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**EPA FALL-OFF  
TEST**

**DATE:**

**2017**

**2017 ANNUAL BOTTOM-HOLE PRESSURE SURVEY  
AND PRESSURE FALLOFF TEST REPORT**  
**NAVAJO REFINING**

MEWBOURNE WELL NO. 1  
Artesia, New Mexico

December 2017

Houston, TX



Project No. 192080A

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## CERTIFICATION STATEMENT

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this document and all attached documents, and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe that the submitted information is true, accurate, and complete.

I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Client: Navajo Refining Company  
Well Name: Mewbourne Well No. 1  
Test Dates: June 16 – 21, 2017

Name: Ted L. Jose  
Title: Project Engineer

Phone Number: 281-589-5900

Signature



New Mexico Professional Engineer  
License No. 23819

Date Signed

12/20/18



## EXECUTIVE SUMMARY

WSP USA Inc. (WSP) was contracted by Navajo Refining Company (Navajo) to perform a pressure falloff test and bottom-hole pressure survey on Navajo's Mewbourne Well No. 1. The test was performed according to New Mexico Oil Conservation Division (OCD) falloff test guidelines (*New Mexico Oil Conservation Division UIC Class I Well Fall-Off Test Guidance, December 3, 2007*).

The test provides the state regulatory agency with the necessary information to access the validity of requested or existing injection well permit conditions and satisfy the permitting objective of protecting the underground sources of drinking water (USDW). Specifically, 40 CFR Part 146 states “the Director shall require monitoring of the pressure buildup in the injection zone annually, including at a minimum, a shutdown of the well for a time sufficient to conduct a valid observation of the pressure fall-off curve” (40 CFR§146.13 for Non-hazardous Class I Wells).

The falloff testing was conducted according to the testing plan submitted to and approved by the NM OCD. The testing plan stated that, all offset wells that inject into the injection interval would be shut-in for the duration of the test period. The testing consisted of a 54-hour injection period and a 40-hour falloff period. Bottom-hole pressure gauges were also placed in the offset wells Gaines Well No. 3 and Chukka Federal Well No. 2. These wells are owned by Navajo and are used to inject plant waste into the same intervals as the Mewbourne Well No. 1.

As prescribed by the guidelines, the report discusses supporting and background information in Sections 1 through 9. The one mile area of review (updated since the 2016 falloff testing) is discussed in Section 10 and geology in Section 11. Information on the offset wells is discussed in Section 12, daily testing activities in Section 13, and point of shut-in, in Section 14. The pressure falloff testing and analysis results are discussed in Section 15. The OCD required record keeping statement is discussed in Section 16.

## **1. FACILITY INFORMATION**

- a. Name: Navajo Refining Company (subsidiary of the Holly Corporation)
- b. Facility Location: Highway 82 East, Artesia, New Mexico 88211
- c. Operator's Oil and Gas Remittance Identifier (OGRID) Number: 223518

## **2. WELL INFORMATION**

- a. OCD UIC Permit Number: UIC-CLI-008-1
- b. Well Classification: Class I Non-hazardous
- c. Well Name and Number: Mewbourne Well No. 1
- d. API Number: 30-015-27592
- e. Well Legal Location: 660 FSL, 2310 FEL

## **3. CURRENT WELLBORE SCHEMATIC**

The Mewbourne Well No. 1 wellbore schematic is presented in Figure 1. The schematic has all data as requested by the guidelines and includes the following:

- a. Tubing: 4 ½ inch, 11.6 pound per foot, steel construction, API grade N-80, with long thread connections (LT&C).
- b. Packer: Arrow X-1, 7 inch by 3 ½ inch set in tension at 7879 feet.
- c. Tubing Length: 7879 feet. There are no profile nipples in the tubing or the packer as this was not a requirement of the permit.
- d. Size, Type, and Depth of Casing: There are three casing strings in the well. The information for these casing strings was obtained from OCD records on file with the state and geophysical logs. The casing strings are:
  - i. 13 3/8 inch, 48 pound per foot (lb/ft), steel construction, API grade J-55, with short thread connections (ST&C), set at a depth of 390 feet. The casing was cemented to the surface with 525 sacks of cement. The casing was set in open hole with a diameter of 17.5 inches. This information was obtained from OCD records.
  - ii. 9 5/8 inch, 36 lb/ft, steel construction, API grade J-55, ST&C, set at a depth of 2555 feet. The casing was cemented to the surface with 1000 sacks of cement. The casing was set in open hole with a diameter of 12.25 inches. This information was obtained from OCD records.

- iii. 7-inch, 26 lb/ft and 29 lb/ft, steel construction, API grade N-80 and P-110, LT&C, set at a depth of 9094 feet. The casing was cemented to surface in two stages with 1390 sacks of cement. The casing was set in open hole with a diameter of 8.75 inches. The top cement was verified with a CBL run on July 23, 1998. The remainder of the information was obtained from OCD records.
- iv. A cement plug at 9004 feet isolates the lower section of the original borehole. This information was obtained from OCD records.
- e. The top of cement was determined from a CBL run in the 7-inch casing string on July 23, 1998. The top of cement in the 7 inch casing was found at the surface. The top of cement in the 9 5/8 inch and 13 3/8 inch casing strings was verified through OCD records and volume calculations.
- f. The 7 inch casing was perforated on July 24 and July 27, 1998. The casing was perforated with a 0.5 inch diameter hole at 2 shots per foot on a 60° phasing. The perforations are located between 7924 feet and 8188 feet and from 8220 feet to 8476 feet.
- g. The total depth of the well is 10,200 feet with the plug back depth at 9004 feet. On June 21, 2017, fill was tagged at 9001 feet.

#### **4. ELECTRIC LOG ENCOMPASSING THE COMPLETED INTERVAL**

The dual induction log is presented in Appendix A and encompasses the completed interval between 7924 feet and 8476 feet. The dual induction log was submitted to the OCD with the original permit after the well was drilled by the Mewbourne Oil Company. The log was resubmitted to the OCD when the well was re-permitted as a Class I injection well.

#### **5. RELEVANT PORTIONS OF THE POROSITY LOG USED TO ESTIMATE FORMATION POROSITY**

The neutron density log is presented in Appendix B and encompasses the completed interval between 7924 feet and 8476 feet. The neutron density log was submitted to the OCD with the original permit after the well was drilled by Mewbourne Oil Company. The log was resubmitted to the OCD when the well was re-permitted as a Class I injection well. The porosity of the formation, 10%, and the reservoir thickness, 175 feet, were determined from this log. These values were used in the analysis of the pressure falloff data (Section 15). Additional information concerning the geology of the injection reservoir is discussed in Section 11.

## 6. PVT DATA OF THE FORMATION AND INJECTION FLUID

The Mewbourne Well No. 1 was recompleted in July 1998, prior to the issuance of the current well testing guidelines (December 3, 2007). At the time, no directives were in place to test formation fluids or derive formation characteristics from cores. However, reservoir fluid samples were obtained during the recompletion and the average density and average total dissolved solids (TDS) were measured at 1.03 g/l and 26,500 mg/l, respectively. The analytical results of the analysis of the formation fluid are summarized in Table I.

The viscosity of the formation fluid, formation water compressibility, and total system compressibility were estimated in reference to bottom-hole temperature using industry accepted correlations. These correlations are found in the Society of Petroleum Engineer's "Advances in Well Test Analysis, Monograph Volume 5" and "Pressure Buildup and Flow Tests in Wells, Monograph Volume 1".

a. Estimation of formation fluid and reservoir rock compressibility:

The fluid compressibility of the formation brine was estimated for a sodium chloride solution (26,500 mg/l) at the bottom-hole temperature of 127°F using Appendix C (Figure D.16 SPE Monograph 5). This value was  $2.9 \times 10^{-6}$  psi<sup>-1</sup>. The formation pore volume compressibility was estimated using Appendix D (Figure G.5 SPE Monograph 1). This value was  $5.5 \times 10^{-6}$  psi<sup>-1</sup>. The total system compressibility is the sum of the fluid compressibility and the pore volume compressibility,  $8.4 \times 10^{-6}$  psi<sup>-1</sup>. The temperature used with the correlations was recorded during the temperature survey conducted in the Mewbourne Well No. 1 on July 23, 1998, and included in this report as Appendix E.

b. Formation fluid viscosity with reference temperature:

The formation fluid had a TDS concentration of 26,500 mg/l. This equates to an approximate equivalent percentage of NaCl of 4.5%. The average viscosity of the formation fluid was estimated using Appendix F (Figure D.35 SPE Monograph 5). This value was 0.57 centipoise (cp) at 127°F.

c. Formation fluid specific gravity/density with reference temperature:

The average formation fluid density was measured at 1.03 g/l at 70°F (Table I).

d. Injection fluid specific gravity, viscosity and compressibility with reference temperature:

The specific gravity of the refinery waste water during the injection portion of the reservoir testing was 1.002 (8.35 pounds per gallon). Using the same methodology described above, the viscosity of the injected fluid was 0.54 cp at 127°F. The compressibility of the injected plant waste was  $2.9 \times 10^{-6}$  psi<sup>-1</sup> at 127°F.

## **7. DAILY RATE HISTORY DATA (MINIMUM OF ONE MONTH PRECEDING THE FALLOFF TEST)**

The rate history used in the analysis of the pressure falloff data began on April 26, 2017 and ends on June 19, 2017. The daily rate history is summarized in Appendix G.

## **8. CUMULATIVE INJECTION INTO THE FORMATION FROM TEST WELL AND OFFSET WELLS**

The total volume of fluid injected into all three wells as of June 19, 2017, was 3,548,540,301 gallons. The volume of fluid injected into the Mewbourne Well No. 1 was 1,738,561,012 gallons. The volume of fluid injected into the Chukka Well No. 2 was 1,151,453,666 gallons. The volume of fluid injected into the Gaines Well No. 3 was 658,525,622 gallons. The injected volumes were obtained from plant records.

## **9. PRESSURE GAUGES**

One (1) downhole pressure gauge (with two readings) was used for the Mewbourne Well No. 1 buildup and falloff testing. The downhole pressure gauge was set at 7924 feet. Bottom-hole pressure gauges were also placed in each of the offset wells: Gaines Well No. 3 and Chukka Well No. 2. The pressure gauges were set at 7660 feet in the Gaines Well No. 3 and at 7570 feet in the Chukka Well No. 2.

- a. Describe the type of downhole surface pressure readout gauge used including manufacture and type:

In the Mewbourne Well No. 1, an MRO pressure gauge was used to record the pressure and temperature data during the injection/falloff testing. The gauge was a sapphire crystal gauge. The manufacturer of the MRO pressure gauge (Serial No. SP-21359Q) is Spartek Systems.

In the Gaines Well No. 3, an MRO pressure gauge was used to monitor the bottom-hole pressure and temperature during the testing of the Mewbourne Well No. 1. The gauge was a sapphire crystal gauge with Serial No. DC-1463. The gauge is manufactured by DataCan.

In the Chukka Well No. 2, an MRO pressure gauge was used to monitor the bottom-hole pressure and temperature during the testing of the Mewbourne Well No. 1. The gauge was a sapphire crystal gauge with Serial No. SP-21726. The gauge is manufactured by Spartek Systems.

- b. List the full range, accuracy and resolution of the gauge:

In Mewbourne Well No. 1, the MRO pressure gauge, Serial No. SP-21359Q has a full range of 15 psi to 16,000 psi, an accuracy of 0.050% of full scale, and a resolution of 0.01% of full scale. A surface pressure gauge was not installed during testing.

In Gaines Well No. 3, the MRO pressure gauge, Serial No. DC-1463 has a full range of 15 psi to 15,000 psi, an accuracy of 0.014% of full scale, and a resolution of 0.01% of full scale.

In Chukka Well No. 2, the MRO pressure gauge, Serial No. SP-21726, has a full range of 15 psi to 16,000 psi, an accuracy of 0.020% of full scale, and a resolution of 0.01% of full scale.

- c. Provide the manufacturer's recommended frequency of calibration and a calibration certificate showing date the gauge was last calibrated:

The certificate of calibration for each of the pressure gauges used during the testing are included as Appendix H. The manufacturer's recommended calibration frequency is one year.

## **10. ONE MILE AREA OF REVIEW (AOR)**

Federal Abstract Company was contracted by WSP and instructed to undertake a review of well changes made within a one-mile area of review (AOR) of the Mewbourne Well No. 1, Chukka Well No. 2, and Gaines Well No. 3. In 2009, an update of the original AOR, submitted with the Discharge Application Permit 2003, was completed within the one-mile AOR for all three wells. The current update includes all existing wells within the one-mile AOR and any changes that have occurred to these wells since the 2016 update.

No new fresh water wells were reported within the search area since the submittal of the 2016 report. The discharge application lists the water wells located in the Area of Review.

- a. Identify wells located within the one mile AOR:

Table II contains a listing of all wells within the one-mile AOR of Mewbourne Well No. 1, Chukka Well No. 2, and Gaines Well No. 3. Figure 6 is a Midland Map Company base map of the area containing the one mile AOR.

- b. Ascertain the status of wells within the one mile AOR:

Table II also contains a listing of all wells within the one-mile AOR, with their current status. Tables III through VII contain a list of all wells within the one-mile AOR that have had modifications to the current permit or have had new drilling and/or completion permits issued since the 2016 pressure falloff report.

Thirty-eight (38) wells were found in which the owner had changed. Fourteen (14) new wells were plugged and abandoned. Sixteen (16) wells were placed in temporarily abandoned status. No wells were found that were returned to production status. Two (2) wells were found that had been recompleted.

There were fourteen (14) new drills and permits to drill, of which none penetrated the Wolfcamp interval. All plugged and abandoned wells were successfully plugged and isolated from the Mewbourne Well No. 1, Chukka Well No. 2, and Gaines Well No. 3 injection intervals according to current OCD records.

- c. Provide details on any offset producers and injectors completed in the same interval:

Navajo has two other injection wells that inject into the same interval. Mewbourne Well No. 1 is listed as ID No. 59 in Table II and no changes have occurred to this well. Chukka Well No. 2 is listed as ID No. 120 in Table II and no changes have occurred to this well. The Gaines Well No. 3 is listed as ID No. 861 in Table II. The wellbore schematics for the Gaines Well No. 3 and Chukka Well No. 2 are presented as Figure 3 and Figure 4, respectively.

## 11. GEOLOGY

The injection zones are porous carbonates of the lower portion of the Wolfcamp Formation, the Cisco Formation, and the Canyon Formation. These formations occur in the Mewbourne Well No. 1, the Chukka Well No. 2, and the Gaines Well No. 3 at the depths shown in the table below.

Injection Zone Formation	Mewbourne Well No. 1 (KB = 3,693 ft)		Chukka Well No. 2 (KB = 3,623 ft)		Gaines Well No. 3 (KB = 3,625 ft)	
	MD below KB (ft)	SS Depth (ft)	MD below KB (ft)	SS Depth (ft)	MD below KB (ft)	SS Depth (ft)
Lower Wolfcamp	7450	-3757	7270	- 3647	7303	-3678
Cisco	7816	-4123	7645	- 4022	7650	-4025
Canyon	8,475	-4,782	8,390	- 4767	8390	-4765
Base of Injection Zone (base of Canyon)	9016	-5323	8894	- 5271	8894	-5269

d. Description of the geological environment of the injection interval:

The lower portion of the Wolfcamp Formation (Lower Wolfcamp) is the shallowest porous unit in the proposed injection interval. The Wolfcamp Formation (Permian-Wolf campain age) consists of light brown to tan, fine to medium-grained, fossiliferous limestones with variegated shale interbeds (Meyer, 1966, page 69). The top of the Wolfcamp Formation was correlated for this study to be below the base of the massive, dense dolomites of the overlying Abo Formation. The base of the Wolfcamp coincides with the top of the Cisco Formation. The thickness of log porosity greater than 5% in the entire Wolfcamp Formation ranges from 0 feet to 295 feet in a band three miles wide that trends northeast-southwest across the study area.

The Cisco Formation (Pennsylvanian-Virgilian age) of the Northwest Shelf is described by Meyer (1966, page 59) as consisting of uniform, light colored, chalky, fossiliferous limestones interbedded with variegated shales. Meyer (1966, page 59) also describes the Cisco at the edge of the Permian basin as consisting of bio thermal (mound) reefs composed of thick, porous, coarse-grained dolomites. Locally, the Cisco consists of porous dolomite that is 745 feet thick in Chukka Well No. 2, 659 feet thick in Mewbourne Well No. 1, and 720 feet in Gaines Well No. 3. The total thickness of intervals with log porosity greater than 5% is approximately 310 feet in Mewbourne Well No. 1, 580 feet in Chukka Well No. 2, and 572 feet in Gaines Well No. 3. The total thickness with log porosity greater than 10% is approximately 100 feet in Mewbourne Well No. 1, 32 feet in Chukka Well No. 2, and 65 feet in Gaines Well No. 3. The thickness of the porous intervals in the Cisco ranges from 0 feet in the northwestern part of the study area to nearly 700 feet in a band three miles wide that trends northeast-southwest.

The Canyon Formation (Pennsylvanian-Missourian age) consists of white to tan to light brown fine grained, chalky, fossiliferous limestone with gray and red shale interbeds (Meyer, 1966, page 53). Locally, the Canyon occurs between the base of the Cisco dolomites and the top of the Strawn Formation (Pennsylvanian-Desmoinesian age). The total thickness of intervals with log porosity greater than 5% is 34 feet in Mewbourne Well No. 1, 30 feet in Chukka Well No. 2, and 10 feet in Gaines Well No. 3. No intervals appear to have log porosity greater than 10% in any of the three injection wells.

e. Discuss the presence of geological features, i.e., pinchouts, channels, and faults, if applicable:

From the geological study completed and submitted in the Discharge Plan Application and Application for Authorization to Inject, the reservoir appears to be continuous, with the possibility of anisotropic conditions extending to the west-southwest. The injection intervals that were studied are well confined by the Abo and Yeso low porosity carbonate beds, Tubbs shale, and Salado salt. The Cisco and Wolfcamp formations follow the Vacuum arch and have a southeasterly dip. No faults existed in the study area although, the study also shows that faulting occurs via the K-M fault located 6 miles northwest of Artesia and trends northeast-southwest. The distance to this fault line occurs no closer than 16 miles. No faults are known to exist in the confining zone within the AOR.

- f. Provide a portion of relevant structure map, if necessary:

The structure map for Strawn is presented as Appendix I. The structure map for the Wolfcamp presented as Appendix J. The structure map for the Cisco is presented as Appendix K.

## **12. OFFSET WELLS**

There are only four offset wells identified in the AOR that inject into the same interval: The Federal No. 1, the Chalk Bluff Federal Com No. 3, the Gaines Well No. 3 and the Chukka Well No. 2.

- a. Identify the distance between the test well and any offset well completed in the same injection interval:

The Mewbourne Well No. 1 (test well) is approximately 7900 feet from Gaines Well No. 3. The Chukka Well No. 2 is approximately 10,860 feet from the Mewbourne Well No. 1.

- b. Report the status of the offset wells during both the injection and shut-in portions of the test:

Both the Gaines Well No. 3 and Chukka Well No. 2 were shut-in approximately 25 hours after the start of the buildup portion of the testing and remained shut in through the remainder of the testing. Bottom-hole pressure gauges were lowered into each well approximately 75 hours before shutting in the Mewbourne Well No. 1. The bottom-hole pressure and temperature data are graphically depicted in Figure 5 for the Gaines Well No. 3 and Figure 2 for the Chukka Well No. 2.

- c. Describe the impact, if any, the offset wells had on the testing:

The offset wells were shut in on June 18, 2017 and remained shut in during the final portion of the buildup period and during the falloff portion of the testing.

## **13. CHRONOLOGICAL LISTING OF THE DAILY TESTING ACTIVITIES (OPERATIONS LOG)**

Appendix L contains the formal Chronology of Field Activities. This chronology was developed from the field activity reports.

- a. Date of the testing:

The buildup portion of the testing started at 1000 hours on June 17, 2017 and continued until June 19, 2017 at 1558 hours when the Mewbourne Well No. 1 was shut-in. The falloff test ended on June 21, 2017 at 0801 hours. The total depth of the well was tagged at 9001 feet and five-minute gradient stops were made while pulling the pressure gauges out of the wellbore. After the pressure gauges were pulled out of the well on June 21, 2017, the well was turned over to Navajo plant operations personnel.

- b. Time of the injection period:



The buildup portion of the testing began on June 17, 2017 when the injection rate was set at an average injection rate of approximately 141 gallons per minute (gpm). The injection rate was held constant for 54 hours.

c. Type of injection fluid:

The injected fluid was non-hazardous waste water from the plant. The density of the injection fluid averaged 8.35 pounds per gallon during the 54-hour injection period.

d. Final injection pressure and temperature prior to shutting in the well:

The final flowing pressure ( $P_{wf}$ ) and temperature ( $T_{wf}$ ) were 4722.74 psia and 100.42°F, respectively.

e. Total shut-in time:

The Mewbourne Well No. 1 was shut-in for 40.23 hours.

f. Final static pressure and temperature at the end of the fall-off portion of the test:

The final static pressure at 7924 feet was 4368.41 psia. The final temperature was 104.20°F.

#### **14. DESCRIBE THE LOCATION OF THE SHUT-IN VALVE USED TO CEASE FLOW TO THE WELL FOR THE SHUT-IN PORTION OF THE TEST**

On the pipeline to the Mewbourne Well No. 1, there are two, 4 inch motor controlled valves installed on the incoming pipeline before the pod filters. Two 4 inch valves are installed between the pod filters and the wellhead. There is one 6 inch valve installed in the main line between the pod filters and the booster pump. A 4 1/16 inch wing valve is installed on the wellhead. All valves were closed during the falloff portion of the testing. A diagram of the wellhead is shown in Figure 7 and a diagram of the valve locations are shown in Figure 8.

#### **15. PRESSURE FALLOFF ANALYSIS**

The following discussion of the analysis of the pressure data recorded during the falloff testing of the Mewbourne Well No. 1 satisfies Sections 15 through 19 of Section IX, Report Components, of the OCD's falloff test guidelines. Where appropriate, the specific guideline addressed is annotated. Specific parameters used in the equations and discussed previously in this report are also annotated. The plots included with this report are summarized in Table VIII. The inclusion of these plots in this report satisfies OCD Guideline Section IX.18.

The pressure data obtained during the falloff test were analyzed using the commercially available pressure transient analysis software program PanSystem©. Appendix M contains the output from this software program. Figure 9 shows the pressure data recorded by the bottom-hole pressure gauge from the time the tool was in place through the 40.23 hour total shut-in period. Figure 10 shows the pressure and temperature data recorded by the bottom-hole pressure gauge from the time the tool was in place through the 40.23 hour falloff shut-in period. Figure 11 is a Cartesian plot of the injection rates versus time for the injection period used in the pressure falloff analysis. The superposition time function was used to account for all rate changes during the injection period used in the analysis of the data. Figure 12 is a plot of the historical injection rates and surface pressures versus calendar time.

Figure 13 is a log-log diagnostic plot of the falloff data, showing change in pressure and pressure derivative versus equivalent shut-in time. The different flow regimes, wellbore storage, radial flow and change in reservoir characteristics, are indicated on the log-log plot and the superposition Horner plot (OCD Guideline Section IX.18.c and IX.18.d)

Wellbore storage begins at 0.008 hours and continues to an elapsed shut in time of 0.090 hours. Radial flow begins at an elapsed shut in time of 10.08 hours and continues until 14.92 hours (OCD Guideline Section IX.15.b).

The reservoir permeability was determined from the radial flow region of the superposition semi-log plot, Figure 14. The radial flow regime begins at a Superposition time of 107.35 and continues until a Superposition time of 72.97 at which time the pressure data departs the semi-log straight-line. Figure 15 shows an expanded view of the radial flow regime. The slope of the radial flow period, as calculated by the analysis software, was 6.12611 psi/cycle (OCD Guideline Section IX.15.c). The injection rate just prior to shut in was 138.98 gpm which is equivalent to 4764.91 barrels per day (bbl/day).

An estimate of mobility-thickness (transmissibility, OCD Guideline Section IX.15.d),  $kh/\mu$ , for the reservoir was determined to be 126,471 md-ft/cp using the following equation:

$$\frac{k h}{\mu} = 162.6 \frac{q B}{m}$$

where,

- |          |   |  |
|----------|---|--|
| $kh/\mu$ | = | formation mobility-thickness, millidarcy-feet/centipoise |
| $q$      | = | rate prior to shut in, bpd                               |
| $B$      | = | formation volume factor, reservoir volume/surface volume |
| $m$      | = | slope of radial flow period, psi/cycle                   |

$$\frac{kh}{\mu} = 162.6 \frac{(4764.91)(1.0)}{6.12611}$$

$$= 126,471 \text{ md-ft/cp}$$

The permeability-thickness (flow capacity, OCD Guideline Section IX.15.i), kh, was determined to be 72,088 md·ft by multiplying the mobility-thickness, kh/μ, by the viscosity of the reservoir fluid (see Section 6), μ<sub>reservoir</sub>, of 0.57 centipoise (cp):

$$kh = \left( \frac{kh}{\mu} \right) \mu_{\text{reservoir}}$$

$$= (126,471)(0.57)$$

$$= 72,088 \text{ md-ft}$$

The reservoir permeability (OCD Guideline Section IX.15.e) using the total thickness (see Section 5 and Section 11) of 175 feet was 412 md:

$$k = \frac{kh}{h}$$

$$= \frac{72,088}{175}$$

$$= 412 \text{ md}$$

To determine whether the proper viscosity was used in arriving at this permeability, the travel time for a pressure transient to pass beyond the waste front needs to be calculated (OCD Guideline Section VIII.5). The distance to the waste front is determined from the following equation:

$$r_{\text{waste}} = \left( \frac{0.13368 V}{\pi h \phi} \right)^{1/2}$$

where,

r <sub>waste</sub>	=	radius to waste front, feet
V	=	total volume injected into the injection interval, gallons
h	=	formation thickness, feet
φ	=	formation porosity, fraction
0.13368	=	constant

A cumulative volume of approximately 1,738,561,012 gallons of waste has been injected into Mewbourne Well No. 1 (see Section 8). The formation has a porosity of 0.10 (see Section 5 and Section 11).

The distance to the waste front was determined to be 2056 feet:

$$r_{\text{waste}} = \left( \frac{(0.13368)(1,738,561,012)}{(\pi)(175)(0.10)} \right)^{1/2}$$

$$= 2056 \text{ feet}$$

The time necessary for a pressure transient to traverse this distance is calculated from the following equation:

$$t_{\text{waste}} = \frac{948 \phi \mu_{\text{waste}} c_t r_{\text{waste}}^2}{k}$$

where,

$t_{\text{waste}}$	=	time for pressure transient to reach waste front, hours
$\phi$	=	formation porosity, fraction
$\mu_{\text{waste}}$	=	viscosity of the waste at reservoir conditions, centipoise
$r_{\text{waste}}$	=	radius to waste front, feet
$c_t$	=	total compressibility of the formation and fluid, psi
$k$	=	formation permeability, millidarcies
948	=	constant

The pore volume compressibility is  $8.4 \times 10^{-6} \text{ psi}^{-1}$  (see Section 6). The viscosity of the waste fluid is 0.54 cp. The time necessary for a pressure transient to traverse the distance from the wellbore to the leading edge of the waste front would be 4.41 hours:

$$t_{\text{waste}} = \frac{948 (0.10)(0.54)(8.4 \times 10^{-6})(2056^2)}{412}$$
$$= 4.41 \text{ hours}$$

Since the time required to pass through the waste is less than the 10.08 hours required to reach the beginning of the radial flow period, the assumption that the pressure transient was traveling through reservoir fluid during the period of the semi-log straight line was correct.

The near wellbore skin damage (OCD Guideline Section IX.15.f) was determined from the following equation:

$$s = 1.151 \left[ \frac{p_{wf} - p_{1hr}}{m_1} - \log \left( \frac{k}{\phi \mu c_t r_w^2} \right) + 3.23 \right]$$

where,

s	=	formation skin damage, dimensionless
1.151	=	constant
p <sub>wf</sub>	=	flowing pressure immediately prior to shut in, psi
p <sub>1hr</sub>	=	pressure determined from extrapolating the first radial flow semi-log line to a Δt of one hour, psi
m <sub>1</sub>	=	slope of the first radial flow semi-log line, psi/cycle
k	=	permeability of the formation, md
φ	=	porosity of the injection interval, fraction
μ	=	viscosity of the fluid the pressure transient is traveling through, cp
c <sub>t</sub>	=	total compressibility of the formation plus fluid, psi <sup>-1</sup>
r <sub>w</sub>	=	radius of the wellbore, feet
3.23	=	constant

The final measured flowing pressure was 4722.74 psia. The pressure determined by extrapolating the radial flow semi-log line to a Δt of one hour, p<sub>1hr</sub>, was 4378.16 psia (calculated from the analysis software). The wellbore radius, r<sub>w</sub>, is 0.3646 feet (completion records). Using these values in addition to the previously discussed parameters results in a skin of 57.17:

$$s = 1.151 \left[ \frac{4722.74 - 4378.16}{6.12611} - \log \left( \frac{412}{(0.10)(0.57)(8.4 \times 10^{-6})(0.3646^2)} \right) + 3.23 \right]$$

$$= 57.17$$

The change in pressure, Δp<sub>skin</sub>, in the wellbore associated with the skin factor (OCD Guideline Section IX.15.g) was calculated using the following equation:

$$\Delta p_{skin} = 0.869(m)(s)$$

where,

0.869	=	constant
m	=	slope from superposition plot of the well test, psi/cycle
s	=	skin factor calculated from the well test

The change in pressure, Δp<sub>skin</sub>, using the previously calculated and defined values was determined to be 304.35 psi:

$$\Delta p_{\text{skin}} = 0.869(m)(s)$$

$$= 0.869(6.12611)(57.17)$$

$$= 304.35 \text{ psi}$$

The flow efficiency (E, OCD Guideline Section IX.15.h) was determined from the following equation:

$$E = \frac{p_{\text{wf}} - \Delta p_{\text{skin}} - p_{\text{static}}}{p_{\text{wf}} - p_{\text{static}}}$$

where,

E = flow efficiency, fraction

$p_{\text{wf}}$  = flowing pressure prior to shutting in the well for the fall-off test,

$p_{\text{static}}$  = final pressure from the pressure falloff test

$\Delta p_{\text{skin}}$  = pressure change due to skin damage

Using the previously determined parameters, the flow efficiency was calculated to be 0.14:

$$E = \frac{4722.74 - 304.35 - 4368.41}{4722.74 - 4368.41}$$

$$= 0.14$$

The radius of investigation (OCD Guideline Section IX.15.a) was calculated using the following equation:

$$R_{\text{inv}} = 0.029 \sqrt{\frac{k \Delta t_s}{\phi \mu G}}$$

where,

k = formation permeability, millidarcies

$\Delta t_s$  = elapsed shut-in time, hours

$\phi$  = formation porosity, fraction

$\mu$  = viscosity of the fluid the pressure transient is traveling through, cp

$c_t$  = total compressibility of the formation plus fluid,  $\text{psi}^{-1}$

0.029 = constant

The radius of investigation,  $r_{\text{inv}}$ , using the previously defined values was determined to be 5409 feet:

$$R_{inv} = 0.029 \sqrt{\frac{(414)(40.23)}{(0.10)(0.57)(8.4 \times 10^{-6})}}$$

$$R_{inv} = 5409 \text{ feet}$$

As indicated on Figure 13, the pressure data departs the radial flow region at an elapsed time from shut in of 14.92 hours. No pressure or temperature anomalies were noted that would cause this type of pressure response observed on the derivative log-log plot (OCD Guideline Section VIII.9). A review of the geology of the injection zones (see Section 11) indicates that all three of the formations in which the Mewbourne Well No. 1 injects into have varying thicknesses and porosities within the mapped area. Changes in formation thickness, porosity, and fluid viscosity can cause the slope changes seen on the derivative log-log plot. Because these changes occurred during the duration of the pressure falloff test, the reservoir analysis results are considered heterogeneous as opposed to homogeneous (OCD Guideline Section IX.17.b).

The Hall plot (OCD Guideline Section IX.18.h) is presented as Figure 16. No slope changes are seen in the plotted data.

A comparison of the current analysis results with previous analysis results as well as with the reservoir parameters submitted with the permit application is presented in Table IX (OCD Guideline Section IX.19).

On June 21, 2017, a static pressure gradient survey was conducted while pulling the pressure gauges out of the well. Static gradient stops were conducted at 7924 feet, 7000 feet, 6000 feet, 5000 feet, 4000 feet, 3000 feet, 2000 feet, 1000 feet, and at the surface. The bottom-hole pressure and temperature, after 40.23 hours of shut-in at 7924 feet, were 4368.41 psia and 104.21°F, respectively. The gradient survey is summarized in Table X. The data are graphically depicted in Figure 17.

## **16. NEW MEXICO OIL CONSERVATION DIVISION THREE YEAR RECORDING KEEPING STATEMENT**

Navajo will keep the raw test data, generated during the testing, on file for a minimum of three years. The raw test data will be made available to OCD upon request.

## TABLES

**TABLE I**  
**FORMATION WATER ANALYSIS SUMMARY**

Chemical	Mewbourne Well No. 1	Chukka Well No. 2	Gaines Well No. 3	Average
Date	July 31, 1998	June 14, 1999	Nov 8, 2006	
Fluoride (mg/l)	2.6	9.7	Not Detected	6.15
Chloride (mg/L)	19,000	15,000	10,447	14,815.67
NO <sub>3</sub> -N (mg/L)	<10	<10	--	<10
SO <sub>4</sub> (mg/L)	2,200	2000	1,908	2,036
CaCO <sub>3</sub> (mg/L)	1000	1210	--	1105
Specific Gravity (g/L)	1.034	1.0249	--	1.0295
TDS (mg/L)	33,000	20,000	--	26,500
Specific Conductance (uMHOs/cm)	52,000	43,000	--	47,500
Potassium (mg/L)	213	235	85.5	177.83
Magnesium (mg/L)	143	128	155	142
Calcium (mg/L)	390	609	393	464
Sodium (mg/L)	12,770	8,074	6,080	8,974.67
pH (s.u.)	8.1	7.2	--	7.65

*The data in the above table was referenced from “Discharge Plan Application and Application for Authorization to Inject per Oil Conservation Division Form C-108, into Class I Wells WDW-1 and Proposed WDW-2 and WDW-3” and the “Discharge Permit Approval Conditions”, “Reentry and Completion Report Waste Disposal Well No. 2”, and “Reentry and Completion Report Waste Disposal Well No. 3”.*

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit No.	TOWNS Sect	HIP	TOWNS	WELL	TYPE	PLUG DATE	STATUS	DATE - Comp or PLUG	
				RNG NS Ftg		EW FTG	WELL NAME				
1	30-015-00693	A	36 175	27E	330N	330E	GEORGE A CHASE & C SERVICE	0	T/A	8/30/1941	
2	30-015-00694	A	36 175	27E	990N	990E	DELHI #013	0	P&A	6/24/1948	
3	30-015-00646	A	36 175	27E	990N	330E	DELHI #007	0	T/A	4/21/1950	
4	30-015-00688	G	36 175	27E	1650N	2310E	SOUTH RED LAKE GRAYBURG UNIT #010	0	SHUT-IN	12/6/1947	
5	30-015-00650	G	36 175	27E	1830N	2205E	CONKLIN #002	0	ACTIVE	3/6/1949	
6	30-015-00667	G	36 175	27E	2310N	2310E	SOUTH RED LAKE GRAYBURG UNIT #011	0	ACTIVE	3/23/1949	
7	30-015-00666	G	36 175	27E	2310N	2310E	CONKLIN #001	0	ACTIVE	3/23/1949	
8	30-015-00659	H	36 175	27E	1650N	330E	GATES STATE #001	0	P&A	1/10/1942	
9	30-015-00647	H	36 175	27E	1650N	990E	GATES STATE #002	0	ACTIVE	8/4/1950	
10	30-015-00659	H	36 175	27E	2310N	330E	HOMAN #001	0	ACTIVE	10/21/2003	
11	30-015-00688	I	36 175	27E	2310S	330E	RAMAPO #001	0	ACTIVE	5/6/2008	
12	30-015-00670	I	36 175	27E	2970N	330E	RAMAPO #003	0	ACTIVE	10/28/1941	
13	30-015-00687	I	36 175	27E	2310S	990E	RAMAPO #002	0	N/A	1/3/1950	
14	30-015-00685	I	36 175	27E	1650S	330E	EMPIRE ABO UNIT #020	0	ACTIVE	5/7/1948	
15	30-015-00671	J	36 175	27E	2310S	2310E	RAMAPO #003	0	ACTIVE	7/10/1989	
16	30-015-01221	J	36 175	27E	2300S	2300E	SOUTH RED LAKE GRAYBURG UNIT #023	0	ACTIVE	1/24/2000	
17	J	J	36 175	27E	27E	DOOLEY STATE #43	BP AMERICA PRODUCTION COMPANY	0	ZONE ABAN	8/13/2002	
18	30-015-00534	J	36 175	27E	1650S	1650E	EMPIRE ABO UNIT #019A	0	ACTIVE	1/24/2000	
19	30-015-01220	K	36 175	27E	2310S	2330W	SOUTH RED LAKE GRAYBURG UNIT #022	0	ACTIVE	2/13/1942	
20	30-015-00674	K	36 175	27E	2310S	2330W	RAMAPO #002	0	ACTIVE	2/27/1948	
21	30-015-01219	K	36 175	27E	2310S	1650W	SOUTH RED LAKE GRAYBURG UNIT #021	0	ACTIVE	4/2/1961	
22	30-015-23913	K	36 175	27E	1650S	1650W	SOUTH RED LAKE GRAYBURG UNIT #043	0	ACTIVE	2/26/1961	
23	K	K	36 175	27E	1650S	DOOLEY STATE #03	MARTIN YATES III	0	ACTIVE	2/3/1949	
24	30-015-00673	K	36 175	27E	1650S	2310W	RAMAPO #001	0	ACTIVE	5/15/1947	
25	30-015-00682	N	36 175	27E	990S	1650W	RAMAPO #004	0	ACTIVE	1/24/2000	
26	30-015-00683	N	36 175	27E	965S	1650W	SOUTH RED LAKE GRAYBURG UNIT #028	0	ACTIVE	1/24/2000	
27	30-015-01218	N	36 175	27E	330S	2310E	EMPIRE ABO UNIT #018	0	ACTIVE	4/16/1948	
28	30-015-00694	O	36 175	27E	990S	STATE B-65961 NO. 1-A	BURNHAM OIL COMPANY	0	ACTIVE	3/11/2009	
29	30-015-01251	O	36 175	27E	660S	1980E	EMPIRE ABO UNIT #019	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	5/13/1947
30	I	I	36 175	27E	330S	990E	EMPIRE ABO UNIT #020	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	5/8/1959
31	30-015-00677	P	36 175	27E	330S	990E	BLAKE STATE #001	4/10/2009	P&A	4/13/2009	
32	30-015-01616	P	30 175	28E	330S	990E	APACHE CORPORATION	0	ACTIVE	3/7/1953	
33	30-015-01638	A	31 175	28E	330N	990E	STATE NO. 1	7/15/1952	P&A	7/15/1952	
34	30-015-21594	B	31 175	28E	330N	1650E	POWCO STATE #001	0	ACTIVE	11/15/1975	
35	30-015-01636	C	31 175	28E	330N	2310E	DELHI STATE NO. 1	0	P&A	12/23/1952	
36	30-015-25621	B	31 175	28E	980N	1620E	POWCO STATE #002	0	ACTIVE	7/15/1986	
37	30-015-01633	I	31 175	28E	330N	330W	ASTON & FAIR A #001	0	ACTIVE	6/23/1942	
38	30-015-01634	D	31 175	28E	350N	345W	STATE 31 NO. 1X	0	ACTIVE	1/5/1946	
39	30-015-01645	F	31 175	28E	990N	990W	BEDINGFIELD STATE 1 NO. 1	0	P&A	2/16/1950	
40	30-015-02666	2	31 175	28E	2310N	330W	HUDSON SAIKIN STATE #001	0	NO COMPL	5/29/1948	
41	30-015-24887	2	31 175	28E	2310N	990W	HUDSON SAIKIN STATE #002	2/16/1950	P&A	7/7/1984	
42	30-015-01643	F	31 175	28E	2310N	2260W	EMPIRE ABO UNIT #022	0	ACTIVE	6/7/1960	
43	30-015-01635	F	31 175	28E	2310N	2310W	ASTON & FAIR #001Y	0	ACTIVE	5/8/1948	
44	30-015-01637	G	31 175	28E	2310N	2310E	MALCO STATE #001	0	ACTIVE	10/22/1953	
45	30-015-01652	G	31 175	28E	2288N	1625E	BOILING #001	0	ACTIVE	8/10/1960	
46	30-015-10537	H	31 175	28E	2277N	330E	NORTHWEST ARTESIA UNIT #004	0	ACTIVE	9/17/2003	
47	30-015-10833	I	31 175	28E	1980S	660E	NORTHWEST ARTESIA UNIT #010	0	ACTIVE	4/10/1960	
48	30-015-01644	I	31 175	28E	1650S	330E	EMPIRE ABO UNIT #024A	6/12/2009	P&A	6/17/1966	
49	30-015-01642	J	31 175	28E	1650S	STATE FV #001	GEORGE A CHASE JR DBA G AND C SERVICE	0	ACTIVE	4/29/1960	
50	30-015-01650	J	31 175	28E	1650S	1625E	KERSEY & CO	0	ACTIVE	12/23/1962	
51	30-015-01651	K	31 175	28E	1650S	LIME ROCK RESOURCES A, L.P.	LIME ROCK RESOURCES A, L.P.	0	ACTIVE	9/17/2003	
52	30-015-01640	3	31 175	28E	2310S	330W	EMPIRE ABO UNIT #002	0	ACTIVE	7/16/1955	
53	30-015-01648	3	31 175	28E	1651S	1089E	EMPIRE ABO UNIT #021A	0	ACTIVE	8/24/2002	
54	30-015-01639	4	31 175	28E	990S	330W	RAMPO #001	0	ACTIVE	5/1/1948	
55	30-015-01647	4	31 175	28E	660S	EMPIRE ABO UNIT #021	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	1/31/1960	

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	TOWNS			WELL	TYPE	PLUG DATE	STATUS	DATE - Comp or PLUG
		No.	Sect	HIP					
56	30-015-01646	N	31	175	28E 660S	EMPIRE ABO UNIT #022A	P&A	1/22/1960	1/22/1960
57	30-015-01618	N	31	175	28E 766S	STATE FX #001	ACTIVE	3/1/1963	3/1/1963
58	30-015-01653	O	31	175	28E 990S	PARKER-STATE NO. 1	P&A	1/18/1942	1/18/1942
59	30-015-27592	O	31	175	28E 660S	WDW #001	-	-	8/4/1998
60	30-015-01649	O	31	175	28E 660S	EMPIRE ABO UNIT #023	ACTIVE	2/24/1960	2/24/1960
61	30-015-20042	P	31	175	28E 990S	NORTHWEST ARTESIA UNIT #011	P&A	5/8/1967	5/8/1967
62	30-015-01641	P	31	175	28E 660S	EMPIRE ABO UNIT #024	ACTIVE	3/12/1960	3/12/1960
63	30-015-01654	D	32	175	28E 330N	ASTON-STATE NO. 1	P&A	5/12/1953	5/12/1953
64	30-015-01671	E	32	175	28E 2280N	EMPIRE ABO UNIT #025B	P&A	9/13/1960	9/13/1960
65	30-015-01657	F	32	175	28E 2280N	AA STATE NO. 1	ACTIVE	8/14/2009	8/14/2008
66	30-015-10818	M	32	175	28E 2310S	NORTHWEST ARTESIA UNIT #008	P&A	11/6/2006	11/6/2006
67	30-015-01661	K	32	175	28E 1650S	EMPIRE ABO UNIT #026B	T/A	3/27/1960	3/27/1960
68	30-015-10795	L	32	175	28E 2310S	NORTHWEST ARTESIA UNIT #009	P&A	5/15/1966	5/15/1966
69	30-015-01662	L	32	175	28E 1650S	EMPIRE ABO UNIT #025A	P&A	4/13/1960	4/13/1960
70	30-015-20043	M	32	175	28E 990S	NORTHWEST ARTESIA UNIT #012	P&A	5/9/1967	5/9/1967
71	30-015-01660	M	32	175	28E 660S	EMPIRE ABO UNIT #025	P&A	3/5/1960	3/5/1960
72	30-015-10834	N	32	175	28E 990S	NORTHWEST ARTESIA UNIT #013	P&A	9/15/2006	9/15/2006
73	30-015-01659	N	32	175	28E 660S	EMPIRE ABO UNIT #026A	P&A	2/14/1960	2/14/1960
74	30-015-21539	N	32	175	28E 150S	EMPIRE ABO UNIT #261	T/A	7/25/1975	7/25/1975
75	30-015-22709	O	32	175	28E 330S	EMPIRE ABO UNIT #272	T/A	7/18/1977	7/18/1977
76	30-015-02606	3	5	18S	28E 330N	EMPIRE ABO UNIT #026E	ACTIVE	7/18/1960	7/18/1960
77	30-015-22697	3	5	18S	28E 1080N	EMPIRE ABO UNIT #261A	P&A	6/16/2009	6/16/2009
78	30-015-02607	4	5	18S	28E 660N	EMPIRE ABO UNIT #025C	ACTIVE	P/A	P/A
79	30-015-22750	4	5	18S	28E 660N	EMPIRE ABO UNIT #251	ACTIVE	P/A	P/A
80	30-015-02608	E	5	18S	28E 1660N	STATE E AI #001	ACTIVE	1/13/2006	1/13/2006
81	30-015-24485	E	5	18S	28E 1980N	ILLINOIS CAMP A COM #001	P&A	8/10/1983	8/10/1983
82	30-015-02602	F	5	18S	28E 1650N	EMPIRE ABO UNIT #026D	ACTIVE	12/30/1959	12/30/1959
83	30-015-22522	L	5	18S	28E 2240S	WALTER SOLT STATE #001	ACTIVE	8/12/1983	8/12/1983
84	30-015-10244	L	5	18S	28E 2310S	STATE AG #001	ACTIVE	3/27/2001	3/27/2001
87	30-015-20019	1	6	18S	28E 330N	NORTHWEST ARTESIA UNIT #015	ACTIVE	3/14/1967	3/14/1967
88	30-015-02615	1	6	18S	28E 660N	EMPIRE ABO UNIT #024B	ACTIVE	2/29/1960	2/29/1960
89	30-015-02625	2	6	18S	28E 470N	EMPIRE ABO UNIT #023C	ACTIVE	12/21/1959	12/21/1959
90	30-015-21542	2	6	18S	28E 1260N	EMPIRE ABO UNIT #231	P/A	11/1/1975	11/1/1975
91	30-015-02621	3	6	18S	28E 660N	EMPIRE ABO UNIT #022E	ACTIVE	12/29/1959	12/29/1959
92	30-015-21526	G	6	18S	28E 1361N	EMPIRE ABO UNIT #231A	P/A	10/22/1975	10/22/1975
93	30-015-02613	4	6	18S	28E 990N	EMPIRE ABO UNIT #022B	ACTIVE	12/30/1959	12/30/1959
94	30-015-23116	5	6	18S	28E 2050N	EMPIRE ABO UNIT #213	ACTIVE	6/2/1980	6/2/1980
95	30-015-02619	5	6	18S	28E 1990N	EMPIRE ABO UNIT #021C	ACTIVE	10/30/1959	10/30/1959
96	30-015-22637	5	6	18S	28E 2450N	EMPIRE ABO UNIT #212	ACTIVE	12/28/1978	12/28/1978
97	30-015-21395	5	6	18S	28E 2650N	EMPIRE ABO UNIT #211	ACTIVE	2/11/1975	2/11/1975
98	30-015-22012	F	6	18S	28E 1350N	EMPIRE ABO UNIT #222	ACTIVE	3/13/1977	3/13/1977
99	30-015-02626	F	6	18S	28E 1650N	STATE NO. 1	ACTIVE	2/21/1942	2/21/1942
100	30-015-10107	F	6	18S	28E 1874N	STATE FX #001	ACTIVE	8/8/1963	8/8/1963
101	30-015-02620	F	6	18S	28E 1990N	EMPIRE ABO UNIT #022D	ACTIVE	11/26/1959	11/26/1959
102	30-015-22527	F	6	18S	28E 2650N	EMPIRE ABO UNIT #223	ACTIVE	5/19/1978	5/19/1978
103	30-015-21746	F	6	18S	28E 2610N	EMPIRE ABO UNIT #221	ACTIVE	4/23/1976	4/23/1976
104	30-015-22913	G	6	18S	28E 1750N	EMPIRE ABO UNIT #235	ACTIVE	7/8/1979	7/8/1979
105	30-015-22593	G	6	18S	28E 1900N	EMPIRE ABO UNIT #234	ACTIVE	8/7/1978	8/7/1978
106	30-015-02614	G	6	18S	28E 1980N	EMPIRE ABO UNIT #023B	ACTIVE	1/26/1960	1/26/1960
107	30-015-21737	G	6	18S	28E 2253N	EMPIRE ABO UNIT #232	ACTIVE	4/13/1976	4/13/1976
108		H	6	18S	28E	SARKIN, DAVID C & OLIVER, HENRY F	P&A		
109	30-015-22490	G	6	18S	28E 2550N	DORAL ENERGY CORP	ACTIVE		
110	30-015-02615	H	6	18S	28E 1650N	APACHE CORPORATION	ACTIVE		
111	30-015-23547	H	6	18S	28E 1950N	BP AMERICA PRODUCTION COMPANY	ACTIVE	9/19/2008	9/19/2008
112	30-015-02617	I	6	18S	28E 2310S	BP AMERICA PRODUCTION COMPANY	ACTIVE	12/12/2002	12/12/2002

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API No.	Unit Sect	TOWNS	HIP RNG NS FTG	WELL	TYPE	PLUG DATE	STATUS	DATE - Comp or Plug
113	30-015-22528	J	6	18S	28E 2300S	BP AMERICA PRODUCTION COMPANY	0	4/7/2009 P&A	2/5/1979
114	30-015-02611	J	6	18S	28E 2310S	BARNEY COCKBURN STATE NO. 1	0	8/15/1949 P&A	8/15/1949
115	30-015-02628	J	6	18S	28E 2260S	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	5/23/1979
116	30-015-22491	J	6	18S	28E 1700S	BP AMERICA PRODUCTION COMPANY	0	9/2/2009 P&A	8/13/1978
117	30-015-02618	J	6	18S	28E 1647S	CAPITOL STATE NO. 1	0	3/21/1955 P&A	3/21/1955
118	30-015-02623	K	6	18S	28E 2248S	EMPIRE ABO UNIT #022F	0	ACTIVE	2/22/1960
119		K	6	18S	28E	WDW-2 (ORIGINAL LOCATION)			
120		L	6	18S	28E 2219S	EMPIRE ABO UNIT #021D	0	ACTIVE	1/2/1960
121	30-015-02622	6	6	18S	28E 2190S	EMPIRE ABO UNIT #211A	0	ACTIVE	7/17/1980
122	30-015-23548	6	6	18S	28E 1950S	STATE MAI #002	0	ACTIVE	10/2/1960
123	30-015-02627	7	6	18S	28E 949S	CHALK BLUFF 6 STATE #001	0	ACTIVE	4/16/1992
124	30-015-26943	7	6	18S	28E 990S	EMPIRE ABO UNIT #022C	0	ACTIVE	8/5/1960
125	30-015-02610	N	6	18S	28E 955S	PAN AMERICAN PETROLEUM CO	0	5/1/1961 P&A	5/1/1961
126	30-015-02624	O	6	18S	28E 968S	DICKSON PETROLEUM CO	0	12/30/1985 P&A	12/30/1985
127	30-015-25503	P	6	18S	28E 660S	D & H OIL CO	0	5/13/1952 P&A	5/13/1952
128	30-015-02612	P	6	18S	28E 330S	APACHE CORPORATION	0	ACTIVE	11/5/1959
129	30-015-01215	1	1	18S	27E 667N	APACHE CORPORATION	0	7/7/1959 P/A	7/7/1959
130	30-015-00708	2	1	18S	27E 660N	APACHE CORPORATION	0	5/10/1948 P&A	5/10/1948
131		C	1	18S	27E	HILL #4	MISPLOT		
132		C	1	18S	27E	NAVAJO REFINING COMPANY			
133	30-015-00710	3	1	18S	27E 660N	APACHE CORPORATION	0	ACTIVE	7/2/2004
134	30-015-26741	F	1	18S	27E 1650N	RUTH OIL CO, LLC	0	ACTIVE	8/24/1991
135	30-015-00706	F	1	18S	27E 2310N	NEWBOURNE OIL CO	0	ACTIVE	5/31/1959
136	30-015-00709	G	1	18S	27E 1980N	EMPIRE ABO UNIT #019C	0	ACTIVE	8/2/1959
137		G	1	18S	27E	CFM OIL, LLC			
138	30-015-21552	G	1	18S	27E 2500N	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	9/7/1975
139	30-015-00711	H	1	18S	27E 1980N	ALAMO PERMIAN RESOURCES, LLC	0	ACTIVE	10/13/1959
140	30-015-21783	H	1	18S	27E 2490N	APACHE CORPORATION	0	ACTIVE	5/13/1976
141	30-015-22656	H	1	18S	27E 2400N	MANHATTAN OIL	0	ACTIVE	10/10/1978
142		H	1	18S	27E	ALAMO PERMIAN RESOURCES, LLC	0	ACTIVE	7/1/1927
143	30-015-21553	H	1	18S	27E 2501N	NEWBOURNE OILCO	0	ACTIVE	7/19/1975
144	30-015-27163	I	1	18S	27E 1980S	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	1/16/1993
145	30-015-00697	I	1	18S	27E 1980S	ALAMO PERMIAN RESOURCES, LLC	0	ACTIVE	1/5/2003
146	30-015-00657	J	1	18S	27E 2490S	APACHE CORPORATION	0	ACTIVE	10/26/1978
147	30-015-00656	J	1	18S	27E 1980S	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	8/20/1959
148	30-015-22560	J	1	18S	27E 2205S	EMPIRE ABO UNIT #132	0	T/A	6/25/1978
149	30-015-21873	J	1	18S	27E 1526S	EMPIRE ABO UNIT #19A	0	ACTIVE	1/5/2003
150	30-015-22658	J	1	18S	27E 1500S	EMPIRE ABO UNIT #020K	0	ACTIVE	1/1/1978
151	30-015-22559	K	1	18S	27E 2290S	EMPIRE ABO UNIT #139	0	ACTIVE	7/25/1978
152	30-015-22096	K	1	18S	27E 2370S	EMPIRE ABO UNIT #183	0	ACTIVE	7/24/1977
153	30-015-21554	K	1	18S	27E 1367S	EMPIRE ABO UNIT #185	0	ACTIVE	9/23/1976
154	30-015-00707	K	1	18S	27E 1980S	EMPIRE ABO UNIT #194	0	ACTIVE	11/14/1978
155	30-015-21792	K	1	18S	27E 1533S	LIME ROCK RESOURCES A, L.P.	0	ACTIVE	6/1/1976
156	30-015-00659	N	1	18S	27E 995S	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	9/27/2003
157	30-015-26575	N	1	18S	27E 790S	NAVAJO REFINING COMPANY	0	ACTIVE	3/7/1991
			1	18S	27E	BP AMERICA PRODUCTION COMPANY	0	ACTIVE	4/17/2003
			1	18S	27E	APACHE CORPORATION	0	ACTIVE	5/22/1959
			1	18S	27E	EMPIRE ABO UNIT #018B	0	ACTIVE	11/14/1978
			1	18S	27E	EMPIRE ABO UNIT #182	0	ACTIVE	6/1/1976
			1	18S	27E	EMPIRE ABO UNIT #184	0	ACTIVE	7/25/1978
			1	18S	27E	EMPIRE ABO UNIT #018D	0	ACTIVE	7/24/1977
			1	18S	27E	EMPIRE ABO UNIT #183	0	ACTIVE	9/23/1976
			1	18S	27E	EMPIRE ABO UNIT #185	0	ACTIVE	11/14/1978
			1	18S	27E	EMPIRE ABO FEDERAL NO. 5	0	ACTIVE	6/1/1976
			1	18S	27E	LAUREL STATE #001	0	ACTIVE	4/9/1971
			1	18S	27E	EMPIRE ABO UNIT #191	0	ACTIVE	11/18/1959
			1	18S	27E	EMPIRE ABO UNIT #020B	0	ACTIVE	12/2/1961
			1	18S	27E	FEDERAL T #001	0	ACTIVE	9/13/1990
			1	18S	27E	HUMBLE OIL & REFINING CO	0	ACTIVE	4/9/1971
			1	18S	27E	BP AMERICA PRODUCTION COMPANY	S	ACTIVE	2/23/1987
			1	18S	27E	APACHE CORPORATION	0	ACTIVE	11/10/1988
			1	18S	27E	APACHE CORPORATION	1	ACTIVE	6/10/1985
			1	18S	27E	HARLOW ENTERPRISES LLC	0	ACTIVE	ABAN LOCATION
			1	18S	27E	EASTLAND OIL CO	0	ACTIVE	
			1	18S	27E	EASTLAND OIL CO	0	ACTIVE	
			1	18S	27E	MOREXCO INC	0	ACTIVE	
			1	18S	27E	DYAD PE	0	ACTIVE	
			1	18S	27E	PRE-ONGUARD WELL #213	0	ACTIVE	
			1	18S	27E	1900N PRE-ONGUARD WELL #212	0	ACTIVE	
169	30-015-22635	J	8	18S	28E	1900N PRE-ONGUARD WELL #212	0	ACTIVE	

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit	TOWNS				WELL	TYPE	PLUG DATE	STATUS	DATE - Comp or Plug	
			No.	Sect	HIP	RNG						
170	30-015-24372	J	8	18S	28E	1980S	EW/FITG WELL NAME	OPERATOR				
171	30-015-27436	H	7	18S	28E	2310N	PRE-ONGUARD WELL #001	DYAD PE	0	ABAN LOCATION	10/11/1993	
353	30-015-27286	M	36	17S	27E	660S	CHALK BLUFF 6 STATE #002	PHILLIPS PETROLEUM	0	ABAN LOCATION	3/30/1993	
354	30-015-24612	M	36	17S	27E	790S	CHALK BLUFF 36 STATE #001	MEWBURNE OIL CO	0	ACTIVE	3/30/1993	
355	30-015-00676	M	36	17S	27E	330N	STATE M #001	PRONGHORN MANAGEMENT CORP	0	ACTIVE	10/11/1993	
356	30-015-10184	M	36	17S	27E	330S	990W	LIME ROCK RESOURCES A, L.P.	455W	4/21/2009 P&A	10/11/1993	
358	30-015-21623	M	36	17S	27E	360S	STATE #006	ASOPEN OIL INC	920W	ACTIVE	10/11/1993	
359	30-015-00862	M	36	17S	27E	330S	STATE #007	GEOERGE A CHASE JR & C SERVICE	455W	ACTIVE	10/11/1993	
359	30-015-02605	B	5	18S	28E	930N	STATE NO. 2	ACREY, BL & FD	330W	10/15/1942 P&A	10/15/1942	
748	30-015-00701	D	1	18S	27E	330N	EMPIRE ABO UNIT #017	BP AMERICA PRODUCTION UNIT	18S	6/12/2009 P&A	3/30/1960	
748	30-015-00715	4	1	18S	27E	330N	SOUTH RED LAKE GRAYBURG UNIT 37 WNW	FAIRWAY RESOURCES OPERATING LLC	18S	ACTIVE	10/11/1993	
749	30-015-00712	D	1	18S	27E	647N	EMPIRE ABO UNIT I NO. 17	LEGACY RESERVES OPERATING LP	18S	ACTIVE	10/11/1993	
750		E	1	18S	27E	1650N	EMPIRE ABO UNIT #17A	ARCO OIL & GAS	18S	1/24/1987 P&A	1/24/1987	
751	30-015-00704	E	1	18S	27E	1980N	EMPIRE ABO UNIT J NO. 17	JONES	18S	5/10/1939 P&A	5/10/1939	
752	30-015-00703	L	1	18S	27E	1980S	EMPIRE ABO UNIT #017A	ARCO OIL & GAS	18S	3/27/2009 P&A	3/26/1959	
753	30-015-22815	M	1	18S	27E	670S	EMPIRE ABO UNIT #171	BP AMERICA PRODUCTION COMPANY	18S	3/27/2009 P&A	5/22/1995	
754		M	1	18S	27E	330W	LIME ROCK RESOURCES A, L.P.	LIME ROCK RESOURCES A, L.P.	18S	ACTIVE	5/22/1979	
755	30-015-00714	N	1	18S	27E	990S	HILL #1	VALLEY REFINING CO	18S	MISPLLOT OF 756		
756	30-015-00705	M	1	18S	27E	990S	EMPIRE ABO UNIT #017B	BP AMERICA PRODUCTION COMPANY	18S	12/20/1943 P&A	12/20/1943	
757		A	2	18S	27E	330N	STATE 2	BP AMERICA PRODUCTION COMPANY	18S	7/21/2004 P&A	6/25/1959	
758	30-015-00721	1	2	18S	27E	330N	SOUTH RED LAKE GRAYBURG UNIT #036	STATE 2	18S	1/31/1942 NO COMPL	1/31/1942	
765	30-015-00724	1	2	18S	27E	990N	EMPIRE ABO UNIT #016	FAIRWAY RESOURCES OPERATING LLC	18S	PROD	11/16/1947	
766	30-015-00737	B	2	18S	27E	905N	SOUTH RED LAKE GRAYBURG UNIT #038	LIME ROCK RESOURCES A, L.P.	18S	ACTIVE	5/23/1948	
772	30-015-00745	H	2	18S	27E	1980N	STATE H #001	MACK ENERGY CORPORATION	18S	3/7/2008 P&A	3/7/2008	
773	30-015-00742	H	2	18S	27E	1650N	SOUTH RED LAKE GRAYBURG UNIT 39 WNW	S&I OPERATING COMPANY	18S	2/8/1991 P&A	2/8/1991	
774	30-015-00740	G	2	18S	27E	1650N	SOUTH RED LAKE GRAYBURG UNIT #040	MCQUADRANGLE, LC	18S	7/10/2002 P&A	7/10/2002	
778		G	2	18S	27E	2310N	HUDSON #2	RUTTER & WILBANKS	18S	ACTIVE	1/1/1957	
779	30-015-00741	G	2	18S	27E	2310N	EMPIRE ABO UNIT #015B	APACHE CORPORATION	18S	ACTIVE	6/6/1959	
781		J	2	18S	27E	2310S	STATE B-2	MALCO REFINING CO	18S	1/1/1947 P&A	1/1/1947	
785	30-015-00717	I	2	18S	27E	1980S	EMPIRE ABO UNIT #016	BP AMERICA PRODUCTION COMPANY	18S	2/8/1991 P&A	2/6/1995	
786	30-015-00716	J	2	18S	27E	1980S	EMPIRE ABO UNIT #015	APACHE CORPORATION	18S	3/23/1959		
789	30-015-22896	K	2	18S	27E	1820S	EMPIRE ABO UNIT #013A	WALTER SOLT, LLC	18S	5/13/1979		
791	30-015-22914	I	2	18S	27E	1310S	EMPIRE ABO UNIT #161	COG OPERATING, LLC	18S	T/A	9/13/1979	
792		O	2	18S	27E	1200S	1900W	APACHE CORPORATION	18S	MISPLLOT OF 814		
793	30-015-22609	N	2	18S	27E	1200S	EMPIRE ABO UNIT #143	APACHE CORPORATION	18S	ACTIVE	12/20/1978	
795		P	2	18S	27E	1200S	1900W	APACHE CORPORATION	18S	MISPLLOT OF 765		
796	30-015-21544	O	2	18S	27E	1110S	1322E	EMPIRE ABO UNIT #151	APACHE CORPORATION	18S	P/A	11/14/1975
797	30-015-22885	O	2	18S	27E	1040S	2025E	EMPIRE ABO UNIT #155	APACHE CORPORATION	18S	T/A	5/1/1979
799	30-015-00722	P	2	18S	27E	660S	660E	EMPIRE ABO UNIT #016A	APACHE CORPORATION	18S	2/4/2009 P&A	1/20/1959
800	30-015-22808	O	2	18S	27E	600S	1330E	EMPIRE ABO UNIT #156	BP AMERICA PRODUCTION COMPANY	18S	2/5/2009 P&A	4/12/1979
801	30-015-00731	O	2	18S	27E	660S	1980E	EMPIRE ABO UNIT #015A	BP AMERICA PRODUCTION COMPANY	18S	2/11/2009 P&A	11/19/1958
802	30-015-22669	O	2	18S	27E	800S	2500E	EMPIRE ABO UNIT #154	BP AMERICA PRODUCTION COMPANY	18S	1/27/2009 P&A	12/14/1978
805	30-015-22013	O	2	18S	27E	905	1456E	EMPIRE ABO UNIT #153	BP AMERICA PRODUCTION COMPANY	18S	10/30/2008 P&A	4/20/1977
806	30-015-21825	O	2	18S	27E	320S	2602E	EMPIRE ABO UNIT #152	APACHE CORPORATION	18S	T/A	6/17/1976
807	30-015-22608	N	2	18S	27E	100S	1950W	EMPIRE ABO UNIT #142	BP AMERICA PRODUCTION COMPANY	18S	(No info on dates)	
808	30-015-21807	M	2	18S	27E	275S	1243W	EMPIRE ABO UNIT #132	BP AMERICA PRODUCTION COMPANY	18S	ACTIVE	7/1/1976
812	30-015-00730	N	2	18S	27E	660S	1980W	EMPIRE ABO UNIT #014	APACHE CORPORATION	18S	ACTIVE	10/21/1958
813	30-015-00720	A	2	18S	27E	990N	1650E	RIVERWOLF UNIT #004	BP AMERICA PRODUCTION COMPANY	18S	12/12/2008 P&A	10/21/1959
814	30-015-22051	K	2	18S	27E	1370S	2445W	EMPIRE ABO UNIT #141A	APACHE CORPORATION	18S	ACTIVE	5/17/1977
836	30-015-00869	A	11	18S	27E	330N	653E	EMPIRE ABO UNIT #016C	BP AMERICA PRODUCTION COMPANY	18S	10/25/2004 P&A	10/25/2004
837	30-015-22568	B	11	18S	27E	400N	1450E	EMPIRE ABO UNIT #151B	BP AMERICA PRODUCTION COMPANY	18S	8/16/2006 P&A	8/16/2006
838	30-015-22838	B	11	18S	27E	200N	1925E	EMPIRE ABO UNIT #153B	BP AMERICA PRODUCTION COMPANY	18S	1/14/2009 P&A	5/6/1979
839	30-015-00868	B	11	18S	27E	660N	1980E	EMPIRE ABO UNIT #015C	BP AMERICA PRODUCTION COMPANY	18S	7/16/2004 P&A	7/16/2004
840	30-015-22569	B	11	18S	27E	560N	2588E	EMPIRE ABO UNIT #152B	BP AMERICA PRODUCTION COMPANY	18S	9/23/1978	

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**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit	TOWNS	WELL			DATE - Comp	
				No.	Sect	HIP	RNG	NS FTG
841	30-015-22834	C	11 18S	27E	225N		5/23/1979	
842	30-015-00864	C	11 18S	27E	660N		9/5/1957	
843	30-015-22833	D	11 18S	27E	450N		9/5/1957	
844	30-015-00867	D	11 18S	27E	660N		5/23/1979	
845	30-015-22556	D	11 18S	27E	1100N		4/26/1958	
848	30-015-20510	F	11 18S	27E	1650N		7/10/1978	
849	30-015-00865	F	11 18S	27E	1650N		10/16/1971	
850	30-015-00866	E	11 18S	27E	1980N		2/3/1961	
851	30-015-00870	J	11 18S	27E	1980S		2/3/1958	
852	30-015-01201	O	11 18S	27E			9/1/1956	
853	30-015-01202	O	11 18S	27E			4/15/2027	
854	30-015-00863	N	11 18S	27E	700S		2/4/2027	
855	30-015-24857	M	11 18S	27E	990W		9/1/1956	
856	30-015-20535	D	12 18S	27E	330N		8/7/1973	
857	30-015-00871	D	12 18S	27E	330N		4/12/1994	
858	30-015-23115	D	12 18S	27E	330N		3/16/1980	
859	30-015-25738	G	12 18S	27E	2310N		4/25/1987	
860	30-015-25270	F	12 18S	27E	2310N		4/23/1985	
861	30-015-20894	E	12 18S	27E	1980N		7/18/1973	
862	30-015-00874	J	12 18S	27E	2310S		6/29/1948	
863	30-015-00872	L	12 18S	27E	310S		2/18/1943	
864	30-015-25201	K	12 18S	27E	1650S		3/16/1985	
865	30-015-25649	L	12 18S	27E	1650S		10/10/1986	
866	30-015-25545	M	12 18S	27E	990S		8/7/1984	
867	30-015-00873	M	12 18S	27E	2355E		5/19/1986	
868	30-015-26017	N	12 18S	27E	990S		2/27/1945	
869	30-015-25100	N	12 18S	27E	330S		1/23/2003	
870	30-015-22202	O	12 18S	27E	330S		12/10/1984	
871	30-015-06171	I	12 18S	27E	1069S		4/19/1985	
872		P	12 18S	27E			5/20/2026	
873	30-015-00875	P	12 18S	27E	330S		2/15/1932	
874	30-015-00876	P	12 18S	27E	100S		7/30/1952	
875	30-015-06170	P	12 18S	27E	200S		2/8/1954	
876	30-015-01200	A	13 18S	27E	0		2/22/2026	
877	30-015-06137	A	13 18S	27E	250N		1/1/2026	
878	30-015-22394	C	13 18S	27E	330N		1/1/2026	
879	30-015-25241	C	13 18S	27E	330N		D&A	
880	30-015-00884	C	13 18S	27E	990N		2/8/1985	
881	30-015-25370	D	13 18S	27E	480N		4/23/1985	
882	30-015-00883	D	13 18S	27E	990N		8/27/1985	
883	30-015-00880	E	13 18S	27E	1650N		12/11/1944	
884	30-015-24881	F	13 18S	27E	1880N		1/26/1945	
885	30-015-00888	F	13 18S	27E	1980N		1/26/1945	
886	30-015-00879	F	13 18S	27E	2310N		6/18/1984	
888	30-015-22078	G	13 18S	27E	1724N		11/28/1954	
895	30-015-00891	A	14 18S	27E	990N		3/14/1945	
896	30-015-00893	G	14 18S	27E	1650N		3/14/1945	
897	30-015-00895	H	14 18S	27E	1650N		12/30/1984	
901	30-015-00695	L	14 18S	27E	1650S		6/30/1944	
910	30-015-00744	J	2 18S	27E	2310S		1/1/1900	
911	30-015-31123	H	36 17S	27E	1980N		1/1/1900	
912	30-015-31036	H	36 17S	27E	2310N		2/8/1945	
916	30-015-31592	N	36 17S	27E	320S		12/21/2001	
917	30-015-30784	A	31 17S	28E	330N		12/21/2001	
918	30-015-30893	A	31 17S	28E	973N		ACTIVE	
959E			NW STATE #028				ACTIVE	
			NW STATE #028				ACTIVE	

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**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit	TOWNS	No.	Sect	HIP	RNG	NS FTG	EW FTG	WELL NAME	WELL	TYPE	PLUG DATE	STATUS	DATE - Comp
919	30-015-33162	1	31	175		28E	460N	990W	ENRON STATE #004	MARROB ENERGY CORP	4/3/2003	or Plug			
920	30-015-30783	H	31	175		28E	1650N	330E	NW STATE #011	LIME ROCK RESOURCES A, LP	O	ACTIVE			
921	30-015-30849	I	31	175		28E	2310S	270E	NW STATE #009	LIME ROCK RESOURCES A, LP	O	ACTIVE			
922	30-015-30760	P	31	175		28E	735S	330E	NW STATE #010	LIME ROCK RESOURCES A, LP	O	ACTIVE			
923	30-015-31920	D	32	175		28E	990N	990W	ENRON STATE #002	APACHE CORPORATION	O	ACTIVE			
924	30-015-30781	K	32	175		28E	1900S	2145W	NW STATE #005	LIME ROCK RESOURCES A, LP	O	ACTIVE			
925	30-015-30777	L	32	175		28E	2310S	990W	NW STATE #006	APACHE CORPORATION	O	ACTIVE			
926	30-015-30685	M	32	175		28E	990S	2310W	NW STATE #007	APACHE CORPORATION	O	ACTIVE			
927	30-015-30815	N	32	175		28E	1900S	2126W	NW STATE #008	LIME ROCK RESOURCES A, LP	O	ACTIVE			
928	30-015-22816	O	1	18S		27E	990N	990E	AAO FEDERAL #004	APACHE CORPORATION	O	ACTIVE			
929	30-015-32309	2	1	18S		27E	330N	1690E	AAO FEDERAL #003	APACHE CORPORATION	O	ACTIVE			
930	30-015-32308	3	1	18S		27E	430N	2310W	AAO FEDERAL #002	APACHE CORPORATION	O	ACTIVE			
931	30-015-32307	4	1	18S		27E	330N	990W	AAO FEDERAL #001	APACHE CORPORATION	O	ACTIVE			
932	30-015-22816	5	1	18S		27E	1120S	1440E	EMPIRE ABO UNIT L #192	ARCO OIL & GAS	O	ACTIVE			
933	30-015-20388	N	1	18S		27E	990S	2297E	EMPIRE ABO #5	ARCO OIL & GAS	O	ACTIVE			
934	30-015-27719	I	12	18S		27E	1650S	990E	CHALK BLUFF 12 FED #001	YATES PETROLEUM CORPORATION	G	ABAN LOCATION	5/23/1980	6/28/1980	
935	30-015-27747	B	14	18S		27E	660N	1980E	BEAUREGARD ANP STATE COM #001	MARROB ENERGY CORP	O	ABAN LOCATION	12/31/1999	SAME AS 158	
936	30-015-31086	E	5	18S		28E	150N	990W	LP STATE #001	APACHE CORPORATION	O	PROPOSED	3/11/2008	3/11/2008	
937	30-015-31109	E	5	18S		28E	2301N	230W	LP STATE #002	APACHE CORPORATION	O	ACTIVE	4/10/2003	4/10/2003	
938	30-015-30785	1	6	18S		28E	430N	330E	NW STATE #015	BARNEY COCKBURN	O	ACTIVE	9/19/2002	9/19/2002	
939	30-015-00264	J	6	18S		28E	2310S	2310E	CAPITAL STATE NO. 1	MARROB ENERGY CORP	O	ACTIVE	12/10/2002		
940	30-015-31087	7	6	18S		28E	990S	330W	LP STATE #003	MARROB ENERGY CORP	O	ACTIVE	6/23/1980	6/28/1980	
941	30-015-31088	7	6	18S		28E	330S	990W	LP STATE #004	MARROB ENERGY CORP	O	ACTIVE	12/31/1999	SAME AS 158	
942	30-015-06250	O	6	18S		28E	470S	2170E	LAUREL STATE #003	BP AMERICA PRODUCTION COMPANY	O	ABAN LOCATION	3/11/2008	3/11/2008	
943	30-015-31319	3	7	18S		28E	2310N	330W	WDM-3 (ORIGINAL LOC.)	EASTLAND OIL CO	O	PROPOSED	3/11/2008	3/11/2008	
944	30-015-26575	D	6	18S		28E	778N	995W	AAO FEDERAL #005	NAVJO REFINING COMPANY	O	ACTIVE	4/14/2005	4/14/2005	
945	30-015-32395	E	1	18S		27E	1650N	875W	AAO FEDERAL #005	APACHE CORPORATION	O	ACTIVE	2/25/2005	2/25/2005	
946	30-015-33473	G	1	18S		27E	1750N	1650S	AAO FEDERAL #007	MARROB ENERGY CORP	O	ACTIVE	8/5/2005	8/5/2005	
947	30-015-33784	H	1	18S		27E	1650N	330W	AAO FEDERAL #008	MARROB ENERGY CORP	O	ACTIVE	1/17/2006	1/17/2006	
948	30-015-34071	F	1	18S		27E	2169N	1963W	AAO FEDERAL #006	MARROB ENERGY CORP	O	ACTIVE	3/9/2006	3/9/2006	
949	30-015-34387	L	1	18S		27E	1980S	630W	AAO FEDERAL #009	MARROB ENERGY CORP	O	ACTIVE	10/26/2006	10/26/2006	
950	30-015-34555	M	1	18S		27E	890S	660W	AAO FEDERAL #011	MARROB ENERGY CORP	O	ACTIVE	9/21/2006	9/21/2006	
951	30-015-34576	K	1	18S		27E	2060S	2160W	AAO FEDERAL #010	MARROB ENERGY CORP	O	ACTIVE	12/17/2006	12/17/2006	
952	30-015-34998	N	1	18S		27E	890S	1650W	AAO FEDERAL #012	BP AMERICA PRODUCTION COMPANY	O	ACTIVE	10/26/2006	10/26/2006	
953	30-015-34028	G	6	18S		28E	2285N	1366E	SLIDER 6 STATE NO. 001	LIME ROCK RESOURCES A, LP	O	ACTIVE	12/17/2006	12/17/2006	
954	30-015-35050	D	32	17S		28E	330N	50W	ENRON STATE NO. 012	YATES PETROLEUM CORP	O	ACTIVE	12/21/2006	12/21/2006	
955	30-015-40187	A	14	18S		27E	660N	990E	VIOLET BIU STATE COM #1	MACK ENERGY CORPORATION	O	ACTIVE	12/17/2006	12/17/2006	
956	30-015-33294	A	36	17S		27E	915N	420E	RED LAKE 36 A STATE #2	EDGE PETROLEUM OPERATING COMPANY, INC	O	ACTIVE	4/20/2005	4/20/2005	
957	30-015-36116	G	35	17S		27E	2305N	1650E	SOUTH RED LAKE UNIT 11 #57	LEGACY RESERVES OPERATING LP	O	ACTIVE	6/6/2008	6/6/2008	
958	30-015-32394	J	2	18S		27E	2210S	1650E	SCBP STATE #1	APACHE CORPORATION	O	ACTIVE	4/26/2005		
959	30-015-33814	H	2	18S		27E	2063N	441E	STATE H NO 2	MACK ENERGY CORPORATION	O	ACTIVE	1/11/2008	2/20/2009	
960	30-015-36343	G	31	17S		28E	1650N	2310E	MALCO STATE NO. 002	GEORGE A CHASE IR DBA G AND C SERVICE	O	ACTIVE	7/19/2008	7/19/2008	
961	30-015-36973	D	31	17S		28E	990N	330W	ENRON STATE NO. 015	LIME ROCK RESOURCES A, LP	O	ACTIVE	7/3/2009	7/3/2009	
962	30-015-36554	L	32	17S		28E	1770S	550W	NW STATE NO. 029	LIME ROCK RESOURCES A, LP	O	ACTIVE	1/30/2009	1/30/2009	
963	30-015-36989	K	32	17S		28E	1650S	1710W	NW STATE NO. 030	LIME ROCK RESOURCES A, LP	O	ACTIVE	4/26/2005	7/14/2009	
964	30-015-37057	N	32	17S		28E	330S	1750W	NW STATE NO. 031	LIME ROCK RESOURCES A, LP	O	ACTIVE	NO COMPL	NO COMPL	
965	30-015-37058	M	32	17S		28E	330S	330W	NW STATE NO. 032	LIME ROCK RESOURCES A, LP	O	ACTIVE	7/28/2009	7/28/2009	
966	30-015-37428	G	31	17S		28E	1980N	1980E	MALCO STATE NO. 3	G&C SERVICE	O	ACTIVE	8/23/2009	8/23/2009	
967	30-015-38240	G	35	17S		27E	1425N	1520E	KIOWA STATE NO. 3	COG OPERATING, LLC	O	ACTIVE	2/10/2010	2/10/2010	
968	30-015-38029	G	35	17S		27E	2210N	2310E	CONKLIN STATE NO. 1-Y	G AND C SERVICE	O	ACTIVE	PERMIT TO DRILL	PERMIT TO DRILL	
969	30-015-39321	M	35	17S		27E	990S	890W	BIG BOY STATE NO. 1	COG OPERATING, LLC	O	ACTIVE	425W	425W	
970	30-015-39322	M	35	17S		27E	840S	840W	BIG BOY STATE NO. 3	COG OPERATING, LLC	O	ACTIVE	1560E	1560E	
971	30-015-39323	O	35	17S		27E	870S	870E	BIG BOY STATE NO. 5	COG OPERATING, LLC	O	ACTIVE	2210E	2210E	
972	30-015-39324	O	35	17S		27E	480S	27E	BIG BOY STATE NO. 6	COG OPERATING, LLC	O	ACTIVE	990S	990S	
973	30-015-39325	O	35	17S		27E	990S	2210E	BIG BOY STATE NO. 7	COG OPERATING, LLC	O	ACTIVE	PERMIT TO DRILL	PERMIT TO DRILL	

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	TOWNS			WELL	TYPE	PLUG DATE	STATUS	DATE - Comp or Plug
		No.	Sect	HIP					
				RNG	NS	FTG	WELL NAME	EW	FTG
974	30-015-39326	O	36	175	27E	275S	BIG BOY STATE NO. 8	150E	
975	30-015-39401	P	36	175	27E	110S	EMPIRE ABO UNIT NO. 417	630E	COG OPERATING, LLC
976	30-015-39009	G	2	18S	27E	1650N	APACHE CORPORATION	2430E	APACHE CORPORATION
977	30-015-39066	L	2	18S	27E	2551S	APACHE CORPORATION	1170W	EMPIRE ABO UNIT NO. 416
978	30-015-38234	P	30	175	28E	430S	ANTHONY NO. 2	800E	MARBLE STATE NO. 5
979	30-015-39299	M	30	175	28E	990S	MARBLE STATE NO. 6	990W	MARBLE STATE NO. 6
980	30-015-39300	M	30	175	28E	330S	MARBLE STATE NO. 6	330W	MARBLE STATE NO. 6
981	30-015-38512	D	30	175	28E	990N	MARBLE STATE NO. 6	940W	ENRON STATE NO. 16
982	30-015-39004	P	31	175	28E	150S	EMPIRE ABO UNIT NO. 401	130E	EMPIRE ABO UNIT NO. 419
983	30-015-39011	O	31	175	28E	1190S	EMPIRE ABO UNIT NO. 419	1320E	EMPIRE ABO UNIT NO. 408
984	30-015-39020	O	31	175	28E	140S	EMPIRE ABO UNIT NO. 408	250E	COG OPERATING, LLC
985	30-015-38513	J	32	175	28E	2310S	COG OPERATING, LLC	2032E	JEFFER 32 STATE NO. 3
986	30-015-39006	J	32	175	28E	2400S	LIME ROCK RESOURCES	2450E	LIME ROCK RESOURCES
987	30-015-39007	M	32	175	28E	70S	APACHE CORPORATION	100W	APACHE CORPORATION
988	30-015-39064	O	32	175	28E	1175S	APACHE CORPORATION	1310E	APACHE CORPORATION
989	30-015-39008	D	6	18S	28E	160N	APACHE CORPORATION	1300W	APACHE CORPORATION
990	30-015-39021	D	6	18S	28E	40N	APACHE CORPORATION	145W	APACHE CORPORATION
991	30-015-39015	D	1	18S	27E	330N	APACHE CORPORATION	930W	LEGACY RESERVES OPERATING LP
992	30-015-39015	D	4	18S	27E	330N	LEGACY RESERVES OPERATING LP	990W	AAO FEDERAL NO. 1
993	30-015-32307		1	18S	27E	330N	APACHE CORPORATION	875W	AAO FEDERAL NO. 5
994	30-015-32299	E	1	18S	27E	1650N	APACHE CORPORATION	1650E	AAO FEDERAL NO. 7
995	30-015-33473	G	1	18S	27E	1750N	APACHE CORPORATION	330E	AAO FEDERAL NO. 8
996	30-015-33784	H	1	18S	27E	1650N	APACHE CORPORATION	1983W	AAO FEDERAL NO. 6
997	30-015-34071	F	1	18S	27E	2169N	APACHE CORPORATION	660W	AAO FEDERAL NO. 11
998	30-015-34555	M	1	18S	27E	890S	APACHE CORPORATION	2160W	AAO FEDERAL NO. 10
999	30-015-34576	K	1	18S	27E	2060S	APACHE CORPORATION	1830W	EMPIRE ABO UNIT NO. 14B
1000	30-015-00735	K	2	18S	27E	1980S	APACHE CORPORATION	950W	EMPIRE ABO UNIT NO. 133
1001	30-015-22824	M	2	18S	27E	800S	APACHE CORPORATION	1400W	EMPIRE ABO UNIT NO. 142A
1003	30-015-22952	K	2	18S	27E	1310S	APACHE CORPORATION	1838E	KIOWA STATE NO. 8
1004	30-015-39956	G	3	17S	27E	2176N	APACHE CORPORATION	485W	BIG BOY STATE NO. 2
1005	30-015-40428	M	3	17S	27E	2005	APACHE CORPORATION	806W	BIG BOY STATE NO. 4
1006	30-015-40429	M	36	175	27E	492S	APACHE CORPORATION	1005E	EMPIRE ABO UNIT NO. 412
1007	30-015-39898	A	1	18S	27E	1258E	APACHE CORPORATION	2535W	EMPIRE ABO UNIT NO. 413
1008	30-015-39899	3	1	18S	27E	1305N	APACHE CORPORATION	1205W	EMPIRE ABO UNIT NO. 414
1009	30-015-39900	4	1	18S	27E	1120N	APACHE CORPORATION	2210E	STALEY STATE NO. 9
1011	30-015-36564	O	30	175	28E	330S	APACHE CORPORATION	1650W	STALEY STATE NO. 12
1012	30-015-37673	N	30	175	28E	330S	APACHE CORPORATION	990W	MARBLE STATE NO. 8
1013	30-015-38203	P	30	175	28E	330S	APACHE CORPORATION	2410W	STALEY STATE NO. 17
1014	30-015-40026	N	30	175	28E	330S	APACHE CORPORATION	1320E	EMPIRE ABO UNIT NO. 419
1015	30-015-39011	O	31	175	28E	1190S	APACHE CORPORATION	2560E	EMPIRE ABO UNIT NO. 408
1016	30-015-39020	O	31	175	28E	140S	APACHE CORPORATION	257W	BIG GIRL 31 STATE NO. 1
1017	30-015-40257	D	31	175	28E	184N	COG OPERATING, LLC	990W	BIG GIRL 31 STATE NO. 2
1018	30-015-40258	D	31	175	28E	195N	COG OPERATING, LLC	2310E	BIG GIRL 31 STATE NO. 5
1019	30-015-40259	G	31	175	28E	2160N	COG OPERATING, LLC	990W	BIG GIRL 31 STATE NO. 7
1020	30-015-40260	D	31	175	28E	1155N	COG OPERATING, LLC	330W	BIG GIRL 31 STATE NO. 9H
1021	30-015-40409	L	31	175	28E	1920S	COG OPERATING, LLC	615S	BIG GIRL 31 STATE NO. 11H
1022	30-015-40410	M	31	175	28E	615S	COG OPERATING, LLC	1765W	AA STATE NO. 2
1023	30-015-39927	K	32	175	28E	1750S	COG OPERATING, LLC	2225E	Russell C 003
1024	30-015-40339	D	32	175	28E	990N	COG OPERATING, LLC	2310W	South Red Lake Grayburg Unit #031
1025	30-015-00643	O	35	17S	27E	990S	COG OPERATING, LLC	990E	South Red Lake Grayburg Unit #041
1026	30-015-37783	O	35	17S	27E	990S	COG OPERATING, LLC	2260E	Jeffers 36 State #44
1027	30-015-00644	N	35	17S	27E	330S	COG OPERATING, LLC	1028	Enron Federal #18
1028	30-015-20104	P	35	17S	27E	990S	COG OPERATING, LLC	1029	Enron Federal #18
1029	30-015-34626	M	36	17S	27E	935N	COG OPERATING, LLC	1030	Enron Federal #18
1031	30-015-41289	O	25	17S	27E	985S	COG OPERATING, LLC	2200E	Williams A Federal No 12
29	17S	28E	330S						

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit	TOWNS	TOwns No.	Sec	HIP	RNG	NS FTG	EW FTG	WELL NAME	WELL	DATE - Comp
											TYPE	or Plug
1032	30-015-40807	N	35	175	27E	330N	2310W	Logan B "35" N Federal #18	990W	Lime Rock Resources A, L.P.	O	ACTIVE
1033	30-015-40808	P	35	175	27E	970S	990E	Logan 35 O Federal #19	1770E	LRE Operating LLC	O	ACTIVE
1034	30-015-41435	O	35	175	27E	720S	1770E	Logan 35 O Federal 10	800W	Lime Rock Resources A, L.P.	O	ACTIVE
1035	30-015-42003	E	2	185	27E	2515N	800W	Sb State 004	990W	Apache Corporation	O	ACTIVE
1036	30-015-42002	E	2	185	27E	1900N	990W	Sb State 002	2035W	Apache Corporation	O	ACTIVE
1037	30-015-36979	C	32	175	28E	990N	1700W	Enron State #14	1700W	LRE Operating LLC	O	ACTIVE
1038	30-015-41833	C	32	175	28E	990N	1700W	Enron State 19	2420W	LRE Operating LLC	O	ACTIVE
1039	30-015-39996	C	32	175	28E	230N	2420W	Enron State 17	2365W	Apache Corporation	O	ACTIVE
1040	30-015-41511	N	32	175	28E	330S	2365W	Ab State 647 016	1090W	Apache Corporation	O	ACTIVE
1041	30-015-41498	M	32	175	28E	330S	1090W	Ab State 647 014	2535W	Apache Corporation	O	ACTIVE
1042	30-015-41493	N	32	175	28E	1080S	2535W	Ab State 647 009	950W	Apache Corporation	O	ACTIVE
1043	30-015-39995	C	32	175	28E	1650S	950W	Ab State 647 007	2320W	Apache Corporation	O	ACTIVE
1044	30-015-41492	K	32	175	28E	1375S	2320W	Ab State 647 008	1500W	Apache Corporation	O	ACTIVE
1045	30-015-40783	C	2	185	27E	990N	1500W	Logan 2c State No. 4	1539E	Apache Corporation	O	ACTIVE
1046	30-015-38420	G	36	175	27E	1460N	1539E	Kiowa State	COG Operating LLC	COG Operating LLC	O	ACTIVE
1047	30-015-39626	G	36	175	27E	2152N	2103E	Kiowa State #04	2600W	Apache Corporation	O	ACTIVE
1048	30-015-41500	K	32	175	28E	2355S	2600W	Ab State 647 002	1650W	Apache Corporation	O	ACTIVE
1049	30-015-41501	K	32	175	28E	2370S	1650W	Ab State 647 003	1185W	Apache Corporation	O	ACTIVE
1050	30-015-41505	L	32	175	28E	2250S	1185W	Ab State 647 004	330W	Apache Corporation	O	ACTIVE
1051	30-015-41502	L	32	175	28E	2310S	330W	Ab State 647 005	1650W	Apache Corporation	O	ACTIVE
1052	30-015-41504	N	32	175	28E	330S	1650W	Ab State 647 015	350W	Apache Corporation	O	ACTIVE
1053	30-015-41497	M	32	175	28E	220S	350W	Ab State 647 013	430W	Apache Corporation	O	ACTIVE
1054	30-015-41503	L	32	175	28E	1730S	430W	Ab State 647 006	960W	Apache Corporation	O	ACTIVE
1055	30-015-41495	M	32	175	28E	920S	960W	Ab State 647 011	1650W	Apache Corporation	O	ACTIVE
1056	30-015-41494	N	32	175	28E	1140S	1650W	Ab State 647 010	930W	Apache Corporation	O	ACTIVE
1057	30-015-41496	M	32	175	28E	910S	930W	Ab State 647 012	2300E	Apache Corporation	O	ACTIVE
1058	30-015-40679	B	2	185	27E	968N	2300E	Blake State No. 4	1650W	Apache Corporation	O	ACTIVE
1059	30-015-40671	C	2	185	27E	968N	1650W	Brad State No. 4	1650W	Apache Corporation	O	ACTIVE
1060	30-015-31530	C	32	175	28E	530N	1650W	Enron State #1	330W	Apache Corporation	O	ACTIVE
1061	30-015-00681	M	36	175	27E	990S	330W	South Red Lake Grayburg Unit #027	Logan 2c State #3	Apache Corporation	O	ACTIVE
1062	30-015-33111	I	2	185	27E	530N	2310W	Empire Abo Unit "I" 272a	2345E	Apache Corporation	O	ACTIVE
1063	30-015-22556	B	5	18S	28E	1300N	990W	Bb State Com #1	990W	Apache Corporation	O	ACTIVE
1064	30-015-32070	I	2	18S	27E	660S	2310W	Bm State #1	2305W	Apache Corporation	O	ACTIVE
1065	30-015-32399	I	2	18S	27E	2310S	2305W	Tdf State #2	2305W	Apache Corporation	O	ACTIVE
1066	30-015-32390	I	2	18S	27E	1650N	330W	Enron State #15	150W	Apache Corporation	O	ACTIVE
1067	30-015-36598	D	31	175	28E	990S	150W	Williams A Federal No. 8	530W	Apache Corporation	O	ACTIVE
1068	30-015-36513	N	29	175	28E	1090S	530W	Williams A Federal 5	645W	Apache Corporation	O	ACTIVE
1069	30-015-33232	M	29	175	28E	690S	645W	Williams A Federal No. 10	150E	Apache Corporation	O	ACTIVE
1070	30-015-40480	M	29	175	28E	600S	150E	Blake State No. 1	150E	Apache Corporation	O	ACTIVE
1071	30-015-40677	B	2	185	27E	380N	2300E	Blake State No. 2	2300E	Apache Corporation	O	ACTIVE
1072	30-015-40678	B	2	185	27E	330N	2300E	Apache Corporation	1505W	Apache Corporation	O	ACTIVE
1073	30-015-41766	F	5	18S	28E	1910N	1505W	Libby State 001	2245W	Apache Corporation	O	ACTIVE
1074	30-015-41767	F	5	18S	28E	1570N	2245W	Libby State 002	2245W	Apache Corporation	O	ACTIVE
1075	30-015-41768	F	5	18S	28E	1570N	2245W	Libby State 002	2270E	Apache Corporation	O	ACTIVE
1076	30-015-41770	B	31	175	28E	330N	2270E	T Rex State 001	150E	Apache Corporation	O	ACTIVE
1077	30-015-41771	B	31	175	28E	575N	150E	T Rex State 002	2430E	Apache Corporation	O	ACTIVE
1078	30-015-41772	B	31	175	28E	875N	2430E	T Rex State 003	1750E	Apache Corporation	O	ACTIVE
1079	30-015-41774	B	31	175	28E	890N	1750E	T Rex State 004	1750E	Apache Corporation	O	ACTIVE
1080	30-015-41892	M	29	175	28E	330S	975W	Williams A Federal 15	1750W	Apache Corporation	O	ACTIVE
1081	30-015-41959	K	2	18S	27E	2310S	1750W	Bm State 002	141E	Apache Corporation	O	ACTIVE
1082	30-015-42024	I	1	18S	27E	126N	141E	Aao Federal #14	2408E	Apache Corporation	O	ACTIVE
1083	30-015-42025	I	1	18S	27E	1130N	2408E	Aao Federal #15	2455W	Apache Corporation	O	ACTIVE
1084	30-015-42026	I	1	18S	27E	1305N	2455W	Aao Federal #16	865E	Apache Corporation	O	ACTIVE
1085	30-015-42029	I	1	18S	27E	1650N	865E	Aao Federal #17	1650E	Apache Corporation	O	ACTIVE
1086	30-015-42035	I	1	18S	27E	2310N	1650E	Aao Federal #18	Permit to Drill	Apache Corporation	O	ACTIVE

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit	TOWNS	No. Sect	HIP	RNG	NS	FG	WELL NAME	WELL TYPE	PLUG DATE	STATUS	DATE - Comp or Plug
1087	30-015-42036	1	1 18S	27E	2188N	909W			Aao Federal #20	0	0	Permit to Drill	
1088	30-015-42051	1	1 18S	27E	2310N	2310W			Aao Federal #19	0	0	Permit to Drill	
1089	30-015-42116	M	29 17S	28E	990S	2160W			Williams A Federal 16	0	0	Permit to Drill	
1090	30-015-42121	C	2 18S	27E	658N	1984W			Brade State No. 5	0	0	Permit to Drill	
1091	30-015-42156	D	32 17S	28E	385N	900W			Enron State 21	0	0	Permit to Drill	
1092	30-015-42334	1	1 18S	27E	4005N	1630W			Aao Federal #21	0	0	Permit to Drill	
1093	30-015-42335	1	1 18S	27E	790N	330W			Aao Federal #22	0	0	Permit to Drill	
1094	30-015-42336	1	1 18S	27E	226N	330E			Aao Federal #23	0	0	Permit to Drill	
1095	30-015-42337	1	1 18S	27E	984S	243E			Aao Federal #24	0	0	Permit to Drill	
1096	30-015-42338	1	1 18S	27E	2270S	1650W			Aao Federal #25	0	0	Permit to Drill	
1097	30-015-42339	1	1 18S	27E	360S	990W			Aao Federal #29	0	0	Permit to Drill	
1098	30-015-42358	1	1 18S	27E	183S	2497W			Aao Federal #28	0	0	Permit to Drill	
1099	30-015-42359	1	1 18S	27E	1960S	2063W			Aao Federal #27	0	0	Permit to Drill	
1100	30-015-42360	1	1 18S	27E	1261S	281W			Aao Federal #30	0	0	Permit to Drill	
1101	30-015-42361	1	1 18S	27E	2000S	1022W			Aao Federal #25	0	0	Permit to Drill	
1102	30-015-42372	D	31 17S	28E	330N	430W			Enron State #20	0	0	Permit to Drill	
1103	30-015-42555	O	29 17S	28E	330S	2310E			Outlaw State #005	0	0	Permit to Drill	
1104	30-015-42563	B	32 17S	28E	330S	2310E			Jackrabbit State #004	0	0	Permit to Drill	
1105	30-015-42864	B	32 17S	28E	1010N	2540E			Jackrabbit State #005	0	0	Permit to Drill	
1106	30-015-42985	G	32 17S	28E	1470N	2405E			Jackrabbit State #012	0	0	Permit to Drill	
1107	30-015-42986	G	32 17S	28E	2460N	2280E			Jackrabbit State #013	0	0	Permit to Drill	
1108	30-015-42776	O	30 17S	28E	505S	2140E			Staley State #029	0	0	Permit to Drill	
1109	30-015-40983	O	30 17S	28E	330S	1650E			Staley State #020	0	0	ACTIVE	
1110	30-015-42597	A	31 17S	28E	570N	250E			Ranger State #001	0	0	Permit to Drill	
1111	30-015-42598	A	31 17S	28E	445N	1090E			Ranger State #002	0	0	Permit to Drill	
1112	--								Apache Corporation	0	0	Permit to Drill	
1113	30-015-42599	B	31 17S	28E	905N	1385E			Ranger State #001	0	0	Permit to Drill	
1114	30-015-42600	A	31 17S	28E	645N	250E			Ranger State #004	0	0	Permit to Drill	
1115	30-015-42673	H	31 17S	28E	1650N	990E			Ranger State #006	0	0	Permit to Drill	
1116	--								Apache Corporation	0	0	Permit to Drill	
1117	30-015-42674	H	31 17S	28E	2310N	990E			Ranger State #007	0	0	Permit to Drill	
1118	30-015-42675	H	31 17S	28E	1875N	110E			Ranger State #008	0	0	Permit to Drill	
1119	30-015-42677	I	31 17S	28E	210S	1130E			Ranger State #010	0	0	Permit to Drill	
1120	30-015-42676	H	31 17S	28E	2520N	195E			Ranger State #009	0	0	Permit to Drill	
1121	30-015-42678	I	31 17S	28E	1535S	760E			Ranger State #011	0	0	Permit to Drill	
1122	30-015-42679	I	31 17S	28E	1760S	245E			Ranger State #012	0	0	Permit to Drill	
1123	30-015-42680	I	31 17S	28E	1710S	245E			Ranger State #013	0	0	Permit to Drill	
1124	30-015-42681	P	16 17S	28E	225S	1300E			Ranger State #014	0	0	Permit to Drill	
1125	30-015-42806	P	31 17S	28E	245S	90E			Ranger State #016	0	0	Permit to Drill	
1126	30-015-42682	P	31 17S	28E	260S	1250E			Ranger State #015	0	0	Permit to Drill	
1127	30-015-42602	B	36 17S	27E	330N	2210E			Jeffers 36 State #005	0	0	Permit to Drill	
1128	30-015-42899	B	36 17S	27E	890N	1655E			Jeffers 36 State #006	0	0	ACTIVE	
1129	30-015-42027	H	1 18S	27E	1650N	865E			AAO Federal #017	0	0	Permit to Drill	
1130	30-015-42549	G	1 18S	27E	2470N	2380E			AAO Federal SWD #001	0	0	SHUT IN	
1131	30-015-25270	F	12 18S	27E	2310N	2310W			Chukka Federal #001	0	0	ACTIVE	
1132	30-015-36252	N	30 17S	28E	990S	1980W			Staley State #004	0	0	ACTIVE	
1133	30-015-37691	P	30 17S	28E	1050S	330E			Anthony #1	0	0	ACTIVE	
1134	30-015-40028	P	30 17S	28E	540S	837E			Anthony State #4	0	0	ACTIVE	
1135	30-015-40338	O	30 17S	28E	990S	2310E			Staley State #016	0	0	ACTIVE	
1136	30-015-41085	N	30 17S	28E	990S	2335W			Staley State #24	0	0	ACTIVE	
1137	30-015-40773	C	2 18S	28E	990N	1500W			Logan 2C State #4	0	0	ACTIVE	
1138	30-015-43066	N	35 17S	27E	870S	1640W			Logan B 35 N Federal 24	0	0	Permit to Drill	
1139	30-015-43252	O	35 17S	27E	720S	1670E			Logan 35 O Federal 22	0	0	Permit to Drill	
1140	30-015-42556	O	29 17S	28E	990S	1650E			The Outlaw State #006	0	0	ACTIVE	
141	30-015-42557	O	29 17S	28E	330S	1650E			The Outlaw State #007	0	0	ACTIVE	

**TABLE II**  
**Tabulation of Wells Within One Mile Area of Review**

ID NO	API	Unit	TOWNS	No.	Sect.	HIP	RNG NS FTG	EW FTG	WELL NAME	WELL	TYPE	PLUG DATE	STATUS	DATE - Comp or Plug
1142	30-015-42558	O	29	17S	28E	990S	2310E	The Outlaw State #008		O	O		ACTIVE	
1143	30-015-42725	O	30	17S	28E	685S	1630E	Staley State #28		O	O		ACTIVE	
1144	30-015-42727	O	30	17S	28E	850S	1630W	Staley State #30		O	O		ACTIVE	
1145	30-015-42601	H	31	17S	28E	1825N	110E	Ranger State 005		O	O		Permit to Drill	
1146	30-015-42984	G	32	17S	28E	1535N	1680E	Jack Rabbit State #11					ACTIVE	
1147	30-015-32554	N	29	17S	28E	590S	2185W	WILLIAMS A FEDERAL #001Z					ACTIVE	
1148	30-015-42556	O	29	17S	28E	990S	1650E	OUTLAW STATE #006					ACTIVE	
1149	30-015-42557	O	29	17S	28E	330S	1650E	OUTLAW STATE #007					ACTIVE	
1150	30-015-42585	O	29	17S	28E	990S	2310E	OUTLAW STATE #008					ACTIVE	
1151	30-015-31285	O	30	17S	28E	890S	1650W	STALEY STATE #002					ACTIVE	
1152	30-015-36564	O	30	17S	28E	330S	2210E	STALEY STATE #009					ACTIVE	
1153	30-015-37673	N	30	17S	28E	330S	1650W	STALEY STATE #012					ACTIVE	
1154	30-015-39638	P	30	17S	28E	412S	679E	ANTHONY STATE #003					ACTIVE	
1155	30-015-40026	N	30	17S	28E	330S	2410W	STALEY STATE #017					ACTIVE	
1156	30-015-38512	P	31	17S	28E	990N	940W	ENRON STATE #016					ACTIVE	
1157	30-015-01665	O	32	17S	28E	940S	1650E	NORTHWEST ARTESIA UNIT #014					ACTIVE	
1158	30-015-02312	G	32	17S	28E	1980N	1650E	NORTHWEST ARTESIA UNIT #005					ACTIVE	
1159	30-015-10109	B	32	17S	28E	990N	1650E	NORTHWEST ARTESIA UNIT #003					ACTIVE	
1160	30-015-30684	G	32	17S	28E	1650N	1650E	NW STATE #003					ACTIVE	
1161	30-015-30734	B	32	17S	28E	1140N	2277E	NW STATE #004					ACTIVE	
1162	30-015-30887	J	32	17S	28E	2141S	1665E	JEFFERS 32 STATE #001					ACTIVE	
1163	30-015-30890	B	32	17S	28E	330N	1650E	NW STATE #016					ACTIVE	
1164	30-015-31934	G	32	17S	28E	2272N	2273E	NW STATE #018					ACTIVE	
1165	30-015-34148	J	32	17S	28E	1370S	1609E	ASPEN 32 STATE COM #001					ACTIVE	
1166	30-015-37045	J	32	17S	28E	1563S	2207E	JEFFERS 32 STATE #002					ACTIVE	
1167	30-015-39927	K	32	17S	28E	1750S	1765W	AB STATE 647 #001					ACTIVE	
1168	30-015-00634	P	35	17S	27E	330S	330E	SOUTH RED LAKE II UNIT No. 029					TEMPORARILY ABANDONED	
1169	30-015-00645	N	35	17S	27E	330S	1650W	SOUTH RED LAKE II UNIT No. 032					ACTIVE	
1170	30-015-01222	O	35	17S	27E	330S	2310E	SOUTH RED LAKE II UNIT No. 030					P&A	
1171	30-015-31541	B	36	17S	27E	460N	1650E	JEFFERS 36 STATE No. 003					ACTIVE	
1172	30-015-34089	B	36	17S	27E	330N	2310E	STATE A No. 003					ACTIVE	
1173	30-015-36342	B	36	17S	27E	990N	1650E	STATE A No. 004					ACTIVE	
1174	30-015-22658	J	1	18S	27E	1500S	2130E	EMPIRE ABO UNIT No. 194					T/A	
1176	30-015-32308	C	1	18S	27E	430N	2310W	AO FEDERAL No. 002					T/A	
1177	30-015-32359	E	1	18S	27E	1650N	875W	AAO FEDERAL No. 005					P&A	
1178	30-015-00775	C	2	18S	27E	330N	2310W	SOUTH RED LAKE II UNIT No. 034					ACTIVE	
1179	30-015-01211	B	2	18S	27E	330N	2310W	SOUTH RED LAKE II UNIT No. 035					ACTIVE	
1180	30-015-22777	M	2	18S	27E	105	640W	EMPIRE ABO UNIT No. 134					ACTIVE	
1181	30-015-32218	E	2	18S	27E	1650N	330W	SB STATE No. 001					ACTIVE	
1182	30-015-34632	A	14	18S	27E	660N	990E	VIOLET BIV STATE COMM No. 001A					NEW	
1183	30-015-40187	A	14	18S	27E	660N	990E	VIOLET BIV STATE COMM No. 001					NEW	
1184	30-015-43628	E	14	18S	27E	1760N	880W	CHOATE DAVIS 14 STATE SWD No. 002					NEW	
1185	30-015-01655	J	32	17S	28E	2310S	1650E	STATE 32 No. 001					NEW	
1186	30-015-01656	J	32	17S	28E	1980S	1980E	STATE 32 No. 002					NEW	
1187	30-015-22526	B	5	18S	28E	1300N	2345E	EMPIRE ABO UNIT No. 272A					T&A	
1188	30-015-25277	O	5	18S	28E	660S	1980E	SOLT STATE No. 001					ACTIVE	
1189	30-015-25390	O	5	18S	28E	990S	1650E	SOLT STATE No. 003					ACTIVE	
1190	30-015-35237	M	18	18S	28E	810S	660W	LEATHERSTOCKING 18 STATE COM No. 002					T/A	
	30-015-36281	J	18S	27E	2193S	1520W	SUN DEVILS FEDERAL No. 001						PERMIT TO DRILL 4/1/12	



**TABLE IV**  
**Wells that have been Plugged and Abandoned since the 2016 PFO REPORT**  
**Well Changes in the Combined One Mile Area of Review for Navajo's WDW-1, WDW-2, and WDW-3**

ID	API No.	Unit	Sect.	Town	Range	Footages	Well Name	Operator	Changes	Change of Owner	P&A	T&A	Prod	Recomp	New	Total
1027	30	15	644	35 N	175	27E	3005-2310W	SOUTH RED LAKES UNIT No. 03-1	REMANANT OIL OPERATING LLC	CHANGE OF OPERATOR AND P&A	X	X				
1028	30	15	20104	35 P	175	27E	9905-990E	SOUTH RED LAKES UNIT No. 04-1	REMANANT OIL OPERATING LLC	CHANGE OF OPERATOR AND P&A	X	X				
154	30	15	707	1 K	105	27E	18805-1980W	EMPIRE A&O UNIT No. 0188	APACHE CORP	P&A	X	X				
129	30	15	1215	1 D	185	27E	657N 666E	EMPIRE A&O UNIT No. 0200	APACHE CORP	P&A	X	X				
140	30	15	21783	1 H	185	27E	2490N 1299E	EMPIRE A&O UNIT No. 202	APACHE CORP	P&A	X	X				
169	30	15	21873	1 J	185	27E	1225S 1410E	EMPIRE A&O UNIT No. 191A	APACHE CORP	P&A	X	X				
1177	30	15	32259	1 E	185	27E	1650N 875W	EMPIRE A&O UNIT No. 005	APACHE CORP	NEW & P&A	X					
1064	30	15	32070	2 M	185	27E	6605-990W	BB STATE COM No. 001	APACHE CORP	P&A	X	X				
976	30	15	39009	2 G	185	27E	1650N 2430E	EMPIRE A&O UNIT No. 415	APACHE CORP	P&A	X	X				
843	30	15	22333	11 D	185	27E	4520N 1175W	EMPIRE A&O UNIT No. 133B	APACHE CORP	P&A	X	X				
841	30	15	22834	11 C	185	27E	225N 2280W	EMPIRE A&O UNIT No. 141B	APACHE CORP	P&A	X	X				
984	30	15	39020	31 O	175	28E	1605-2360E	EMPIRE A&O UNIT No. 408	APACHE CORP	P&A	X	X				
74	30	15	21539	31 N	175	28E	1605-1400W	EMPIRE A&O UNIT No. 261	APACHE CORP	P&A	X	X				
988	30	15	39064	31 O	175	28E	1175S 1310E	EMPIRE A&O UNIT No. 403	APACHE CORP	P&A	X	X				

**TABLE V**  
**Wells that have been Temporally Abandoned since the 2016 PFO REPORT**  
**Wells Changes in the Combined One Mile Area of Review for Navajo's WDW-1, WDW-2, and WDW-3**

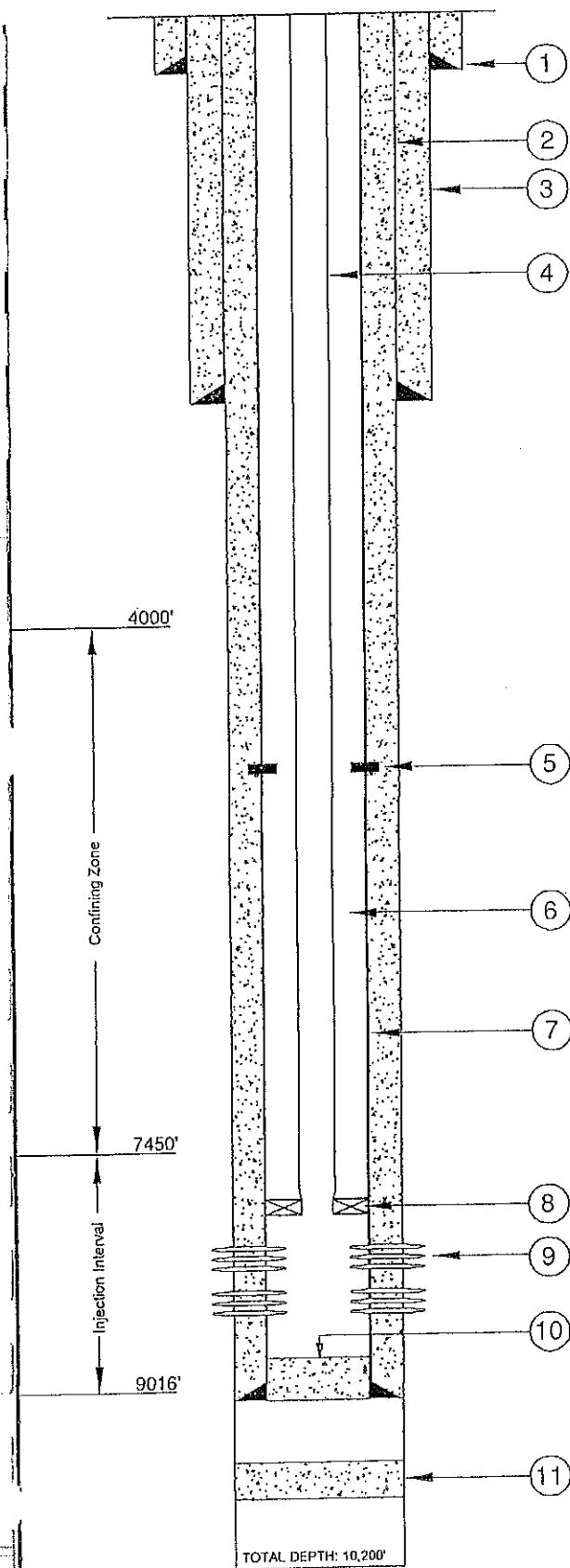
ID	API No.	Unit	Sect	Town	Range	Foothills	Well Name	Operator	Changes	Change of Owner	P&A	T&A	Prod	Recomp	New	Total
1168	3D	35	634	35P	175	28E	330S 330E	SOUTH RED LAKE UNIT NO. 029	REMANANT OIL OPERATING LLC	NEW AND TEMPORARILY ABANDONED	X	X		X		
148	3D	35	5934	36J	175	27E	1650S 1650E	EMPIRE ABO UNIT NO. 019A	APACHE CORP	TEMPORARILY ABANDONED	X	X				
975	3D	35	39401	36P	175	27E	1110S 50E	EMPIRE ABO UNIT NO. 417	APACHE CORP	TEMPORARILY ABANDONED	X	X				
155	3D	35	21792	1K	185	27E	1533S 3370W	EMPIRE ABO UNIT NO. 182	APACHE CORP	T&A	X	X				
152	3D	35	22095	1K	185	27E	2370S 1510W	EMPIRE ABO UNIT NO. 183	APACHE CORP	T&A	X	X				
148	3D	35	21565	1J	185	27E	2205-1590E	EMPIRE ABO UNIT NO. 192	APACHE CORP	T&A	X	X				
146	3D	35	22857	1J	185	27E	2490S 2200E	EMPIRE ABO UNIT NO. 193	APACHE CORP	T&A	X	X				
174	3D	35	22658	1J	185	27E	1500S 210E	EMPIRE ABO UNIT NO. 194	APACHE CORP	NEW & T&A	X	X				
1176	3D	35	32308	1C	185	27E	430N 2310W	A&O FEDERAL NO. 002	APACHE CORP	NEW & T&A	X	X				
765	3D	35	774	2A	185	27E	590N 330E	EMPIRE ABO UNIT NO. 015B	APACHE CORP	CHANGE OF OPERATOR & T&A	X	X				
67	3D	35	1661	32K	175	28E	1650S 2310W	EMPIRE ABO UNIT NO. 026B	APACHE CORP	T&A	X	X				
75	3D	35	22095	32J	175	28E	330S 2481E	EMPIRE ABO UNIT NO. 272	APACHE CORP	T&A	X	X				
76	3D	35	2606	51C	185	28E	310N 1841W	EMPIRE ABO UNIT NO. 026E	APACHE CORP	T&A	X	X				
187	3D	35	22526	5B	185	28E	1800N 3458E	EMPIRE ABO UNIT NO. 272A	APACHE CORP	T&A	X	X				
102	3D	35	24221	6F	185	28E	2830N 1930W	EMPIRE ABO UNIT NO. 223	APACHE CORP	T&A	X	X				
1190	3D	35	35237	18M	185	28E	810S 660W	LEATHERSTOCKING 18 STATE COM.V.F PETROLEUM INC.			X	X				





## FIGURES

## BELOW GROUND DETAILS



All depths are referenced to the Kelly bushing elevation of 12.5' above ground level. Ground level elevation is 3,678' above mean sea level.

1. Surface Casing: 13  $\frac{3}{8}$ ", 48 lb/ft, J-55, ST&C set at 390' in a 17  $\frac{1}{2}$ " hole. Cemented with 150 sx Class C with 3 % calcium chloride, 375 sx Class C Litecate w/3 % calcium chloride and  $\frac{1}{2}$  lb/sx flocole. Circulated 86 sx to surface.
2. Intermediate Casing: 9  $\frac{5}{8}$ ", 36 lb/ft, J-55, ST&C set at 2,555' in a 12  $\frac{1}{4}$ " hole. Cemented w/800 sx of Class C Lite w/  $\frac{1}{2}$  lb/sx flocole and 1 lb/sx Gilsonite and 12 % salt. Followed by 200 sx of Class C w/2 % calcium chloride. Circulated 133 sx to surface.
3. Base of the USDW at 493'.
4. Injection Tubing: 4  $\frac{1}{2}$ ", 11.6 lb/ft, N-80, SMLS, R3, LT&C set at 7,879'.
5. DV Tool: at 5,498'.
6. Annulus Fluid: 8.7 lb/gal brine water mixed w/UniChem Techni-Hib 370 corrosion inhibitor.
7. Protection Casing: 7", 29 lb/ft, N-80, LT&C: 9094' to 7031'. 7", 29 lb/ft, P-110, LT&C: 7031' to 5845'. 7", 26 lb/ft, P-110, LT&C: 5845' to surface. Casing cemented in two stages as follows:  
 First Stage - 600 sx modified Class H w/0.4 % CFR-3, 5 lb/sx Gilsonite, 0.5% Halad-344, and 1 lb/sx salt mixed at 13.0 ppg. Opened DV tool at 5498' and circulated 142 sx to surface.  
 Second Stage - Lead Slurry: 220 sx Interfill "C" (35:65:6) mixed at 11.7 ppg. Tail Slurry: 550 sx modified Class H w/0.4 % CFR-3, 5 lb/sx, Gilsonite, 0.5 % Halad-344, 0.1% HR-7, and 1 lb/sx mixed at 13.0 ppg. Circulated 75 sx to surface. Top out w/20 sx permium plus 3 % calcium chloride.
8. Packer: 7" x 3.5" EVI Oil Tools (Arrow), Model X-1 retrievable packer set at 7879'. Minimum I.D. is 3.0". Wireline re-entry guide on bottom. To release: turn  $\frac{1}{4}$  turn to the right and pick up.
9. Perforations (2 SPF):  
 Upper Zone - 7924-7942', 7974-8030', 8050-8056', 8066-8080', 8118-8127', 8132-8140', 8160-8164', 8170-8188'.  
 Lower Zone - 8220-8254', 8260-8270', 8280-8302', 8360-8366', 8370-8378', 8400-8410', 8419-8423', 8430-8446', 8460-8464', 8470-8476'.
10. PBTD: 9004'.
11. Cement Plug: 45 sx Class H from 9624' to 9734'.

SUBSURFACE		HOUSTON, TX. SOUTH BEND, IN. BATON ROUGE, LA.
NAVAJO REFINING COMPANY ARTESIA, NEW MEXICO		
<b>Below Ground Details</b> <b>Waste Disposal Well No. 1</b>		
DATE: 07/13/01	CHECKED BY:	JOB NO: 700526
DRAWN BY: WDL	APPROVED BY:	DWG. NO:

FIGURE 1

### Chukka Pressure and Temperature

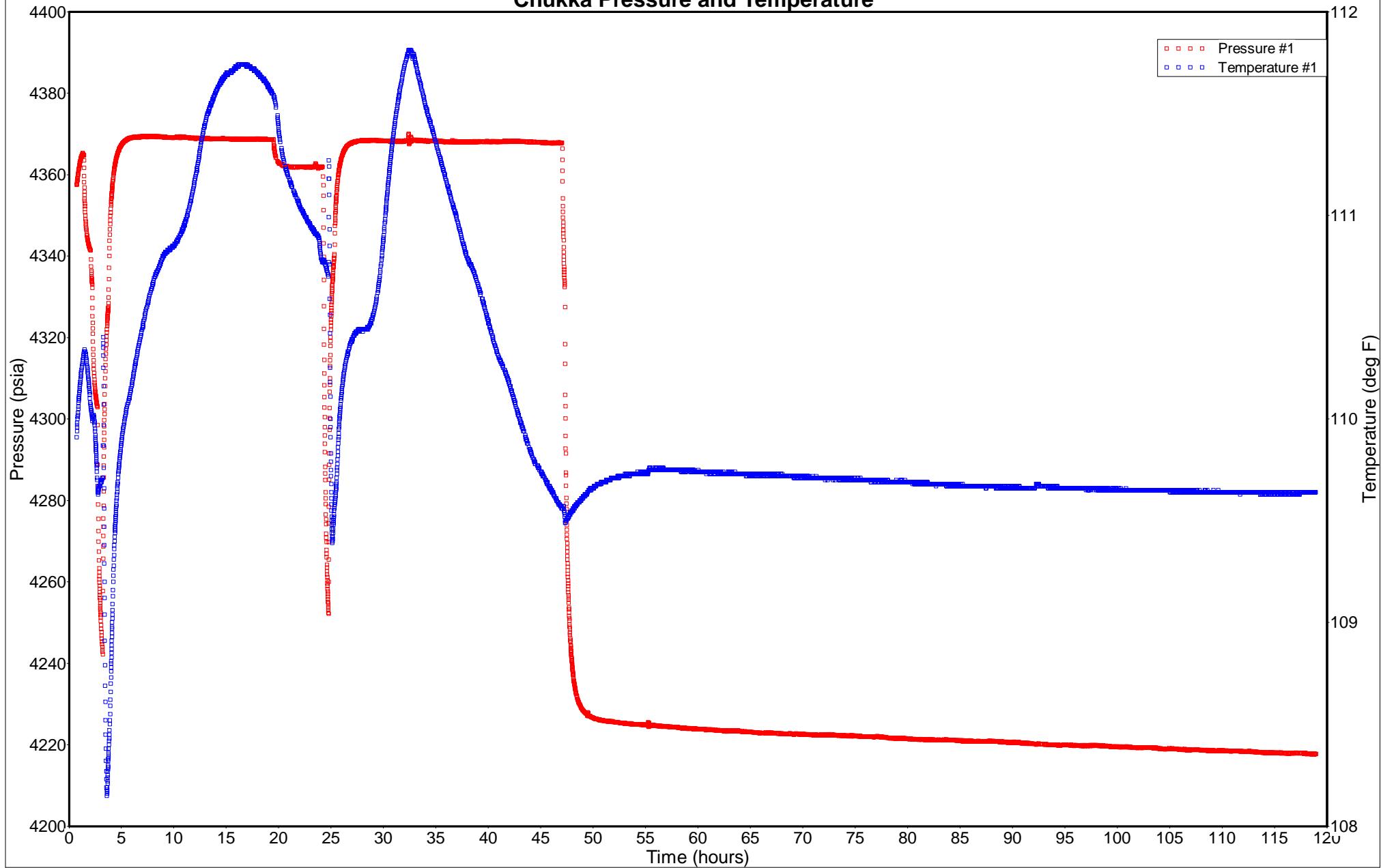
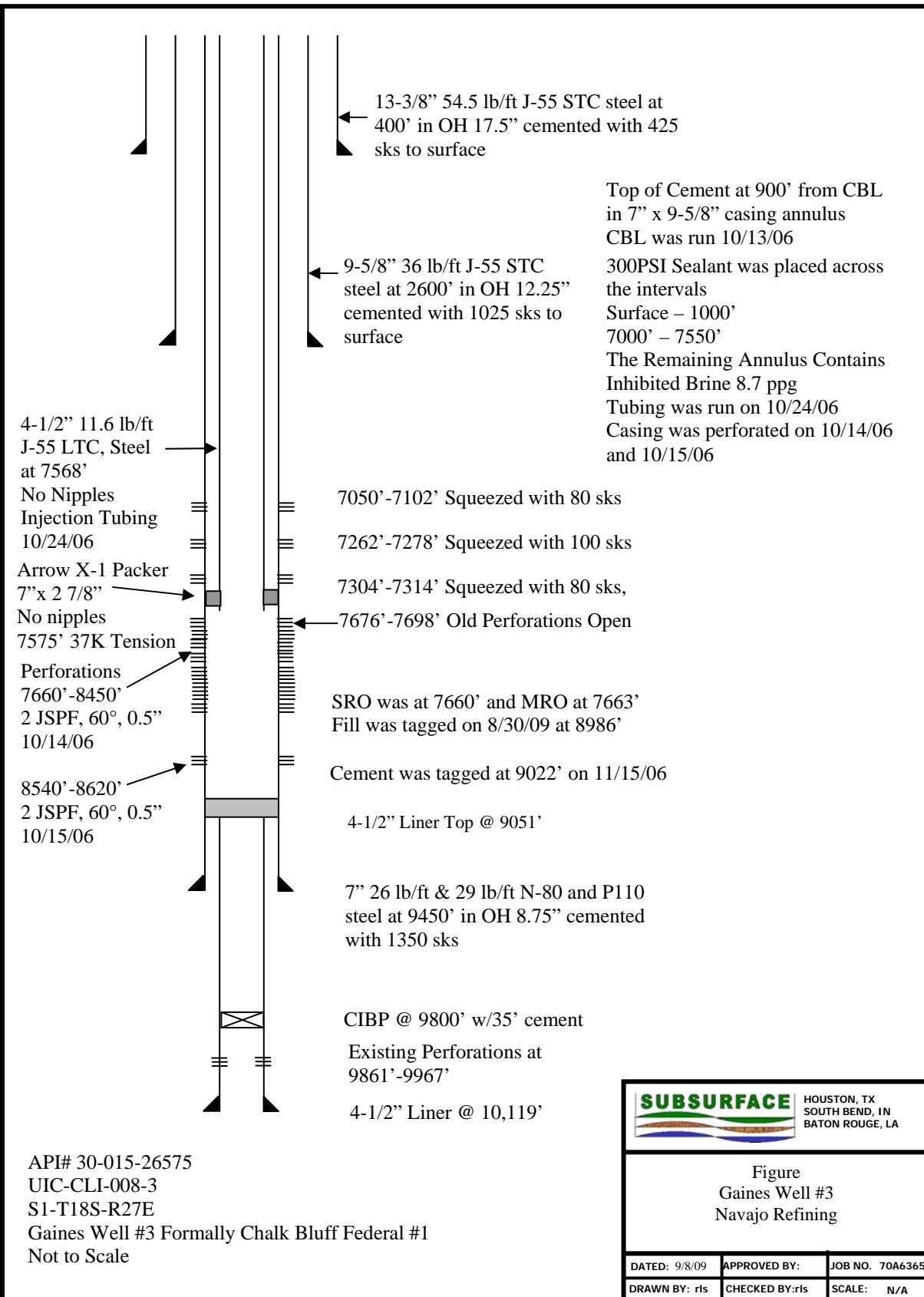
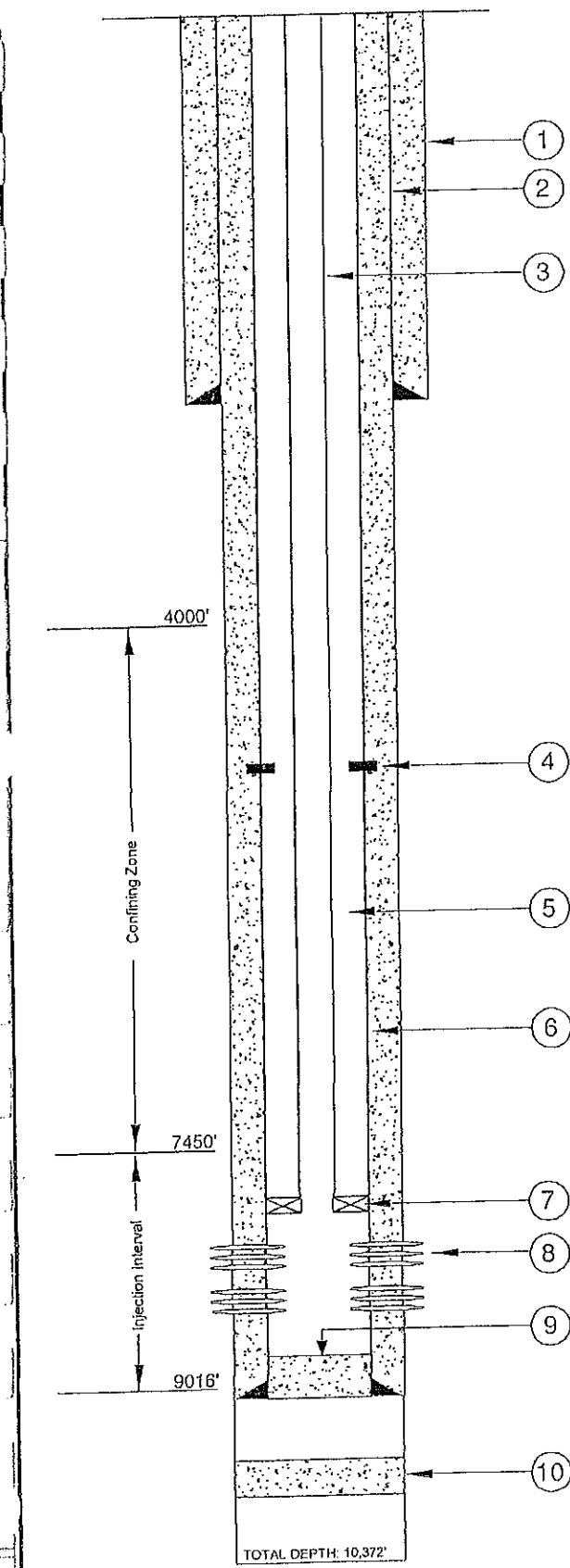


FIGURE 2



<b>SUBSURFACE</b>		HOUSTON, TX SOUTH BEND, IN BATON ROUGE, LA
Figure Gaines Well #3 Navajo Refining		
DATED: 9/8/09	APPROVED BY:	JOB NO. 70A6365
DRAWN BY: rls	CHECKED BY: rls	SCALE: N/A

**FIGURE 3**



### BELOW GROUND DETAILS

All depths are referenced to the Kelly bushing elevation of 13' above ground level. Ground level elevation is 3610' above mean sea level.

1. Base of the USDW at 473'.
2. Surface Casing: 8 5/8", 32 lb/ft, set at 1995' in an 11" hole. Cemented to surface with 800 sacks of cement.
3. Injection Tubing: 3 1/2", 9.2 lb/ft, J-55, smls, NUE 10 rd, set at 7528'.
4. DV Tool: at 5,785'.
5. Annulus Fluid: 8.7 lb/gal brine water mixed w/UniChem Techni-Hib 370 corrosion inhibitor.
6. Protection Casing: 5 1/2", 17 lb/ft, L-80, LT&C: 8869' to the surface and set in a 7 7/8" hole. Casing cemented in two stages as follows:
 

First Stage - 575 sacks of modified Class "H" with 0.4 % CFR-3, 5 lb/sk Gilsonite, 0.5 % Halad-344, and 3 lb/sk salt. Mixed at 13.0 ppg. Opened DV tool at 5785 and circulated 20 sacks to surface.

Second Stage - Lead Slurry: 300 sacks of Interfill "C" (35:65:6) mixed at 11.7 ppg. Tail slurry: 695 sacks modified Class "H" with 0.4% CFR-3, 5 lb/sk Gilsonite, 0.5 % Halad-344 and 3 lb/sk salt mixed at 13.0 ppg. Circulated 150 sacks to surface. Topped out with 10 yards of Redi-mix.
7. Packer: 5 1/2" x 2 7/8" Weatherford Completion Tools (Arrow) Model X-1 retrievable packer set at 7528'. Minimum ID is 2.4375". Wireline re-entry guide is on bottom. To release: turn 1/4 turn to the right and pick up.
8. Perforations (2 SPF):
 

Zone 1: 7570-7620', 7676-7736'

Zone 2: 7826-7834', 7858-7880', 7886-7904', 7916-7936', 7944-7964', 7990-8042', 8096-8116', 8191-8201', 8304-8319', 8395-8399'.
9. PBTD: 8770'
10. Cement Plug: 45 sacks from 9675' to 9775'.

SUBSURFACE		HOUSTON, TX. SOUTH BEND, IN. BATON ROUGE, LA.
NAVajo REFINING COMPANY ARTESIA, NEW MEXICO		
<b>BELow GROUND DETAILS</b> <b>WASTE DISPOSAL WELL NO. 2</b>		
DATE: 07/13/01	CHECKED BY:	JOB NO: 7005256
DRAWN BY: WDL	APPROVED BY:	DWG. NO:

FIGURE 4

### Gaines Pressure and Temperature

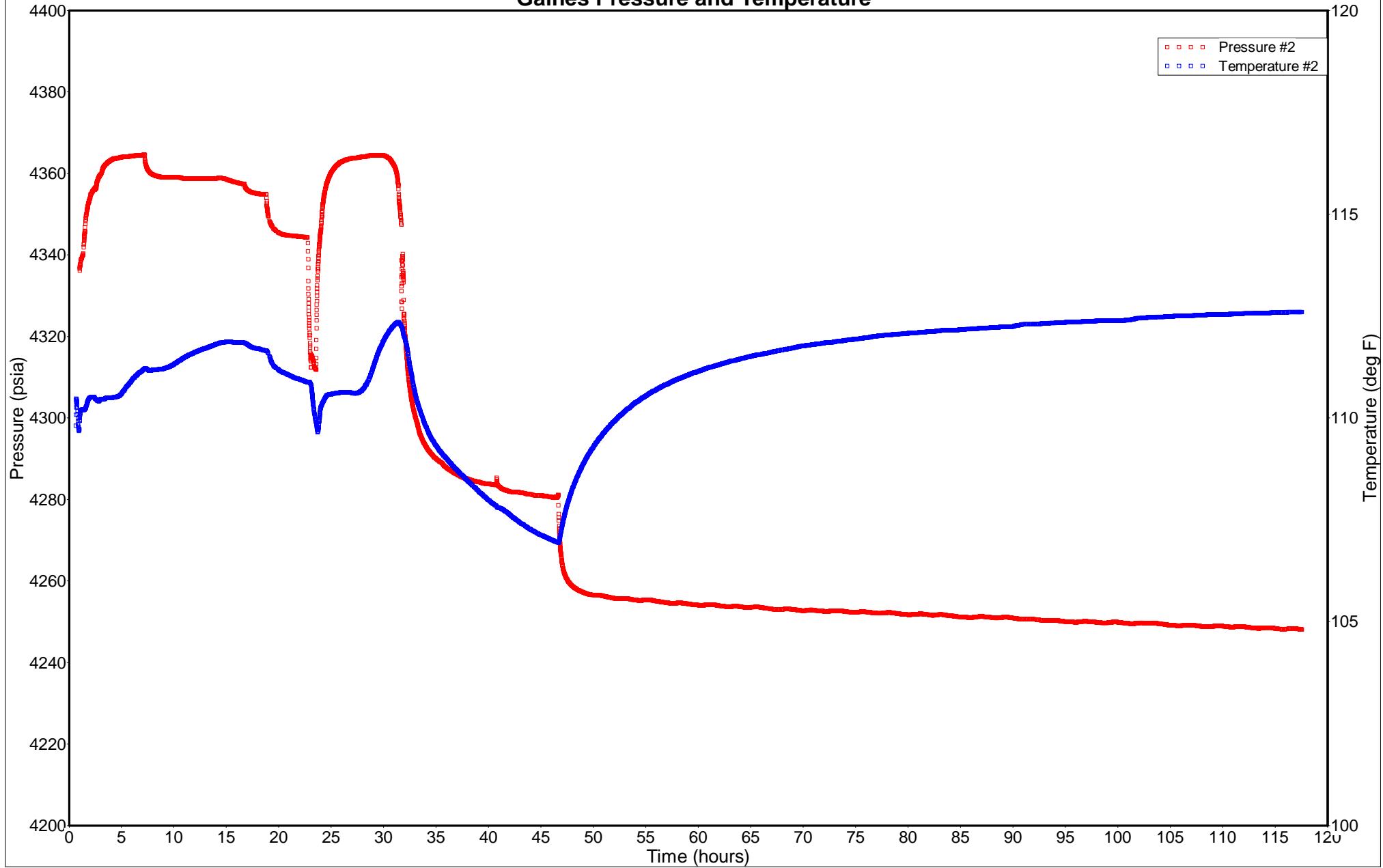



FIGURE 5



The image features the WSP USA Inc. logo on the left, consisting of the letters 'WSP' in a stylized red font. To the right of the logo is a vertical red bar. To the right of the bar is a white rectangular area containing the company's address and contact information in black text.

**NAVAJO REFINING COMPANY, L.L.C.  
ARTESIA, NEW MEXICO**

# **NON-FRESHWATER WELLS IN THE AREA OF REVIEW**

WELL: NAVAJO REFINING MEWBURNE WELL NO. 1

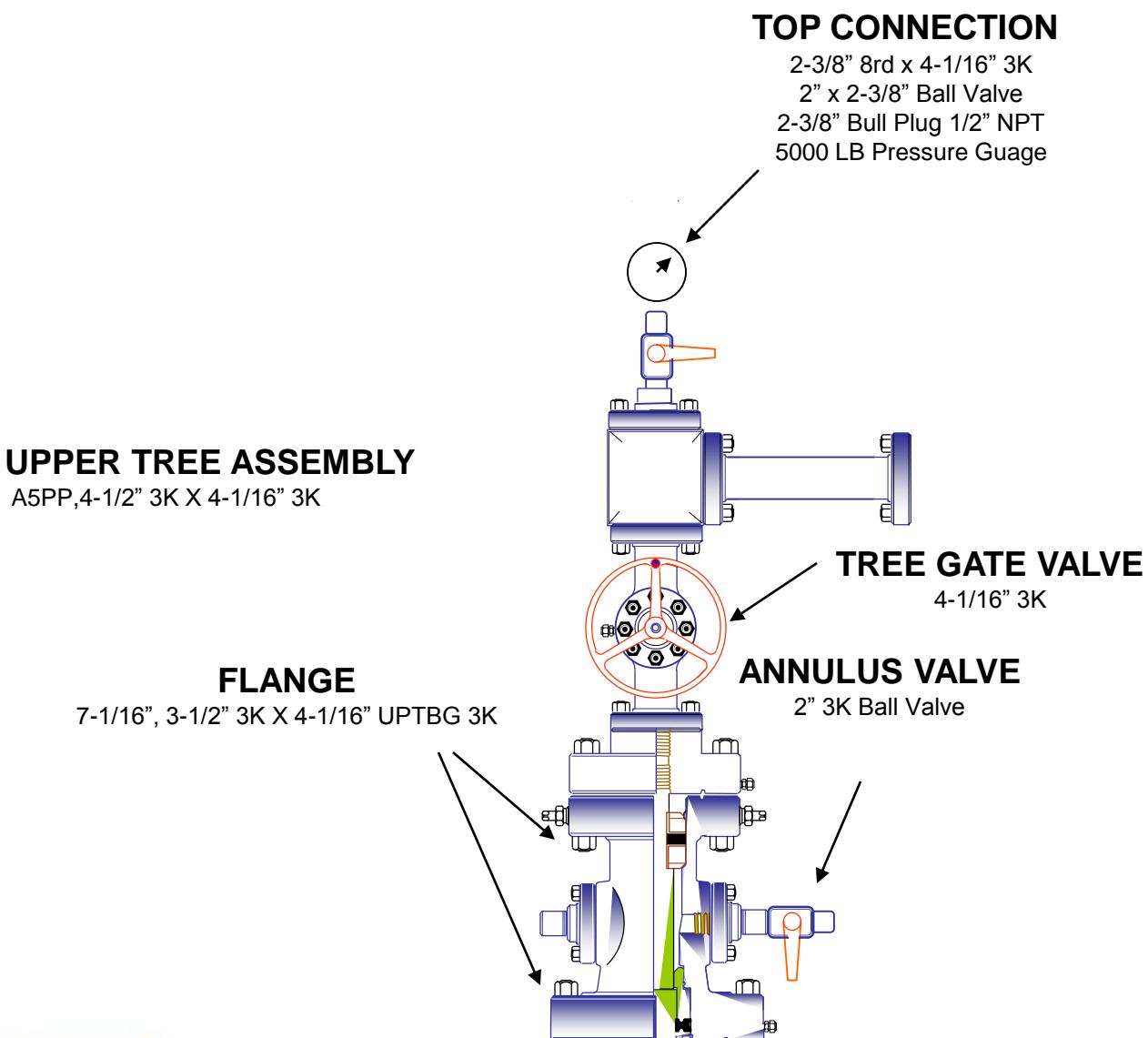
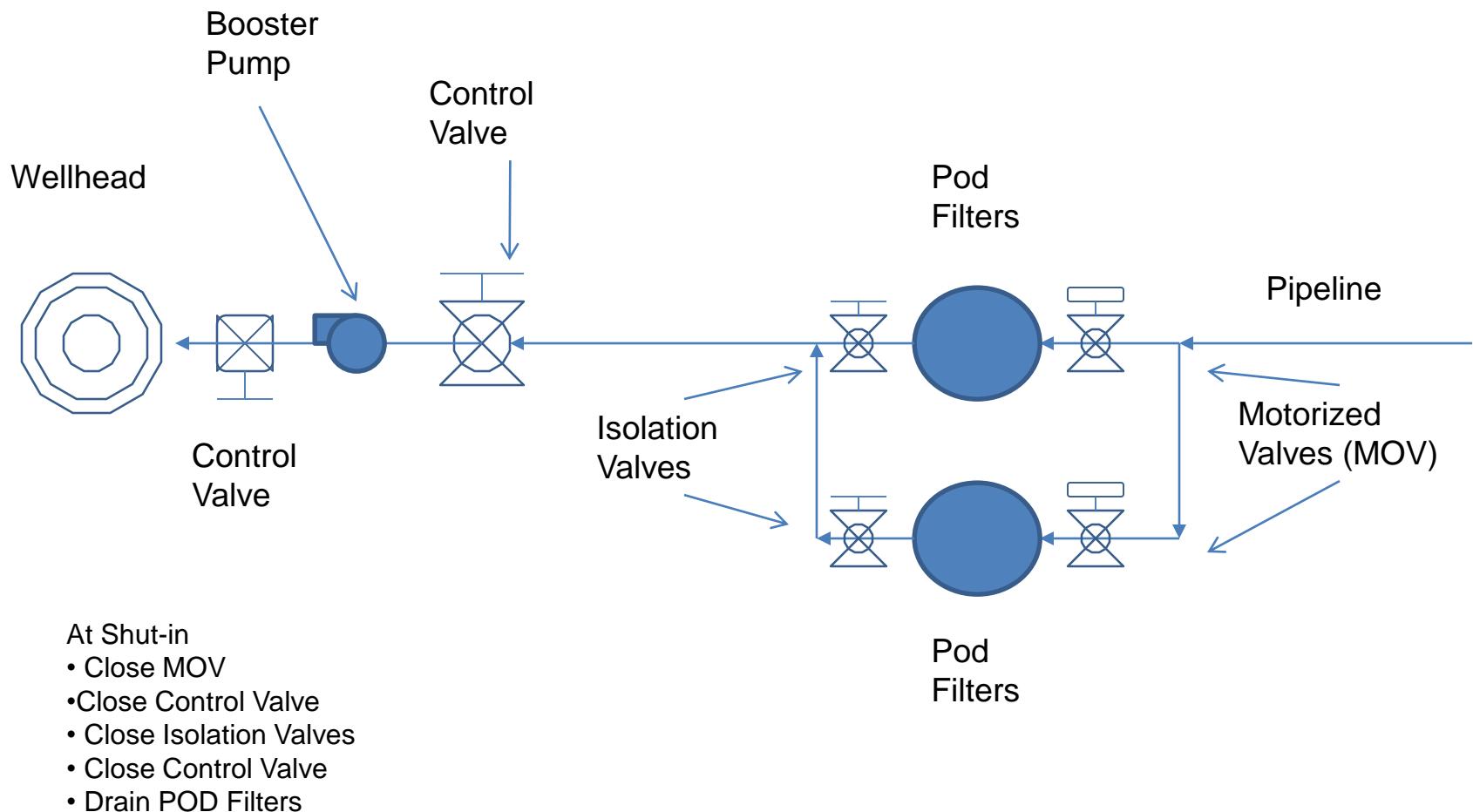


FIGURE 8  
Mewbourne Well No. 1  
Diagram of Shut-in Valve Control



### Test Overview

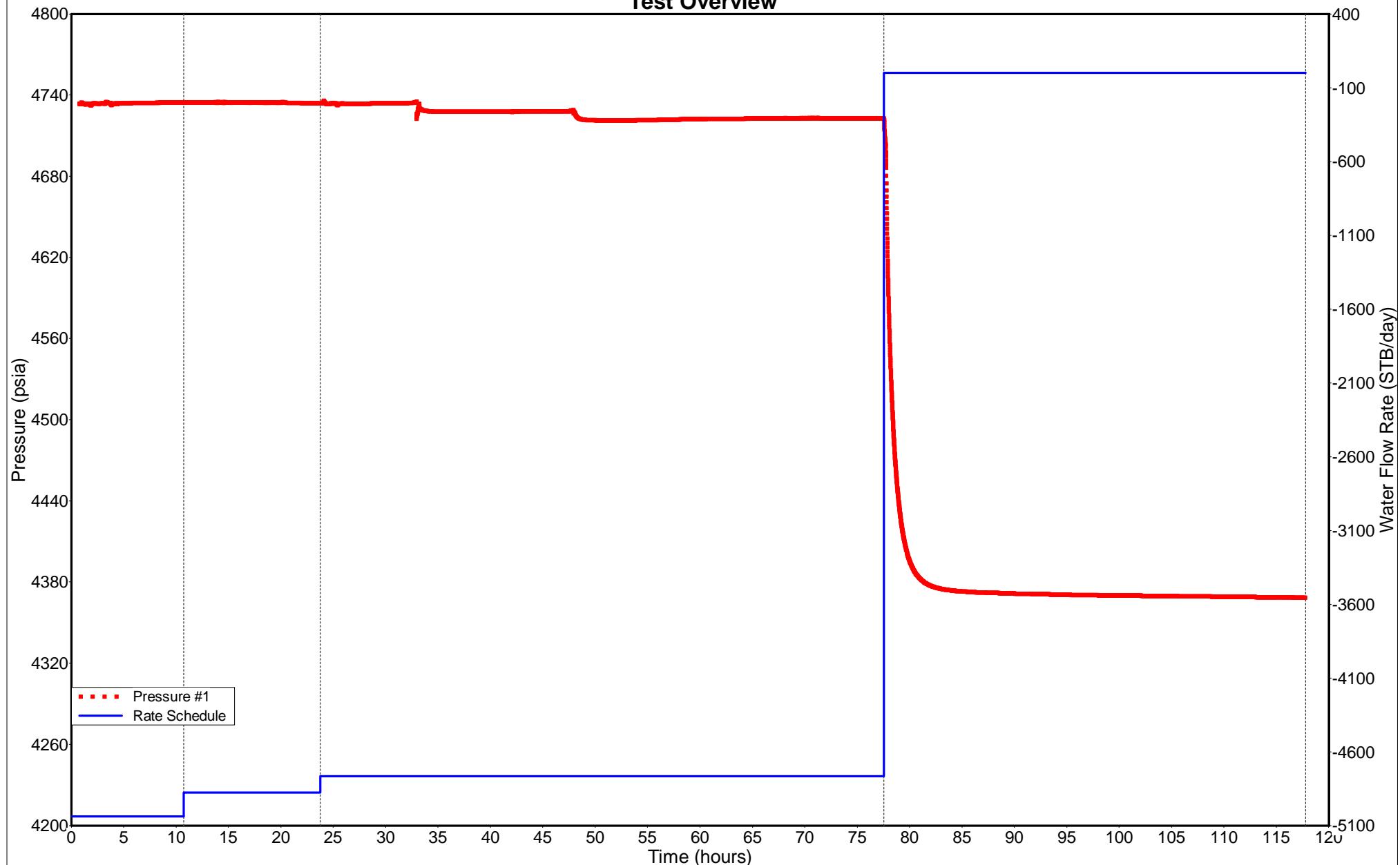


FIGURE 9

### Mewbourne Pressure and Temperature

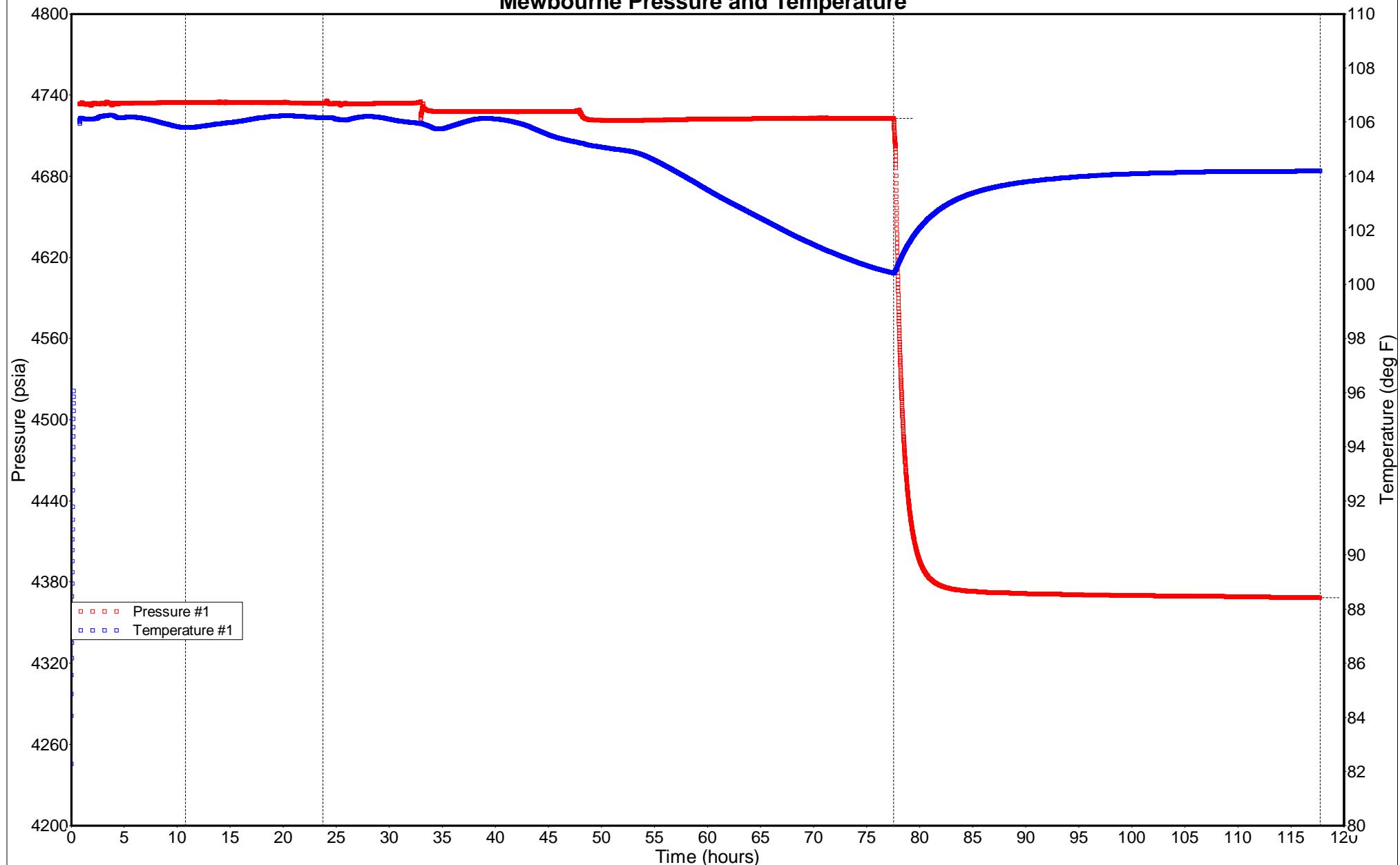


FIGURE 10

### Mewbourne Pressure and Injection Rates

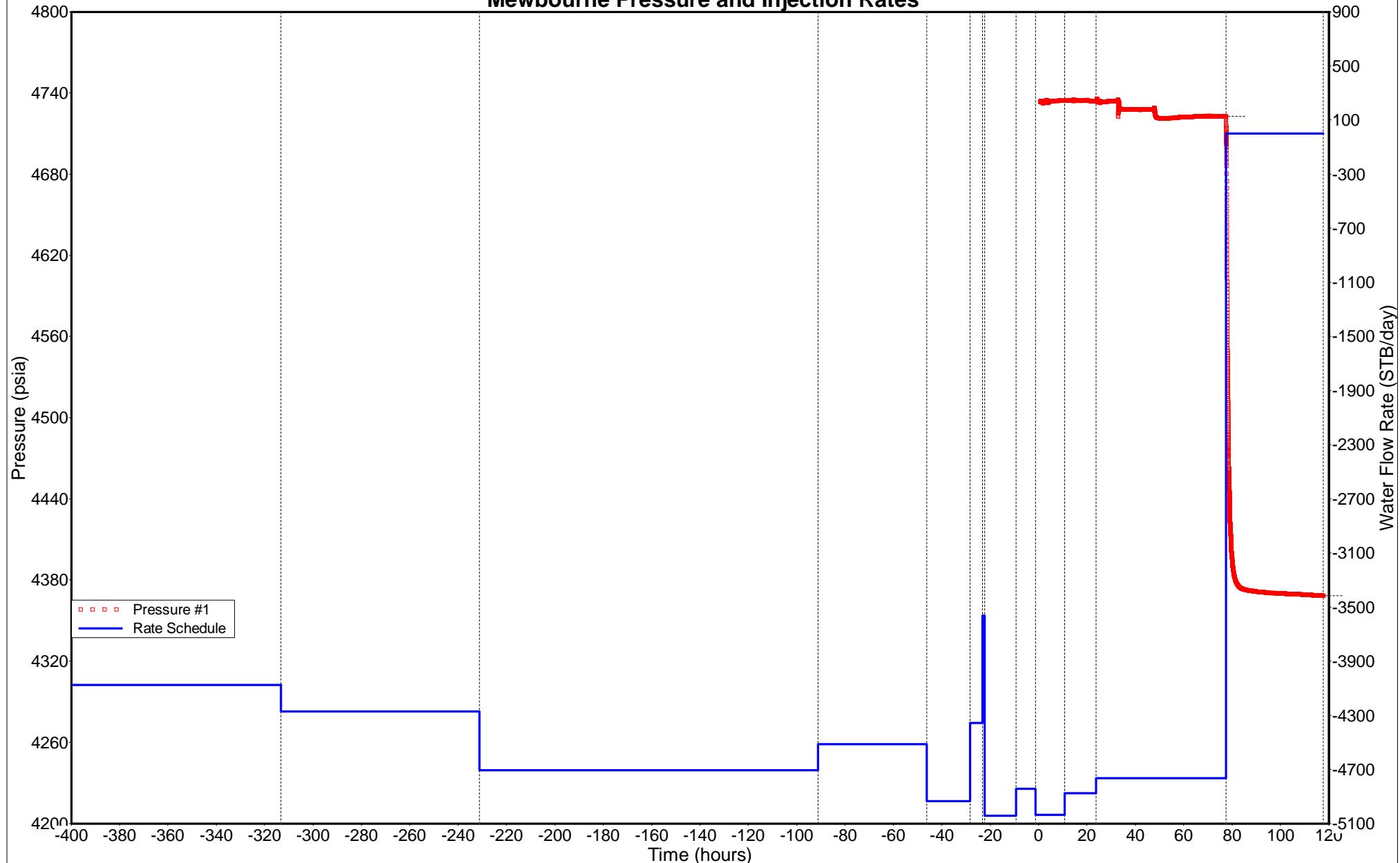
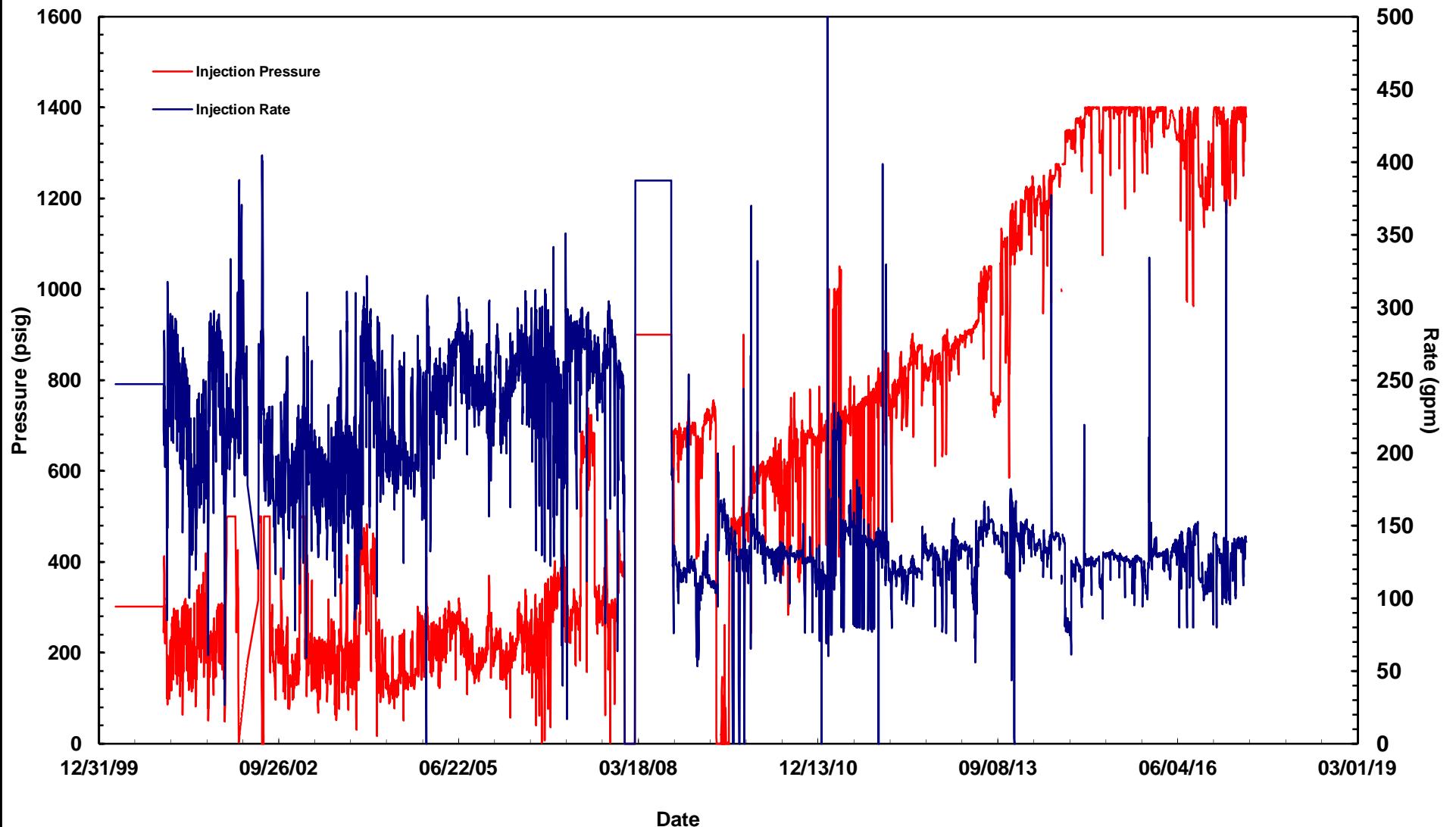


FIGURE 11

**Mewbourne Well No. 1**  
**Cartesian Plot of Surface Pressure and Injection Rates**  
**December 24, 2000 to June 19, 2017**



**FIGURE 12**

### Log-Log Plot

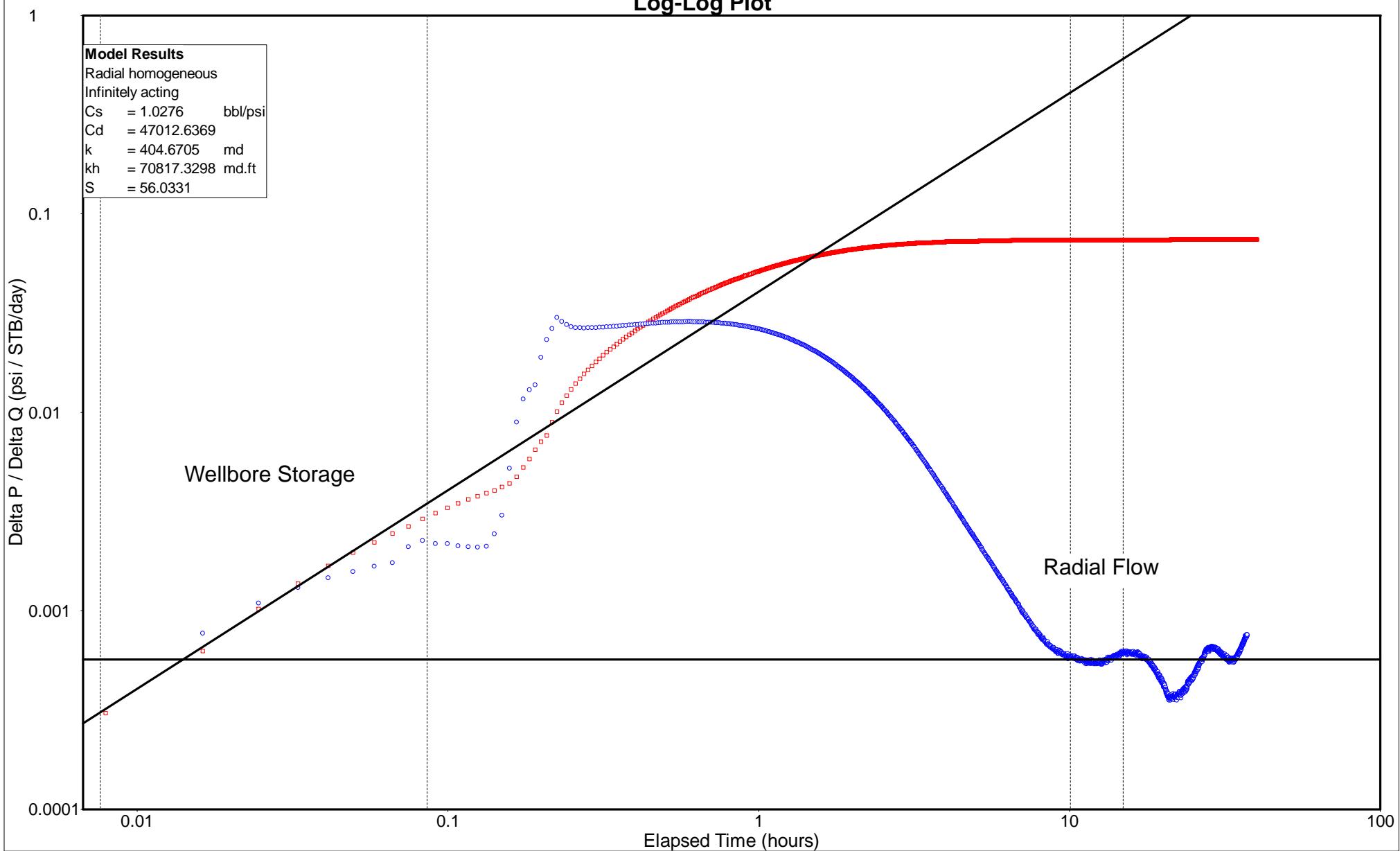


FIGURE 13

### Superposition Horner Plot

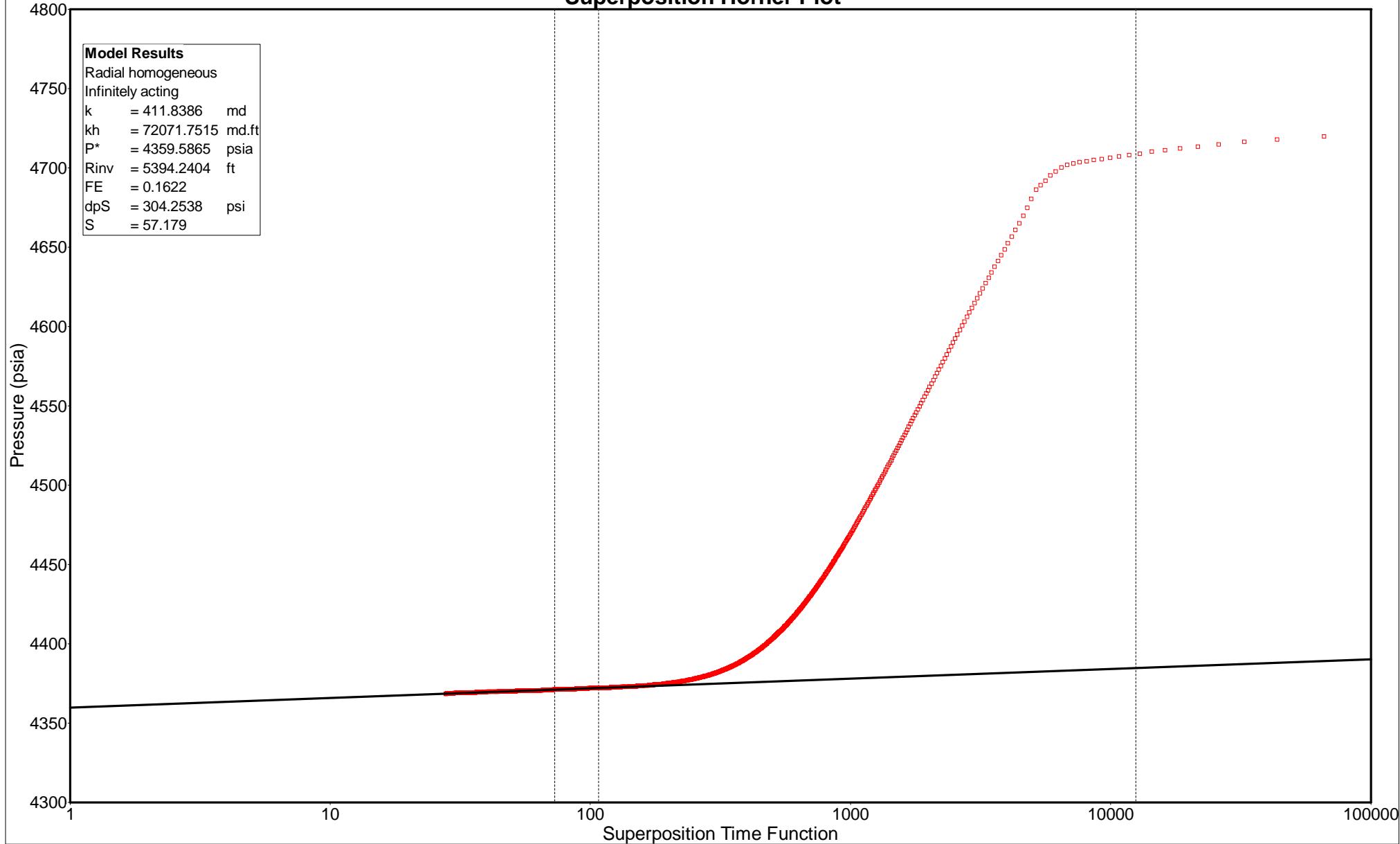


FIGURE 14

### Superposition Horner Plot

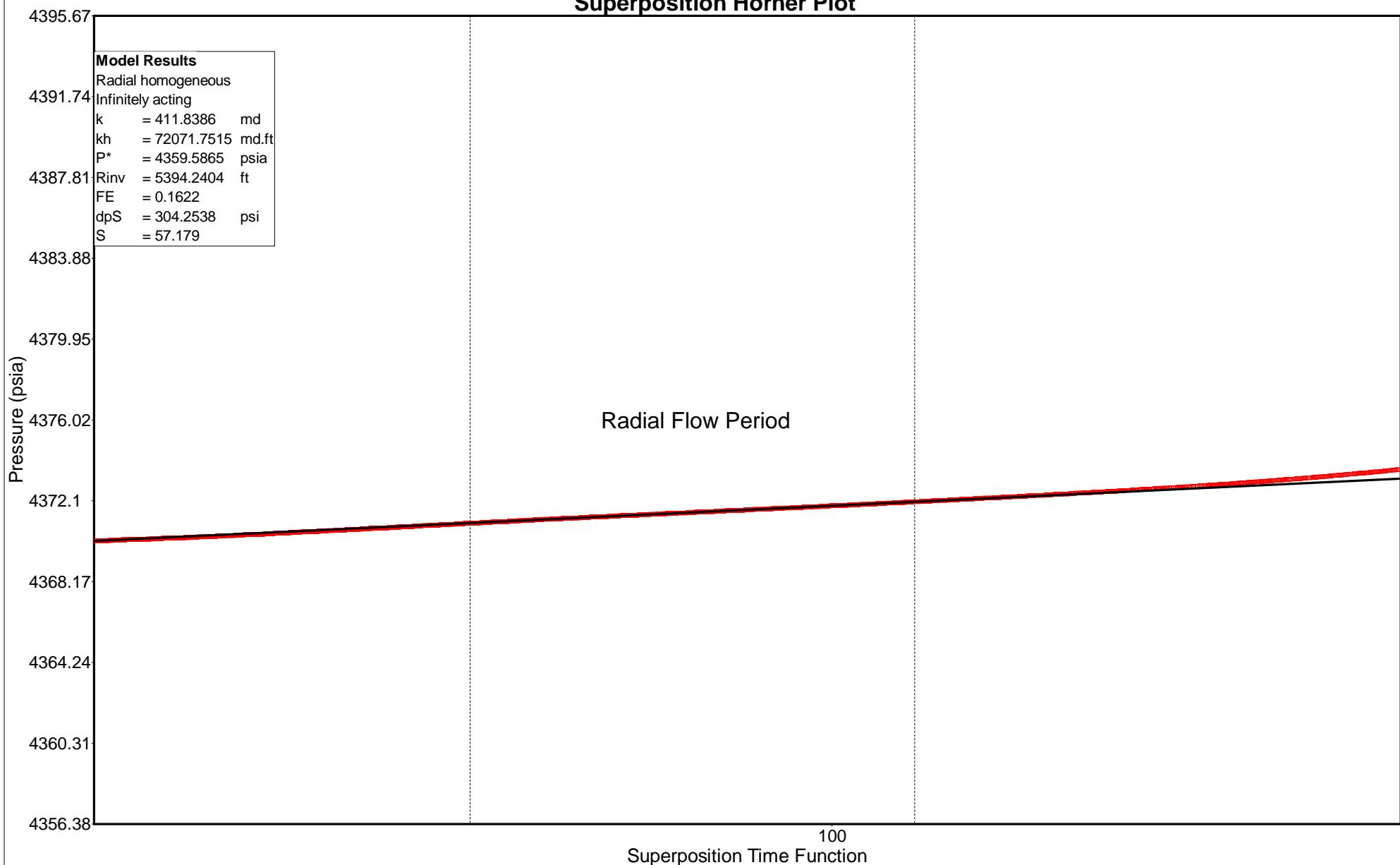
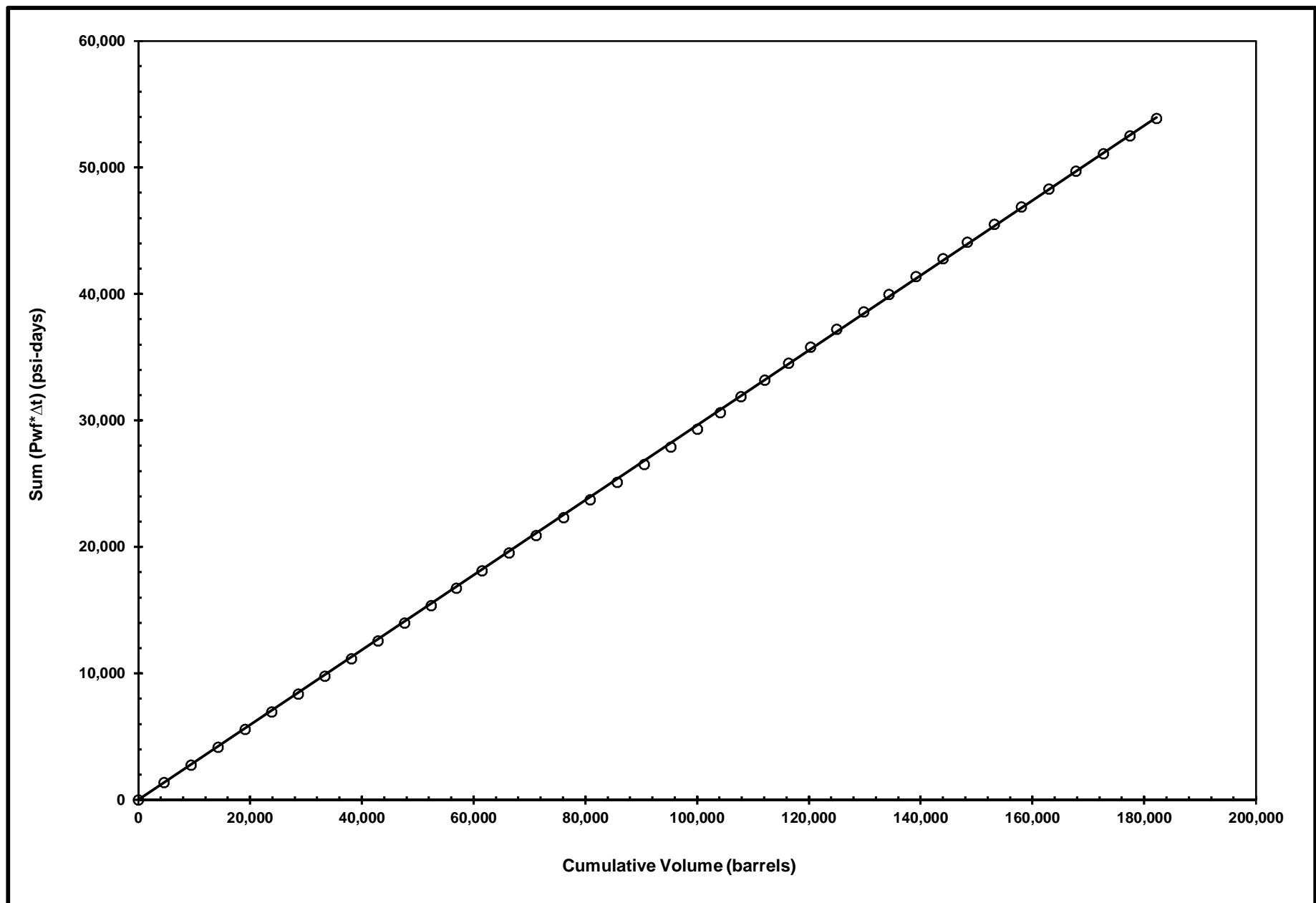


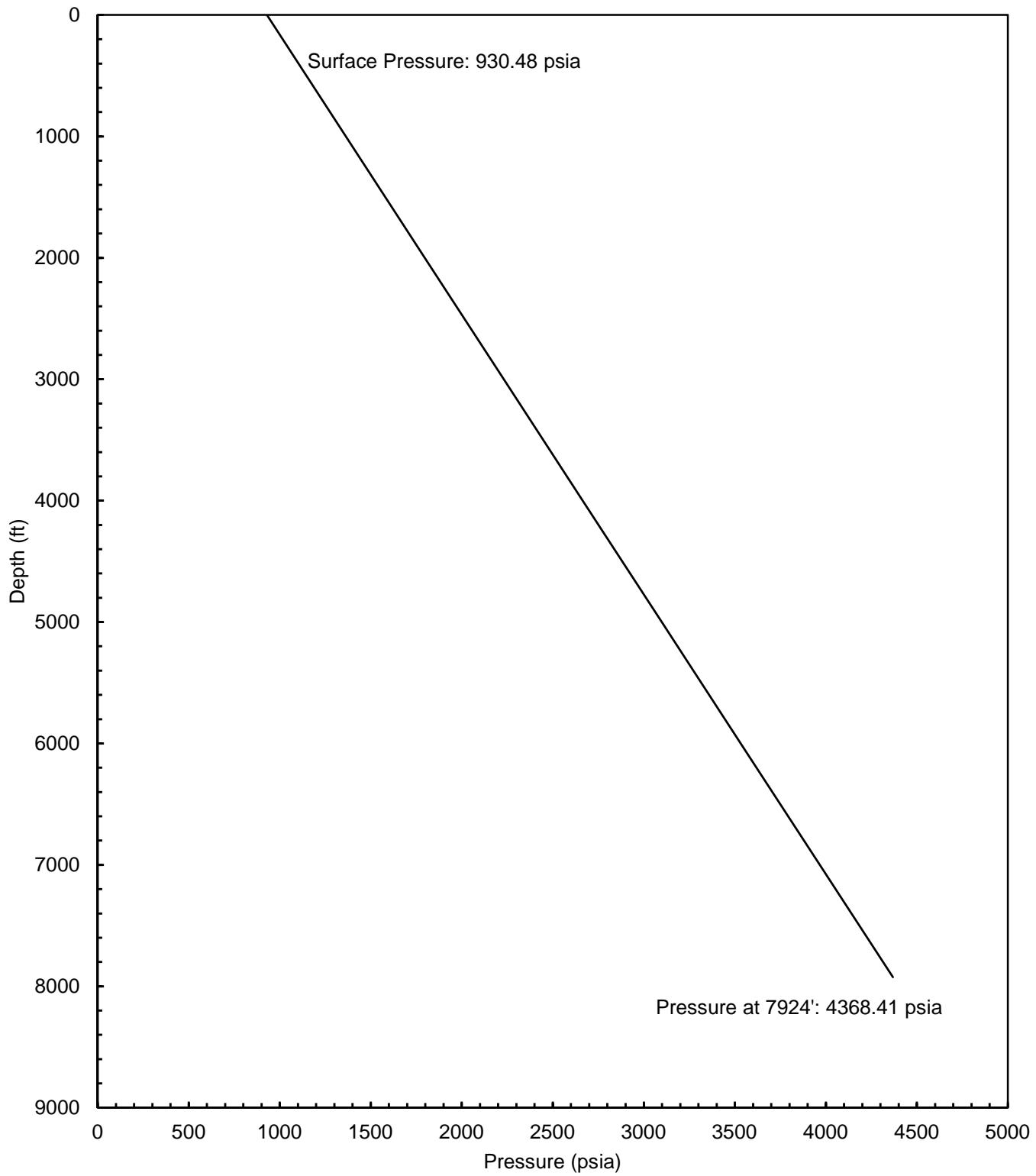
FIGURE 15

**Navajo Refining Company**  
**Mewbourne Well No. 1**  
**May 11, 2017 to June 19, 2017**  
**Hall Plot**



**FIGURE 16**

**Navajo Refining  
Static Pressure Gradient Survey  
Mewbourne Well No. 1  
June 21, 2017**



**FIGURE 17**

## APPENDICES

## APPENDIX A

### DUAL INDUCTION LOG SECTIONS FROM 7924 FEET TO 8476 FEET

## APPENDIX B

### NEUTRON DENSITY LOG SECTIONS FROM 7924 FEET TO 8476 FEET

## **APPENDIX C**

### **COMPRESSIBILITY OF FLUID**

## APPENDIX C

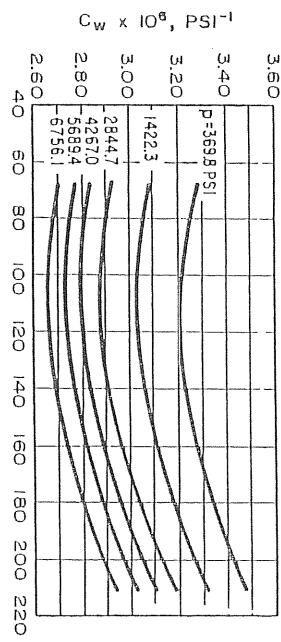


Fig. D.16 Average compressibility of distilled water. After Long and Chierici.<sup>13</sup>

Source: Earlougher, 1977, Advances in Well Test Analysis

## COMPRESSIBILITY OF PORE VOLUME AND DISTILLED WATER

## APPENDIX D

### COMPRESSIBILITY OF PORE VOLUME

APPENDIX D

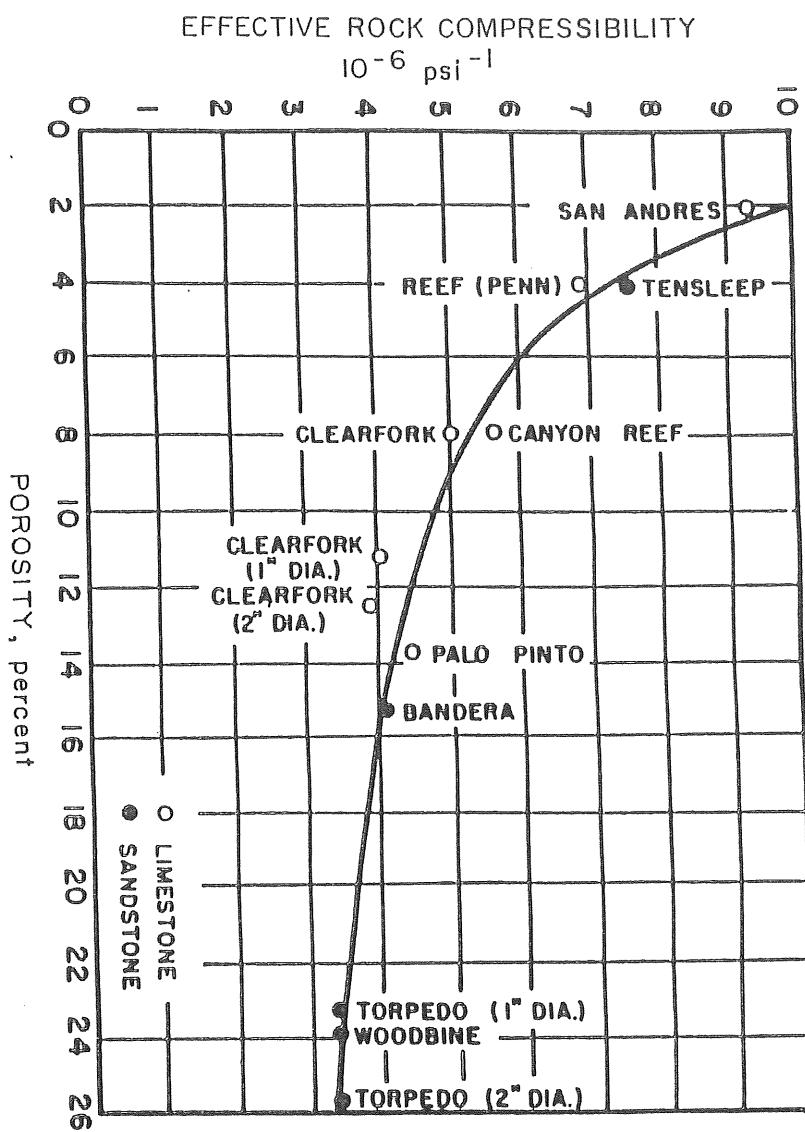


Fig. G.5 Effective formation (rock) compressibility. From Hall, *Trans., AIME* (1953) 198, 309.

Source: Matthews and Russell, 1967, Pressure Buildup and Flow Tests in Wells

## APPENDIX E

### **MEWBOURNE WELL NO. 1, JULY 23, 1998, TEMPERATURE LOG**

## APPENDIX F

### WATER VISCOSITIES AT VARIOUS SALINTIES AND TEMPERATURES

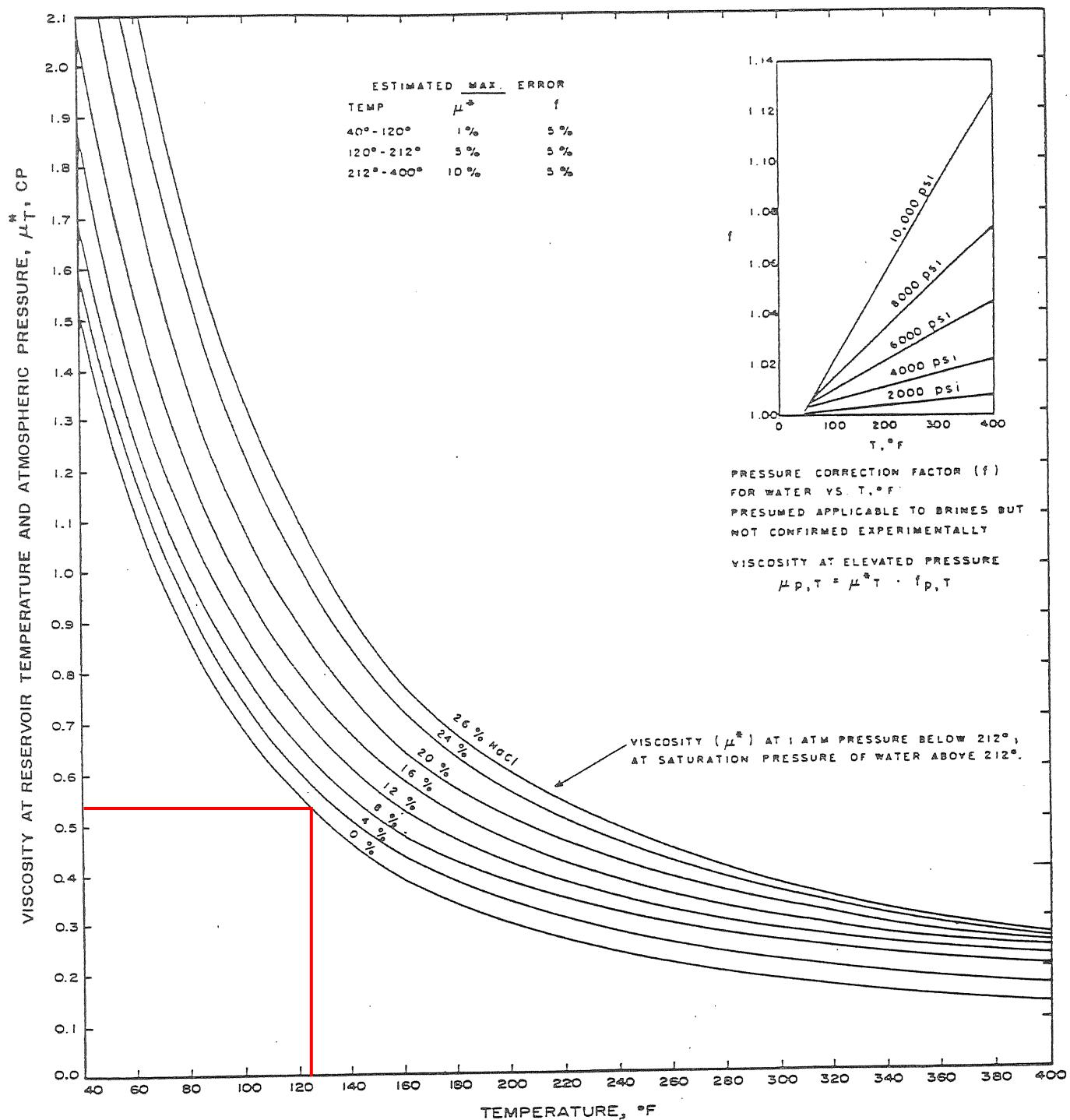


Fig. D.35 Water viscosity at various salinities and temperatures. After Matthews and Russell, data of Chesnut.<sup>18</sup>

FROM: Earlougher, R.C., 1977, "Advances in Well Test Analysis", SPE of AIME, Dallas, Texas

## **APPENDIX G**

### **DAILY RATE HISTORY DATA**

**APPENDIX G**  
**MEWBURNE #1**  
**DAILY RATE HISTORY**

Date	Rate	Pressure	Date	Rate	Pressure
	(gpm)	(psia)		(gpm)	(psia)
06/16/2016	138.27	1392.68	08/01/2016	134.88	1400.14
06/17/2016	143.57	1356.61	08/02/2016	148.08	1385.65
06/18/2016	136.13	1359.17	08/03/2016	145.17	1382.63
06/19/2016	135.89	1367.41	08/04/2016	144.39	1390.23
06/20/2016	137.19	1323.93	08/05/2016	146.05	1386.89
06/21/2016	128.47	1277.77	08/06/2016	145.09	1394.28
06/22/2016	119.12	1150.71	08/07/2016	147.00	1400.24
06/23/2016	106.65	1400.28	08/08/2016	147.88	1263.31
06/24/2016	145.86	1400.19	08/09/2016	122.36	1129.91
06/25/2016	145.75	1393.68	08/10/2016	107.24	1390.22
06/26/2016	143.70	1396.15	08/11/2016	146.28	1367.76
06/27/2016	143.87	1393.95	08/12/2016	141.77	1390.27
06/28/2016	144.37	1395.53	08/13/2016	145.33	1390.18
06/29/2016	145.39	1383.13	08/14/2016	145.47	1383.95
06/30/2016	142.27	1369.97	08/15/2016	144.84	1370.23
07/01/2016	139.08	1360.16	08/16/2016	142.00	1370.18
07/02/2016	137.61	1361.30	08/17/2016	141.99	1362.80
07/03/2016	138.03	1282.63	08/18/2016	140.45	1345.46
07/04/2016	121.45	1323.28	08/19/2016	136.75	1267.00
07/05/2016	131.26	1298.15	08/20/2016	118.71	1255.28
07/06/2016	125.03	1300.11	08/21/2016	115.19	1310.19
07/07/2016	125.34	1309.48	08/22/2016	127.75	1318.14
07/08/2016	126.77	1327.88	08/23/2016	130.06	1362.47
07/09/2016	130.67	1300.07	08/24/2016	138.96	1350.10
07/10/2016	125.41	1300.13	08/25/2016	136.89	1350.06
07/11/2016	126.11	1300.06	08/26/2016	137.16	1167.60
07/12/2016	125.95	1292.70	08/27/2016	108.09	965.41
07/13/2016	124.52	1275.20	08/28/2016	80.00	965.41
07/14/2016	121.25	1264.33	08/29/2016	80.00	962.44
07/15/2016	118.64	1275.18	08/30/2016	110.20	1148.73
07/16/2016	119.49	1275.22	08/31/2016	140.94	1360.46
07/17/2016	119.91	1288.11	09/01/2016	147.80	1390.16
07/18/2016	122.31	1300.09	09/02/2016	141.41	1360.54
07/19/2016	124.37	1320.28	09/03/2016	142.52	1366.28
07/20/2016	128.90	1348.93	09/04/2016	150.01	1396.43
07/21/2016	135.29	1350.14	09/05/2016	145.52	1376.00
07/22/2016	135.64	1350.13	09/06/2016	138.26	1344.45
07/23/2016	135.68	1163.78	09/07/2016	136.71	1333.27
07/24/2016	105.59	975.89	09/08/2016	142.60	1365.36
07/25/2016	80.00	972.38	09/09/2016	147.35	1377.41
07/26/2016	80.00	1184.29	09/10/2016	149.73	1395.77
07/27/2016	115.86	1375.22	09/11/2016	151.37	1400.19
07/28/2016	142.58	1381.10	09/12/2016	147.04	1378.17

**APPENDIX G**  
**MEWBOURNE #1**  
**DAILY RATE HISTORY**

Date	Rate	Pressure	Date	Rate	Pressure
	(gpm)	(psia)		(gpm)	(psia)
07/29/2016	143.64	1386.69	09/13/2016	148.59	1381.42
07/30/2016	145.03	1381.81	09/14/2016	151.08	1393.72
07/31/2016	143.68	1339.88	09/15/2016	145.43	1369.68
09/16/2016	145.77	1371.60	11/03/2016	102.42	1175.20
09/17/2016	144.41	1364.20	11/04/2016	102.95	1175.21
09/18/2016	147.36	1376.00	11/05/2016	118.30	1246.46
09/19/2016	147.43	1376.64	11/06/2016	111.22	1211.52
09/20/2016	149.67	1387.02	11/07/2016	112.51	1219.48
09/21/2016	144.93	1365.24	11/08/2016	108.14	1200.05
09/22/2016	144.09	1360.98	11/09/2016	107.50	1200.04
09/23/2016	152.43	1399.69	11/10/2016	107.66	1200.06
09/24/2016	148.76	1385.53	11/11/2016	107.69	1200.06
09/25/2016	139.68	1346.62	11/12/2016	107.59	1200.04
09/26/2016	139.45	1347.22	11/13/2016	106.55	1193.15
09/27/2016	134.43	1317.82	11/14/2016	103.06	1175.15
09/28/2016	120.38	1257.69	11/15/2016	103.43	1175.19
09/29/2016	118.76	1250.17	11/16/2016	104.00	1178.24
09/30/2016	114.82	1236.71	11/17/2016	109.72	1202.17
10/01/2016	113.00	1225.10	11/18/2016	118.48	1257.22
10/02/2016	113.90	1225.13	11/19/2016	120.54	1270.15
10/03/2016	113.17	1223.01	11/20/2016	119.86	1264.67
10/04/2016	112.82	1225.17	11/21/2016	118.03	1260.51
10/05/2016	112.20	1225.14	11/22/2016	128.44	1308.25
10/06/2016	112.78	1225.13	11/23/2016	130.25	1325.70
10/07/2016	112.19	1228.44	11/24/2016	123.18	1282.20
10/08/2016	111.82	1225.17	11/25/2016	123.94	1286.89
10/09/2016	111.37	1223.03	11/26/2016	104.46	1189.45
10/10/2016	110.78	1204.47	11/27/2016	104.53	1184.67
10/11/2016	113.00	1225.03	11/28/2016	112.28	1225.06
10/12/2016	113.03	1225.11	11/29/2016	112.03	1225.06
10/13/2016	111.69	1225.05	11/30/2016	111.00	1225.12
10/14/2016	112.37	1225.05	12/01/2016	120.38	1225.05
10/15/2016	113.77	1225.06	12/02/2016	117.32	1225.07
10/16/2016	113.91	1225.07	12/03/2016	122.03	1250.70
10/17/2016	111.16	1209.53	12/04/2016	122.99	1258.07
10/18/2016	116.33	1234.66	12/05/2016	131.02	1296.70
10/19/2016	124.50	1275.15	12/06/2016	130.89	1300.08
10/20/2016	113.51	1225.07	12/07/2016	125.91	1277.53
10/21/2016	107.59	1200.13	12/08/2016	104.84	1246.36
10/22/2016	108.23	1200.07	12/09/2016	109.77	1293.72
10/23/2016	108.63	1200.11	12/10/2016	124.56	1309.94
10/24/2016	105.44	1186.59	12/11/2016	129.70	1320.10
10/25/2016	105.08	1180.09	12/12/2016	126.29	1309.56

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**MEWBOURNE #1**  
**DAILY RATE HISTORY**

Date	Rate	Pressure	Date	Rate	Pressure
	(gpm)	(psia)		(gpm)	(psia)
10/26/2016	101.88	1167.51	12/13/2016	124.11	1300.09
10/27/2016	98.55	1150.15	12/14/2016	122.96	1300.12
10/28/2016	99.31	1136.62	12/15/2016	121.25	1300.06
10/29/2016	108.91	1200.18	12/16/2016	114.27	1261.38
10/30/2016	106.95	1188.82	12/17/2016	107.04	1266.62
11/01/2016	108.62	1200.08	12/18/2016	81.80	1173.42
11/02/2016	106.39	1192.01	12/19/2016	124.70	1351.47
12/20/2016	142.15	1379.63	02/06/2017	110.03	1285.25
12/21/2016	141.61	1379.71	02/07/2017	99.90	1249.12
12/22/2016	142.68	1389.50	02/08/2017	95.78	1229.69
12/23/2016	145.17	1400.18	02/09/2017	98.10	1244.20
12/24/2016	145.27	1400.14	02/10/2017	109.15	1283.96
12/25/2016	144.59	1400.21	02/11/2017	113.66	1300.10
12/26/2016	143.81	1400.20	02/12/2017	127.00	1366.60
12/27/2016	142.86	1397.14	02/13/2017	131.71	1400.22
12/28/2016	143.79	1395.94	02/14/2017	124.27	1365.28
12/29/2016	143.52	1400.21	02/15/2017	136.54	1366.68
12/30/2016	143.50	1400.16	02/16/2017	139.54	1376.31
01/01/2017	143.86	1400.24	02/17/2017	141.64	1384.30
01/02/2017	143.73	1400.22	02/18/2017	128.20	1318.59
01/03/2017	141.75	1388.07	02/19/2017	107.20	1224.86
01/04/2017	143.87	1399.77	02/20/2017	100.15	1194.66
01/05/2017	141.62	1398.32	02/21/2017	100.84	1195.92
01/06/2017	80.00	1383.49	02/22/2017	109.76	1235.90
01/07/2017	93.95	1375.50	02/23/2017	133.16	1350.16
01/08/2017	111.58	1400.22	02/24/2017	132.44	1352.63
01/09/2017	128.11	1359.54	02/25/2017	135.33	1370.12
01/10/2017	136.59	1396.20	02/26/2017	130.75	1346.21
01/11/2017	135.43	1395.48	02/27/2017	109.23	1239.06
01/12/2017	132.38	1386.10	03/01/2017	373.52	1167.66
01/13/2017	134.06	1396.60	03/02/2017	122.15	1297.83
01/14/2017	133.09	1398.64	03/03/2017	96.77	1183.27
01/15/2017	131.33	1395.20	03/04/2017	116.70	1268.20
01/16/2017	132.46	1395.19	03/05/2017	134.93	1353.57
01/17/2017	131.94	1396.51	03/06/2017	134.24	1346.49
01/18/2017	133.13	1400.17	03/07/2017	131.81	1335.43
01/19/2017	133.72	1400.26	03/08/2017	131.27	1338.58
01/20/2017	134.01	1400.23	03/09/2017	139.02	1374.36
01/21/2017	133.36	1400.23	03/10/2017	132.24	1350.96
01/22/2017	128.76	1374.36	03/11/2017	135.17	1361.16
01/23/2017	129.58	1379.00	03/12/2017	111.29	1265.53
01/24/2017	126.72	1364.82	03/13/2017	105.44	1234.46
01/25/2017	124.31	1364.18	03/14/2017	109.82	1250.05

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**MEWBOURNE #1**  
**DAILY RATE HISTORY**

Date	Rate	Pressure	Date	Rate	Pressure
	(gpm)	(psia)		(gpm)	(psia)
01/26/2017	127.57	1381.79	03/15/2017	99.99	1205.21
01/27/2017	127.23	1384.19	03/16/2017	98.79	1200.06
01/28/2017	128.48	1385.20	03/17/2017	98.93	1200.06
01/29/2017	130.80	1390.15	03/18/2017	101.40	1213.15
01/30/2017	130.14	1385.29	03/19/2017	104.52	1225.07
01/31/2017	130.67	1384.16	03/20/2017	99.49	1200.10
02/01/2017	128.40	1379.32	03/21/2017	96.14	1184.98
02/02/2017	124.17	1365.69	03/22/2017	95.92	1190.38
02/03/2017	126.23	1375.95	03/23/2017	96.49	1194.45
02/04/2017	129.14	1390.18	03/24/2017	118.89	1305.90
02/05/2017	116.81	1327.56	03/25/2017	128.99	1353.28
03/26/2017	131.01	1357.38	05/12/2017	134.39	1373.80
03/27/2017	131.23	1361.96	05/13/2017	140.21	1400.20
03/28/2017	130.75	1357.39	05/14/2017	141.08	1400.19
03/29/2017	131.19	1372.91	05/15/2017	140.49	1400.17
03/30/2017	118.80	1301.07	05/16/2017	139.34	1399.51
03/31/2017	130.24	1284.62	05/17/2017	138.60	1399.26
04/01/2017	120.87	1318.61	05/18/2017	139.50	1400.27
04/02/2017	132.75	1379.48	05/19/2017	138.84	1400.20
04/03/2017	134.00	1368.71	05/20/2017	138.46	1400.21
04/04/2017	137.79	1392.34	05/21/2017	138.39	1400.21
04/05/2017	136.32	1388.73	05/22/2017	137.74	1400.24
04/06/2017	125.16	1328.32	05/23/2017	131.59	1366.91
04/07/2017	112.07	1256.10	05/24/2017	135.58	1377.43
04/08/2017	127.87	1334.38	05/25/2017	141.19	1400.29
04/09/2017	133.21	1360.38	05/26/2017	141.08	1400.18
04/10/2017	122.86	1310.90	05/27/2017	141.52	1400.13
04/11/2017	126.50	1329.93	05/28/2017	140.34	1400.24
04/12/2017	133.70	1372.93	05/29/2017	140.43	1400.11
04/13/2017	137.18	1385.99	05/30/2017	140.68	1400.24
04/14/2017	140.99	1400.19	05/31/2017	139.97	1400.21
04/15/2017	139.87	1389.70	06/01/2017	138.33	1400.52
04/16/2017	140.45	1390.13	06/02/2017	118.25	1300.10
04/17/2017	125.29	1317.92	06/03/2017	109.03	1250.15
04/18/2017	107.53	1225.09	06/04/2017	124.29	1325.11
04/19/2017	104.91	1211.64	06/05/2017	124.75	1325.25
04/20/2017	102.04	1200.11	06/06/2017	115.05	1281.66
04/21/2017	102.51	1200.05	06/07/2017	136.45	1400.10
04/22/2017	100.45	1200.06	06/08/2017	139.01	1400.42
04/23/2017	99.75	1200.04	06/09/2017	132.37	1380.61
04/24/2017	107.08	1222.91	06/10/2017	140.26	1395.47
04/25/2017	129.11	1336.27	06/11/2017	141.66	1398.69
04/26/2017	138.48	1392.56	06/12/2017	126.84	1325.14

**APPENDIX G**  
**MEWBOURNE #1**  
**DAILY RATE HISTORY**

Date	Rate	Pressure
	(gpm)	(psia)
04/27/2017	136.07	1372.31
04/28/2017	134.69	1365.76
04/29/2017	137.51	1400.20
04/30/2017	136.24	1389.66
05/01/2017	140.50	1394.06
05/02/2017	137.89	1381.01
05/03/2017	137.06	1380.10
05/04/2017	138.63	1392.11
05/05/2017	140.24	1397.39
05/06/2017	139.60	1387.29
05/07/2017	141.83	1400.20
05/08/2017	141.06	1400.15
Date	Rate	Pressure
	(gpm)	(psia)
06/13/2017	140.89	1400.05
06/14/2017	141.63	1400.24
06/15/2017	142.55	1400.18
06/16/2017	142.39	1399.82
06/17/2017	142.60	1400.14
06/18/2017	140.31	1390.06
06/19/2017	138.90	1380.17

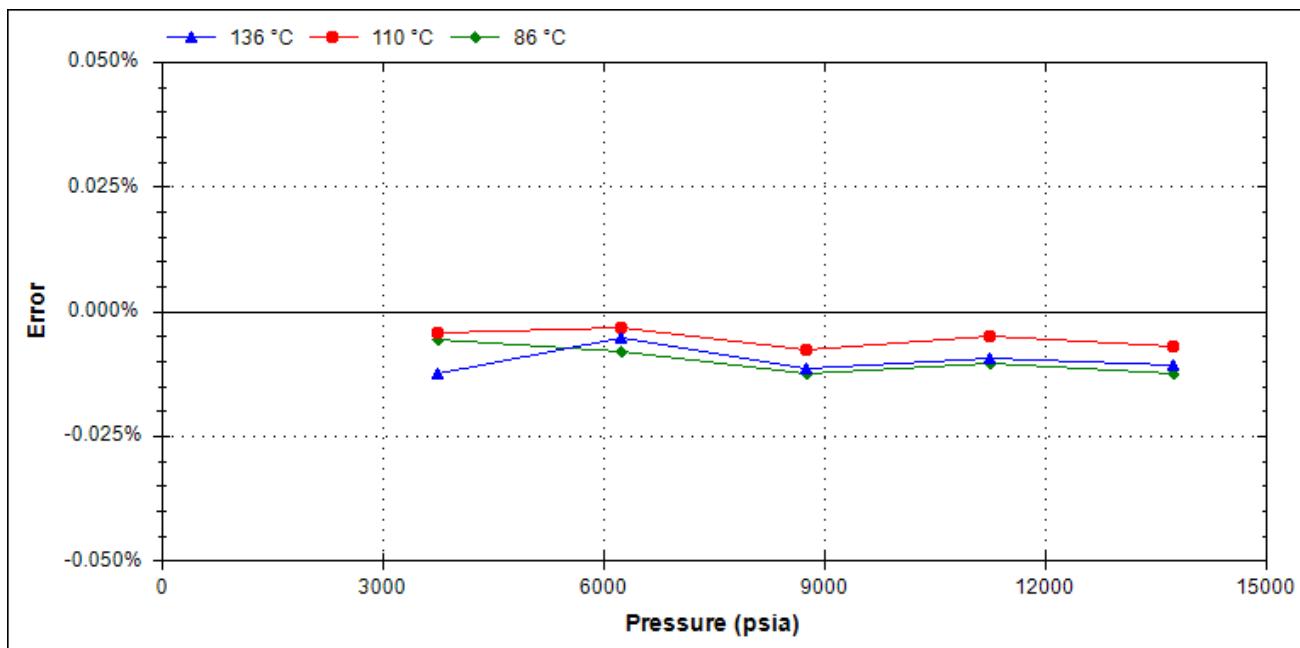
## **APPENDIX H**

### **GAUGE CALIBRATION SHEETS**

**Calibration Date:** 12-Dec-16  
**Max Pressure Error:** 0.014% F.S.  
**Max Temperature Error:** 0.123 °C  
**Part Number:** 104199  
**Serial Number:** DC1463

1.25 OD P3 RTD Assembly I-718			
Max Pressure		Max Temperature	
psi	kPa	°F	°C
15,000	103,421	351	177

**Accuracy:** As shown in the graph below, this DataCan Pressure gauge conforms to within +/- 0.030% F.S. of the pressure standard used in calibration, which is accurate to within +/- 0.01% of reading.



### Working Standards

Sun Electronic Systems Environmental Chamber, Model: EC127  
 DHI Instruments Pressure Controller, Model: PPCH-200M (30,000psi Reference)

### Traceability Statement

All working standards are traceable to nationally or internationally recognized standards.



Approved By:  
 DataCan Services Corp.

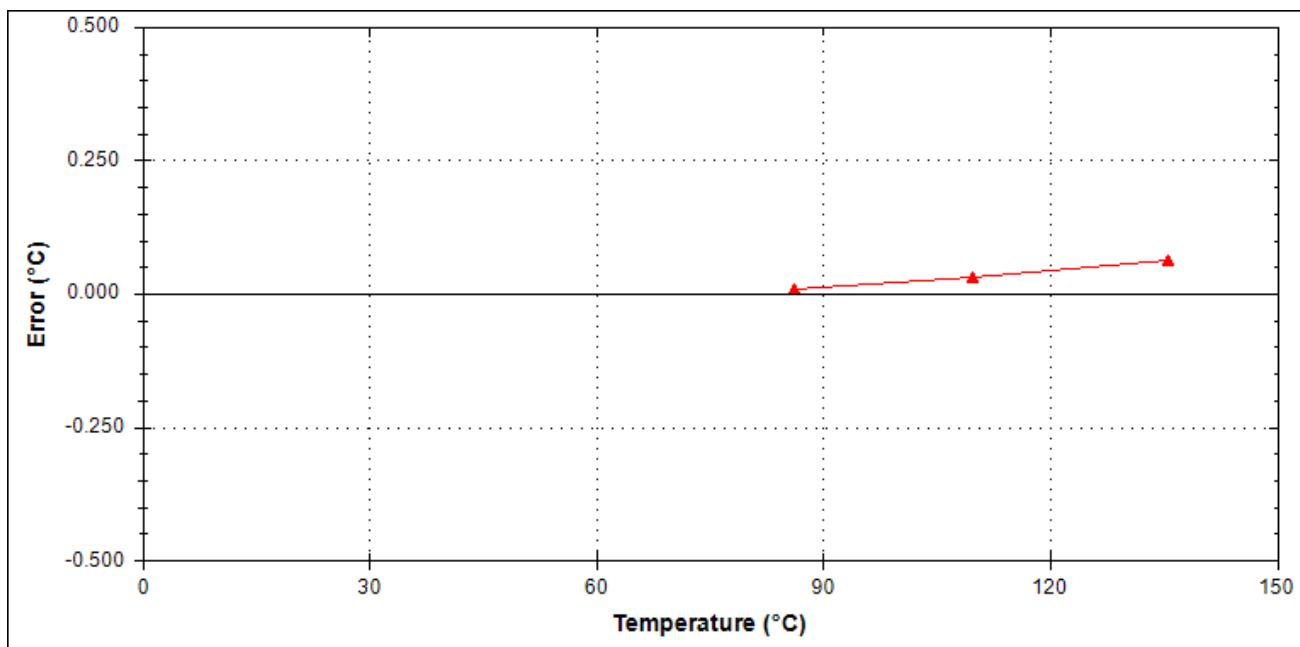
Calibrated By:  
 Angelo Pulido

Calibration Date: 12-Dec-16  
Max Temperature Error: 0.063 °C  
Part Number: 104199  
Serial Number: DC1463

Calibration System: CALIBRATION03  
Batch Number: 20150310.143657

1.25 OD, P3 RTD Assembly, I-718	
Max Temperature	
°F	°C
302	150

**Accuracy:** As shown in the graph below, this DataCan Pressure gauge conforms to within 0.250 °C of the temperature standard used in calibration, which is accurate to within 0.065 °C of reading.



## Working Standards

Sun Electronic Systems Environmental Chamber, Model: EC127, Serial: EC0020

## Traceability Statement

All working standards are traceable to nationally or internationally recognized standards.

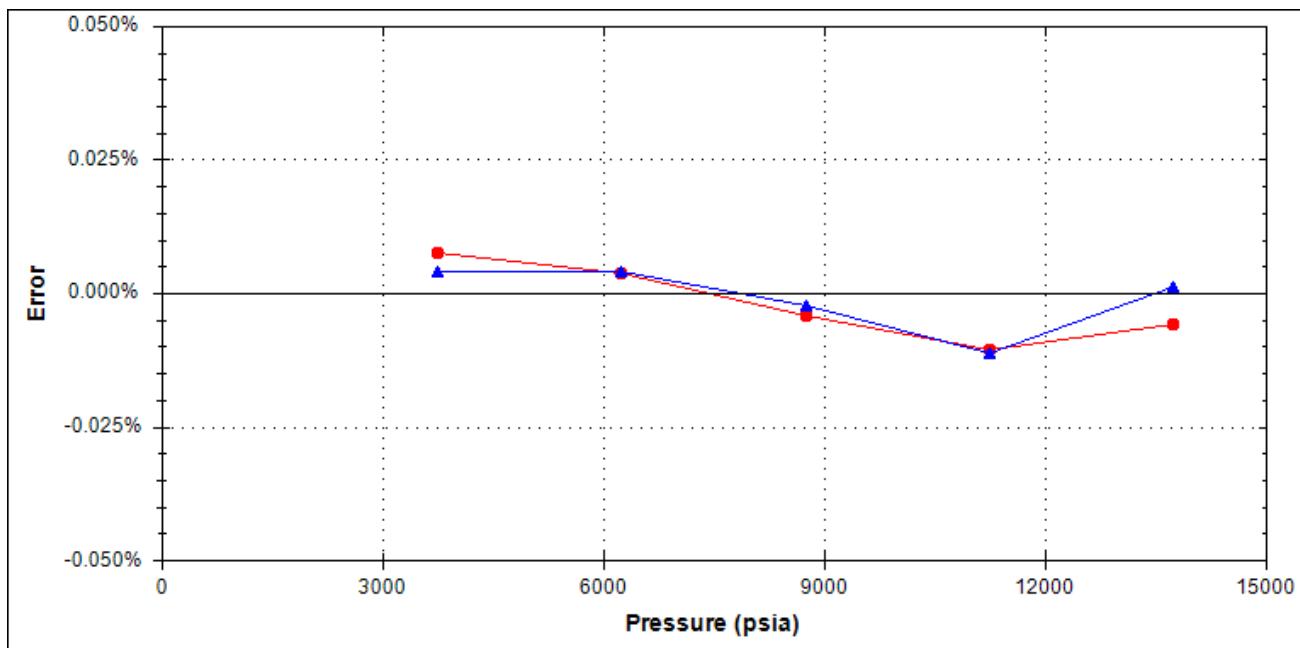
Approved By:  
DataCan Services Corp.

Calibrated By:  
Angelo Pulido

**Calibration Date:** 06-Feb-17      **Calibration System:** CALIBRATION01  
**Max Pressure Error:** 0.012% F.S.      **Batch Number:** 20170201.164803  
**Max Temperature Error:** 0.195 °C  
**Part Number:** 104199  
**Serial Number:** DC1464

1.25 OD P3 RTD Assembly I-718			
Max Pressure		Max Temperature	
psi	kPa	°F	°C
15,000	103,421	351	177

**Accuracy:** As shown in the graph below, this DataCan Pressure gauge conforms to within +/- 0.030% F.S. of the pressure standard used in calibration, which is accurate to within +/- 0.01% of reading.



### Working Standards

Sun Electronic Systems Environmental Chamber, Model: EC127, Serial: EC00022

DHI Instruments Pressure Controller, Model: PPCH-200M (30,000psi Reference), Serial: 269

### Traceability Statement

All working standards are traceable to nationally or internationally recognized standards.



Approved By:  
DataCan Services Corp.

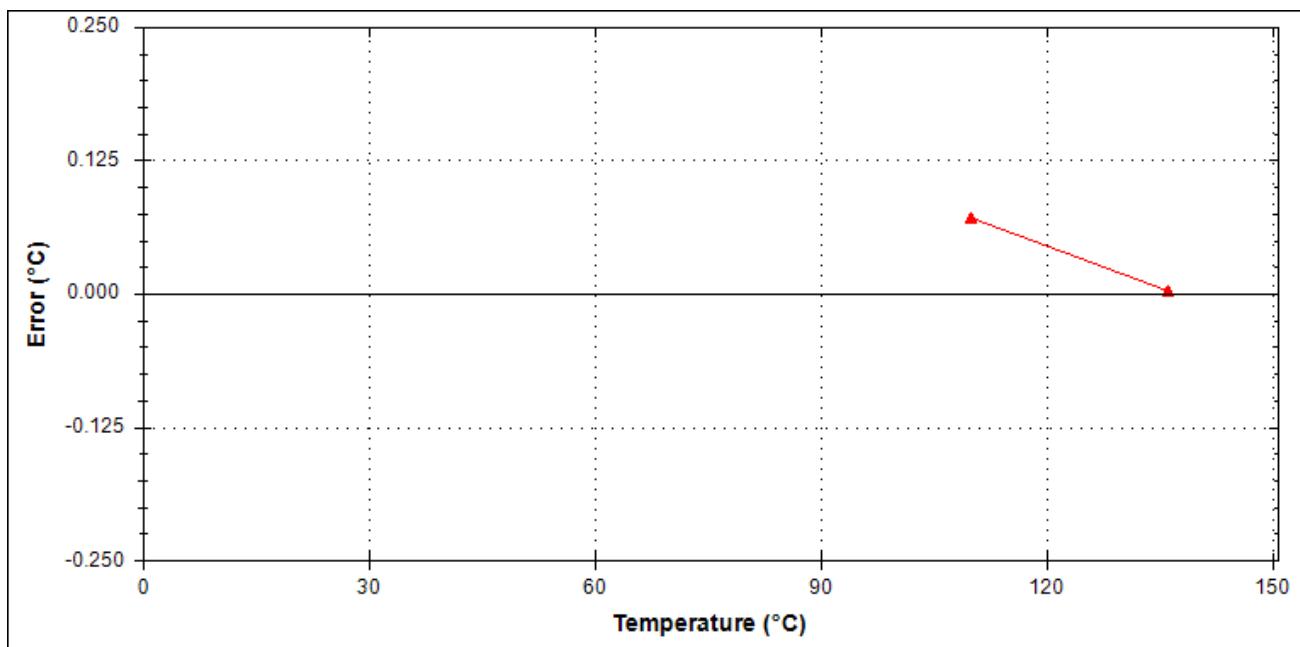
Calibrated By:  
Angelo Pulido

Calibration Date: 06-Feb-17  
Max Temperature Error: 0.072 °C  
Part Number: 104199  
Serial Number: DC1464

Calibration System: CALIBRATION01  
Batch Number: 20170201.164803

1.25 OD_P3 RTD Assembly_I-718	
Max Temperature	
°F	°C
303	151

**Accuracy:** As shown in the graph below, this DataCan Pressure gauge conforms to within 0.250 °C of the temperature standard used in calibration, which is accurate to within 0.065 °C of reading.



## Working Standards

Sun Electronic Systems Environmental Chamber, Model: EC127, Serial: EC00022

## Traceability Statement

All working standards are traceable to nationally or internationally recognized standards.

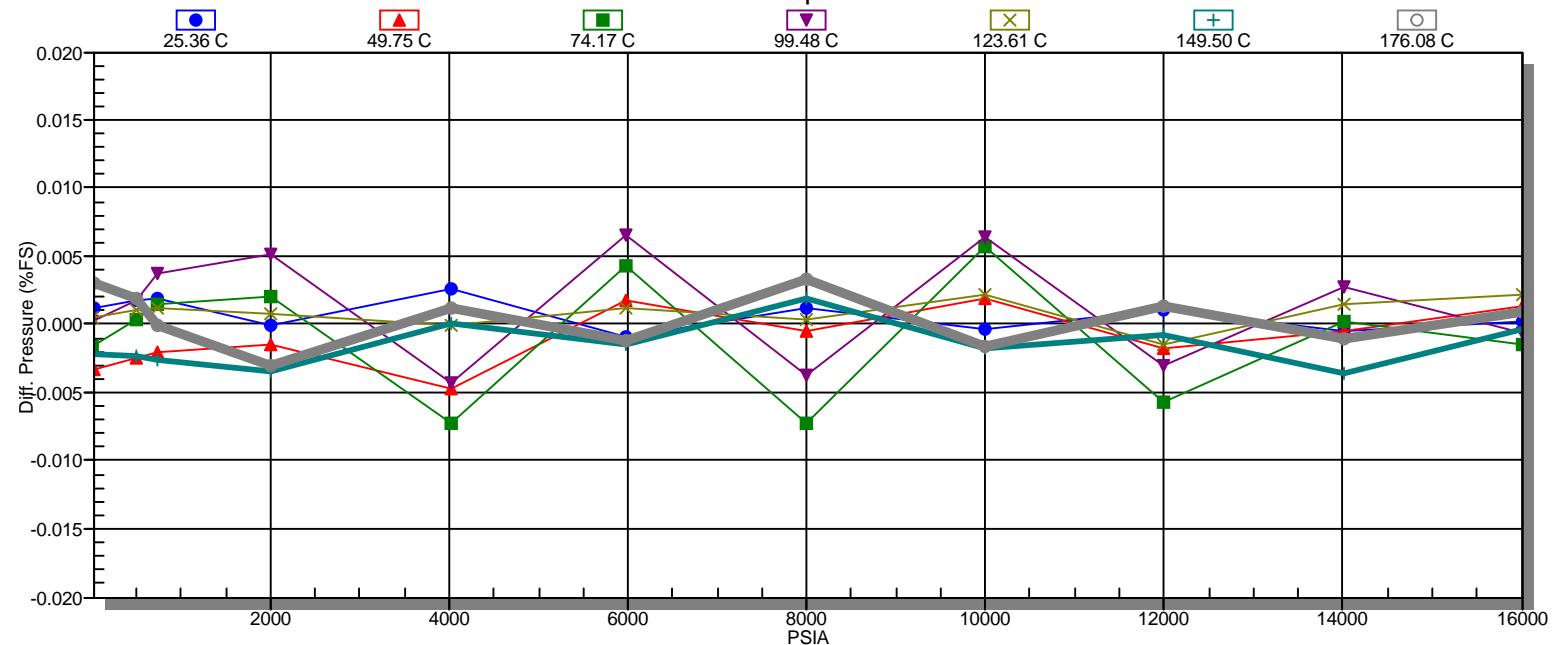
Approved By:  
DataCan Services Corp.

Calibrated By:  
Angelo Pulido



## Pressure Gauge Certificate of Calibration

Calibration Report - 21726



GAUGE NUMBER: 21726

2-D POLYNOMIAL LMS CURVEFIT

Source of f: Pres	Temp	Pressure Equation:
Fit Order: 3	3	$\text{Pressure (PSI)} = A + xp(B + xp(C + xp(D)))$
Prescale: $xp = m * (fp - fp0)$	$xt = m * (ft - ft0)$	
m:	0.01	Temperature Compensation:
$fp0 = 16759$	$ft0 = 64464$	$A = A0 + xt(A1 + xt(A2 + xt(A3 + xt(A4))))$
		$B = B0 + xt(B1 + xt(B2 + xt(B3 + xt(B4))))$
		$C = C0 + xt(C1 + xt(C2 + xt(C3 + xt(C4))))$
		$D = D0 + xt(D1 + xt(D2 + xt(D3 + xt(D4))))$

0	1	2	3	4
Pressure (psi) STANDARD FIT COEFFICIENTS:				
A 13.09857717	0.127974273	-0.0186245155	1.046101332E-05	41.65885005
B -0.02111438644	2.462165166E-05	-5.793793432E-08	-0.001862508604	1.174064763E-05
C -2.608216969E-08	6.391731223E-11	4.460150877E-07	-6.422382048E-09	1.390778757E-11
D -2.509008954E-14	1	-13.5	25.33	176.11

Temperature (C) STANDARD FIT COEFFICIENTS

A 25.4075362
B -0.723763381
C -0.0008530980666
D -6.801162841E-07

## Error File: Gauge # 21726

Pressure psi	Temperature Deg. C	Count (Pres)	Count (Temp)	DIFF (press) psi
13.14	25.36	16759.58	64464.11	0.20
506.90	25.40	17945.65	64463.05	0.28
740.66	25.38	18507.57	64465.61	0.30
1992.36	25.39	21520.14	64466.13	-0.02
4010.72	25.33	26396.85	64468.40	0.42
5985.66	25.40	31185.37	64464.48	-0.14
8006.60	25.34	36107.33	64466.94	0.19
9993.61	25.35	40963.28	64463.78	-0.07
11996.07	25.37	45876.52	64463.48	0.18
14010.78	25.38	50836.37	64464.11	-0.08
16001.81	25.41	55755.36	64462.74	0.02
13.15	49.75	16823.05	60969.38	-0.54
506.91	49.75	17987.91	60970.17	-0.39
740.67	49.71	18539.91	60970.00	-0.33
1992.38	49.72	21500.59	60971.49	-0.23
4010.75	49.73	26292.40	60970.50	-0.74
5985.69	49.72	31007.22	60970.83	0.28
8006.64	49.77	35850.39	60965.11	-0.07
9993.65	49.74	40635.70	60970.02	0.30
11996.11	49.74	45475.78	60968.01	-0.27
14010.83	49.73	50367.00	60965.86	-0.07
16001.85	49.74	55219.50	60964.93	0.21
13.12	74.17	17020.30	57135.56	-0.26
506.88	74.13	18160.96	57136.28	0.06
740.64	74.15	18701.56	57138.37	0.25
1992.34	74.11	21601.25	57140.60	0.33
4010.72	74.18	26296.00	57137.43	-1.17
5985.66	74.16	30923.44	57136.78	0.69
8006.62	74.13	35675.53	57134.25	-1.15
9993.63	74.12	40381.43	57138.07	0.90
11996.10	74.18	45137.45	57133.32	-0.92
14010.82	74.14	49952.23	57138.42	0.04
16001.85	74.13	54727.45	57135.74	-0.24
13.12	99.48	17402.82	52764.11	0.03
506.89	99.49	18513.60	52765.01	0.28
740.64	99.44	19040.47	52766.66	0.59
1992.35	99.42	21866.83	52769.57	0.81
4010.73	99.46	26447.35	52762.61	-0.69
5985.69	99.49	30966.64	52766.79	1.05
8006.65	99.47	35613.60	52761.18	-0.60
9993.67	99.42	40218.28	52766.21	1.02
11996.15	99.47	44878.26	52762.29	-0.47
14010.88	99.44	49598.31	52764.78	0.44
16001.91	99.46	54282.83	52763.30	-0.09
13.12	123.61	17978.62	48174.80	0.09
506.88	123.58	19055.91	48175.42	0.16
740.64	123.55	19566.85	48174.89	0.19
1992.34	123.56	22310.53	48176.23	0.12
4010.72	123.59	26766.17	48172.09	0.00
5985.66	123.59	31161.53	48176.51	0.18
8006.61	123.57	35694.26	48169.28	0.06
9993.61	123.56	40184.20	48178.46	0.34
11996.09	123.54	44738.58	48170.05	-0.24
14010.80	123.56	49353.01	48174.25	0.23
16001.83	123.57	53939.45	48172.15	0.36
13.14	149.50	18879.80	42723.01	-0.34
506.90	149.50	19915.53	42721.54	-0.37
740.66	149.46	20406.01	42725.10	-0.42
1992.36	149.44	23046.06	42726.60	-0.56
4010.74	149.45	27341.17	42727.88	0.00
5985.68	149.45	31584.06	42729.59	-0.23
8006.64	149.51	35969.30	42724.43	0.31
9993.64	149.50	40316.58	42727.97	-0.29
11996.11	149.49	44736.68	42721.54	-0.12
14010.83	149.46	49217.30	42725.13	-0.58
16001.86	149.47	53679.47	42721.21	-0.05
13.18	176.08	20177.19	36469.09	0.49
506.94	176.11	21162.22	36468.21	0.30
740.70	176.04	21629.28	36467.58	-0.01
1992.40	176.04	24142.94	36471.28	-0.49

4010.76	176.06	28242.32	36470.96	0.20
5985.71	176.08	32300.04	36471.41	-0.18
8006.65	176.10	36503.31	36468.08	0.54
9993.66	176.04	40677.92	36472.38	-0.26
11996.12	176.11	44931.99	36469.42	0.21
14010.84	176.02	49251.81	36472.07	-0.16
16001.86	176.07	53560.72	36466.48	0.16



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[www.sparteksystems.com](http://www.sparteksystems.com)

## Pressure Gauge Certificate of Conformance

SERIAL NUMBER	21726	CALIBRATION DATE	JUN 01/15
MODEL NUMBER	1251 FF3	TRACEABILITY DOC.	CAL-STANDARD-001
PRESSURE RANGE	13.14 - 16001.81 psi	PRESSURE REFERENCE	NIST Traceable
TEMP. RANGE	25.36 - 176.08 °C	TEMP. REFERENCE	NIST Traceable

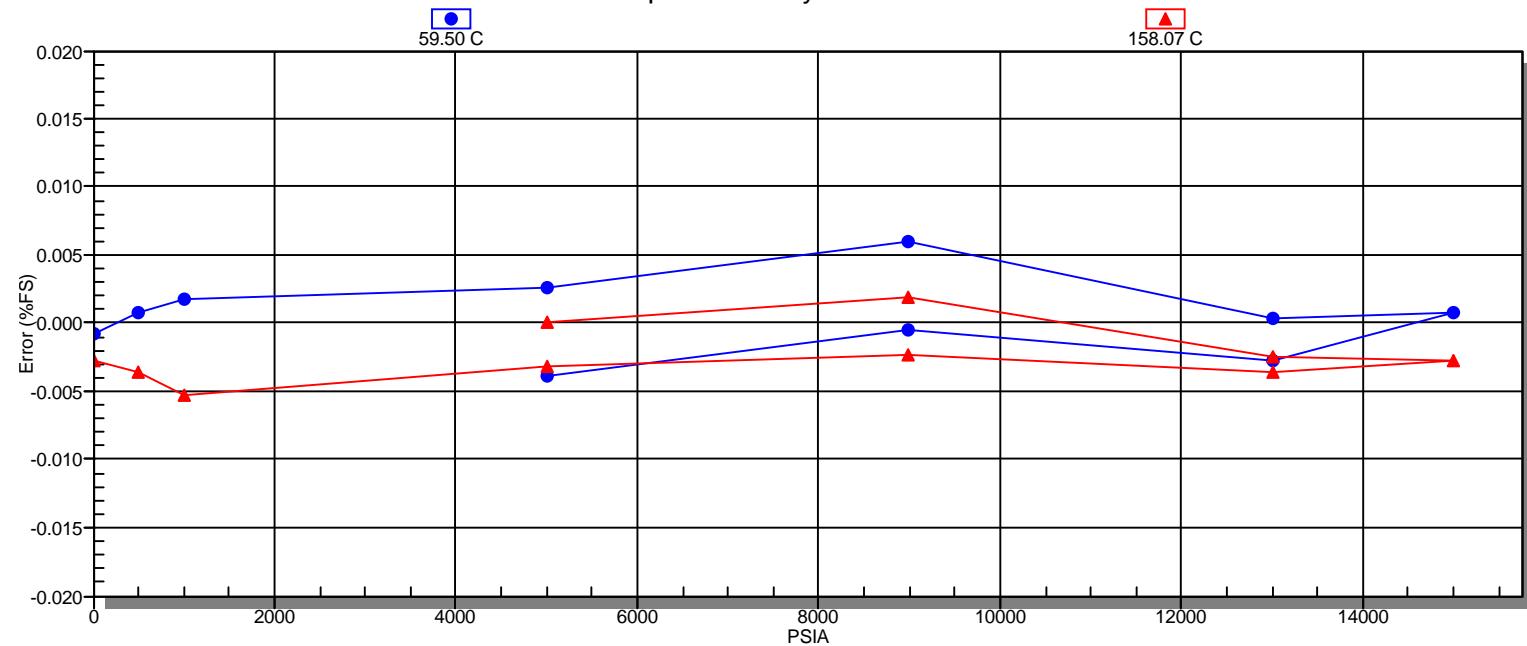
Testing and Verification Completed on JUN 02/15. The instrument response is within the stated specifications for this type of pressure gauge.

As shown in the graph below, this Spartek Gauge conformed to within +/- 0.020 %F.S. of the pressure standard used in calibration, which is accurate to within +/- 0.01% of reading. This gives an overall accuracy of +/- (0.020%F.S. + 0.01% of reading)

### NOTE

Units calibrated with a bellows meet performance specifications from 200 psi to full scale. Operating range is from 0 to full scale.

Spartek Quality Assurance



Accepted By: \_\_\_\_\_



Date: JUN 05/15

Ramp report: Serial # 21726

Gauge range = 16001.910 PSI. Max. DIFF. = 3.200

Ramp check result: PASS, Max Err = 0.006% F.S.

DW Pressure	Gauge Pressure	RPM4 Pressure	Differential	%F.S.	Oven Temp.	Gauge Temp.
4999.88	4999.25	4999.83	-0.63	0.0039	59.50	59.45
8990.61	8990.54	8990.19	-0.07	0.0004	59.50	59.46
12997.68	12997.25	12996.95	-0.43	0.0027	59.47	59.46
14999.84	14999.96	14998.87	0.12	0.0007	59.48	59.46
12997.68	12997.73	12996.82	0.05	0.0003	59.51	59.45
8990.61	8991.58	8990.29	0.97	0.0061	59.49	59.45
4999.87	5000.28	4999.80	0.41	0.0026	59.45	59.45
1002.92	1003.21	1003.08	0.29	0.0018	59.44	59.45
506.88	507.00	507.10	0.12	0.0008	59.48	59.45
13.11	13.00	13.11	-0.11	0.0007	59.51	59.46
4999.91	4999.92	4999.87	0.01	0.0001	158.07	158.01
8990.64	8990.93	8990.08	0.29	0.0018	158.12	158.02
12997.70	12997.31	12996.87	-0.39	0.0024	158.08	158.03
14999.87	14999.44	14998.81	-0.43	0.0027	158.10	158.02
12997.70	12997.13	12996.84	-0.57	0.0036	158.08	158.01
8990.63	8990.26	8990.23	-0.37	0.0023	158.08	157.99
4999.90	4999.40	4999.84	-0.50	0.0031	158.07	157.99
1002.95	1002.10	1003.05	-0.85	0.0053	158.02	157.97
506.91	506.34	507.14	-0.57	0.0036	158.05	157.98
13.15	12.72	13.25	-0.43	0.0027	158.01	157.97



# SPARTEK SYSTEMS

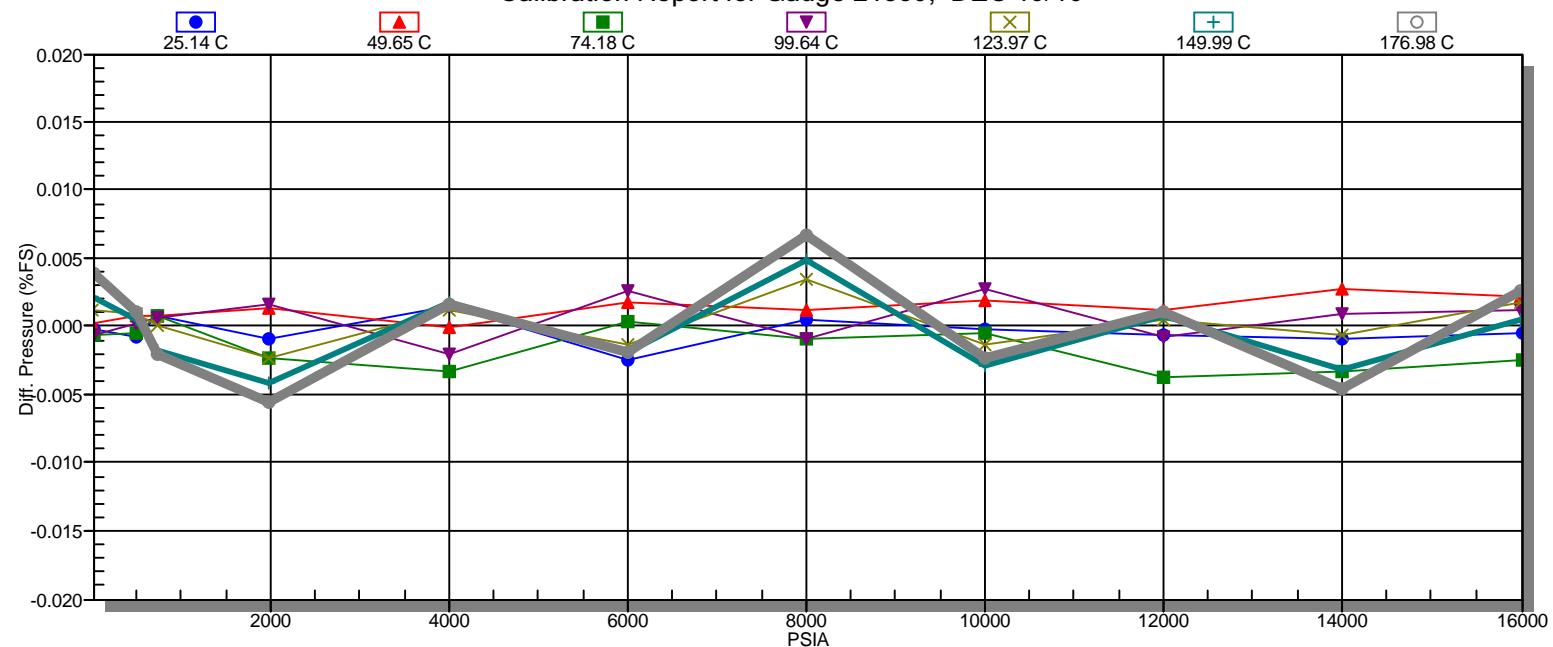
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## Pressure Gauge Certificate of Calibration

Calibration Report for Gauge 21359, DEC 19/16



GAUGE NUMBER: 21359

2-D POLYNOMIAL LMS CURVEFIT

Source of f: Pres	Temp	Pressure Equation:
Fit Order: 3	4	Pressure (PSI) = A + xp(B + xp(C + xp(D)))
Prescale: $xp = m * (fp - fp0)$	$xt = m * (ft - ft0)$	
m: 0.01	0.01	Temperature Compensation:
fp0 = 20903	ft0 = 56922	A = A0 + xt(A1 + xt(A2 + xt(A3 + xt(A4)))) B = B0 + xt(B1 + xt(B2 + xt(B3 + xt(B4)))) C = C0 + xt(C1 + xt(C2 + xt(C3 + xt(C4)))) D = D0 + xt(D1 + xt(D2 + xt(D3 + xt(D4))))

0	1	2	3	4
Pressure (psi) STANDARD FIT COEFFICIENTS:				
A 12.94029412	-0.9759096632	-0.01923039694	3.660298188E-06	-9.541527842E-09
B 40.89169333	-0.01990615547	2.939517939E-05	-7.804681741E-09	9.341871594E-11
C -0.001903553074	1.076599124E-05	-2.909240164E-08	-2.142808214E-11	-2.337591061E-13
D 5.981875664E-07	-4.464051219E-09	1.946700076E-11	5.398170348E-14	2.524203856E-16

Temperature (C) STANDARD FIT COEFFICIENTS

A 25.14862604
B -0.7221040553
C -0.0008523703489
D -6.875264685E-07

Error File: Gauge # 21359, DEC 19/16

Pressure psi	Temperature Deg. C	Count (Pres)	Count (Temp)	DIFF (press) psi
13.00	25.14	20903.07	56922.92	-0.04
505.89	25.16	22108.93	56924.38	-0.13
739.58	25.12	22681.98	56929.10	0.12
1989.94	25.17	25748.65	56933.29	-0.15
3992.32	25.10	30678.34	56924.19	0.23
5996.46	25.11	35631.83	56931.86	-0.40
8000.57	25.12	40605.76	56916.51	0.09
10003.69	25.07	45597.96	56929.50	-0.04
12004.75	25.15	50599.63	56914.28	-0.09
14006.39	25.12	55623.50	56922.82	-0.14
16013.80	25.09	60675.48	56913.63	-0.07
12.87	49.65	20878.21	53384.84	0.03
505.77	49.67	22063.07	53386.80	0.12
739.47	49.69	22625.32	53391.65	0.13
1989.83	49.63	25639.62	53394.59	0.21
3992.28	49.66	30485.75	53380.56	-0.02
5996.35	49.71	35361.98	53390.95	0.28
8000.52	49.72	40258.54	53371.50	0.19
10003.59	49.74	45177.75	53386.64	0.30
12004.68	49.68	50109.18	53370.40	0.19
14006.28	49.73	55065.63	53379.96	0.43
16013.71	49.69	60051.52	53369.88	0.35
13.07	74.18	20984.91	49524.87	-0.10
505.95	74.17	22144.73	49527.82	-0.08
739.65	74.16	22695.65	49531.79	0.11
1990.00	74.21	25647.09	49536.71	-0.38
3992.39	74.18	30398.70	49523.54	-0.52
5996.52	74.18	35184.00	49533.51	0.05
8000.64	74.23	39992.82	49511.39	-0.14
10003.74	74.21	44827.35	49530.19	-0.09
12004.80	74.23	49676.56	49508.70	-0.59
14006.43	74.19	54554.48	49521.92	-0.53
16013.84	74.22	59465.00	49508.94	-0.39
13.04	99.64	21271.29	45112.58	-0.09
505.93	99.67	22401.61	45112.52	0.02
739.62	99.64	22937.79	45119.00	0.09
1989.96	99.68	25816.16	45127.63	0.25
3992.36	99.62	30452.32	45113.34	-0.33
5996.45	99.65	35126.88	45124.01	0.42
8000.58	99.69	39829.26	45101.48	-0.15
10003.66	99.65	44562.30	45121.82	0.45
12004.72	99.67	49313.81	45099.27	-0.13
14006.33	99.62	54097.33	45113.67	0.15
16013.73	99.65	58916.43	45100.07	0.20
12.98	123.97	21755.80	40460.80	0.20
505.87	123.95	22852.13	40463.09	0.14
739.57	123.91	23371.78	40471.18	0.02
1989.92	123.98	26165.94	40479.25	-0.37
3992.31	124.00	30677.68	40451.62	0.19
5996.43	123.97	35224.92	40473.62	-0.21
8000.53	124.03	39812.41	40438.54	0.55
10003.65	123.96	44427.37	40467.46	-0.21
12004.69	123.99	49071.56	40436.16	0.09
14006.31	124.00	53748.08	40455.91	-0.09
16013.71	123.98	58465.76	40437.92	0.27
12.91	149.99	22558.17	34940.94	0.36
505.80	150.03	23611.52	34946.02	0.08
739.49	149.95	24110.32	34955.52	-0.29
1989.84	150.01	26799.96	34964.13	-0.66
3992.25	149.98	31151.12	34944.18	0.29
5996.35	150.02	35542.25	34958.71	-0.30
8000.48	150.03	39982.09	34926.83	0.78
10003.77	150.09	44451.96	34952.39	-0.46
12004.64	150.04	48959.60	34923.60	0.13
14006.45	150.02	53502.18	34939.35	-0.51
16013.66	149.98	58092.28	34922.63	0.08
13.00	176.98	23759.43	28594.02	0.61
505.89	176.95	24761.63	28595.28	0.17
739.58	176.96	25235.52	28605.09	-0.33
1989.93	176.96	27796.37	28615.71	-0.88

3992.30	176.95	31951.87	28585.81	0.26
5996.44	176.93	36150.77	28608.37	-0.31
8000.55	176.92	40410.08	28565.73	1.08
10003.67	176.94	44701.70	28600.83	-0.37
12004.72	176.94	49042.05	28560.80	0.16
14006.35	176.91	53420.33	28583.12	-0.72
16013.76	176.99	57855.01	28561.10	0.42



# SPARTEK SYSTEMS

GEOPHYSICAL INSTRUMENTATION

"Providing our customers with Best in Class Technology"

#1 Thevenaz Industrial Trail  
Sylvan Lake, AB, Ca, T4S 2J6  
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Fax (403) 887-4050  
[www.sparteksystems.com](http://www.sparteksystems.com)

## Pressure Gauge Certificate of Conformance

SERIAL NUMBER	21359	CALIBRATION DATE	DEC 19/16
MODEL NUMBER	1282 FF5	TRACEABILITY DOC.	CAL-STANDARD-001
PRESSURE RANGE	13.00 - 16013.80 psi	PRESSURE REFERENCE	NIST Traceable
TEMP. RANGE	25.14 - 176.98 °C	TEMP. REFERENCE	NIST Traceable

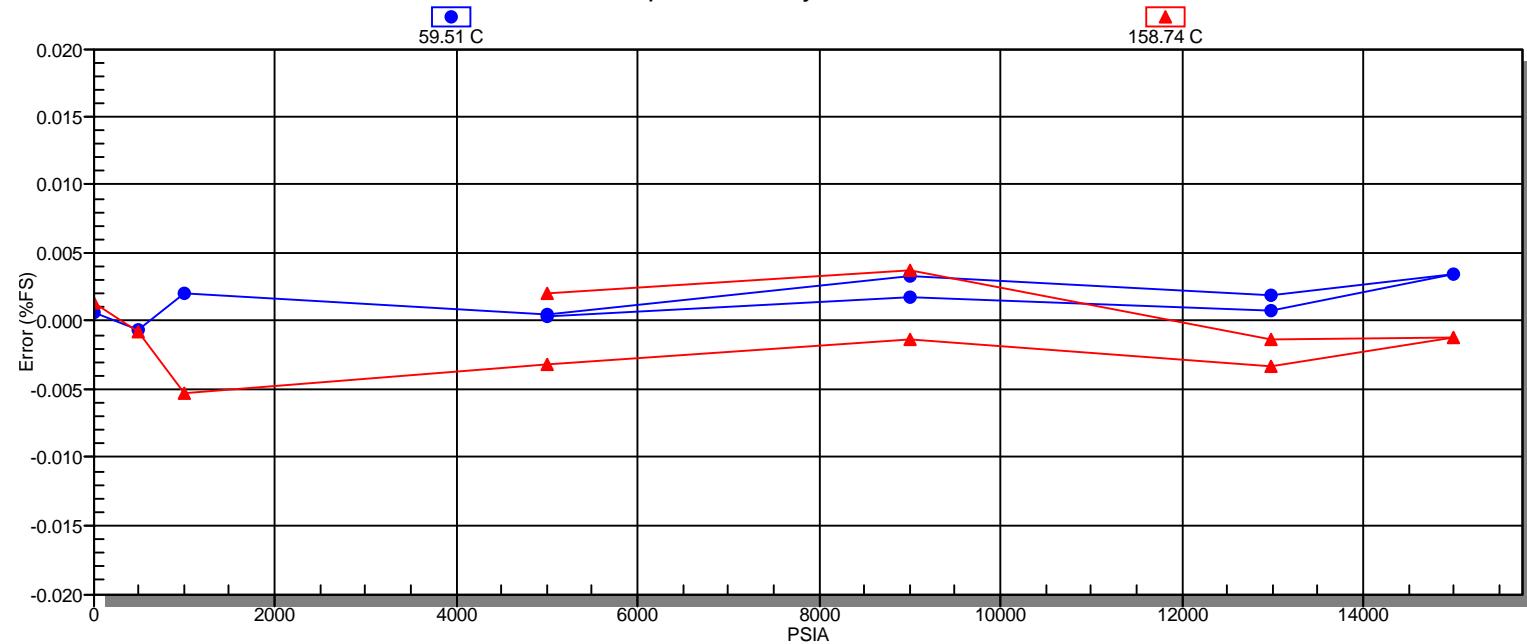
Testing and Verification Completed on DEC 20/16. The instrument response is within the stated specifications for this type of pressure gauge.

As shown in the graph below, this Spartek Gauge conformed to within +/- 0.020 %F.S. of the pressure standard used in calibration, which is accurate to within +/- 0.01% of reading. This gives an overall accuracy of +/- (0.020%F.S. + 0.01% of reading)

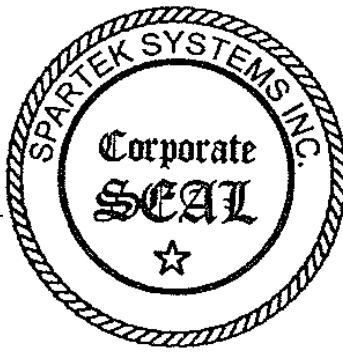
### NOTE

Units calibrated with a bellows meet performance specifications from 200 psi to full scale. Operating range is from 0 to full scale.

Spartek Quality Assurance



Accepted By: \_\_\_\_\_



Date: DEC 27/16 \_\_\_\_\_

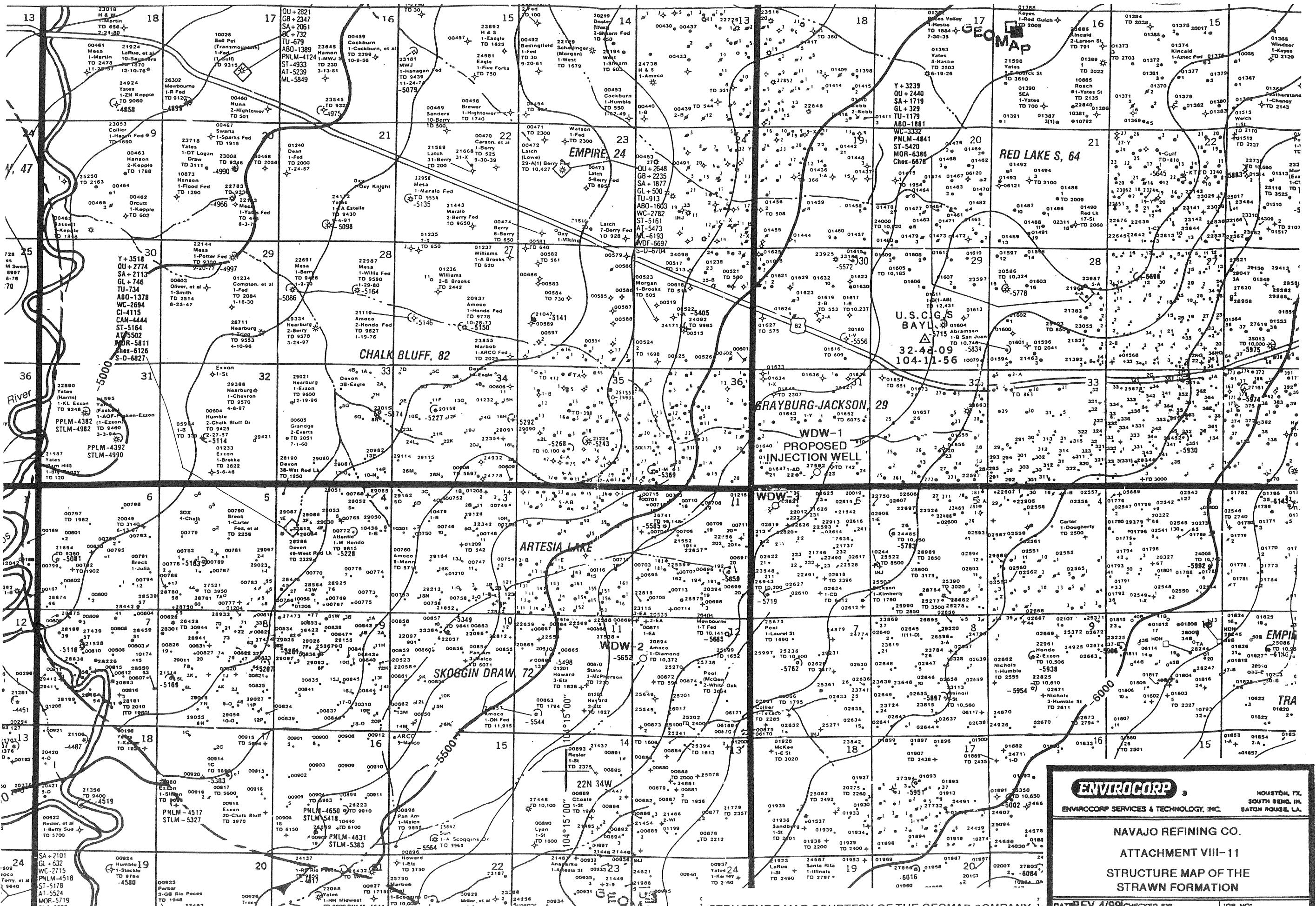
Ramp report: Serial # 21359, DEC 19/16  
Gauge range = 16013.840 PSI. Max. DIFF. = 3.203

Ramp check result: PASS, Max Err = 0.005% F.S.

DW Pressure	Gauge Pressure	Differential	%F.S.	Oven Temp.	Gauge Temp.
5010.02	5010.07	0.05	0.0003	59.51	59.46
9013.05	9013.34	0.29	0.0018	59.48	59.53
12990.69	12990.81	0.12	0.0008	59.49	59.54
14996.23	14996.79	0.56	0.0035	59.50	59.52
12990.71	12991.01	0.30	0.0018	59.50	59.45
9013.07	9013.59	0.52	0.0033	59.48	59.42
5010.07	5010.14	0.07	0.0004	59.53	59.42
1001.63	1001.95	0.32	0.0020	59.46	59.40
505.87	505.77	-0.10	0.0006	59.47	59.45
12.98	13.08	0.10	0.0006	59.51	59.48
5009.99	5010.31	0.32	0.0020	158.74	158.66
9013.00	9013.60	0.60	0.0037	158.67	158.73
12990.64	12990.42	-0.22	0.0014	158.73	158.75
14996.17	14995.98	-0.19	0.0012	158.71	158.72
12990.64	12990.11	-0.53	0.0033	158.68	158.64
9013.01	9012.79	-0.22	0.0014	158.66	158.58
5010.00	5009.50	-0.50	0.0031	158.68	158.55
1001.57	1000.72	-0.84	0.0053	158.63	158.53
505.80	505.68	-0.12	0.0007	158.71	158.60
12.91	13.12	0.20	0.0013	158.78	158.63

**APPENDIX I**

**STRAWN STRUCTURE MAPS**

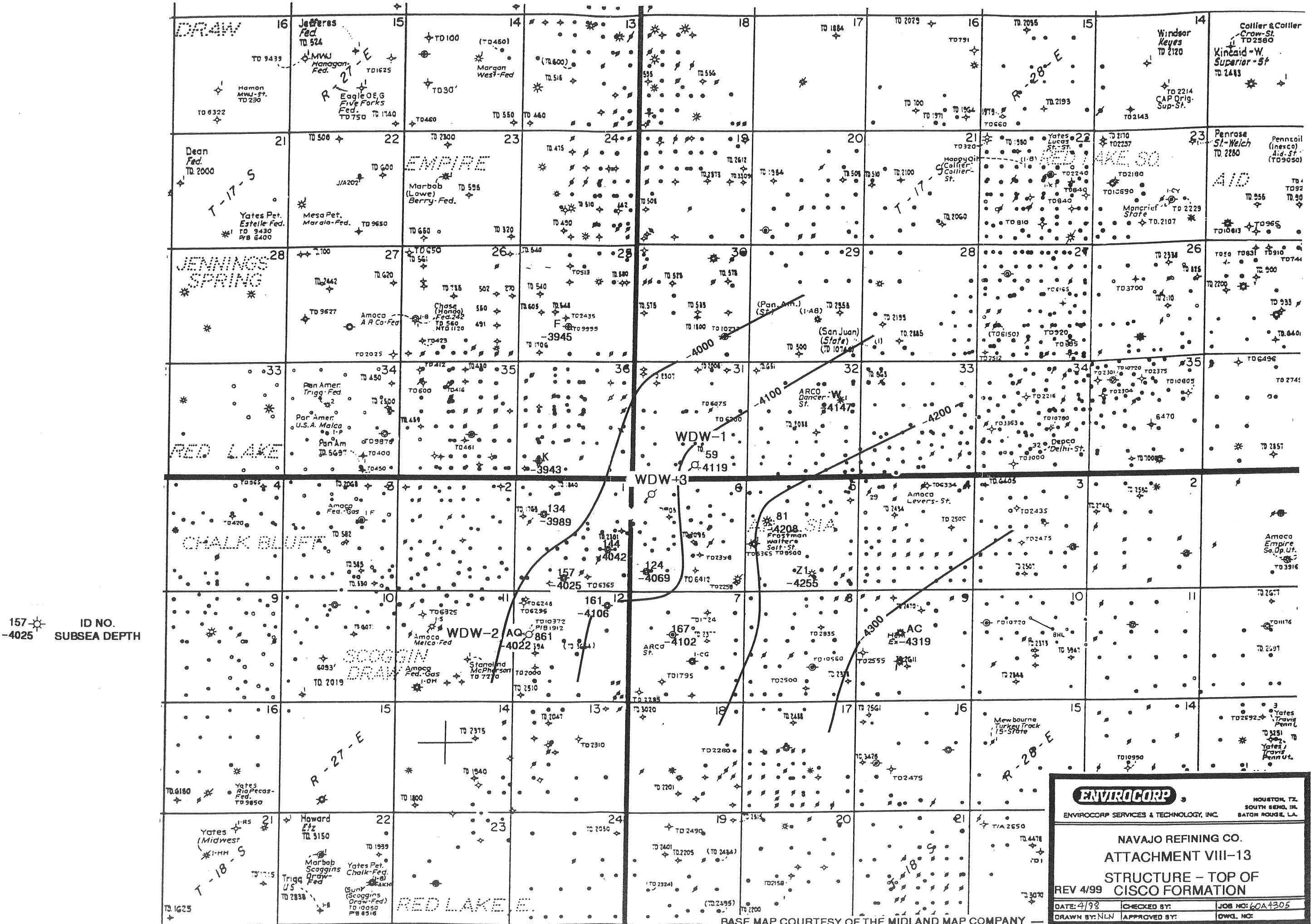


STRUCTURE MAP COURTESY OF THE GEOMAP COMPANY  
Poster July 1997

DATE REV 4/99 CHECKED BY: JOB NO:  
DRAWN BY: APPROVED BY: DWG. NO:

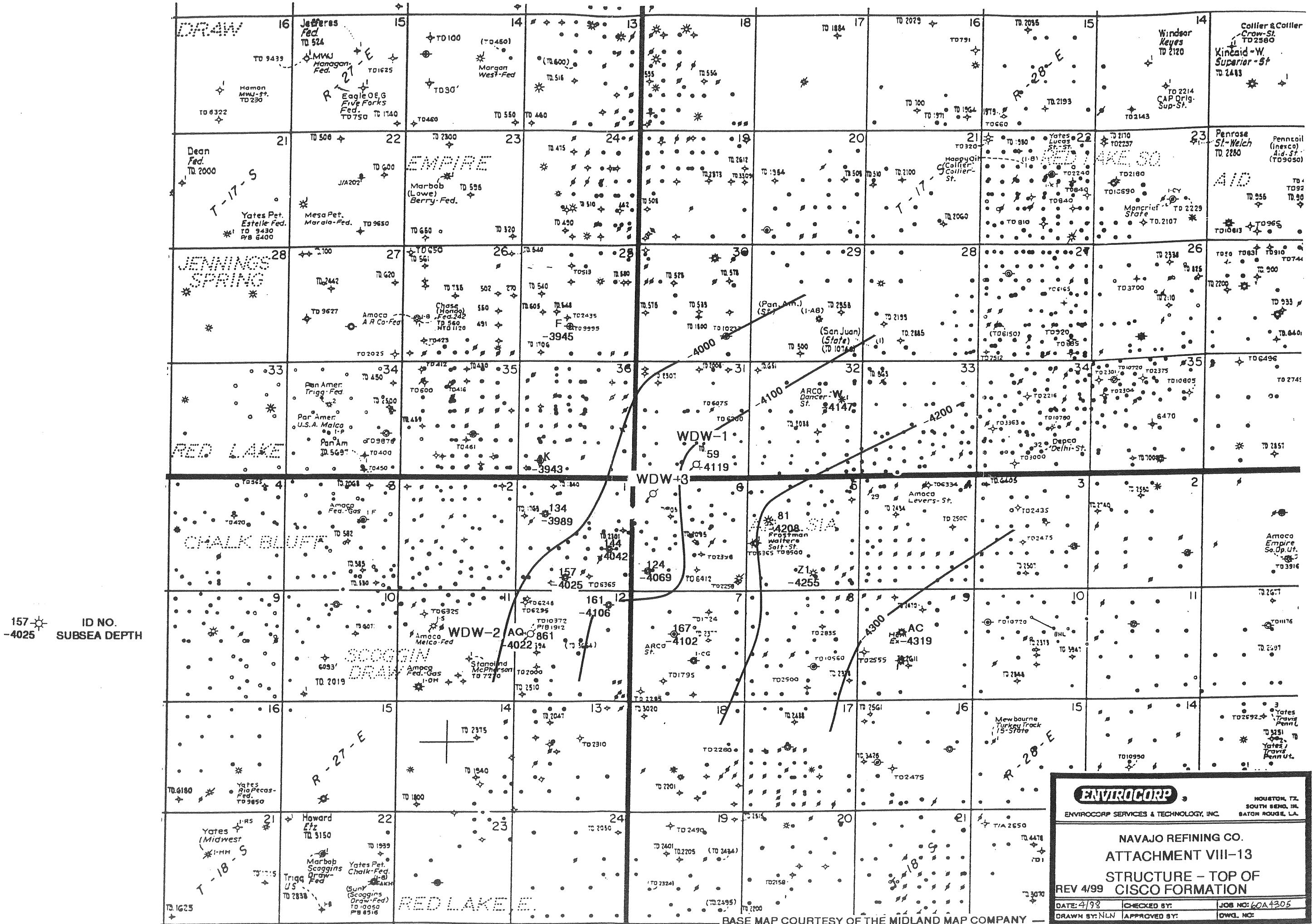
## **APPENDIX J**

### **WOLFCAMP STRUCTURE MAPS**



## **APPENDIX K**

### **CISCO STRUCTURE MAPS**



## **APPENDIX L**

### **CHRONOLOGY OF FIELD ACTIVITIES**

## **APPENDIX L**

### **CHRONOLOGY OF FIELD ACTIVITIES**

#### **Wednesday, June 14, 2017**

Hank Lichtenwaldt:

Travel to Artesia, NM from Morenci, AZ.

#### **Thursday, June 15, 2017**

Hank Lichtenwaldt:

Attend safety training at Navajo Refining facility with Fesco Wireline.  
Supervise Harcrow Surveying during the surveying and staking of WDW-4's well pad.

#### **Friday, June 16, 2017**

Hank Lichtenwaldt:

Travel to WDW-1 for permit and safety meeting. Rig up Fesco slickline units and complete a dummy run (using sinker bar) on each well. Tagged bottom in WDW-1 at 9013.5 ft KB, WDW-2 at 8391.0 ft KB, and WDW-3 at 8729.0 ft KB. Set downhole pressure recorders in all three wells. Set at the following depths: WDW-1: 7924.5 ft KB at 1105 hours, WDW-2: 7570 ft KB at 1145 hours, WDW-3: 7660 ft KB at 1230 hours. Secure well sites and return to Morenci, AZ.

#### **Tuesday, June 20, 2017**

Hank Lichtenwaldt:

Travel to Artesia, NM from Morenci, AZ.

#### **Wednesday, June 21, 2017**

Hank Lichtenwaldt:

Travel to WDW-1 for permit and safety meeting. Pull downhole pressure gauge out of WDW-1 and conduct 7-minute static gradient stops at 7000 ft, 6000 ft, 5000 ft, 4000 ft, 3000 ft, 2000 ft, 1000 ft, and surface (0 ft). Fesco crews pulled the downhole pressure gauges out of WDW-2 and WDW-3 while conducting WDW-1 static gradient stops. Rig down Fesco slickline units and secure well sites. Return wells to Navajo Refining.

#### **Thursday, June 22, 2017**

Hank Lichtenwaldt:

Travel from Artesia, NM to Fort Stockton, TX.

**APPENDIX M**

**PANSYSTEM© ANALYSIS OUTPUT**



WSP USA

Report File:

2017 WDW-1 PFO.pan

PanSystem Version 3.4.1

## Well Test Analysis Report

Company:	Navajo Refining Company
Location:	Artesia, New Mexico
Well Name:	Mewbourne Well No. 1
Testing Date:	June 17 to June 21, 2017
Gauge Depth:	7924 feet RGL
Injection Interval:	7924 feet - 8476 feet
Completion Type:	Perforated
Top Of Fill:	9001 feet
Analyst:	LKM
WSP USA Project No.:	192080A

**Reservoir Description**

Fluid type : Water

Well orientation : Vertical

Number of wells : 1

Number of layers : 1

**Layer Parameters Data**

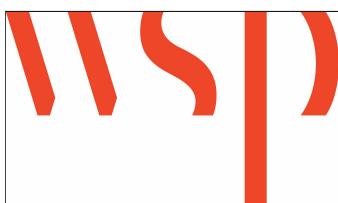
	Layer 1
Formation thickness	175.0000 ft
Average formation porosity	0.1000
Water saturation	1.0000
Gas saturation	0.0000
Formation compressibility	0.000000 psi-1
Total system compressibility	8.4000e-6 psi-1
Layer pressure	4359.586451 psia
Temperature	0.000000 deg F

**Well Parameters Data**

	Well 1
Well radius	0.3646 ft
Distance from observation to active well	0.000000 ft
Wellbore storage coefficient	1.027609 bbl/psi
Storage Amplitude	0.000000 psi
Storage Time Constant	0.000000 hr
Second Wellbore Storage	0.000000 bbl/psi
Time Change for Second Storage	0.000000 hr
Well offset - x direction	0.0000 ft
Well offset - y direction	0.0000 ft

**Fluid Parameters Data**

	Layer 1
Oil gravity	0.000000 API
Gas gravity	0.000000 sp grav
Gas-oil ratio (produced)	0.000000 scf/STB
Water cut	0.000000
Water salinity	0.000000 ppm
Check Pressure	0.000000 psia
Check Temperature	0.000000 deg F
Gas-oil ratio (solution)	0.000000 scf/STB
Bubble-point pressure	0.000000 psia
Oil density	0.000 lb/ft3

**Fluid Parameters Data (cont)**

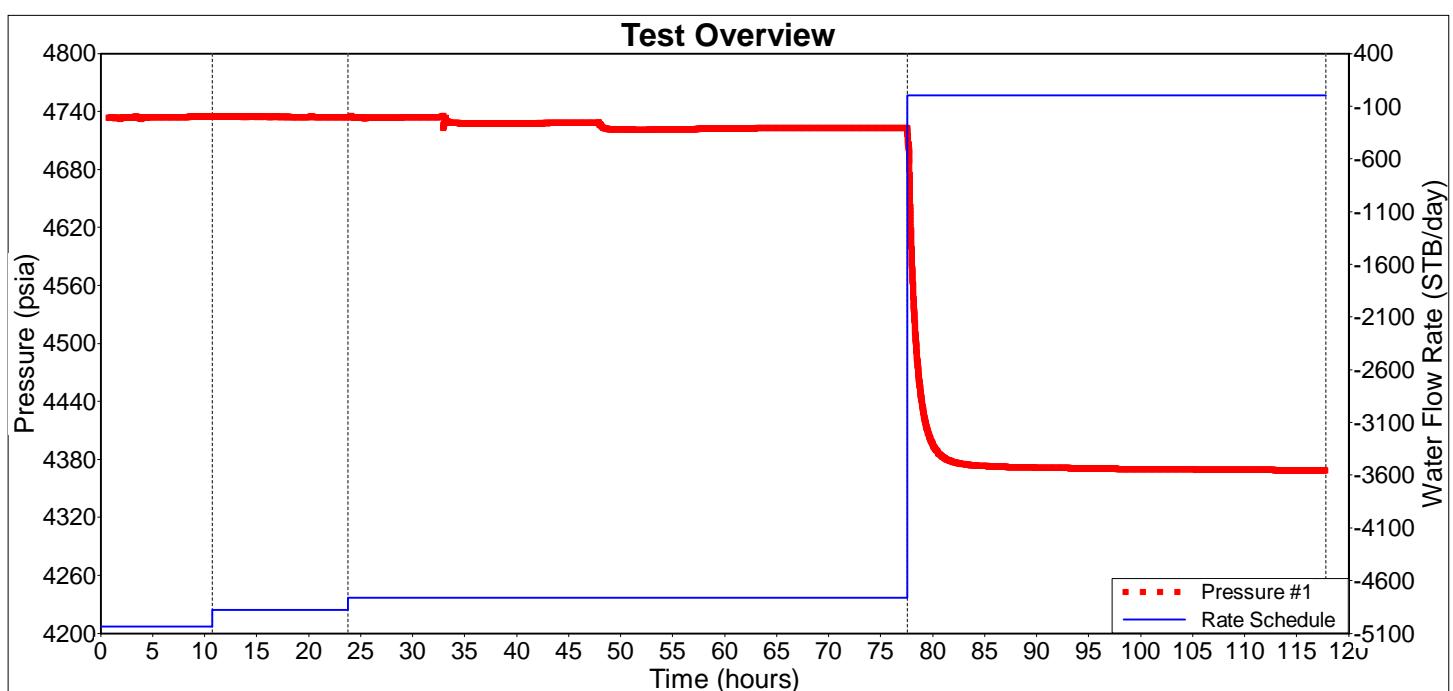
	Layer 1
Oil viscosity	0.000 cp
Oil formation volume factor	0.000 RB/STB
Gas density	0.000 lb/ft3
Gas viscosity	0.0 cp
Gas formation volume factor	0.000 ft3/scf
Water density	0.000 lb/ft3
Water viscosity	0.570 cp
Water formation volume factor	1.000 RB/STB
Oil compressibility	0.000000 psi-1
Initial Gas compressibility	0.000000 psi-1
Water compressibility	0.000000 psi-1

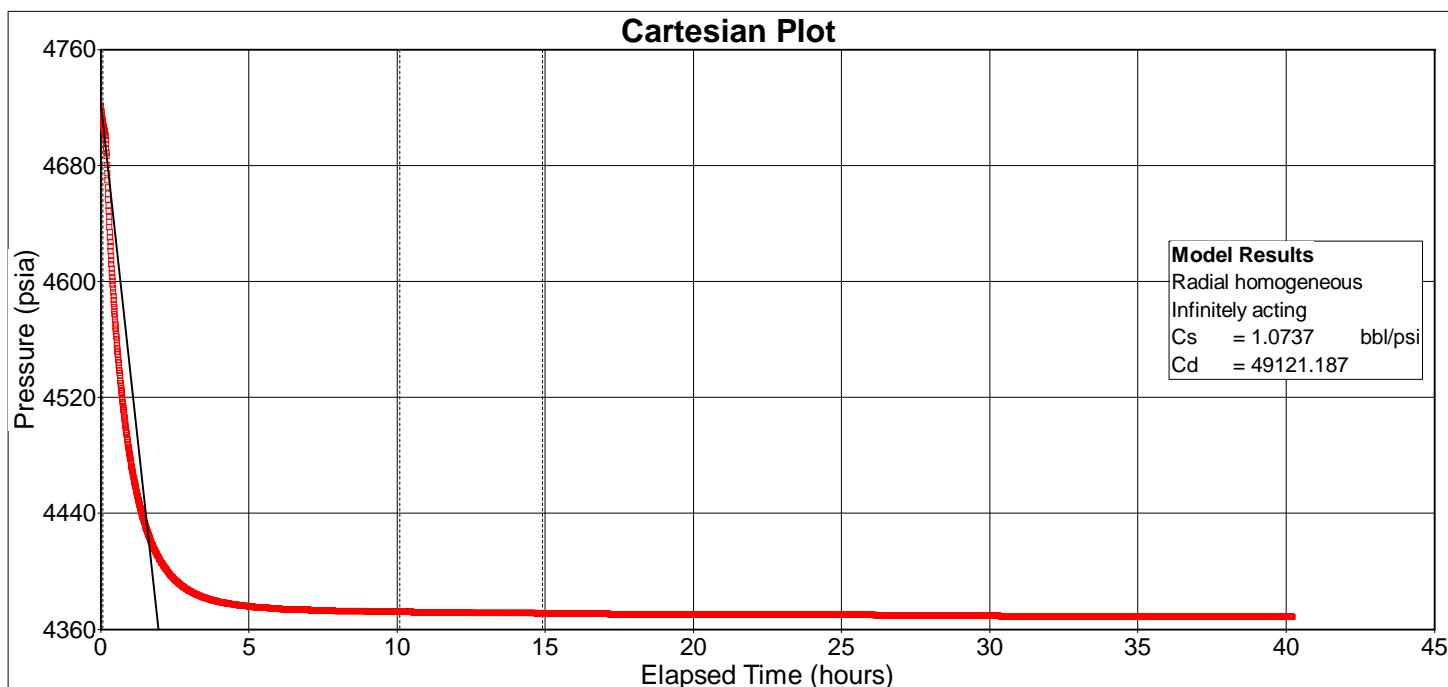
**Layer 1 Correlations**

Not Used

**Rate Change Data**

Time Hours	Pressure psia	Rate STB/day
-1234.244340	0.000000	-4753.130000
-313.244340	0.000000	-4074.580000
-231.244340	0.000000	-4271.230000
-91.244340	0.000000	-4706.220000
-46.244340	0.000000	-4512.180000
-28.244340	0.000000	-4936.270000
-23.244340	0.000000	-4357.810000
-22.244340	0.000000	-3562.980000
-9.244340	0.000000	-5043.390000
-1.244340	0.000000	-4844.780000
10.755660	0.000000	-5037.910000
23.755660	0.000000	-4876.980000
77.561791	4722.738000	-4764.910000
117.786389	4368.406000	0.000000



**Cartesian Plot Model Results**

Radial homogeneous - Infinitely acting

Classic Wellbore Storage

	Value
Wellbore storage coefficient	1.073698 bbl/psi
Dimensionless wellbore storage	4.9121e4

**Cartesian Plot Line Details**

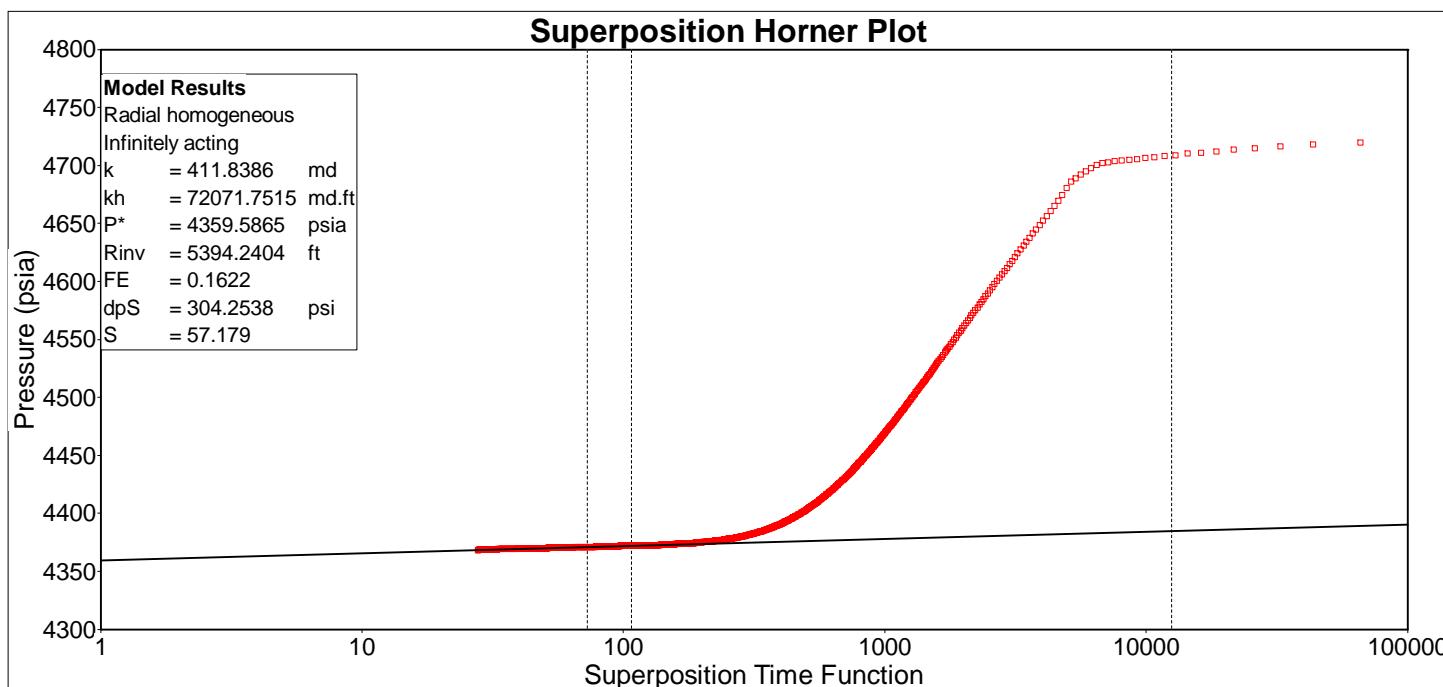
Line type : Wellbore storage

Slope : -184.91

Intercept : 4722.58

Coefficient of Determination : 0.995232

Number of Intersections = 0



#### Superposition Horner Plot Model Results

Radial homogeneous - Infinitely acting

Classic Wellbore Storage

	Value
Permeability	411.83858 md
Permeability-thickness	7.2072e4 md.ft
Extrapolated pressure	4359.586451 psia
Radius of investigation	5394.240398 ft
Flow efficiency	0.162185
dP skin (constant rate)	304.253771 psi
Skin factor	57.179031

#### Superposition Horner Plot Line Details

Line type : Radial flow

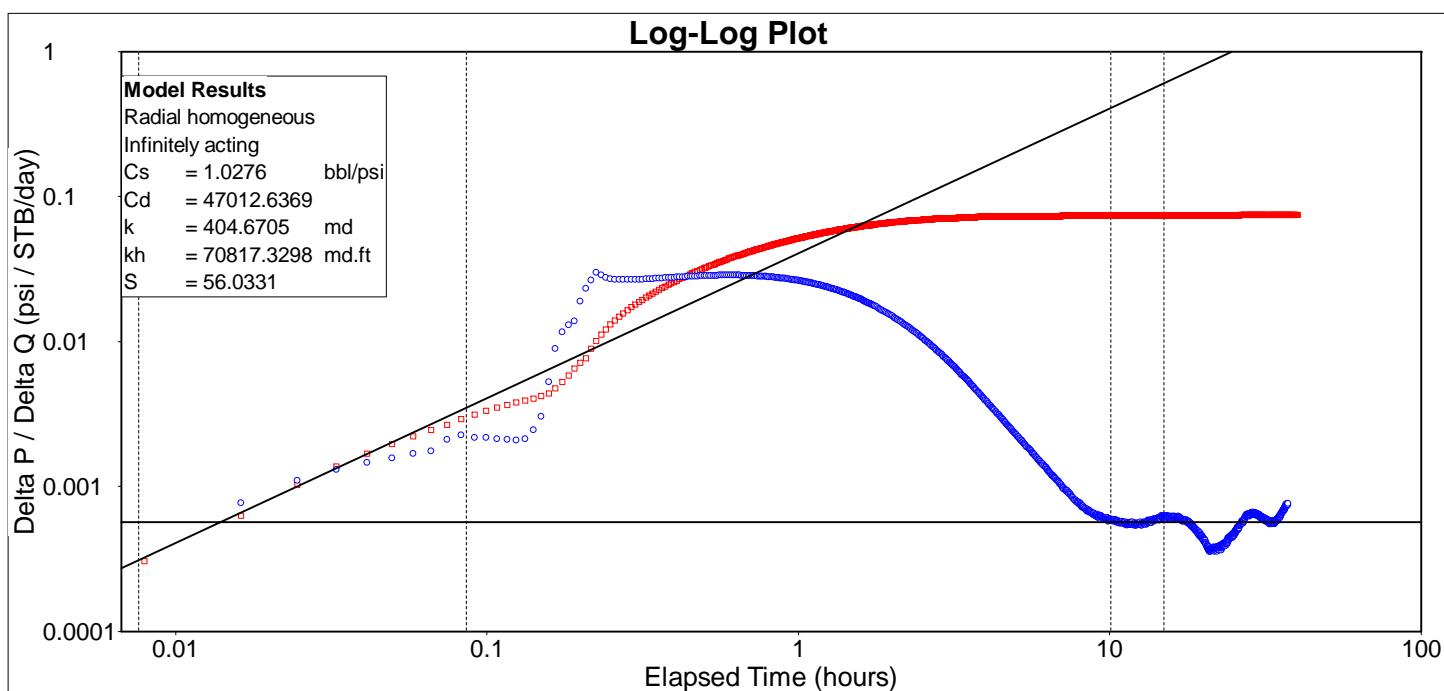
Slope : 6.12611

Intercept : 4359.59

Coefficient of Determination : 0.999706

	Radial flow
Extrapolated pressure	4359.586451 psia
Pressure at dt = 1 hour	4378.156194 psia

Number of Intersections = 0



#### Log-Log Plot Model Results

Radial homogeneous - Infinitely acting

Classic Wellbore Storage

	Value
Wellbore storage coefficient	1.027609 bbl/psi
Dimensionless wellbore storage	4.7013e4
Permeability	404.670456 md
Permeability-thickness	7.0817e4 md.ft
Skin factor	56.033142

#### Log-Log Plot Line Details

Line type : Radial flow

Slope : 0

Intercept : 0.000568251

Coefficient of Determination : Not Used

Line type : Wellbore storage

Slope : 1

Intercept : 0.0405472

Coefficient of Determination : Not Used

Number of Intersections = 0

## LOGS

- **Dual Induction Log Sections from 7924 feet to 8476 feet**
- **Neutron Density Log Sections from 7924 feet to 8476 feet**
- **Mewbourne Well No. 1, July 23, 1998, Temperature Log**