NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 6-26-87	
Company: Amoco Production Company			Connection:		
Pool: Bravo Dome			Formation: Tubb		Unit: BDCDGU
Completion Date: 9-18-79	Total Depth: 2488		Plug Back TD: 2485	Elevation: 4749	Farm or Lease Name:
Csg. Size: 4.50 / Wt.: 9.5 / d: 4.1	Set At: 2488		Perforations: From 2261 To 2444		Well No.: 1934-231K
Tbg. Size: 2.375 / Wt.: 4.6 / d: 1.995	Set At: 2261		Perforations: From To		Unit: K / Sec.: 23 / Twp.: 19 / Rge.: 34
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 2261		County: Union
Producing Thru: Tubing	Reservoir Temp. °F: 90	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25		State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
			100	0	0		4.0	Flange

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							309		0		24 hrs
1.	4.026	x	2.750	187	20	56	185	56	0		24 hrs
2.	4.026	x	2.750	196	14	58	195	58	0		24 hrs
3.	4.026	x	2.750	206	12	58	204	58	0		24 hrs
4.	4.026	x	2.750	219	9	58	219	58	0		24 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							
2.							2221
3.							1969
4.							1844
5.							1683

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: 1.529 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 1072 P.S.I.A. P.S.I.A.
Critical Temperature: 496 R R

P_c 321.25 P_c^2 103,201

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		197.25	38.907	64,294
2		207.25	42,952	60,249
3		216.25	46,764	56,437
4		231.25	53,476	49,725
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.6051$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.5467$

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3435$

Absolute Open Flow: 3435 Mcfd @ 15.025 | Angle of Slope θ: 42.67 | Slope, n: .9218

Remarks: Test was run from a low flowing tubing pressure to a high flowing tubing pressure to minimize liquid loading effects.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	RANDY MAHANNAH	RICHARD ROETH	