NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special — Test Date: 4-19-85

Company: Amoco Production Company	Connection:		
Pool: Carbon Dioxide Gas Unit Bravo Dome 640 acre area	Formation: Tubb		Unit: BDCDGU
Completion Date: 11-9-83	Total Depth: 2668	Plug Back TD: 2660	Elevation: 4933
Farm or Lease Name:			
Csg. Size: 7" / Wt.: 20 / d: / Set At: 2668	Perforations: From 2355 To 2534		Well No.: 2033 241G
Tbg. Size: 3.5 / Wt.: 9.3 / d: / Set At: 2343	Perforations: From To		Unit: G / Sec.: 24 / Twp.: 20 / Rge.: 33
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 2312		County: Harding
Producing Thru: Tubing	Reservoir Temp. °F: 90° @ 2445	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.2
			State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2445	2445	1.529	100	0	0		4.0	Flange

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					310				
1.	4.026 x 1.875	240	23	63	252.2	50			24 hr.
2.	4.026 x 1.875	240	22	61	252.2	50			24 hr.
3.	4.026 x 1.875	267	11	60	279.2	50			24 hr.
4.	4.026 x 1.875	301	3	57	313.2	50			24 hr.
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							1037
3.							1037
4.							765
5.							397

NO.	P_r	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: 0 Deg.
Specific Gravity Separator Gas: 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 1072 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 547 R ____ R

P_c 322.2 P_c^2 103.813

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		252.2		40.208
2		252.2		40.208
3		279.2		26.860
4		315.2		5.719
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.58$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.59$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1650$

Absolute Open Flow 1650 Mcfd @ 15.025 Angle of Slope θ ____ Slope, n .49

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		D. D. Kimble	