

AMERADA HESS CORPORATION

August 22, 1984

P. O. DRAWER "D"
MONUMENT, NEW MEXICO 88265

State of New Mexico
Energy and Minerals Department
Oil Conservation Division
P. O. Box 2088
Santa Fe, New Mexico 87501

AB BAKER #4, UNIT P, Sec. 10, T22S, R37E.

Re: 

Request to downhole commingle the Tubb/Drinkard
and the Blinebry/Drinkard Gas Zones.

Dear Sir:

Amerada Hess Corporation is requesting approval for an exception to Rule 303-C to permit the downhole commingling of the Tubb and Drinkard gas zones in the A. B. Baker #3 and the Blinebry and Drinkard gas zones in the A. B. Baker #4. Permission to dually complete these wells was authorized by administrative orders MC-2085 and MC-2072, respectively.

In the A. B. Baker #3, the Tubb zone is perforated from 5960'-6135' and the Drinkard zone from 6205'-6404'. In 1984, both zones have made more fluid than in previous years and gas flow rates have decreased. If downhole permission to commingle is received this well will be placed on sucker rod pump to effectively lift formation fluids from the wellbore resulting in increased gas flow rates. The A. B. Baker #4 is perforated in the Blinebry zone from 5422'-5686' and in the Drinkard zone from 6220'-6473'. The Drinkard side of this wellbore is temporarily abandoned due to 1100' of fluid on the formation face which has killed the gas flow. Before the fluid encroachment the Drinkard zone was capable of producing 20,000 to 30,000 MCFPM. With the approval to downhole commingle, this well will also be placed on sucker rod pump to remove formation fluids. This will result in a significant increase in gas production from this wellbore.

Shut-in pressures from packer leakage tests and fluid levels revealed from acoustic well sounders were utilized to determine bottom hole pressures. These results are presented below.

A. B. Baker #3	Tubb Gas	SBHP = 364 psia
A. B. Baker #3	Drinkard Gas	SBHP = 234 psia
A. B. Baker #4	Blinebry Gas	SBHP = 497 psia
A. B. Baker #4	Drinkard Gas	SBHP = 376 psia

These pressures are corrected to a common datum and the small pressure differences between zones indicate no crossflow problems will exist. Details of the method used to derive these figures is attached with this proposal.

The fluid characteristics of each zone are similar and there is no indication there will be incompatibility problems in the wellbore.

The value of the commingled production will not be less than the sum of the values of the individual streams since Amerada Hess is receiving \$1.10/MCF for the gas from all zones in consideration in both wellbores.

To figure the allocation of production to each zone, decline curves were used. This method revealed the following and details of it are attached.

Production Allocations To Each Zone:

A. B. Baker #3	Tubb	4%
A. B. Baker #3	Drinkard	96%
A. B. Baker #4	Blinebry	13%
A. B. Baker #4	Drinkard	87%

The ownership of the zones to be commingled is common with respect to working interest, royalty and overriding royalty.

All offset operators have been notified of this proposal by receipt of this recommendation. If you have any questions concerning this matter, please contact me.

Respectfully,

D. W. Holmes

D. W. Holmes
Sr. Petroleum Engineer

AMERADA HESS CORPORATION
Drawer "D"
Monument, New Mexico 88265

Phone: (505-393-2144)

DWH/dg

Enclosures:

XC: Division Director (2)
Hobbs District Office
Offset Operators
File

OFFSET OPERATORS

Gulf Oil
Gulf Building
Midland, Texas 79702

Getty Oil
Box 1231
Midland, Texas 79702

Marathon
Box 552
Midland, Texas 79702

Exxon Company, USA
Box 1600
Midland, Texas 79701

John H. Hendrix
525 Midland Tower
Midland, Texas 79701

Sun Production Company
Two Lincoln Centre
Dallas, Texas 75240

Anadarko Production Co.
Box 2497
Midland, Texas 79702

Sun Texas Co.
1700 One Main Place
Dallas, Texas 75250

Robert L. Parker
Eight East Third
Tulsa, Oklahoma 74103

CALCULATION OF
STATIC BOTTOM-HOLE PRESSURES

Equations To Be Used:

$$P_{sfs} = P_{whs} \times e^{c/\bar{z}} \quad \text{Where: } c = \frac{(\gamma_g)(TVD)}{53.34 \bar{T}}$$

P_{sfs} = Static sandface pressure, psia

P_{whs} = Static wellhead pressure, psia

$$e = 2.7183$$

γ_g = Gas gravity

TVD = True vertical depth, feet

\bar{T} = Average temperature, °R

\bar{z} = Average compressibility factor

Assumptions:

$$P_{atm} = 13.025 \text{ psia}$$

$$\text{Temp. Grad.} = 0.017 \text{ } ^\circ\text{F/ft.}$$

$$\text{Avg. Surf. Temp.} = 60^\circ\text{F}$$

$$\gamma_g = 0.70$$

A. B. Baker #3

Tubb Zone:

$$\gamma_g = 0.70$$

$$P_{whs} = 310 \text{ psia from pkr. leak. test}$$

$$TVD = 6,048' \text{ (mid perms.)}$$

$$\bar{T} = (60 + 103)(1 = 82^\circ\text{F} = 542^\circ\text{R}$$

$$c = \frac{(0.7)(6048)}{53.34 (542)} = 0.146$$

$$P_{pc} = 668 \text{ psia}$$

$$T_r = 542/390 = 1.39$$

$$T_{pc} = 390^\circ\text{R}$$

Assume: $P_{sfs} = 360 \text{ psia}$ $\bar{P} = (360 + 310) / 2 = 335 \text{ psia}$

$$P_r = 335/668 = 0.50 \therefore \bar{Z} = 0.938$$

$$P_{sfs} = (310) e^{.146/.938} = 362 \text{ psia}$$

Assume: $P = (362 + 310)/2 = 336 \text{ psia}$

$$P_r = 336/668 = 0.50 \therefore \bar{Z} = 0.938$$

$$P_{sfs} = (310) e^{.146/.938} = 362 \text{ psia}$$

$$\underline{P_{sfs} = 362 \text{ psia for Tubb zone}}$$

Drinkard Zone:

$$\gamma_g = 0.70$$

$$P_{whs} = 200 \text{ psia from pkr. leak. test}$$

$$\text{TVD} = 6305' \text{ (mid perms.)}$$

$$\bar{T} = (60 + 107)/2 = 84^\circ\text{F} = 544^\circ\text{R}$$

$$C = \frac{(0.7)(6305')}{53.34 (544)} = 0.152$$

$$P_{pc} = 668 \text{ psia}$$

$$T_r = 544/390 = 1.39$$

$$T_{pc} = 390^\circ\text{R}$$

Assume: $P_{sfs} = 250 \text{ psia}$ $\bar{P} = (250 + 200)/2 = 225 \text{ psia}$

$$P_r = 225/668 = 0.34 \therefore \bar{Z} = 0.950$$

$$P_{sfs} = (200) e^{.152/.95} = 235 \text{ psia}$$

Assume: $\bar{P} = (235+200)/2 = 218 \text{ psia}$

$$P_r = 218/668 = 0.33 \quad \therefore \bar{Z} = 0.960$$

$$P_{sfs} = (200) e^{.152/.96} = 234 \text{ psia}$$

$$\underline{P_{sfs} = 234 \text{ psia for Drinkard zone}}$$

To correct Tubb press. to common datum of 6305':

$$\bar{T} = (82 + 84)/2 = 83^\circ\text{F} = 543^\circ\text{R}$$

$$P_{pc} = 668 \text{ psia} \quad T_r = 543/390 = 1.39$$

$$T_{pc} = 390^\circ\text{R}$$

$$c = \frac{(0.7)(257)}{53.34(543)} = 0.0062$$

Assume: $P_{sfs} = 365 \text{ psia} \quad \bar{P} = (365 + 362)/2 = 364 \text{ psia}$

$$P_r = 364/668 = 0.54 \quad \therefore \bar{Z} = 0.935$$

$$P_{sfs} = (362)e^{.0062/.935} = 364 \text{ psia}$$

$$P_{sfs} = 364 \text{ psia for Tubb zone at common datum of 6305'}$$

Tubb zone SBHP at 6305' = 364 psia

Drinkard zone SBHP at 6305' = 234 psia

A. B. Baker #4

Blinebry Zone:

$$\gamma_g = 0.70$$

$$P_{whs} = 420 \text{ psia from pkr. leak. test}$$

$$\text{TVD} = 5564' \text{ (mid perms.)}$$

$$\bar{T} = (60 + 95)/2 = 78^\circ\text{F} = 538^\circ\text{R}$$

$$c = \frac{(0.7)(5564)}{53.34(538)} = 0.136$$

$$P_{pc} = 668 \text{ psia} \quad T_r = 538/390 = 1.38$$

$$T_{pc} = 390^\circ\text{R}$$

Assume: $P_{sfs} = 470 \text{ psia}$ $\bar{P} = (470+420)/2 = 445 \text{ psia}$

$$P_r = 445/668 = 0.67 \quad \therefore \bar{z} = 0.918$$

$$P_{sfs} = (420) e^{.136/.918} = 487 \text{ psia}$$

Assume: $\bar{P} = (487 + 420)/2 = 454 \text{ psia}$

$$P_r = 454/668 = 0.68 \quad \therefore \bar{z} = 0.917$$

$$P_{sfs} = (420) e^{.136/.917} = 487 \text{ psia}$$

$$P_{sfs} = 487 \text{ psia for Blinebry zone}$$

Drinkard Zone:

This gas zone has been TA'd since 1979. It is capable of producing gas at high volumes as long as formation fluids are removed from the wellbore. An acoustic well sounder has revealed 1073' of fluid in the hole. Using a 45°API oil gravity and 0 psi tubing pressure, the bottom hole static pressure in the Drinkard zone in this well is 376 psi.

To correct Blinebry press. to common datum of 6347'

$$\bar{T} = (78 + 108)/2 = 93^\circ\text{F} = 553^\circ\text{R}$$

$$P_{pc} = 668 \text{ psia}$$

$$T_r = 553/390 = 1.42$$

$$T_{pc} = 390^\circ\text{R}$$

$$c = \frac{(0.7)(783)}{53.34(553)} = 0.019$$

Assume: $P_{sfs} = 500 \text{ psia}$ $\bar{P} = (500 + 487)/2 = 494 \text{ psia}$

$$P_r = 494/668 = 0.74 \quad \therefore \bar{z} = 0.910$$

$$P_{sfs} = (487) e^{.019/.910} = 497 \text{ psia}$$

$$P_{sfs} = 497 \text{ psia for Blinebry zone at common datum of 6347'.$$

Blinebry zone SBHP at 6347' = 497 psia

Drinkard zone SBHP at 6347' = 376 psia

Allocation Of Production To Each Zone

A. B. Baker #3

Decline Rate Computations:

Tubb Zone

$$\begin{aligned}q_i &= 670 \text{ MCF/mo.} \\q &= 330 \text{ MCF/mo.} \\t &= 4 \text{ years}\end{aligned}$$

$$a_N = \ln \frac{(670/330)}{4}$$

$$a_N(\text{Tubb}) = 0.17705/\text{yr.}$$

Drinkard Zone

$$\begin{aligned}q_i &= 14,000 \text{ MCF/mo.} \\q &= 8,400 \text{ MCF/mo.} \\t &= 4 \text{ years}\end{aligned}$$

$$a_N = \ln \frac{(14,000/8,400)}{4}$$

$$a_N(\text{Drink.}) = 0.12771/\text{yr.}$$

Tubb/Drinkard Combined

$$\begin{aligned}q_i &= 14,670 \text{ MCF/mo.} \\q &= 8,730 \text{ MCF/mo.} \\t &= 4 \text{ years}\end{aligned}$$

$$a_N = \ln \frac{(14,670/8,730)}{4}$$

$$a_N(\text{Comb.}) = 0.12976/\text{yr.}$$

Actual Allocation:

X = Tubb Allocation
 $X-1$ = Drinkard Allocation

$$\begin{aligned}0.12976 &= (X)(0.17705) + (1-X)(0.12771) \\0.12976 &= (X)(0.17705) + (0.12771) - (X)(0.12771) \\0.00205 &= (X)(0.04934)\end{aligned}$$

$$\begin{aligned}X &= 0.04155 \\1-X &= 0.95845\end{aligned}$$

Therefore:

Tubb Production Allocation = 4%
Drinkard Production Allocation = 94%

Allocation Of Production To Each Zone

A. B. Baker #4

Decline Rate Computations:

Blinebry Zone

$$\begin{aligned}q_i &= 7,200 \text{ MCF/mo.} \\q &= 1,900 \text{ MCF/mo.} \\t &= 4 \text{ years}\end{aligned}$$

$$\begin{aligned}a_N &= \ln \frac{(7,200/1,900)}{4} \\a_{N(\text{Blin.})} &= 0.33306/\text{yr.}\end{aligned}$$

Drinkard Zone

$$\begin{aligned}q_i &= 30,000 \text{ MCF/mo.} \\q &= 23,700 \text{ MCF/mo.} \\t &= 4 \text{ years}\end{aligned}$$

$$\begin{aligned}a_N &= \ln \frac{(30,000/23,700)}{4} \\a_{N(\text{Drink.})} &= 0.05893/\text{yr.}\end{aligned}$$

Blinebry/Drinkard Combined

$$\begin{aligned}q_i &= 37,200 \text{ MCF/mo.} \\q &= 25,600 \text{ MCF/mo.} \\t &= 4 \text{ years}\end{aligned}$$

$$\begin{aligned}a_N &= \ln \frac{(37,200/25,600)}{4} \\a_{N(\text{Comb.})} &= 0.09343/\text{yr.}\end{aligned}$$

Actual Allocation:

$$\begin{aligned}X &= \text{Blinebry zone} \\X-1 &= \text{Drinkard zone}\end{aligned}$$

$$\begin{aligned}0.09343 &= (X)(0.33306) + (1-X)(0.05893) \\0.09343 &= (X)(0.33306) + (0.05893) - (X)(0.05893) \\0.03450 &= (X)(.27413)\end{aligned}$$

$$\begin{aligned}X &= 0.12585 \\1-X &= 0.87415\end{aligned}$$

Therefore:

$$\begin{aligned}\text{Blinebry Production Allocation} &= 13\% \\ \text{Drinkard Production Allocation} &= 87\%\end{aligned}$$

Equations Used:

Decline Rates

$$a_N = \frac{q_i/q}{t}$$

a_N = nominal decline, per yr.

q_i = initial rate, MCF/mo.

q = later rate, MCF/mo.

t = time between rates, yrs.

Allocation

$a_N(\text{Comb.})$ = Combined decline rates

$a_N(\text{Blin.})$ = Blinbry decline rate

$a_N(\text{Drink.})$ = Drinkard decline rate

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

GAS-OIL RATIO TESTS

Form C-116
Revised 10-1-78

Operator		Pool		County											
Amerada Hess Corporation		Drinkard Gas		Lea											
Address Drawer "D", Monument, New Mexico 88265		TYPE OF TEST - (X)		Completion <input type="checkbox"/> Special <input checked="" type="checkbox"/>											
LEASE NAME	WELL NO.	LOCATION			DATE OF TEST	CHOKE SIZE	TBG. PRESS.	DAILY ALLOW-ABLE	LENGTH OF TEST HOURS	PROD. DURING TEST			GAS - OIL RATIO CU.FT/BBL		
		U	S	T						R	WATER BBL'S.	GRAV. OIL BBL'S.		GAS M.C.F.	
A. B. Baker	3	I	10	22-S	37-E	8-15-84	F	2"	-	24	0	-	.25	272	1,088,000
A. B. Baker	4	P	10	22-S	37-E	8-15-84	F	2"	-	Zone TA'd					

No well will be assigned an allowable greater than the amount of oil produced on the official test.

During gas-oil ratio test, each well shall be produced at a rate not exceeding the top unit allowable for the pool in which well is located by more than 25 percent. Operator is encouraged to take advantage of this 25 percent tolerance in order that well can be assigned increased allowable when authorized by the Division.

Gas volumes must be reported in MCF measured at a pressure base of 15.025 psia and a temperature of 60° F. Specific gravity base will be 0.60.

Report casing pressure in lieu of tubing pressure for any well producing through casing.

Mail original and one copy of this report to the district office of the New Mexico Oil Conservation Division in accordance with Rule 301 and appropriate pool rules.

I hereby certify that the above information is true and complete to the best of my knowledge and belief.

A. M. Adams
(Signature)
Sr. Petroleum Engineer
8-22-84 (Date)

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION
P. O. BOX 2028
SANTA FE, NEW MEXICO 87501

Form C-116
Revised 10-1-78

GAS-OIL RATIO TESTS

Operator Amerada Hess Corporation		Pool Blinebry (Pro Gas)		County Lea											
Drawer "D", Monument, New Mexico 88265				TYPE OF TEST - (X)	Scheduled <input type="checkbox"/>	Completion <input type="checkbox"/>	Special <input checked="" type="checkbox"/>								
LEASE NAME	WELL NO.	LOCATION			DATE OF TEST	CHOKE SIZE	TGB. PRESS.	DAILY ALLOW-ABLE	LENGTH OF TEST HOURS	PROD. DURING TEST			GAS - OIL RATIO CU.FT/BBL.		
		U.	S.	T.						R.	WATER BBL.S.	CRAV. OIL BBL.S.		GAS M.C.F.	
A. B. Baker	4	P	10	22-S	37-E	8-15-84	F 2"	-	66	24	0	-	0	35	-

No well will be assigned an allowable greater than the amount of oil produced on the official test.
During gas-oil ratio test, each well shall be produced at a rate not exceeding the top unit allowable for the pool in which well is located by more than 25 percent. Operator is encouraged to take advantage of this 25 percent tolerance in order that well can be assigned increased allowable when authorized by the Division.
Gas volumes must be reported in MCF measured at a pressure base of 15.025 psia and a temperature of 60° F. Specific gravity base will be 0.60.

Report casing pressure in lieu of tubing pressure for any well producing through casing.
Mail original and one copy of this report to the district office of the New Mexico Oil Conservation Division in accordance with Rule 301 and appropriate pool rules.

I hereby certify that the above information is true and complete to the best of my knowledge and belief.

A. W. Adams
(Signature)
Sr. Petroleum Engineer
8-15-84
(Date)

OIL CONSERVATION DIVISION
P. O. BOX 2018
SANTA FE, NEW MEXICO 87501

GAS-OIL RATIO TESTS

No well will be assigned an allowable greater than the amount of oil produced on the official test.

During gas-oil ratio test, each well shall be produced at a rate not exceeding the top unit allowable for the pool in which well is located by more than 25 percent. Operator is encouraged to take advantage of this 25 percent tolerance in order that well can be assigned increased allowances when authorized by the Dividlog.

Gas volumes must be reported in MCF measured at a pressure base of 15.025 psia and a temperature of 60° F. Specific gravity base will be 0.86.

Report casing pressure in lieu of tubing pressure for any well producing through casing

Mail original and one copy of this report to the district office of the New Mexico Oil Conservation Division in accordance with Rule 301 and appropriate pool rules.

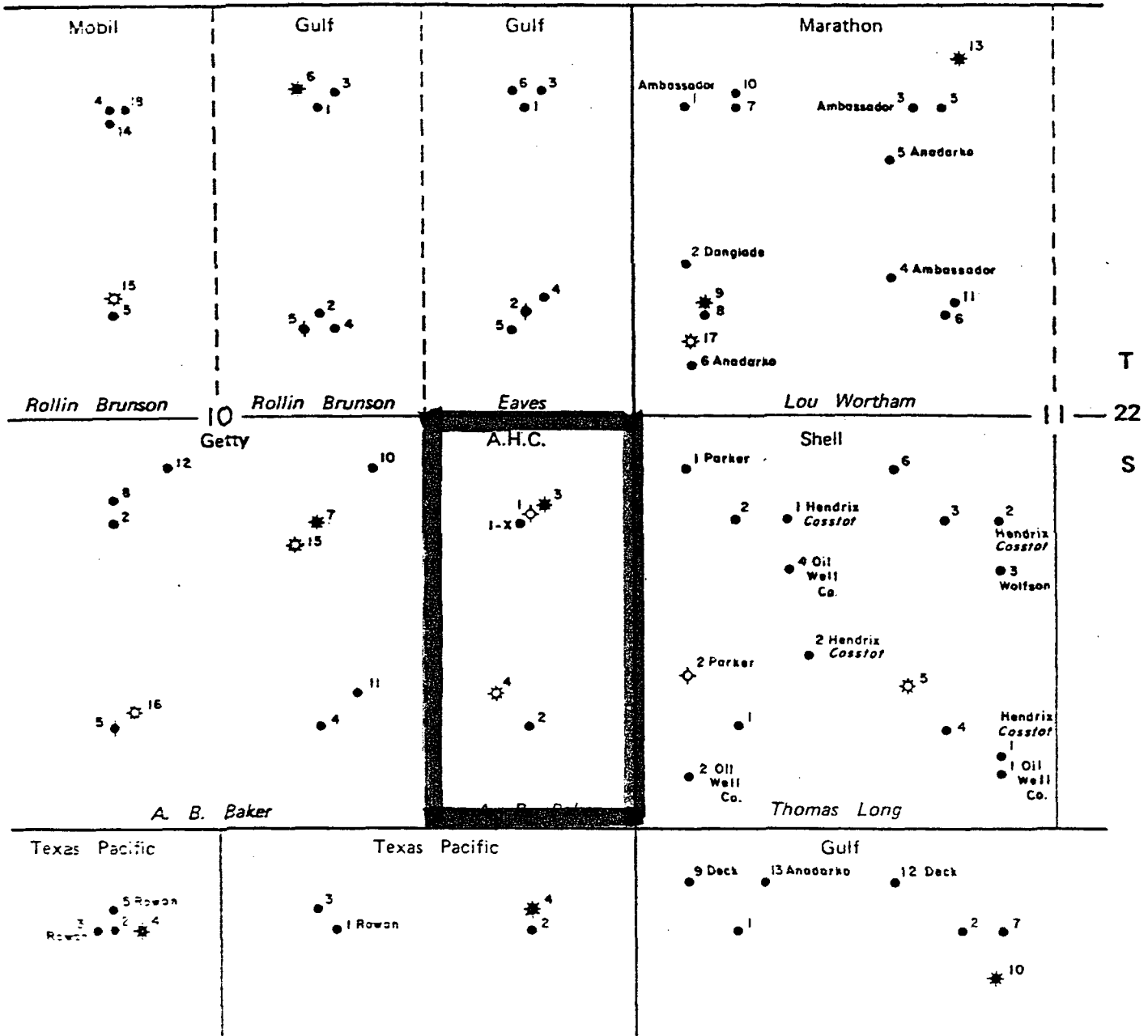
I hereby certify that the above information is true and complete to the best of my knowledge and belief.

Sr. Petroleum Engineer

8-15-84

(Dur)

R 37 E



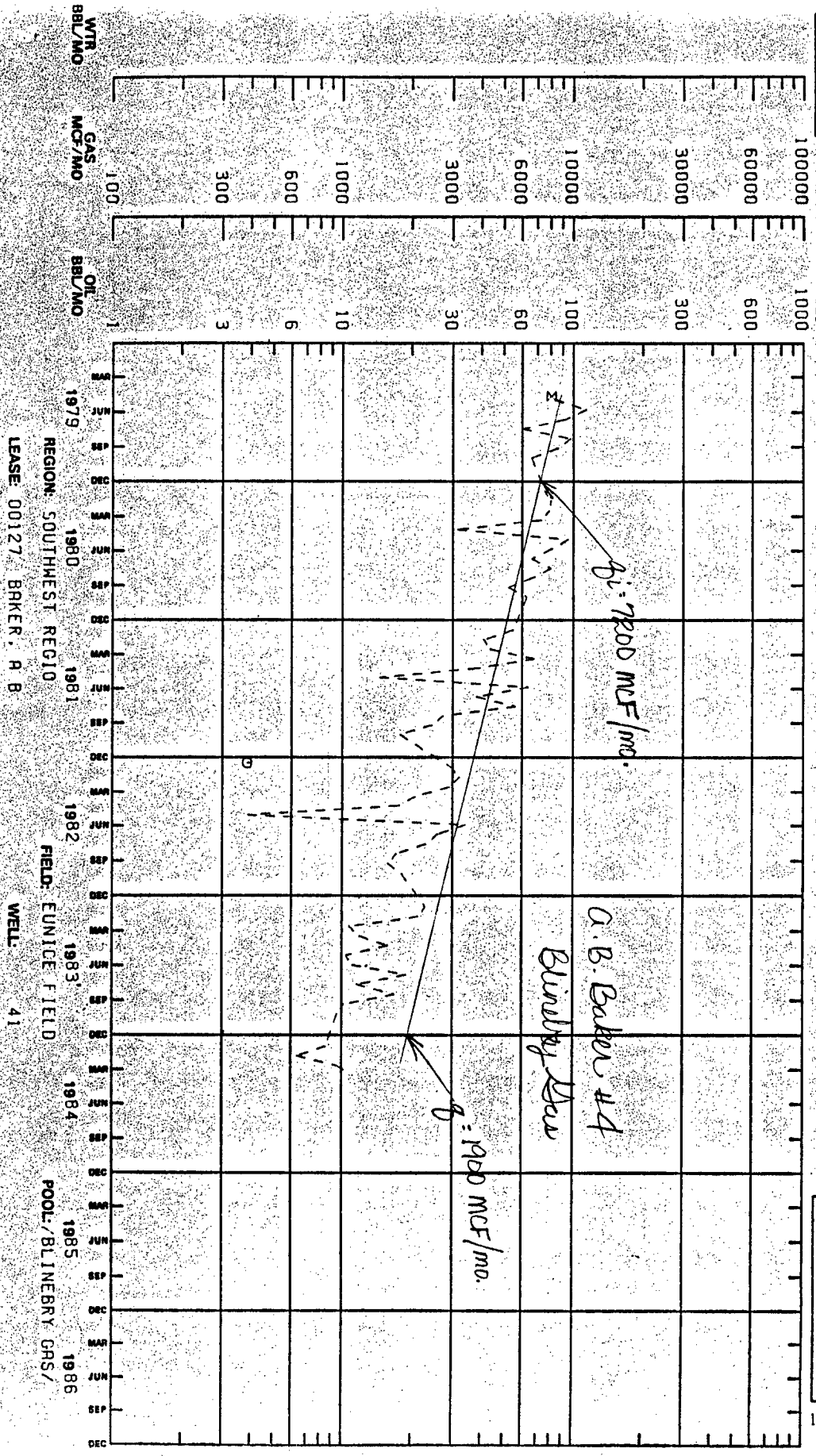
<p>Location Map</p>	<p>LEGEND</p> <ul style="list-style-type: none"> Oil Gas Dry & Abn Injection 	<p>SOUTHWEST PRODUCTION REGION EUNICE FIELD Lea County, New Mexico</p> <p>AMERADA HESS</p> <p>A. B. Baker Lease</p> <p>0 1000' 2000'</p> <p>Date: _____ Page No. _____</p> <p>Originator: _____ Ref No. _____</p>
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DATA CODES
 OIL = \bigcirc
 GAS = Σ
 WTR = \ast

CUMULATIVES:
 OIL MBBL 0.4
 GAS MMCF 59.0
 WTR MBBL 144.8
 198.9
 225.8
 243.9
 248.4

STATUS:
 41 ON 4 / 26 / 84

PRODUCTION PLOT



Hand-drawn graph on a grid showing production data for Zone TA'D from 1974 to 1979. The top part of the graph shows a decline in production from 30,000 MCF/mo. to 23,700 MCF/mo. The bottom part shows a sharp increase in production starting in 1977, peaking at 10,000 MCF/mo. in 1978, and then declining. A note states: "Last two years of production do not reflect natural decline due to wellbore fluids."

Year	Month	Production (MCF/mo.)
1974	Mar	30,000
1974	June	28,000
1974	Sept	27,000
1974	Dec	26,000
1975	Mar	25,000
1975	June	24,000
1975	Sept	23,000
1975	Dec	22,000
1976	Mar	21,000
1976	June	20,000
1976	Sept	19,000
1976	Dec	18,000
1977	Mar	17,000
1977	June	16,000
1977	Sept	15,000
1977	Dec	14,000
1978	Mar	13,000
1978	June	12,000
1978	Sept	11,000
1978	Dec	10,000
1979	Mar	9,000
1979	June	8,000
1979	Sept	7,000
1979	Dec	6,000
1980	Mar	5,000
1980	June	4,000
1980	Sept	3,000
1980	Dec	2,000
1981	Mar	1,000
1981	June	500
1981	Sept	200
1981	Dec	100

Zone TA'D

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DATA CODES
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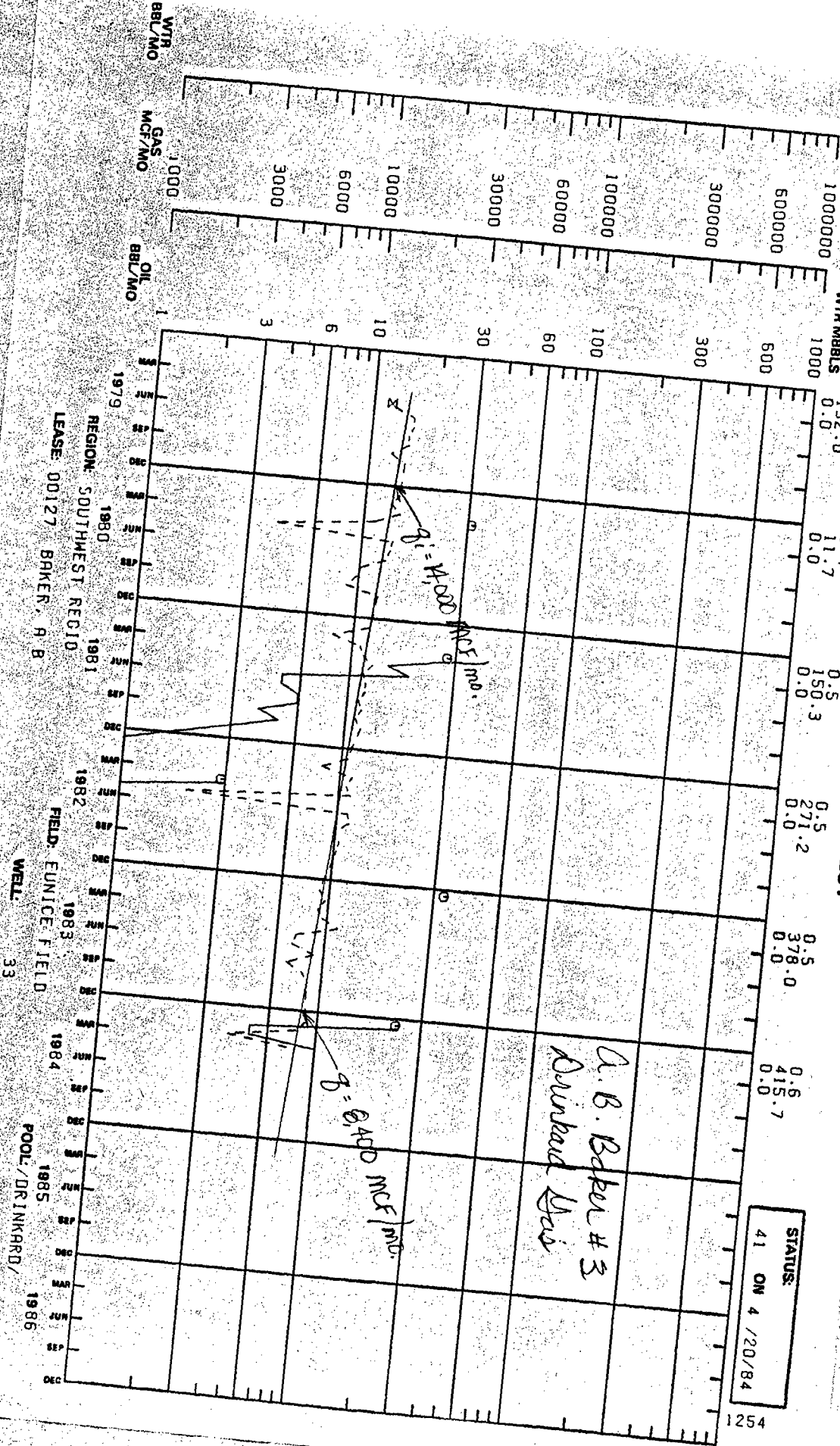
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PRODUCTION PLOT

STATUS:

41 ON 4 /20/84

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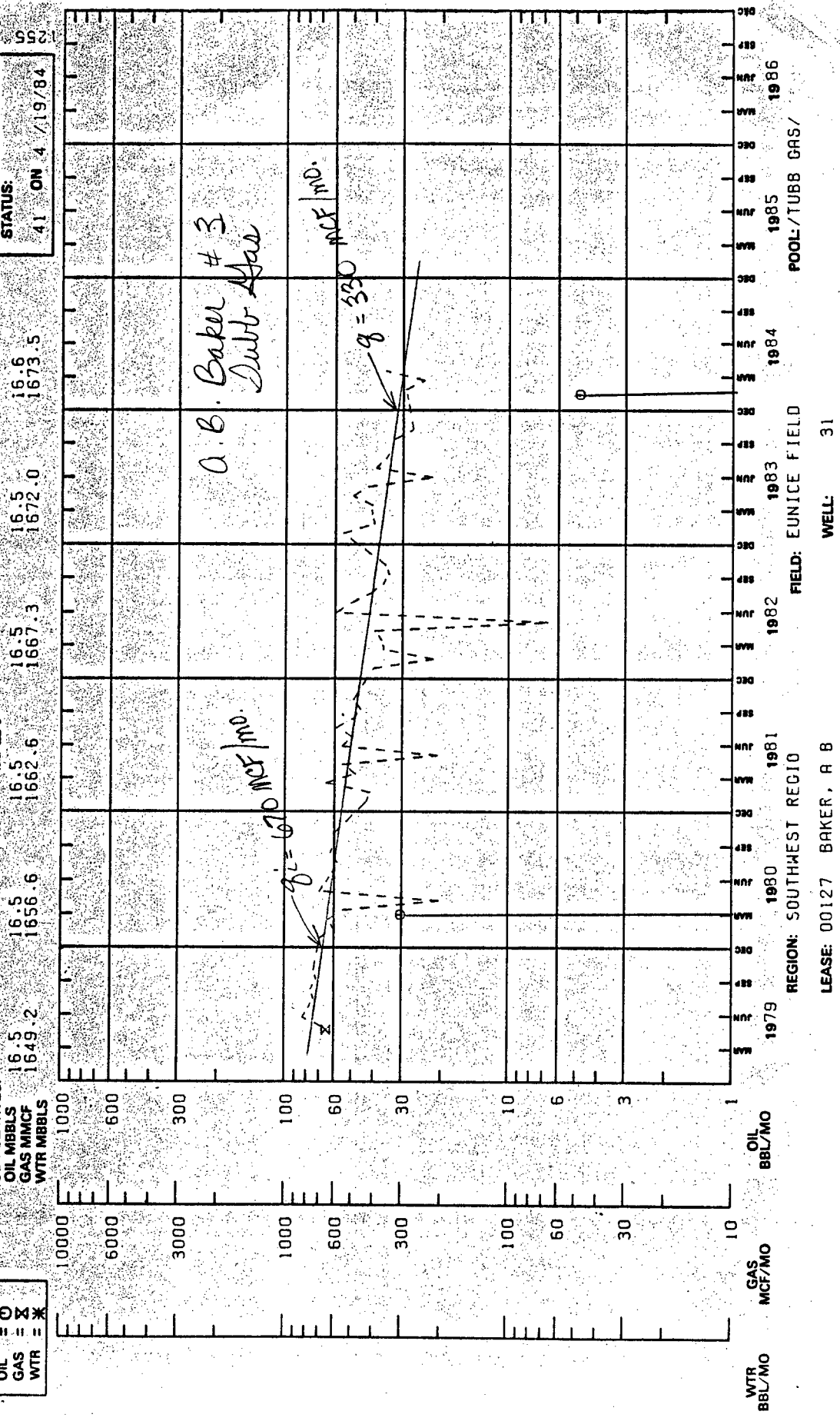


DATA CODES:
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PRODUCTION PLOT

CUMULATIVES:
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 GAS MMCF
 WTR MBBLs

STATUS:
 41 ON 4 / 19/84



REGION: SOUTHWEST REGIO
 FIELD: EUNICE FIELD
 POOL: TUBB GAS/
 LEASE: 00127 BAKER, A B
 WELL: 31



STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT
OIL CONSERVATION DIVISION
HOBBS DISTRICT OFFICE
August 30, 1984

TONEY ANAYA
GOVERNOR

POST OFFICE BOX 1980
HOBBS, NEW MEXICO 88240
(505) 393-6161

OIL CONSERVATION DIVISION
P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

RE: Proposed:

MC _____
DHC _____ X _____
NSL _____
NSP _____
SWD _____
WFX _____
PMX _____

Gentlemen:

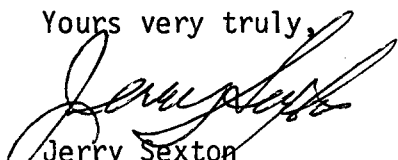
I have examined the application for the:

Amerada Hess Corp.	A. B. Baker	No. 4-P	10-22-37
Operator	Lease & Well No.	Unit	S-T-R

and my recommendations are as follows:

O.K.--J.S.

Yours very truly,


Jerry Sexton
Supervisor, District 1

/mc

OIL CONSERVATION DIVISION

SEP 04 1984

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