	8.962	0	8.962	0	3.744	0	0	8.962	8.962	0 MWD+IFR1+ MS
														OWSG
	2600 1	1.999	96.72	2599.98	9.305	0	9.31	0	3.848	0	0	9.31	9.31	0 MWD+IFR1+
														MS 🕺
•														6

	2700	4	06.72	2500 020	0.620	0	0.640	0	2.052	0	0	0.640	0.640	OWSG
Released to Imaging: 10/23/2025 11:24:01 AM	2700	4	96.72	2699.838	9.629	0	9.648	0	3.953	0	0	9.649	9.648	3.803 MWD+IFR1+
ased	2800	6	96.72	2799.452	9.943	0	9.986	0	4.061	0	0	9.989	9.986	OWSG 5.307 MWD+IFR1+
to I	2800	О	90.72	2799.452	9.943	U	9.980	U	4.001	U	U	9.989	9.980	MS
mag			0.5 = 0									40.00	40.00-	OWSG 🖁
ging	2900	7.999	96.72	2898.702	10.248	0	10.325	0	4.169	0	0	10.33	10.325	4.579 MWD+IFR1+. MS
: 10														owsg
/23/	2998.7	9.975	96.72	2996.24	10.537	0	10.658	0	4.277	0	0	10.663	10.658	6.699 MWD+IFR1+ MS
202														OWSG
5 11	3000	9.975	96.72	2997.465	10.54	0	10.663	0	4.276	0	0	10.668	10.663	8.606 MWD+IFR1+
.24														MS OWSG
10:	3100	9.975	96.72	3095.954	10.887	0	11.004	0	4.394	0	0	11.009	11.004	7.4 MWD+IFR1+
AM														MS OWSG
	3200	9.975	96.72	3194.442	11.232	0	11.349	0	4.518	0	0	11.35	11.348	45 MWD+IFR1+
														MS
	3300	9.975	96.72	3292.93	11.58	0	11.692	0	4.643	0	0	11.692	11.691	OWSG 45 MWD+IFR1+
	3300	3.373	30.72	3232.33	11.50	Ü	11.032	ŭ	1.0 15	· ·	Ü	11.032	11.031	MS
	2400	0.075	06.73	2201 410	11 026	0	12.027	0	4.773	0	0	12.038	12.022	OWSG 80.212 MWD+IFR1+
	3400	9.975	96.72	3391.419	11.926	0	12.037	0	4.773	0	0	12.038	12.033	MS
														OWSG
	3500	9.975	96.72	3489.907	12.279	0	12.385	0	4.905	0	0	12.386	12.381	77.583 MWD+IFR1+ MS
														OWSG
	3600	9.975	96.72	3588.395	12.631	0	12.735	0	5.04	0	0	12.736	12.728	81.54 MWD+IFR1+
														MS OWSG
	3700	9.975	96.72	3686.884	12.985	0	13.088	0	5.178	0	0	13.088	13.077	82.6 MWD+IFR1+
														MS OWSG
	3800	9.975	96.72	3785.372	13.341	0	13.438	0	5.32	0	0	13.439	13.427	80.649 MWD+IFR1+
														MS
	3900	9.975	96.72	3883.86	13.699	0	13.791	0	5.464	0	0	13.792	13.78	OWSG 78.466 MWD+IFR1+
														MS
	4000	9.975	96.72	3982.349	14.059	0	14.145	0	5.611	0	0	14.146	14.134	OWSG 76.125 MWD+IFR1+
	4000	9.973	90.72	3362.343	14.039	U	14.143	O	5.011	O	U	14.140	14.134	MS
			00 =0					_						OWSG
	4100	9.975	96.72	4080.837	14.417	0	14.497	0	5.76	0	0	14.499	14.487	73.699 MWD+IFR1+ MS
														owsg 🦹
	4200	9.975	96.72	4179.325	14.777	0	14.855	0	5.913	0	0	14.857	14.841	75.061 MWD+IFR1+
														MS

														OWSG
Released to Imaging: 10/23/2025 11:24:01 AM	4300	9.975	96.72	4277.813	15.138	0	15.211	0	6.068	0	0	15.213	15.197	72.912 MWD+IFR1+ MS
ase														owsg 🧍
d to	4400	9.975	96.72	4376.302	15.501	0	15.568	0	6.226	0	0	15.571	15.555	70.775 MWD+IFR1+
Im														MS OWSG
agi	4500	9.975	96.72	4474.79	15.862	0	15.923	0	6.386	0	0	15.927	15.91	68.716 MWD+IFR1+
ng.														MS
10														owsg
/23	4600	9.975	96.72	4573.278	16.228	0	16.283	0	6.55	0	0	16.288	16.27	66.761 MWD+IFR1+
/20														MS
25	4700	9.975	96.72	4671.767	16.591	0	16.641	0	6.716	0	0	16.647	16.628	OWSG 64.926 MWD+IFR1+
11:	4700	3.373	30.72	40/1./0/	10.591	U	10.041	O	0.710	O	U	10.047	10.026	MS MS
24:														OWSG T
01	4800	9.975	96.72	4770.255	16.956	0	17.001	0	6.884	0	0	17.007	16.987	63.239 MWD+IFR1+
$A\lambda$														MS
1														OWSG
	4900	9.975	96.72	4868.743	17.32	0	17.359	0	7.055	0	0	17.366	17.345	61.692 MWD+IFR1+
														MS OWSG
	5000	9.975	96.72	4967.232	17.687	0	17.72	0	7.229	0	0	17.728	17.706	60.284 MWD+IFR1+
	3000	3.373	30.72	4307.232	17.007	O	17.72	O	7.225	O .	U	17.720	17.700	MS
														OWSG
	5100	9.975	96.72	5065.72	18.052	0	18.081	0	7.406	0	0	18.089	18.066	59.017 MWD+IFR1+
														MS
														OWSG
	5200	9.975	96.72	5164.208	18.422	0	18.442	0	7.585	0	0	18.452	18.428	54.941 MWD+IFR1+
														MS OWSG
	5300	9.975	96.72	5262.697	18.789	0	18.804	0	7.767	0	0	18.816	18.79	54.104 MWD+IFR1+
	3300	3.373	50.72	3232.037	2017-00	· ·	20.00	· ·	,,,,	· ·		10.010	20.75	MS
														OWSG
	5400	9.975	96.72	5361.185	19.155	0	19.167	0	7.951	0	0	19.179	19.151	55.917 MWD+IFR1+
														MS
	5500	0.075	06.72	E4E0 672	10 525	0	10 520	0	0.120	0	0	10 542	10 514	OWSG
	5500	9.975	96.72	5459.673	19.525	0	19.529	0	8.138	0	0	19.543	19.514	52.7 MWD+IFR1+ MS
														OWSG
	5600	9.975	96.72	5558.161	19.892	0	19.891	0	8.327	0	0	19.906	19.876	52.109 MWD+IFR1+
														MS
														OWSG
	5700	9.975	96.72	5656.65	20.263	0	20.255	0	8.519	0	0	20.272	20.24	49.429 MWD+IFR1+
														MS
	5800	9.975	96.72	5755.138	20.633	0	20.616	0	8.714	0	0	20.636	20.602	OWSG 47.062 MWD+IFR1+
	3000	3.373	30.72	3733.138	20.033	U	20.010	O	0.714	O	U	20.030	20.002	MS MS
														owsg 1
	5900	9.975	96.72	5853.626	21.003	0	20.982	0	8.911	0	0	21.002	20.967	46.914 MWD+IFR1+
														MS 🚶
•														6

														OWSG
R	6000	9.975	96.72	5952.115	21.372	0	21.345	0	9.111	0	0	21.367	21.329	46.782 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM														MS 🚦
ase														owsg
<i>1 b</i>	6100	9.975	96.72	6050.603	21.743	0	21.709	0	9.313	0	0	21.734	21.694	45 MWD+IFR1+₺
0 ]														MS 🕺
ma														owsg 🖁
gi.	6200	9.975	96.72	6149.091	22.113	0	22.075	0	9.518	0	0	22.1	22.059	45 MWD+IFR1+
So														MS 🐧
10														OWSG
23	6300	9.975	96.72	6247.58	22.484	0	22.438	0	9.726	0	0	22.466	22.422	43.545 MWD+IFR1+
2														MS
925														OWSG
	6400	9.975	96.72	6346.068	22.855	0	22.803	0	9.936	0	0	22.833	22.787	42.275 MWD+IFR1+
1:2														MS 🗼
4:0														OWSG
1	6500	9.975	96.72	6444.556	23.227	0	23.168	0	10.149	0	0	23.201	23.152	41.169 MWD+IFR1+
È														MS
	CE CO 4	0.075	06.70	6500 76	22.454		22 200	•	40.076	•	•	22.422	22 272	OWSG
(	6560.1	9.975	96.72	6503.76	23.451	0	23.389	0	10.276	0	0	23.423	23.373	41.303 MWD+IFR1+
														MS
	6600	0.177	06.72	6542.001	22.616	0	22 524	0	10.262	0	0	22 560	22 517	OWSG
	6600	9.177	96.72	6543.091	23.616	0	23.534	0	10.363	0	0	23.568	23.517	41.384 MWD+IFR1+
														MS OWSG
	6700	7.177	96.72	6642.07	24.012	0	23.896	0	10.583	0	0	23.932	23.88	40.43 MWD+IFR1+
	0700	7.177	30.72	0042.07	24.012	O	23.030	U	10.363	U	U	23.932	23.86	MS
														OWSG
	6800	5.177	96.72	6741.484	24.379	0	24.257	0	10.798	0	0	24.294	24.24	40.61 MWD+IFR1+
	0000	3.177	30.72	0, 11, 10 1	21.373	Ü	2 11.237	Ü	10.750	Ü	Ū	2 1.23 1	22.	MS
														OWSG
	6900	3.177	96.72	6841.213	24.718	0	24.615	0	11.018	0	0	24.653	24.598	40.746 MWD+IFR1+
														MS
														OWSG
	7000	1.177	96.72	6941.136	25.026	0	24.968	0	11.238	0	0	25.006	24.95	40.835 MWD+IFR1+
														MS
														OWSG
	7058.8	0	0	7000	25.179	0	25.185	0	11.367	0	0	25.21	25.155	41.871 MWD+IFR1+
														MS
														OWSG
	7100	0	0	7041.132	25.32	0	25.326	0	11.454	0	0	25.35	25.296	41.86 MWD+IFR1+
														MS
														OWSG
	7200	0	0	7141.132	25.663	0	25.667	0	11.675	0	0	25.692	25.639	42.882 MWD+IFR1+
														MS
														OWSG
	7300	0	0	7241.132	26.008	0	26.01	0	11.9	0	0	26.034	25.983	43.929 MWD+IFR1+
														MS
	7466	•	_	7044 100	26.674	_	26.674	•	40.40	•	•	26.2==	26.222	OWSG
	7400	0	0	7341.132	26.351	0	26.351	0	12.124	0	0	26.377	26.326	45 MWD+IFR1+
														MS
-														

														OWSG
R	7500	0	0	7441.132	26.696	0	26.695	0	12.353	0	0	26.72	26.671	46.091 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM														MS 🚦
ise														OWSG 📑
d to	7600	0	0	7541.132	27.041	0	27.039	0	12.586	0	0	27.064	27.016	46.102 MWD+IFR1+
In														MS
nag								_			_		0= 004	OWSG
in	7700	0	0	7641.132	27.386	0	27.382	0	12.822	0	0	27.408	27.361	47.221 MWD+IFR1+
99:														MS OWSG
0/2	7800	0	0	7741.132	27.733	0	27.727	0	13.061	0	0	27.753	27.707	48.358 MWD+IFR1+
23/	7000	O	O	7741.132	27.733	O	27.727	O	13.001	· ·	U	27.733	27.707	MS MS
202														OWSG 1
5 1	7900	0	0	7841.132	28.078	0	28.071	0	13.3	0	0	28.098	28.052	49.506 MWD+IFR1+
1:														MS
24:														owsg 🦹
01	8000	0	0	7941.132	28.425	0	28.417	0	13.546	0	0	28.443	28.399	50.659 MWD+IFR1+‡
A														MS
														OWSG
	8100	0	0	8041.132	28.772	0	28.761	0	13.791	0	0	28.788	28.744	51.821 MWD+IFR1+
														MS
	8200	0	0	8141.132	29.119	0	29.107	0	14.043	0	0	29.135	29.091	OWSG 52.985 MWD+IFR1+
	8200	U	U	0141.132	29.119	U	29.107	U	14.045	U	U	29.155	29.091	MS
														OWSG
	8300	0	0	8241.132	29.465	0	29.453	0	14.297	0	0	29.481	29.438	53.06 MWD+IFR1+
														MS
														OWSG
	8400	0	0	8341.132	29.813	0	29.799	0	14.553	0	0	29.827	29.785	54.232 MWD+IFR1+
														MS
														OWSG
	8500	0	0	8441.132	30.16	0	30.146	0	14.812	0	0	30.174	30.132	54.326 MWD+IFR1+
														MS
	8600	0	0	8541.132	30.507	0	30.493	0	15.073	0	0	30.521	30.479	OWSG 55.494 MWD+IFR1+
	8000	U	U	0341.132	30.307	U	30.493	U	15.075	U	U	30.321	30.479	33.494 MVD+IFK1+ MS
														OWSG
	8700	0	0	8641.132	30.856	0	30.84	0	15.339	0	0	30.868	30.828	56.659 MWD+IFR1+
														MS
														OWSG
	8735.8	0	0	8677	30.981	0	30.964	0	15.434	0	0	30.993	30.952	56.704 MWD+IFR1+
														MS
														OWSG
	8800	6.413	179.7	8740.998	31.074	0	31.182	0	15.604	0	0	31.212	31.169	57.169 MWD+IFR1+
														MS
	8900	16.41	179.7	0020 006	30.631	0	31.508	0	15.865	0	0	31.545	31.492	OWSG
	8900	10.41	1/9./	8838.896	30.031	U	31.306	U	13.603	U	0	31.343	31.492	55.519 MWD+IFR1++ MS
														OWSG
	9000	26.41	179.7	8931.875	29.504	0	31.812	0	16.109	0	0	31.854	31.786	51.629 MWD+IFR1+
		·· <b>-</b>				•		· ·		•	-			MS T
•														6

														OWSG
Re	9100	36.41	179.7	9017.11	27.778	0	32.109	0	16.334	0	0	32.145	32.058	39.824 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM														MS
sed	9200	46.41	179.7	9092.011	25.589	0	32.388	0	16.538	0	0	32.416	32.299	OWSG 29.009 MWD+IFR1+
to	9200	40.41	1/9./	9092.011	25.589	U	32.388	U	10.538	U	U	32.416	32.299	29.009 MWD+IFK1+ MS
Im														OWSG
agi	9300	56.41	179.7	9154.302	23.118	0	32.634	0	16.727	0	0	32.651	32.479	18.16 MWD+IFR1+
8:														MS
10														OWSG
/23	9400	66.41	179.7	9202.09	20.663	0	32.848	0	16.912	0	0	32.856	32.611	10.443 MWD+IFR1+
/20														MS
25	9500	76.41	179.7	9233.924	18.623	0	33.015	0	17.097	0	0	33.017	32.693	OWSG 4.667 MWD+IFR1+
11:	9300	70.41	1/9./	9233.924	10.025	U	35.013	U	17.097	U	U	33.017	32.093	MS
24														OWSG
01	9600	86.41	179.7	9248.835	17.474	0	33.136	0	17.289	0	0	33.136	32.726	-0.343 MWD+IFR1+
A														MS
														OWSG
!	9635.8	90	179.7	9249.958	17.361	0	33.181	0	17.361	0	0	33.182	32.741	-2.014 MWD+IFR1+
														MS OWSG
	9700	90	179.7	9249.958	17.496	0	33.242	0	17.496	0	0	33.245	32.738	-4.554 MWD+IFR1+
	3700	50	175.7	3243.330	17.430	O	33.242	Ü	17.430	O	Ü	33.243	32.730	MS
														OWSG
	9800	90	179.7	9249.958	17.734	0	33.347	0	17.734	0	0	33.357	32.746	-7.438 MWD+IFR1+
														MS
					40.000									OWSG
	9900	90	179.7	9249.958	18.003	0	33.468	0	18.003	0	0	33.485	32.738	-9.093 MWD+IFR1+
														MS OWSG
	10000	90	179.7	9249.958	18.303	0	33.602	0	18.303	0	0	33.628	32.744	-10.23 MWD+IFR1+
														MS
														OWSG
	10100	90	179.7	9249.958	18.631	0	33.751	0	18.631	0	0	33.786	32.75	-10.908 MWD+IFR1+
														MS
	10200	90	179.7	9249.958	18.984	0	33.914	0	18.984	0	0	33.957	32.756	OWSG -11.273 MWD+IFR1+
	10200	90	1/3./	3243.336	10.504	U	33.314	O	10.304	U	U	33.337	32.730	MS
														OWSG
	10300	90	179.7	9249.958	19.362	0	34.076	0	19.362	0	0	34.127	32.762	-11.553 MWD+IFR1+
														MS
														OWSG
	10400	90	179.7	9249.958	19.766	0	34.267	0	19.766	0	0	34.325	32.769	-11.553 MWD+IFR1+
														MS OWSG
	10500	90	179.7	9249.958	20.192	0	34.456	0	20.192	0	0	34.521	32.776	-11.553 MWD+IFR1+
	10300	50	1,5.7	J2+J.JJ0	20.132	O	J-1 <b>1</b> .50	Ü	20.132	J	5	J-1.J21	32.770	MS MS
														owsg 1
	10600	90	179.7	9249.958	20.64	0	34.674	0	20.64	0	0	34.744	32.785	-11.387 MWD+IFR1+
														MS 🖠
•														0

														OWSG
R	10700	90	179.7	9249.958	21.105	0	34.89	0	21.105	0	0	34.966	32.793	-11.258 MWD+IFR1+
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1se														OWSG 📑
d to	10800	90	179.7	9249.958	21.592	0	35.119	0	21.592	0	0	35.2	32.817	-11.153 MWD+IFR1+
In														MS
gan						_					_			OWSG
, in	10900	90	179.7	9249.958	22.093	0	35.36	0	22.093	0	0	35.446	32.826	-10.945 MWD+IFR1+
00														MS
9	11000	90	179.7	9249.958	22.612	0	35.614	0	22.612	0	0	35.704	32.836	OWSG -10.722 MWD+IFR1+
23/	11000	90	1/5./	3243.336	22.012	U	33.014	U	22.012	U	U	33.704	32.830	MS MS
202														OWSG
5	11100	90	179.7	9249.958	23.145	0	35.88	0	23.145	0	0	35.975	32.861	-10.536 MWD+IFR1+
$\Xi$														MS
24:														owsg 🚶
01	11200	90	179.7	9249.958	23.692	0	36.144	0	23.692	0	0	36.242	32.871	-10.334 MWD+IFR1+🔭
A														MS
														OWSG
	11300	90	179.7	9249.958	24.253	0	36.434	0	24.253	0	0	36.535	32.897	-10.128 MWD+IFR1+
														MS
	11400	90	179.7	9249.958	24.825	0	36.722	0	24.825	0	0	36.826	32.922	OWSG -9.949 MWD+IFR1+
	11400	90	1/9./	9249.936	24.025	U	30.722	U	24.025	U	U	30.020	32.922	-9.949 WWD+IFK1+ MS
														OWSG
	11500	90	179.7	9249.958	25.409	0	37.034	0	25.409	0	0	37.14	32.949	-9.731 MWD+IFR1+
														MS
														OWSG
	11600	90	179.7	9249.958	26.004	0	37.343	0	26.004	0	0	37.452	32.96	-9.513 MWD+IFR1+
														MS
							07.664							OWSG
	11700	90	179.7	9249.958	26.608	0	37.664	0	26.608	0	0	37.774	32.986	-9.325 MWD+IFR1+
														MS OWSG
	11800	90	179.7	9249.958	27.221	0	37.995	0	27.221	0	0	38.107	33.013	-9.136 MWD+IFR1+
			_,,,,,	32 131333		Ū	07.000	· ·		· ·	· ·	00.107	33.023	MS
														OWSG
	11900	90	179.7	9249.958	27.842	0	38.336	0	27.842	0	0	38.449	33.04	-8.949 MWD+IFR1+
														MS
														OWSG
	12000	90	179.7	9249.958	28.473	0	38.686	0	28.473	0	0	38.802	33.067	-8.762 MWD+IFR1+
														MS
	12100	00	170.7	0240.050	20.11	0	20.024	0	20.11	0	0	20.454	22.004	OWSG
	12100	90	179.7	9249.958	29.11	0	39.034	0	29.11	0	0	39.151	33.094	-8.598 MWD+IFR1+
														MS OWSG
	12200	90	179.7	9249.958	29.756	0	39.404	0	29.756	0	0	39.522	33.136	-8.435 MWD+IFR1+
										-				MS 8
														owsg 🚺
	12300	90	179.7	9249.958	30.407	0	39.771	0	30.407	0	0	39.889	33.164	-8.273 MWD+IFR1+
														MS
•														6

														OWSG
R	12400	90	179.7	9249.958	31.064	0	40.159	0	31.064	0	0	40.278	33.191	-8.098 MWD+IFR1+
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use														OWSG 📑
d to	12500	90	179.7	9249.958	31.718	0	40.543	0	31.718	0	0	40.663	33.219	-7.942 MWD+IFR1+
Ĭ														MS
gan	13600	00	170.7	0240.050	22.200	0	40.027	0	22.200	0	0	44.057	22.264	OWSG
ing	12600	90	179.7	9249.958	32.388	0	40.937	0	32.388	0	0	41.057	33.261	-7.802 MWD+IFR1+ MS
														OWSG
9/2	12700	90	179.7	9249.958	33.061	0	41.338	0	33.061	0	0	41.459	33.289	-7.651 MWD+IFR1+
3/2														MS
02														owsg
5 1	12800	90	179.7	9249.958	33.749	0	41.748	0	33.749	0	0	41.869	33.332	-7.516 MWD+IFR1+
1:2														MS 💃
4:0														OWSG
1 1	12900	90	179.7	9249.958	34.424	0	42.153	0	34.424	0	0	42.275	33.374	-7.393 MWD+IFR1+
3														MS OWSG
	13000	90	179.7	9249.958	35.114	0	42.578	0	35.114	0	0	42.7	33.403	-7.251 MWD+IFR1+
	13000	30	173.7	3243.330	55.114	O	42.570	O	33.114	O	O	72.7	33.403	MS
														OWSG
	13100	90	179.7	9249.958	35.805	0	43.011	0	35.805	0	0	43.132	33.445	-7.123 MWD+IFR1+
														MS
														OWSG
	13200	90	179.7	9249.958	36.497	0	43.439	0	36.497	0	0	43.561	33.488	-7.006 MWD+IFR1+
														MS
	12200	00	170.7	0240.059	27 202	0	42.075	0	37.202	0	0	42.006	22 521	OWSG
	13300	90	179.7	9249.958	37.202	0	43.875	0	37.202	0	0	43.996	33.531	-6.891 MWD+IFR1+ MS
														OWSG
	13400	90	179.7	9249.958	37.895	0	44.329	0	37.895	0	0	44.45	33.574	-6.77 MWD+IFR1+
														MS
														OWSG
	13500	90	179.7	9249.958	38.601	0	44.778	0	38.601	0	0	44.899	33.617	-6.657 MWD+IFR1+
														MS
	13600	00	170.7	0240.050	20.240	0	45.224	0	20.240	0	0	45.254	22.66	OWSG
	13600	90	179.7	9249.958	39.319	0	45.234	0	39.319	0	0	45.354	33.66	-6.549 MWD+IFR1+ MS
														OWSG
	13700	90	179.7	9249.958	40.025	0	45.696	0	40.025	0	0	45.816	33.703	-6.442 MWD+IFR1+
														MS
														OWSG
	13800	90	179.7	9249.958	40.743	0	46.153	0	40.743	0	0	46.274	33.745	-6.344 MWD+IFR1+
														MS
										•				OWSG
	13900	90	179.7	9249.958	41.461	0	46.628	0	41.461	0	0	46.748	33.803	-6.248 MWD+IFR1+
														MS OWSG
	14000	90	179.7	9249.958	42.178	0	47.108	0	42.178	0	0	47.228	33.846	-6.147 MWD+IFR1+
	2.000		_, ,,,	32.3.330		-	255	J		•	•		33.010	MS MS
•														6

														OWSG
Re	14100	90	179.7	9249.958	42.895	0	47.584	0	42.895	0	0	47.703	33.904	-6.059 MWD+IFR1+
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ed 1	14200	90	179.7	9249.958	43.623	0	48.065	0	43.623	0	0	48.184	33.946	-5.972 MWD+IFR1+
o I														MS 🏌
mag	11200	00	470.7	0240.050	44.054	•	40.560	•	44.054	•	•	40.60	24.004	OWSG
ging	14300	90	179.7	9249.958	44.351	0	48.562	0	44.351	0	0	48.68	34.004	-5.882 MWD+IFR1+ MS
: 10														owsg 🖁
9/23	14400	90	179.7	9249.958	45.078	0	49.054	0	45.078	0	0	49.171	34.047	-5.793 MWD+IFR1+
1/20														MS
25	14500	90	179.7	9249.958	45.804	0	49.551	0	45.804	0	0	49.668	34.104	OWSG -5.715 MWD+IFR1+
11:	14300	30	173.7	3243.330	45.004	O	45.551	O .	45.004	O	U	43.000	34.104	MS MS
24:(														owsg 🚶
7 10	14600	90	179.7	9249.958	46.53	0	50.053	0	46.53	0	0	50.17	34.161	-5.634 MWD+IFR1+
3														MS OWSG
	14700	90	179.7	9249.958	47.265	0	50.561	0	47.265	0	0	50.676	34.204	-5.555 MWD+IFR1+
														MS
						•				_				OWSG
	14800	90	179.7	9249.958	48	0	51.063	0	48	0	0	51.178	34.261	-5.48 MWD+IFR1+ MS
														OWSG
	14900	90	179.7	9249.958	48.734	0	51.579	0	48.734	0	0	51.694	34.318	-5.407 MWD+IFR1+
														MS
	15000	90	179.7	9249.958	49.477	0	52.091	0	49.477	0	0	52.205	34.375	OWSG -5.335 MWD+IFR1+
	13000	30	175.7	3243.330	43.477	Ü	32.031	· ·	73.77	· ·	Ū	32.203	34.373	MS
														OWSG
	15100	90	179.7	9249.958	50.21	0	52.616	0	50.21	0	0	52.73	34.432	-5.264 MWD+IFR1+
														MS OWSG
	15200	90	179.7	9249.958	50.951	0	53.137	0	50.951	0	0	53.249	34.489	-5.198 MWD+IFR1+
														MS
						•				_			24.50	OWSG
	15300	90	179.7	9249.958	51.691	0	53.661	0	51.691	0	0	53.773	34.56	-5.132 MWD+IFR1+ MS
														OWSG
	15400	90	179.7	9249.958	52.44	0	54.19	0	52.44	0	0	54.302	34.617	-5.068 MWD+IFR1+
														MS
	15500	90	179.7	9249.958	53.179	0	54.723	0	53.179	0	0	54.834	34.674	OWSG -5.004 MWD+IFR1+
	13300	90	1/9./	9249.936	33.179	U	34.723	O	33.179	O	U	34.034	34.074	MS
														OWSG
	15600	90	179.7	9249.958	53.926	0	55.26	0	53.926	0	0	55.37	34.745	-4.945 MWD+IFR1+
														MS OWSG
	15700	90	179.7	9249.958	54.672	0	55.791	0	54.672	0	0	55.901	34.801	-4.886 MWD+IFR1+
					<u>-</u>	ŭ		ŭ	<b></b>	•	•			MC
•														IVIS

														OWSG
Released to Imaging: 10/23/2025 11:24:01 AM	15800	90	179.7	9249.958	55.426	0	56.335	0	55.426	0	0	56.444	34.872	-4.828 MWD+IFR1+ MS
ase														owsg
d to	15900	90	179.7	9249.958	56.169	0	56.874	0	56.169	0	0	56.983	34.928	-4.771 MWD+IFR1+ MS
Ima														OWSG -4.714 MWD+IFR1+
lgin	16000	90	179.7	9249.958	56.921	0	57.426	0	56.921	0	0	57.533	34.999	
8: 1														MS OWSG
0/2	16100	90	179.7	9249.958	57.671	0	57.972	0	57.671	0	0	58.079	35.069	-4.661 MWD+IFR1+
3/20														MS
25 i	16200	90	179.7	9249.958	58.421	0	58.522	0	58.421	0	0	58.628	35.125	OWSG -4.607 MWD+IFR1+
11:2														MS 🖟
4:0	16300	90	179.7	9249.958	59.178	0	59.075	0	59.178	0	0	59.18	35.195	OWSG -4.555 MWD+IFR1+
A	10300	90	1/9./	3243.336	33.178	U	39.073	U	33.178	U	U	33.16	33.133	MS
_														OWSG
	16400	90	179.7	9249.958	59.925	0	59.631	0	59.925	0	0	59.736	35.266	-4.504 MWD+IFR1+ MS
														OWSG
	16500	90	179.7	9249.958	60.679	0	60.19	0	60.679	0	0	60.294	35.336	-4.454 MWD+IFR1+
														MS OWSG
	16600	90	179.7	9249.958	61.433	0	60.745	0	61.433	0	0	60.848	35.405	-4.409 MWD+IFR1+
														MS OWSG
	16700	90	179.7	9249.958	62.193	0	61.31	0	62.193	0	0	61.413	35.475	-4.36 MWD+IFR1+
														MS
	16800	90	179.7	9249.958	62.944	0	61.87	0	62.944	0	0	61.972	35.559	OWSG -4.315 MWD+IFR1+
	10000	30	175.7	3243.330	02.544	U	01.07	O	02.544	O	O	01.572	33.333	MS MS
														OWSG
	16900	90	179.7	9249.958	63.702	0	62.442	0	63.702	0	0	62.543	35.628	-4.27 MWD+IFR1+ MS
														OWSG
	17000	90	179.7	9249.958	64.459	0	63.008	0	64.459	0	0	63.109	35.697	-4.225 MWD+IFR1+
														MS OWSG
	17100	90	179.7	9249.958	65.223	0	63.577	0	65.223	0	0	63.677	35.766	-4.183 MWD+IFR1+
														MS OWSG
	17200	90	179.7	9249.958	65.977	0	64.149	0	65.977	0	0	64.248	35.849	-4.14 MWD+IFR1+
														MS
	17300	90	179.7	9249.958	66.738	0	64.723	0	66.738	0	0	64.822	35.918	OWSG -4.099 MWD+IFR1+
	27000			52 151555	00.700	Ū	0 20	Ū	33.7.33	v		0	00.010	MS 🦸
	17400	00	170 7	0240.050	67.400	0	CF 2	0	67.400	0	0	CE 200	26.004	OWSG
	17400	90	179.7	9249.958	67.498	0	65.3	0	67.498	0	0	65.398	36.001	-4.06 MWD+IFR1+ MS
•														IVIS S

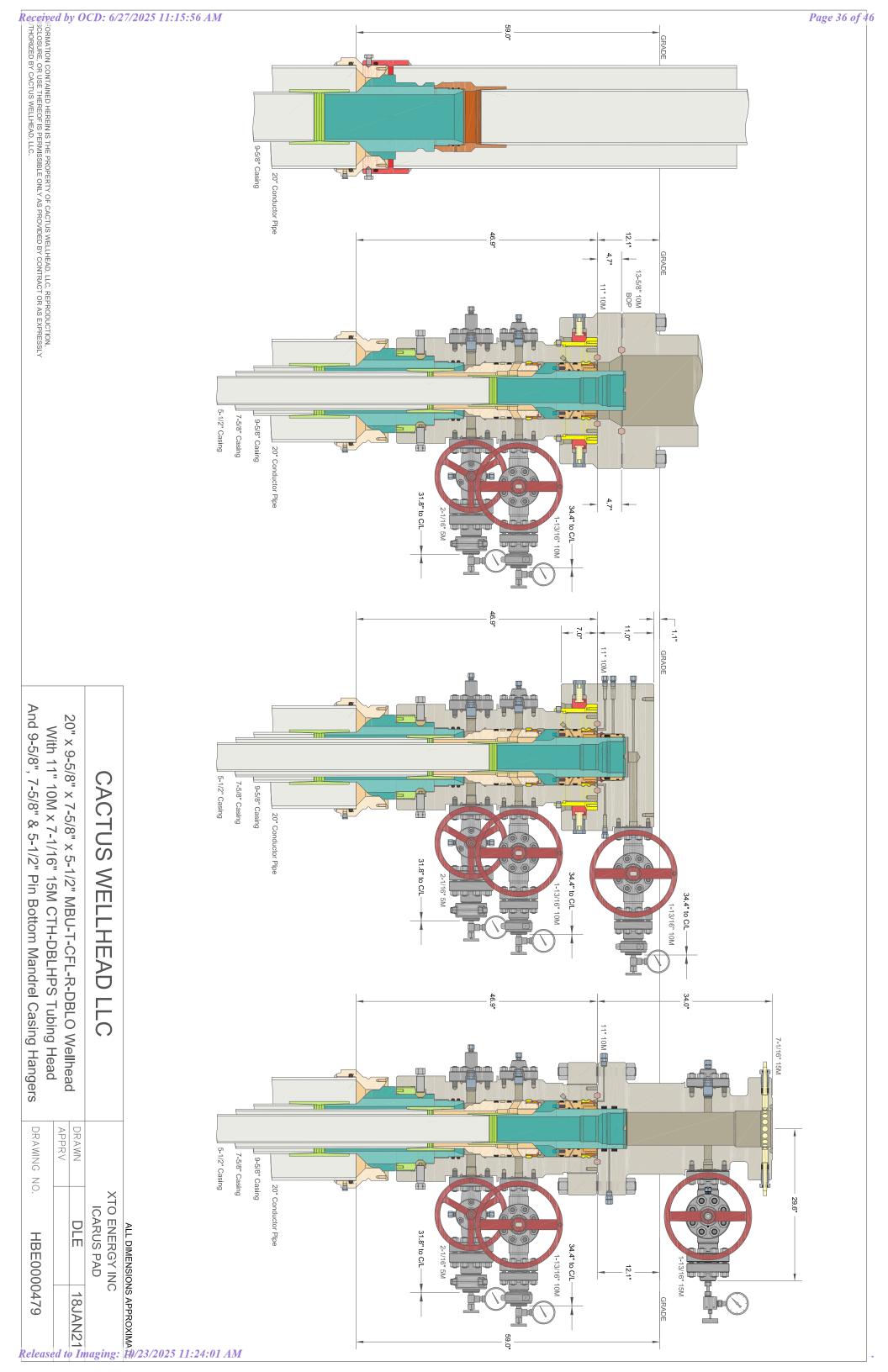
														OWSG
R	17500	90	179.7	9249.958	68.257	0	65.88	0	68.257	0	0	65.977	36.083	-4.019 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM						-		-		•	-			MS
ase														OWSG
d t	17600	90	179.7	9249.958	69.022	0	66.454	0	69.022	0	0	66.551	36.152	-3.98 MWD+IFR1+
o I														MS 🦹
ma														OWSG 🥈
gin	17700	90	179.7	9249.958	69.778	0	67.039	0	69.778	0	0	67.135	36.234	-3.943 MWD+IFR1+
0.0														MS 👔
10/	4=000						c= c.c		-0					OWSG
23/	17800	90	179.7	9249.958	70.541	0	67.618	0	70.541	0	0	67.714	36.316	-3.906 MWD+IFR1+
20.														MS OWSG
25	17900	90	179.7	9249.958	71.302	0	68.2	0	71.302	0	0	68.295	36.398	-3.869 MWD+IFR1+
11:	17500	30	175.7	3243.330	71.502	U	00.2	Ü	71.502	O	Ü	00.233	30.330	MS MS
24														OWSG 1
01	18000	90	179.7	9249.958	72.069	0	68.784	0	72.069	0	0	68.879	36.479	-3.833 MWD+IFR1+
A														MS
														OWSG
	18100	90	179.7	9249.958	72.829	0	69.371	0	72.829	0	0	69.464	36.561	-3.798 MWD+IFR1+
														MS
														OWSG
	18200	90	179.7	9249.958	73.593	0	69.96	0	73.593	0	0	70.053	36.642	-3.764 MWD+IFR1+
														MS
	18300	90	179.7	9249.958	74.357	0	70.551	0	74.357	0	0	70.643	36.723	OWSG -3.73 MWD+IFR1+
	10300	90	1/9./	9249.936	74.557	0	70.551	0	74.557	0	U	70.043	30.723	MS
														OWSG
	18400	90	179.7	9249.958	75.127	0	71.144	0	75.127	0	0	71.235	36.804	-3.696 MWD+IFR1+
														MS
														OWSG
	18500	90	179.7	9249.958	75.888	0	71.732	0	75.888	0	0	71.823	36.885	-3.664 MWD+IFR1+
														MS
						_		_		_				OWSG
	18600	90	179.7	9249.958	76.655	0	72.329	0	76.655	0	0	72.419	36.979	-3.633 MWD+IFR1+
														MS OWSG
	18700	90	179.7	9249.958	77.421	0	72.921	0	77.421	0	0	73.011	37.059	-3.602 MWD+IFR1+
	10700	30	175.7	3243.330	,,,,,,,,	Ü	72.321	Ü	77.421	Ü	Ü	75.011	37.033	MS
														OWSG
	18800	90	179.7	9249.958	78.186	0	73.515	0	78.186	0	0	73.605	37.153	-3.571 MWD+IFR1+
														MS
														OWSG
	18900	90	179.7	9249.958	78.956	0	74.118	0	78.956	0	0	74.207	37.233	-3.54 MWD+IFR1+
														MS
	10000	00	470 7	0240.050	70 705		74.747	•	70 705			74.005	27.226	OWSG
	19000	90	179.7	9249.958	79.725	0	74.717	0	79.725	0	0	74.805	37.326	-3.511 MWD+IFR1+
														MS OWSG
	19100	90	179.7	9249.958	80.486	0	75.31	0	80.486	0	0	75.398	37.419	-3.483 MWD+IFR1+
		30	1, 5.,	32 13.330	30.100	J	, 5.51	J	20.100	•	J	, 5.550	37.123	MS MS
•														6

														OWSG
K	19200	90	179.7	9249.958	81.259	0	75.912	0	81.259	0	0	75.999	37.499	-3.453 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM	13200	50	175.7	3243.330	01.233	U	75.512	O	01.233	O	Ū	73.333	37.433	MS MS
as														OWSG
ed	19300	90	179.7	9249.958	82.024	0	76.516	0	82.024	0	0	76.602	37.591	-3.425 MWD+IFR1+
0						-		-		-	-			MS
Ta														owsg 🖁
181	19400	90	179.7	9249.958	82.795	0	77.121	0	82.795	0	0	77.207	37.684	-3.397 MWD+IFR1+
80														MS
1														owsg 🖁
2	19500	90	179.7	9249.958	83.564	0	77.722	0	83.564	0	0	77.807	37.776	-3.371 MWD+IFR1+🐇
3/2														MS
92														owsg 📜
5 1	19600	90	179.7	9249.958	84.333	0	78.325	0	84.333	0	0	78.409	37.868	-3.344 MWD+IFR1+
1:2														MS
4.														OWSG 🚶
91	19700	90	179.7	9249.958	85.1	0	78.935	0	85.1	0	0	79.02	37.959	-3.318 MWD+IFR1+鞣
														MS
														OWSG
	19800	90	179.7	9249.958	85.872	0	79.541	0	85.872	0	0	79.625	38.051	-3.292 MWD+IFR1+
														MS
														OWSG
	19900	90	179.7	9249.958	86.637	0	80.149	0	86.637	0	0	80.232	38.142	-3.266 MWD+IFR1+
														MS
	20000	00	4707	0040.050	07.407		00 750	•	07.407	•		00.044	20.222	OWSG
	20000	90	179.7	9249.958	87.407	0	80.758	0	87.407	0	0	80.841	38.233	-3.241 MWD+IFR1+
														MS OWSG
	20100	00	170.7	0240.059	00 103	0	91 360	0	00 102	0	0	81.451	20 227	
	20100	90	179.7	9249.958	88.182	0	81.369	0	88.182	0	0	81.451	38.337	-3.217 MWD+IFR1+ MS
														OWSG
	20200	90	179.7	9249.958	88.949	0	81.975	0	88.949	0	0	82.057	38.428	-3.194 MWD+IFR1+
	20200	30	1,3.,	32 13.330	00.5 15	Ü	01.373	Ü	00.3 13	Ü	Ü	02.037	30.120	MS
														OWSG
	20300	90	179.7	9249.958	89.722	0	82.589	0	89.722	0	0	82.67	38.531	-3.17 MWD+IFR1+
														MS
														OWSG
	20400	90	179.7	9249.958	90.493	0	83.198	0	90.493	0	0	83.279	38.621	-3.147 MWD+IFR1+
														MS
														OWSG
	20500	90	179.7	9249.958	91.263	0	83.815	0	91.263	0	0	83.895	38.724	-3.124 MWD+IFR1+
														MS
														OWSG
	20600	90	179.7	9249.958	92.033	0	84.428	0	92.033	0	0	84.507	38.814	-3.101 MWD+IFR1+
														MS
														OWSG
	20700	90	179.7	9249.958	92.806	0	85.042	0	92.806	0	0	85.121	38.916	-3.079 MWD+IFR1+
														MS
	20800	00	170 7	0240.050	02 570	0	05.657	0	02.570	0	0	05 700	20.040	OWSG
	20800	90	179.7	9249.958	93.579	0	85.657	0	93.579	0	0	85.736	39.018	-3.057 MWD+IFR1+
														MS
														-,

Rele	20900	90	179.7	9249.958	94.35	0	86.274	0	94.35	0	0	86.352	39.12	OWSG -3.036 MWD+IFR1+
Released to Imaging: 10/23/2025 11:24:01 AM	21000	90	179.7	9249.958	95.121	0	86.892	0	95.121	0	0	86.969	39.222	OWSG -3.014 MWD+IFR1+ MS
maging:	21100	90	179.7	9249.958	95.896	0	87.511	0	95.896	0	0	87.588	39.323	OWSG -2.993 MWD+IFR1+ MS
10/23/20	21200	90	179.7	9249.958	96.67	0	88.126	0	96.67	0	0	88.203	39.424	OWSG -2.973 MWD+IFR1+ MS
925 11:2	21300	90	179.7	9249.958	97.442	0	88.748	0	97.442	0	0	88.824	39.525	OWSG -2.953 MWD+IFR1+ MS
4:01 AM	21400	90	179.7	9249.958	98.214	0	89.366	0	98.214	0	0	89.442	39.625	OWSG -2.932 MWD+IFR1+ MS
	21500	90	179.7	9249.958	98.99	0	89.985	0	98.99	0	0	90.06	39.726	OWSG -2.913 MWD+IFR1+ MS
	21600	90	179.7	9249.958	99.76	0	90.605	0	99.76	0	0	90.68	39.826	OWSG -2.894 MWD+IFR1+ MS
	21700	90	179.7	9249.958	100.499	0	91.227	0	100.499	0	0	91.301	39.938	OWSG -2.875 MWD+IFR1+ MS OWSG
	21800	90	179.7	9249.958	101.292	0	91.85	0	101.292	0	0	91.924	40.038	-2.856 MWD+IFR1+ MS OWSG
	21900	90	179.7	9249.958	102.078	0	92.474	0	102.078	0	0	92.548	40.149	-2.838 MWD+IFR1+ MS OWSG
	22000	90	179.7	9249.958	102.859	0	93.099	0	102.859	0	0	93.172	40.248	-2.819 MWD+IFR1+ MS OWSG
	22100	90	179.7	9249.958	103.634	0	93.725	0	103.634	0	0	93.798	40.359	-2.801 MWD+IFR1+ MS OWSG
	22200	90	179.7	9249.958	104.403	0	94.348	0	104.403	0	0	94.42	40.458	-2.783 MWD+IFR1+ MS OWSG
	22300	90	179.7	9249.958	105.167	0	94.971	0	105.167	0	0	95.043	40.568	-2.766 MWD+IFR1+ MS OWSG
	22389	90	179.7	9250	105.877	0	95.538	0	105.877	0	0	95.61	40.667	-2.75 MWD+IFR1+1 MS

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Pi Targets Pi eleased to	Brushy Draw 30 Fed 102H				
Imagi	Measured Depth	Grid Northing	<b>Grid Easting</b>	TVD MSL Target Shape	
Taget Name	(ft)	(ft)	(ft)	(ft)	
FT 21	9638.8	397645.87	627153.86	6080 CIRCLE	
LT 👸 .	22240.55	385041.85	627216.69	6080 CIRCLE	
BH№1	22390.17	384891.98	627217.26	6080 CIRCLE	



Subject: Request for a Variance Allowing break Testing of the Blowout Preventer Equipment (BOPE)

XTO Energy requests a variance to ONLY test broken pressure seals on the BOPE and function test BOP when skidding a drilling rig between multiple wells on a pad.

# **Background**

Onshore Oil and Gas Order (OOGO) No. 2, Drilling Operations, Sections III.A.2.i.iv.B states that the BOP test must be performed whenever any seal subject to test pressure is broken. The current interpretation of the Bureau of Land Management (BLM) requires a complete BOP test and not just a test of the affected component. OOGO No. 2, Section I.D.2 states, "Some situation may exist either on a well-by-well basis or field-wide basis whereby it is commonly accepted practice to vary a particular minimum standard(s) established in this order. This situation can be resolved by requesting a variance...". XTO Energy feels the break testing the BOPE is such a situation. Therefore, as per OOGO No. 2, Section IV., XTO Energy submits this request for the variance.

# **Supporting Documentation**

OOGO No. 2 became effective on December 19, 1988 and has remained the standard for regulating BLM onshore drilling operations for over 30 years. During this time there have been significant changes in drilling technology. BLM continues to use the variance request process to allow for the use of modern technology and acceptable engineering practices that have arisen since OOGO No. 2 was originally released. The XTO Energy drilling rig fleet has many modern upgrades that allow the intact BOP stack to be moved between well slots on a multi-well pad, as well as, wellhead designs that incorporate quick connects facilitating release of the BOP from the wellhead without breaking any BOP stack components apart. These technologies have been used extensively offshore, and other regulators, API, and many operators around the world have endorsed break testing as safe and reliable.



Figure 1: Winch System attached to BOP Stack



Figure 2: BOP Winch System

American Petroleum Institute (API) standards, specification and recommended practices are considered the industry standard and are consistently utilized and referenced by the industry. OOGO No. 2 recognizes API recommended Practices (RP) 53 in its original development. API Standard 53, *Well Control Equipment Systems for Drilling Wells* (Fifth Edition, December 2018, Annex C, Table C.4) recognizes break testing as an acceptable practice. Specifically, API Standard 53, Section 5.3.7.1 states "A pressure test of the pressure containing component shall be performed following the disconnection or repair, limited to the affected component." See Table C.4 below for reference.

Table C.4—Initial Pressure Testing, Surface BOP Stacks  Pressure Test—High Pressure									
Component to be Pressure Tested	Pressure Test—Low Pressure <sup>ac</sup> psig (MPa)	Change Out of Component, Elastomer, or Ring Gasket	No Change Out of Component, Elastomer, or Ring Gasket						
Annular preventer <sup>b</sup>	250 to 350 (1.72 to 2.41)	RWP of annular preventer	MASP or 70% annular RWP, whichever is lower.						
Fixed pipe, variable bore, blind, and BSR preventers <sup>bd</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventer or wellhead system, whichever is lower	ITP						
Choke and kill line and BOP side outlet valves below ram preventers (both sides)	250 to 350 (1.72 to 2.41)	RWP of side outlet valve or wellhead system, whichever is lower	ITP						
Choke manifold—upstream of chokes <sup>e</sup>	250 to 350 (1.72 to 2.41)	RWP of ram preventers or wellhead system, whichever is lower	ITP						
Choke manifold—downstream of chokese	250 to 350 (1.72 to 2.41)	RWP of valve(s), line(s), or M whichever is lower	MASP for the well program,						
Kelly, kelly valves, drill pipe safety valves, IBOPs	250 to 350 (1.72 to 2.41)	MASP for the well program							
Annular(s) and VBR(s) shall be prespected for pad drilling operations, moving pressure-controlling connections of For surface offshore operations, the pressure of the pres	during the evaluation period. The passure tested on the largest and sm from one wellhead to another within when the integrity of a pressure see ram BOPs shall be pressure testalland operations, the ram BOPs sh	pressure shall not decrease below the allest OD drill pipe to be used in well in the 21 days, pressure testing is req	program.  uired for pressure-containing and the closing and locking pressure						

The Bureau of Safety and Environmental Enforcement (BSEE), Department of Interior, has also utilized the API standards, specification and best practices in the development of its offshore oil and gas regulations and incorporates them by reference within its regulations.

Break testing has been approved by the BLM in the past with other operators based on the detailed information provided in this document.

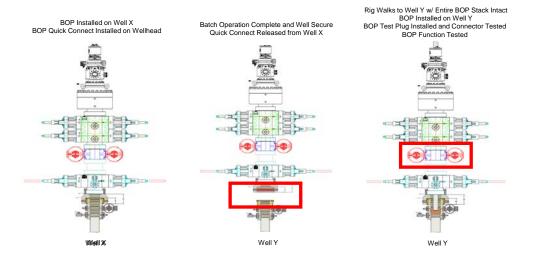
XTO Energy feels break testing and our current procedures meet the intent of OOGO No. 2 and often exceed it. There has been no evidence that break testing results in more components failing than seen on full BOP tests. XTO Energy's internal standards requires complete BOPE tests more often than that of OOGO No. 2 (Every 21 days). In addition to function testing the annular, pipe rams and blind rams after each BOP nipple up, XTO Energy performs a choke drill with the rig crew prior to drilling out every casing shoe. This is additional training for the rig crew that exceeds the requirements of the OOGO No. 2.

# **Procedures**

- XTO Energy will use this document for our break testing plan for New Mexico Delaware basin.
   The summary below will be referenced in the APD or Sundry Notice and receive approval prior to implementing this variance.
- 2. XTO Energy will perform BOP break testing on multi-wells pads where multiple intermediate sections can be drilled and cased within the 21-day BOP test window.
  - a. A full BOP test will be conducted on the first well on the pad.
  - b. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
    - i. Our Lower WC targets set the intermediate casing shoe no deeper than the Wolfcamp B.
    - ii. Our Upper WC targets set the intermediate casing shoe shallower than the Wolfcamp B.
  - c. A Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
  - d. A full BOP test will be required prior to drilling any production hole.
- 3. After performing a complete BOP test on the first well, the intermediate hole section will be drilled and cased, two breaks would be made on the BOP equipment.
  - a. Between the HCV valve and choke line connection
  - b. Between the BOP quick connect and the wellhead
- 4. The BOP is then lifted and removed from the wellhead by a hydraulic system.
- 5. After skidding to the next well, the BOP is moved to the wellhead by the same hydraulic system and installed.
- 6. The connections mentioned in 3a and 3b will then be reconnected.
- 7. Install test plug into the wellhead using test joint or drill pipe.
- 8. A shell test is performed against the upper pipe rams testing the two breaks.
- 9. The shell test will consist of a 250 psi low test and a high test to the value submitted in the APD or Sundry (e.g. 5,000 psi or 10,000psi).
- 10. Function test will be performed on the following components: lower pipe rams, blind rams, and annular.

- 11. For a multi-well pad the same two breaks on the BOP would be made and on the next wells and steps 4 through 10 would be repeated.
- 12. A second break test would only be done if the intermediate hole section being drilled could not be completed within the 21 day BOP test window.

Note: Picture below highlights BOP components that will be tested during batch operations



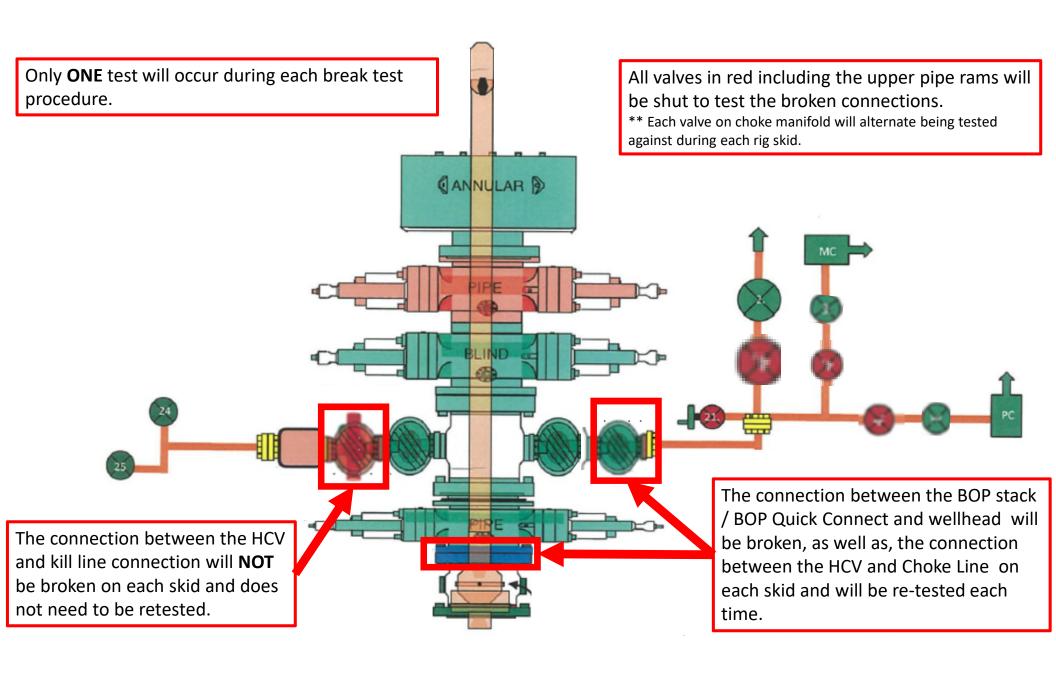
# **Summary**

A variance is requested to **ONLY** test broken pressure seals on the BOP equipment when moving from wellhead to wellhead which is in compliance with API Standard 53. API Standard 53 states, that for pad drilling operation, moving from one wellhead to another within 21 days, pressure testing is required for pressure-containing and pressure-controlling connections when the integrity of a pressure seal is broken.

The BOP will be secured by a hydraulic carrier or cradle. The BLM will be contacted if a Well Control event occurs prior to the commencement of a BOPE Break Testing operation.

Based on discussions with the BLM on February 27th 2020 and the supporting documentation submitted to the BLM, we will request permission to ONLY retest broken pressure seals if the following conditions are met:

- 1. After a full BOP test is conducted on the first well on the pad.
- 2. The first intermediate hole section drilled on the pad will be the deepest. All of the remaining hole sections will be the same depth or shallower.
- 3. Full BOP test will be required if the intermediate hole section being drilled has a MASP over 5M.
- 4. Full BOP test will be required prior to drilling the production hole.



# **XTO Permian Operating, LLC Offline Cementing Variance Request**

XTO requests the option to cement the surface and intermediate casing strings offline as a prudent batch drilling efficiency of acreage development.

# 1. Cement Program

No changes to the cement program will take place for offline cementing.

# 2. Offline Cementing Procedure

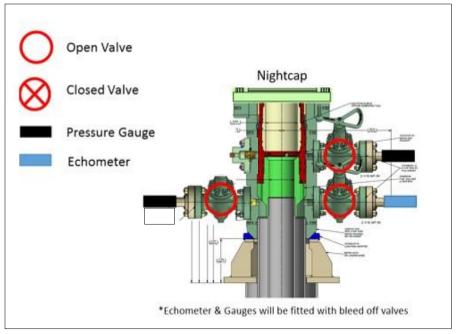
The operational sequence will be as follows. If a well control event occurs, the BLM will be contacted for approval prior to conducting offline cementing operations.

- 1. Run casing as per normal operations. While running casing, conduct negative pressure test and confirm integrity of the float equipment (float collar and shoe)
- 2. Land casing with mandrel
- 3. Fill pipe with kill weight fluid, do not circulate through floats and confirm well is static
- 4. Set annular packoff shown below and pressure test to confirm integrity of the seal. Pressure ratings of wellhead components and valves is 5,000 psi.
- 5. After confirmation of both annular barriers and internal barriers, nipple down BOP and install cap flange.
  - a. If any barrier fails to test, the BOP stack will not be nippled down until after the cement job is completed with cement 500ft above the highest formation capable of flow with kill weight mud above or after it has achieved 50-psi compressive strength if kill weight fluid cannot be verified.



Annular packoff with both external and internal seals

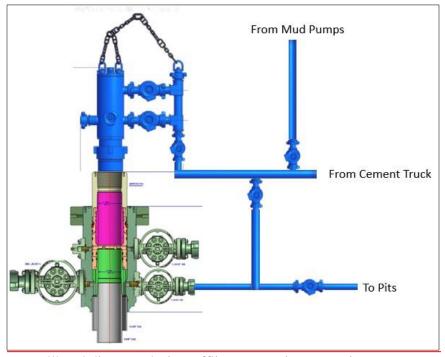
# **XTO Permian Operating, LLC Offline Cementing Variance Request**



Wellhead diagram during skidding operations

- 6. Skid rig to next well on pad.
- 7. Confirm well is static before removing cap flange, flange will not be removed and offline cementing operations will not commence until well is under control. If well is not static, casing outlet valves will provide access to both the casing ID and annulus. Rig or third party pump truck will kill well prior to cementing or nippling up for further remediation.
  - a. Well Control Plan
    - i. The Drillers Method will be the primary well control method to regain control of the wellbore prior to cementing, if wellbore conditions do not permit the drillers method other methods of well control may be used
    - ii. Rig pumps or a 3<sup>rd</sup> party pump will be tied into the upper casing valve to pump down the casing ID
    - iii. A high pressure return line will be rigged up to lower casing valve and run to choke manifold to control annular pressure
    - iv. Once influx is circulated out of the hole, kill weight mud will be circulated
    - v. Well will be confirmed static
    - vi. Once confirmed static, cap flange will be removed to allow for offline cementing operations to commence
- 8. Install offline cement tool
- 9. Rig up cement equipment

# **XTO Permian Operating, LLC Offline Cementing Variance Request**



Wellhead diagram during offline cementing operations

- 10. Circulate bottoms up with cement truck
  - a. If gas is present on bottoms up, well will be shut in and returns rerouted through gas buster to handle entrained gas
  - b. Max anticipated time before circulating with cement truck is 6 hrs
- 11. Perform cement job taking returns from the annulus wellhead valve
- 12. Confirm well is static and floats are holding after cement job
- 13. Remove cement equipment, offline cement tools and install night cap with pressure gauge for monitoring.

XTO respectfully requests approval to utilize a spudder rig to pre-set surface casing.

# Description of Operations:

- 1. Spudder rig will move in to drill the surface hole and pre-set surface casing on the well.
  - a. After drilling the surface hole section, the spudder rig will run casing and cement following all of the applicable rules and regulations (OnShore Order 2, all COAs and NMOCD regulations).
  - b. The spudder rig will utilize fresh water-based mud to drill the surface hole to TD. Solids control will be handled entirely on a closed loop basis. No earth pits will be used.
- 2. The wellhead will be installed and tested as soon as the surface casing is cut off and WOC time has been reached.
- 3. A blind flange at the same pressure rating as the wellhead will be installed to seal the wellbore. Pressure will be monitored with needle valves installed on two wing valves.
  - a. A means for intervention will be maintained while the drilling rig is not over the well.
- 4. Spudder rig operations are expected to take 2-3 days per well on the pad.
- 5. The BLM will be contacted and notified 24 hours prior to commencing spudder rig operations.
- 6. Drilling Operations will begin with a larger rig and a BOP stack equal to or greater than the pressure rating that was permitted will be nippled up and tested on the wellhead before drilling operations resume on each well.
  - a. The larger rig will move back onto the location within 180 days from the point at which the wells are secured and the spudder rig is moved off location.
  - b. The BLM will be notified 24 hours before the larger rig moves back on the pre-set locations
- 7. XTO will have supervision on the rig to ensure compliance with all BLM and NMOCD regulations and to oversee operations.
- 8. Once the rig is removed, XTO will secure the wellhead area by placing a guard rail around the cellar area.

Sante Fe Main Office Phone: (505) 476-3441

General Information Phone: (505) 629-6116

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# State of New Mexico Energy, Minerals and Natural Resources Oil Conservation Division 1220 S. St Francis Dr. Santa Fe, NM 87505

CONDITIONS

Action 479782

## **CONDITIONS**

Operator:	OGRID:
XTO PERMIAN OPERATING LLC.	373075
6401 HOLIDAY HILL ROAD	Action Number:
MIDLAND, TX 79707	479782
	Action Type:
	[C-103] NOI Change of Plans (C-103A)

# CONDITIONS

Created By	Condition	Condition Date
ward.rikala	Work was performed without OCD approval.	10/23/2025