AMERADA HESS CORPORATION

AUG 27 1984
OIL CONSERVATION DIVISION
SANTA FE

P. O. DRAWER "D"
MONUMENT, NEW MEXICO 88265

State of New Mexico Energy and Minerals Department Oil Conservation Division P. O. Box 2088 Santa Fe, New Mexico 87501



Request to downhole commingle the Tubb/Drinkard and the Blinebry/Drinkard Gas Zones.

Dear Sir:

Amerada Hess Corporation is requesting approval for an exception to Rule 303-C to permit the downhole commingling of the Tubb and Drinkard gas zones in the A. B. Baker #3 and the Blinebry and Drinkard gas zones in the A. B. Baker #4. Permission to dually complete these wells was authorized by administrative orders MC-2085 and MC-2072, respectively.

In the A. B. Baker #3, the Tubb zone is perforated from 5960'-6135' and the Drinkard zone from 6205'-6404'. In 1984, both zones have made more fluid than in previous years and gas flow rates have decreased. If downhole permission to commingle is received this well will be placed on sucker rod pump to effectively lift formation fluids from the wellbore resulting in increased gas flow rates. The A. B. Baker #4 is perforated in the Blinebry zone from 5422'-5686' and in the Drinkard zone from 6220'-6473'. The Drinkard side of this wellbore is temporarily abandoned due to 1100' of fluid on the formation face which has killed the gas flow. Before the fluid encroachment the Drinkard zone was capable of producing 20,000 to 30,000 MCFPM. With the approval to downhole commingle, this well will also be placed on sucker rod pump to remove formation fluids. This will result in a significant increase in gas production from this wellbore.

Shut-in pressures from packer leakage tests and fluid levels revealed from acoustic well sounders were utilized to determine bottom hole pressures. These results are presented below.

	Baker Baker	Tubb Gas Drinkard	SBHP SBHP		
	Baker Baker	Blinebry Drinkard	SBHP SBHP		psia psia

These pressures are corrected to a common datum and the small pressure differences between zones indicate no crossflow problems will exist. Details of the method used to derive these figures is attached with this proposal.

The fluid characteristics of each zone are similar and there is no indication there will be incompatibility problems in the wellbore.

The value of the commingled production will not be less than the sum of the values of the individual streams since Amerada Hess is receiving \$1.10/MCF for the gas from all zones in consideration in both wellbores.

To figure the allocation of production to each zone, decline curves were used. This method revealed the following and details of it are attached.

Production Allocations To Each Zone:

	Baker Baker	Tubb Drinkard	4% 96%
	Baker Baker	Blinebry Drinkard	13% 87%

The ownership of the zones to be commingled is common with respect to working interest, royalty and overriding royalty.

All offset operators have been notified of this proposal by receipt of this recommendation. If you have any questions concerning this matter, please contact me.

Respectfully,

D. W. Holmes

D. W. Holmes Sr. Petroleum Engineer

AMERADA HESS CORPORATION Drawer "D" Monument, New Mexico 88265

Phone: (505-393-2144)

DWH/dg

Enclosures:

XC: Division Director (2)
Hobbs District Office
Offset Operators
File

OFFSET OPERATORS

Gulf Oil Gulf Building Midland, Texas 79702

Getty Oil Box 1231 Midland, Texas 79702

Marathon Box 552 Midland, Texas 79702

Exxon Company, USA Box 1600 Midland, Texas 79701

John H. Hendrix 525 Midland Tower Midland, Texas 79701

Sun Production Company Two Lincoln Centre Dallas, Texas 75240

Anadarko Production Co. Box 2497 Midland, Texas 79702

Sun Texas Co. 1700 One Main Place Dallas, Texas 75250

Robert L. Parker Eight East Third Tulsa, Oklahoma 74103

CALCULATION OF STATIC BOTTOM-HOLE PRESSURES

Equations To Be Used:

$$P_{sfs} = P_{whs} \times e^{c/\overline{z}}$$
 Where: $c = (\chi g)(TVD)$

P_{sfs} = Static sandface pressure, psia

 P_{whs} = Static wellhead pressure, psia

e = 2.7183

%g = Gas gravity

TVD = True vertical depth, feet

T = Average temperature, °R

 \overline{z} = Average compressibility factor

Assumptions:

$$P_{a,tm}$$
 = 13.025 psia
Temp. Grad. = 0.017 °F/ft.
Avg. Surf. Temp. = 60°F
 V_g = 0.70

A. B. Baker #3

Tubb Zone:

$$\chi_g = 0.70$$

 $P_{whs} = 310$ psia from pkr. leak. test
 $TVD = 6.048'$ (mid perfs.)
 $T = (60 + 103)(1 = 82°F = 542°R)$

$$c = \frac{(0.7)(6048)}{53.34(542)} = 0.146$$
 $P_{pc} = 668 \text{ psia}$
 $T_{r} = 542/390 = 1.39$
 $T_{pc} = 390^{\circ}R$

Assume:
$$P_{sfs} = 360 \text{ psia}$$
 $\overline{P} = (360 + 310) / 2 = 335 \text{ psia}$ $P_r = 335/668 = 0.50 \therefore \overline{z} = 0.938$ $P_{sfs} = (310) \text{ e} \frac{.146/.938}{.938} = 362 \text{ psia}$

Assume:
$$P = (362 + 310)/2 = 336 \text{ psia}$$

 $P_r = 336/668 = 0.50 \cdot \overline{z} = 0.938$
 $P_{sfs} = (310) e = 362 \text{ psia}$
 $P_{sfs} = 362 \text{ psia for Tubb zone}$

Drinkard Zone:

$$g = 0.70$$
 $P_{whs} = 200 \text{ psia from pkr. leak.test}$
 $TVD = 6305' \text{ (mid perfs.)}$
 $T = (60 + 107)/2 = 84^{\circ}F = 544^{\circ}R$
 $C = \frac{(0.7)(6305')}{53.34(544)} = 0.152$
 $P_{pc} = 668 \text{ psia}$
 $T_{pc} = 390^{\circ}R$
 $T_{pc} = 390^{\circ}R$
 $T_{pc} = 390^{\circ}R$
 $T_{pc} = 390^{\circ}R$
 $T_{pc} = 390^{\circ}R$

Assume:
$$P_{sfs} = 250 \text{ psia}$$
 $\overline{P} = (250 + 200)/2 = 225 \text{ psia}$ $P_{r} = 225/668 = 0.34$ $\therefore \overline{z} = 0.950$ $P_{sfs} = (200) \text{ e}^{-152/.95} = 235 \text{ psia}$

$$\overline{P}$$
 = (235+200)/2 = 218 psia
 P_r = 218/668 = 0.33 $\therefore \overline{z}$ = 0.960
 P_{sfs} = (200) e $\cdot \frac{152}{.96}$ = 234 psia

 P_{sfs} = 234 psia for Drinkard zone

To correct Tubb press. to common datum of 6305':

$$\overline{T} = (82 + 84)/2 = 83^{\circ}F = 543^{\circ}R$$

$$P_{pc} = 668 \text{ psia}$$
 $T_r = 543/390 = 1.39$

$$T_{pc} = 390^{\circ}R$$

$$c = \frac{(0.7)(257)}{53.34(543)} = 0.0062$$

Assume:

$$P_{sfs} = 365 \text{ psia}$$
 $\overline{P} = (365 + 362)/2 = 364 \text{ psia}$
 $P_r = 364/668 = 0.54$ $\therefore \overline{z} = 0.935$
 $P_{sfs} = (362)e^{.0062/.935} = 364 \text{ psia}$

 P_{sfs} = 364 psia for Tubb zone at common datum of 6305'

Tubb zone SBHP at 6305' = 364 psia Drinkard zone SBHP at 6305' = 234 psia

A. B. Baker #4

Blinebry Zone:

$$Y_g = 0.70$$
 $P_{whs} = 420 \text{ psia from pkr. leak. test}$
 $TVD = 5564' \text{ (mid perfs.)}$
 $T = (60 + 95)/2 = 78^{\circ}F = 538^{\circ}R$
 $C = \frac{(0.7)(5564)}{53.34(538)} = 0.136$
 $P_{pc} = 668 \text{ psia}$
 $T_{pc} = 390^{\circ}R$
 $T_{pc} = 390^{\circ}R$

Assume:
$$P_{sfs} = 470 \text{ psia}$$
 $\overline{P} = (470+420)/2 = 445 \text{ psia}$ $P_{r} = 445/668 = 0.67$ $\therefore \overline{z} = 0.918$ $P_{sfs} = (420) \text{ e} \cdot \frac{136}{.918} = 487 \text{ psia}$ Assume: $\overline{P} = (487 + 420)/2 = 454 \text{ psia}$ $P_{r} = 454/668 = 0.68$ $\therefore \overline{z} = 0.917$ $P_{sfs} = (420) \text{ e} \cdot \frac{136}{.917} = 487 \text{ psia}$ $P_{sfs} = 487 \text{ psia}$ for Blinebry zone

Drinkard Zone:

This gas zone has been TA'd since 1979. It is capable of producing gas at high volumes as long as formation fluids are removed from the wellbore. An acoustic well sounder has revealed 1073' of fluid in the hole. Using a 45°API oil gravity and 0 psi tubing pressure, the bottom hole static pressure in the Drinkard zone in this well is 376 psi.

To correct Blinebry press. to common datum of 6347'

$$\overline{T}$$
 = (78 + 108)/2 = 93°F = 553°R
 P_{pc} = 668 psia T_r = 553/390 = 1.42
 T_{pc} = 390°R
 $C = \frac{(0.7)(783)}{53.34(553)}$ = 0.019

Assume:

$$P_{sfs} = 500 \text{ psia}$$
 $\overline{P} = (500 + 487)/2 = 494 \text{ psia}$
 $P_r = 494/668 = 0.74$ $\therefore \overline{z} = 0.910$
 $P_{sfs} = (487) \text{ e}$ $\cdot 019/.910 = 497 \text{ psia}$

 P_{SfS} = 497 psia for Blinebry zone at common datum of 6347'.

Blinebry zone SBHP at 6347' = 497 psia Drinkard zone SBHP at 6347' = 376 psia

Allocation Of Production To Each Zone

A. B. Baker #3

Decline Rate Computations:

Tubb Zone

$$a_{\text{N}} = \frac{(57673367)}{4}$$

 $a_{\text{N}}(\text{Tubb}) = 0.17705/\text{yr}.$

t = 4 years

W(10DD) - 0.17700/3

Drinkard Zone

$$a_N = \ln \frac{(14,000/8,400)}{4}$$

 $a_N(Drink.) = 0.12771/yr.$

Tubb/Drinkard Combined

$$a_N = In \frac{(14,670/8,730)}{4}$$

 $a_{N(Comb.)} = 0.12976/yr.$

Actual Allocation:

$$0.12976 = (X)(0.17705) + (1-X)(0.12771)$$

 $0.12976 = (X)(0.17705) + (0.12771) - (X)(0.12771)$
 $0.00205 = (X)(0.04934)$

$$X = 0.04155$$

 $1-X = 0.95845$

Therefore:

Tubb Production Allocation = 4%
Drinkard Production Allocation = 94%

Allocation Of Production To Each Zone

A. B. Baker #4

Decline Rate Computations:

Blinebry Zone

 $\dot{t} = 4 \text{ years}$

Drinkard Zone

qi = 30,000 MCF/mo.

q = 23,700 MCF/mo.

t = 4 years

 $a_N = \ln \frac{(7,200/1,900)}{4}$

 $a_{N(Blin.)} = 0.33306/yr.$

 $a_{N(Drink.)} = 0.05893/yr.$

Blinebry/Drinkard Combined

t = 4 years

 $a_N = \ln (37,290/25,600)$

 $a_{N(Comb.)} = 0.09343/yr.$

Actual Allocation:

X = Blinebry zone

X-1 = Drinkard zone

0.09343 = (X)(0.33306) + (1-X)((0.05893)0.09343 = (X)(0.33306) + (0.05893) - (X)(0.05893)

0.03450 = (X)(.27413)

X = 0.12585

1-X = 0.87415

Therefore:

Blinebry Production Allocation = 13% Drinkard Production Allocation = 87%

Equations Used:

Decline Rates

$$a_N = \frac{qi/q}{t}$$

a_N = nominal decline, per yr.
qi = initial rate, MCF/mo.
q = later rate, MCF/mo.
t = time between rates, yrs.

Allocation

 $a_{N(Comb.)}$ = Combined decline rates

 $a_{N(Blin.)}$ = Blinebry decline rate

aN(Drink.) = Drinkard decline rate

OIL CONSERVATION DIVISION

ENERGY NO MINERALS DEPARTMENT STATE OF NEW MEXICO SANTA FE, NEW MEXICO 87501

Form C-116
Revised 10-1-78

GAS-OIL RATIO TESTS

OURING TEST O OIL GAS 0 3	Amerada Hess Corporation 'Amerada Hess Corporation	exico 88	3265	2	P∞I Blin	lebry	Blinebry (Pro Gas) T	TYPE	TYPE OF	Sch	Scheduled	County Lea	Comp	Complation		tp ac	\$5 ectat (X)
B. Baker 4 P 10 22-5 37-E 8-15-84 F 2" - 66 24 0 - 0 35		WELL		רסנ	ATION		DATEOF	rus	CHOKE		סאורא	. EN 67H	ס	ROD. D	, ,	1 1	6
B. Baker 4 P 10 22-S 37-E 8-15-84 F 2" - 66 24 0 - 0	r	NO.	c	s	4	Я	TEST	STAT	SIZE	PRESS.	ABLE ALLOW-	TEST	WATER	GRAV.	89L&	GAS M.C.F.	2
	₽.			10	22-5	37-E		77	2"	ı	66	24	0 .	ı	0	35	
											,						
	• •		•		•	***************************************								•			
		-					,		٠.					·			
								· · · · · · · · · · · · · · · · · · ·							1		

No well will be easigned an allowable greater than the amount of oil produced on the official test.

During gas-oil ratio test, each well shall be produced at a rate not exceeding the top unit allowable for the pool in which well is leasted by more than 23 percent. Operator is encouraged to take advantage of this 25 percent tolerance in order that well can be assigned. cacreesed allowables when sucherized by the Division.

will be 0.40. Cas volumes must be reperted in MCP measured at a pressure base of 15,025 pale and a temperature of 60° P. Specific gravity base

Report casing pressure in flew of tubing pressure for any well producing through casing.

Rule 101 and appropriate pool rules. Mail original and one copy of this report to the district office of the New Mexico Oil Conservation Division in accordance with

Sr. Petroleum Engineer ledge and belief. is true and complete to the best of my know-I hereby certify that the above information Signature)

(Due)

(Tide)

8-15-84

OIL CONSERVATION DIVISION P. O. BOX 2088

SANTA FE, NEW MEXICO 87501

ENERGY AND MINERALS DEPARTMENT STATE OF NEW MEXICO

GAS-OIL RATIO TESTS

Form C-116
Revised 10-1-78

Charles			1022	<u>-</u>			l			,						
Amerada Hess Corporation					Drinkand Cac	ה י			,	Allings	- 17					
Drawer "D", Monument, New Mexico 88265	xico 88	3265					1531 3441	(X)	SC	Scheduled	~ s	Carre			?	
	WELL		Loc	LOCATION		DATEOF		OIOX M	твс.	DAILY	. 64 67 11	g	PROD. DURING		TEST	GAS - OIL
LEASE XAME	х 0	c	ا. ا	4	20	TEST	3747			ALLOW-	TEST	WATER BBLS.	CRAV.	89L& 01L	GAS	RATIO CU.FT/BBL
A. B. Baker	ω	н .	10	22-S	37-E	8-15-84	π	2"	1	1	24	0	ı	.25	272	1,088,000
A. B. Baker	4	·P	. 10	22-S	37-E	8-15-84	П	2"	! ! !	 	zor	zone TA'd	!		 - - - - -	
· .		<u></u>										·-··	•		•	
								·.								
											······································					

No well will be essigned an allowable greater than the amount of all produced on the official test.

Dwing gas-oil rolle test, each well shall be produced at a role not exceeding the top unit allowable for the pool in which well is located by more than 25 percent. Operator is encouraged to take advantage of this 25 percent tolerance in order that well can be assigned. sacreased allowables when susherized by the Division.

will be 0.60. Gas volumes must be reperted in MCP measured at a pressure base of 15,025 pala and a temperature of 60° P. Specific gravity base

Report cosing pressure in lieu of tubing pressure for any well producing through casing.

Rule 101 and appropriate pool rules. Mail original and one copy of this report to the district office of the New Mexico Oil Conservation Division in accordance with

> ledge and belief. is true and complete to the best of my know-I hereby certify that the above information

Petroleum Engineer

(Tide)

8-22-84

(Date)

ENERGY WO MINERALS DEPARTMENT STATE OF NEW MEXICO

SANTA FE, NEW MEXICO 87501

Form C-116 Revised 10-1-78

GAS-OIL RATIO TESTS

LEASE NAME	LEASE NAME	S		·		P∞I Tut	оь (Т	Tubb (Pro Gas)		Y P E	0.7		County	Lea				
LEASE NAME WELL NO. U S T A TEST I SIZE PRESS. ABLE WATE B. Baker 3 I 10 22-S 37-E 8-15-84 F 2" - 9 24 0	LEASE NAME WELL LOCATION DATE OF CHOKE TBG. DAILY COMMENT TEST SIZE PRESS. ABLE WATE WATE	er "D",	Mexico 8	3265					4-	TEST - ()		Sche	duled		Comp	,Jelioi	$\dot{\Box}$	
B. Baker NO. U S T A TEST SIZE PRESS. ALLOW: VATER ABLE HOUSE BBLS.	B. Baker 3 I 10 22-S 37-E 8-15-84 F 2" - 9 24 0		₩ELL		ך	CATIO	O		DATEOF		CHOKE	TBG.		. 674	ט	ROD.	ا ہا	PROD. DURING
B. Baker 3 I 10 22-S 37-E 8-15-84 F 2" - 9 24 0	B. Baker 3 I 10 22-S 37-E 8-15-84 F 2" - 9 24 0	L M ASM N AMM	N O	c	5			2	TEST			PRESS.	ALLOW-	TEST HOURS	WATER	CRAV.		88L%
B. Baker 3 I 10 22-S 37-E 8-15-84 F 2" - 9 24 0	B. Baker 3 I 10 22-S 37-E 8-15-84 F 2" - 9 24 0			•														
		8	, ω	н	10	22-		37-E	8-15-84	П	2"	1	φ	24	0	. ,		0
		٠.			-		•	····			·							
					~				-		• .							
			•			· · · · · · · · · · · · · · · · · · ·	·											

No well will be easigned an allowable greater than the amount of oil produced on the official test.

sacreased allowables when authorized by the Division. During gas-oil ratio test, each well shall be produced at a rate not exceeding the top unit allowable for the pool in which well to located by more than 25 percent. Operator is encouraged to take advantage of this 25 percent tolorance in order that well can be assigned.

will be 0.40. Cas volumes must be reported in MCF measured at a pressure base of 15,025 pala and a temperature of 60° F. Specific gravity base

Report casing pressure in lieu of tubing pressure for any well producing through casing.

Rule 101 and appropriate pool rules. Mail original and one copy of this report to the district office of the New Mexico Oli Conservation Division in accordance with

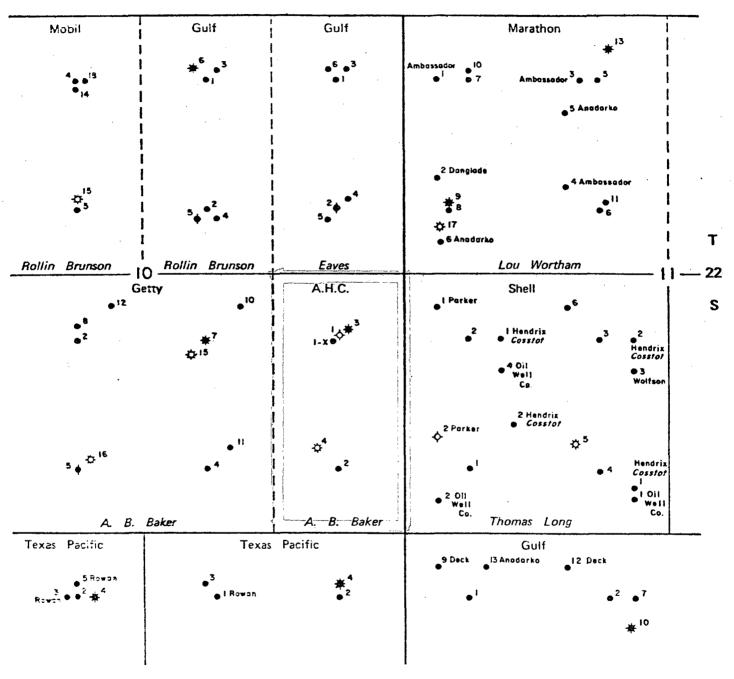
> ledge and belief. is true and complete to the best of my know-I hereby certify that the above information

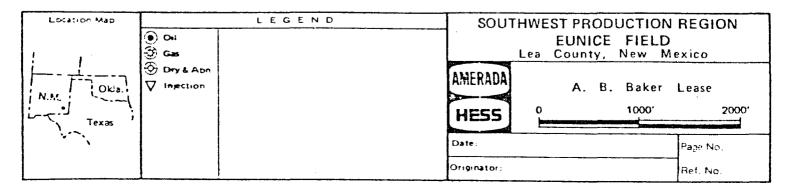
(Signature)

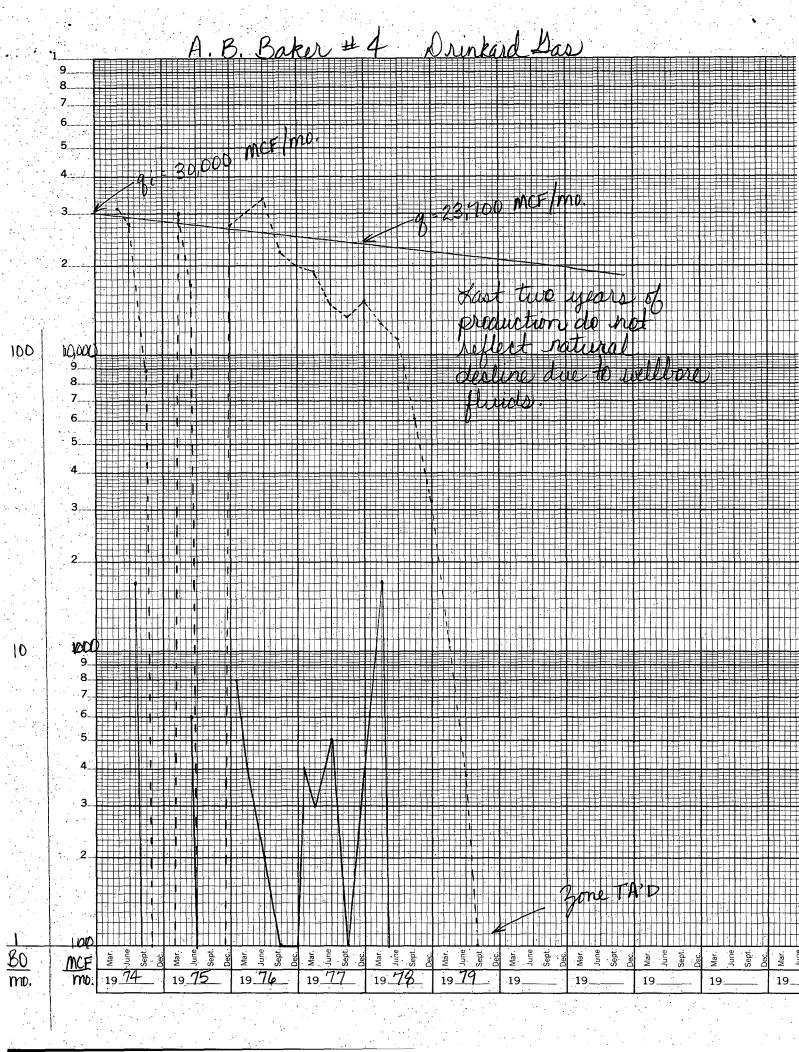
Sr. Petroleum Engineer (Tide)

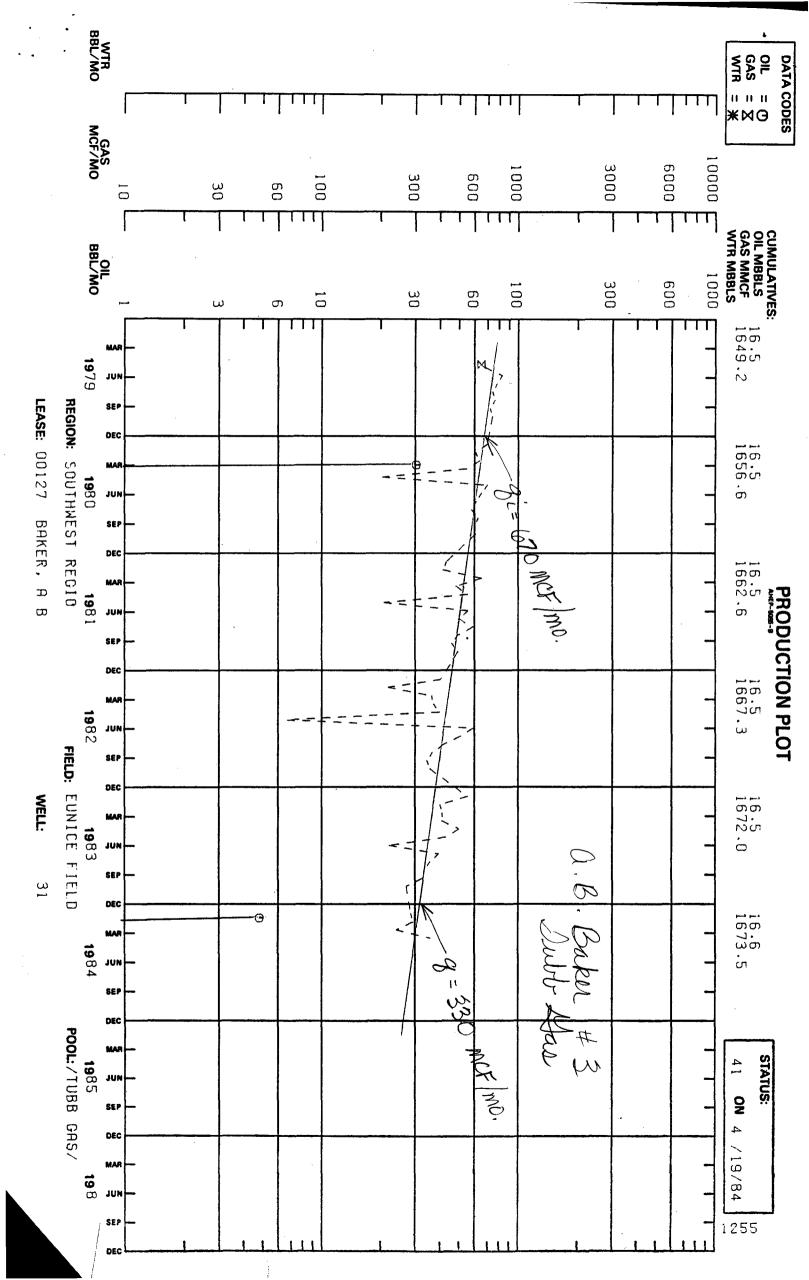
8-15-84

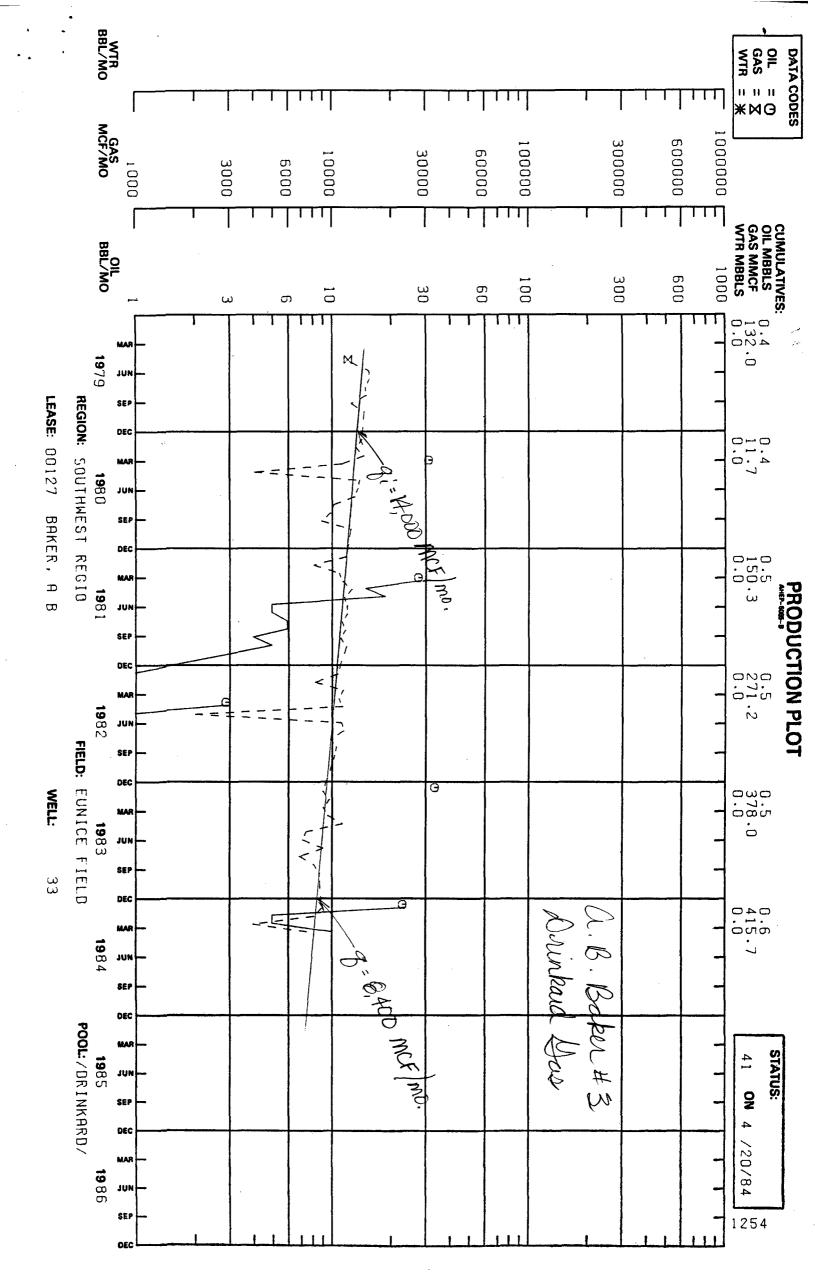
(DEC)

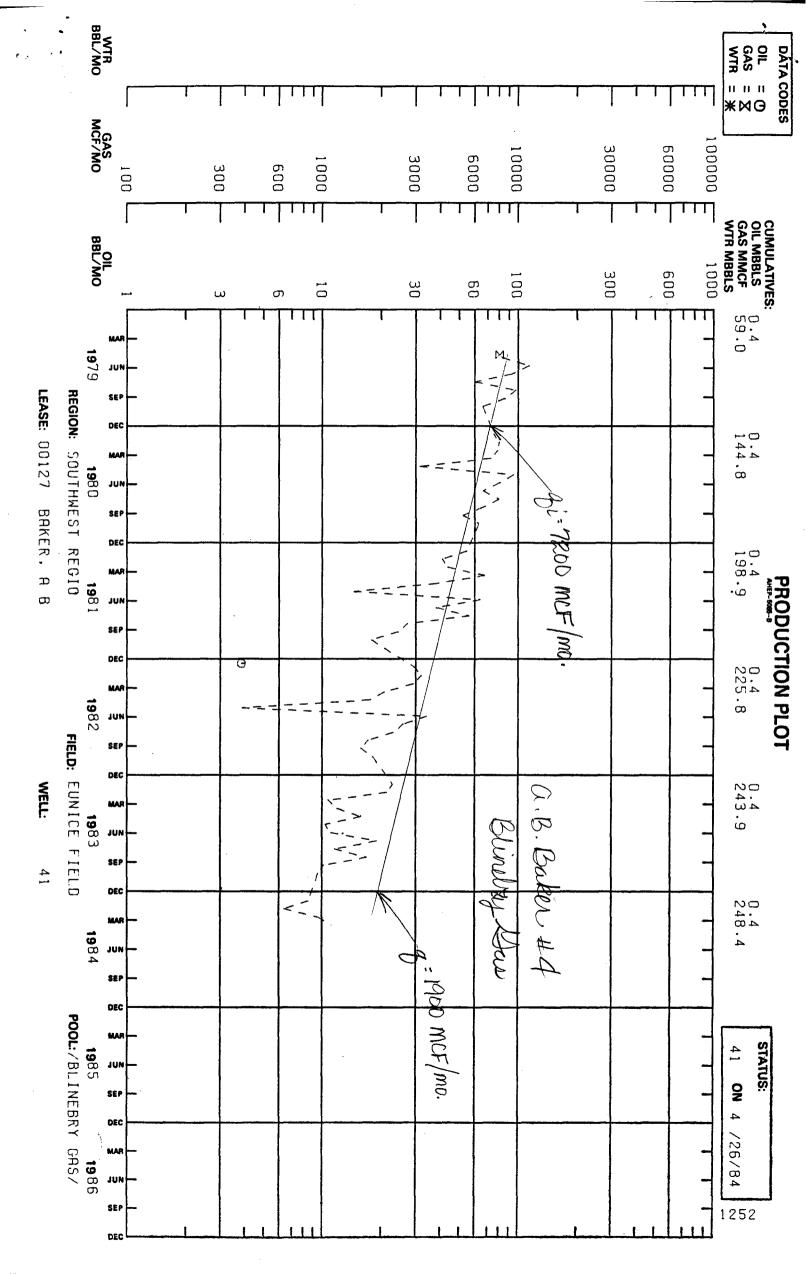














STATE OF NEW MEXICO

ENERGY AND MINERALS DEPARTMENT

OIL CONSERVATION DIVISION HOBBS DISTRICT OFFICE

August 31, 1984

TONEY ANAYA GOVERNOR

V3

POST OFFICE BOX 1980 HOBBS, NEW MEXICO 88240 (505) 393-6161

SANTA FE, NEW MEXICO 8750 RE: Proposed: MC DHC X	D1 		OIL COMS	ERVATION -
NSL NSP SWD WFX PMX			RECEN	ERVATION DIVISION
Gentlemen:	•			
I have examined the appl	ication for the:			
Amerada Hess Corp.	A. B. Baker	No. 3-I	10-22-37	
Operator	Lease & Well	No. Unit	S-T-R	
and my recommendations a	re as follows:			
0.KJ.S.	v			

Yours very truly, Jerry Sexton Supervisor, District 1	<u>/</u>	,		
/mc				