

NEW MEXICO OIL CONSERVATION COMMISSION MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date										
Company Amoco Production Company		Connection										
Pool Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area		Formation										
Completion Date 11-7-85	Total Depth 2683	Plug Back TD 2653	Elevation 5022									
Csg. Size 7	Wt. 20	Set At 2683	Perforations: From 2395 To 2624									
Tbg. Size 3-1/2	Wt. 9.3	Set At 2256	Perforations: From To									
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 2225	Unit BDCDGU									
Producing Thru Tubing	Reservoir Temp. °F 90 @ 2510	Mean Annual Temp. °F 50	Baro. Press. - P _a 12.25									
L 2510	H 2510	G _g 1.529	% CO ₂ 100									
		% N ₂ 0	% H ₂ S 0									
Prover		Meter Run 4.0	Taps Flange									
FLOW DATA												
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w '	Temp. °F	TUBING DATA Press. p.s.i.g.	Temp. °F	CASING DATA Press. p.s.i.g.	Temp. °F	Duration of Flow		
1.	4.026 x 3.000		184.0	30	47	307						
2.	4.026 x 3.000		160.5	39	48	196.25	47			1.5		
3.	4.026 x 3.000		135.0	54	47	172.75	48			1.5		
4.	4.026 x 3.000		106.0	81	44	147.25	47			1.5		
5.						118.25	44			1.5		
RATE OF FLOW CALCULATIONS												
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd					
1.												
2.												
3.							3150					
4.							3500					
5.							3746					
							3972					
NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature	P.S.I.A.	P.S.I.A.
1.					0							
2.							1.529		1072	496		
3.												
4.												
5.												
$P_c = 319.2$ $P_w^2 = 101.888$												
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.16$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.11$							
1.		196		63.473	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4409$							
2.		172		72.304								
3.		147		80.280								
4.		118		87.965								
5.												
Absolute Open Flow					4409 Mcfd @ 15.025							
Remarks:					Angle of Slope θ Slope, n .71							
Approved by Commission:					Conducted By:							
					Calculated By: Don Kimble							
					Checked By:							