

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2/11/72	
Company Amoco Production Company			Connection None		
Pool Wildcat			Formation Tubb		Unit API #30-021-20021
Completion Date 2/11/72		Total Depth 2670		Plug Back TD 2660	Elevation 4993 RDB
Csg. Size 4-1/2"	Wt. 9.5#	d 4.090	Set At 2670'	Perforations: From 2407 To 2661	
Tbg. Size 2-3/8"	Wt. 4.7#	d 1.995	Set At 2408	Perforations: From Open End To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2376	
Producing Thru 2-3/8" Tbg		Reservoir Temp. °F 87°		Mean Annual Temp. °F 60°	
Baro. Press. - P _a 13.2		State New Mexico			
L 2408	H 2408	G _g 1.5194	% CO ₂ 99.92	% N ₂ 0.08	% H ₂ S 0
Prover -		Meter Run 4.00"		Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w hg	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
1.	4"	1"	13.2	16.5	50	188	50	Pkr.	Pkr.	1.5 hr.
2.	4"	1"	13.2	25	58	151	58	Pkr.	Pkr.	1.0 hr.
3.	4"	1"	13.2	42	60	113	60	Pkr.	Pkr.	1.0 hr.
4.	4"	1.5"	13.2	19	62	76	62	Pkr.	Pkr.	1.0 hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	366.1	-	13.2	1.0098	0.6284	1.000	232
2	463.4	-	13.2	1.0019	0.6284	1.000	295
3	650.6	-	13.2	1.000	0.6284	1.000	409
4	908.2	-	13.2	0.9931	0.6284	1.000	570
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.0123	510	0.9307	1.000	Dry gas	Dry gas	1.5194 (CO₂)	X X X X X X X X	1073	548
2	0.0123	513	0.9452	1.000						
3	0.0123	520	0.9489	1.000						
4	0.0123	522	0.9525	1.000						
5										

P_c **366.2*** P_c² **134.1** From Curve, Q = 1000 MCFD, P_c² - P_w² = **85.5**
 (1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{134.1}{134.1 - 85.5} = 1.553$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.856$

NO.	P _t ²	P _w ²	P _w ²	P _c ² - P _w ²
1		324.2	105.1	29.0
2		312.2	97.5	36.6
3		297.2	83.3	45.6
4		220.2	78.5	55.6
5				

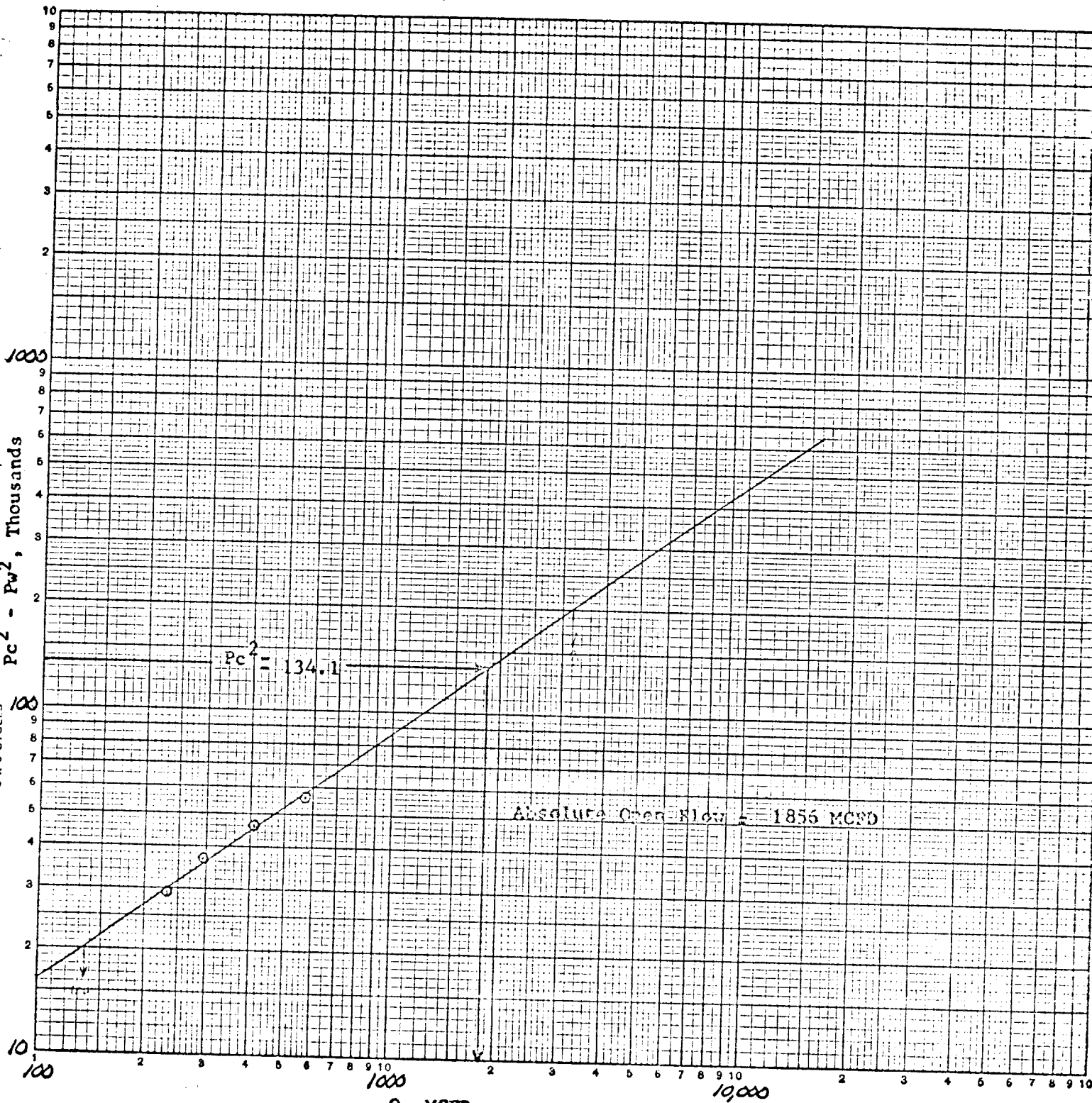
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1856$

Absolute Open Flow 1856 Mcfd @ 15.025		Angle of Slope θ	1.375
* P _c and P _w measured with bottom hole pressure recorder			
Remarks:			

Approved By Commission:	Conducted By: Thompson	Calculated By: J. E. York	Checked By: E. J. Snook
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Amoco Production Company
 State "EN" Well No. 1
 J-23-20N-33E
 Harding County
 2/11/72

LOG-ARTIFICIAL 359-120
 KEUFFEL & ESSER CO. MADE IN U.S.A.
 3 X 3 CYCLES



$Q = 3200$ MCFD
 $Q_2 = 135$ MCFD

$\log Q_1 = 3.50515$
 $\log Q_2 = 2.13033$

$N = 1.37482 \quad 1.375$