NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date	
Company: Amoco Production Company		Connection			
Pool: Bravo Dome Carbon Dioxide Gas Unit-640 Acre Area		Formation		Unit: BDCDGU	
Completion Date: 12-1-85	Total Depth: 2550	Plug Back TD: 2454	Elevation: 4550	Farm or Lease Name	
Csg. Size: 7 / Wt.: 20 / d: / Set At: 2550		Perforations: From 2345 To 2408		Well No.: 1835 271G	
Tbg. Size: 3-1/2 / Wt.: 9.3 / d: / Set At: 2194		Perforations: From To		Unit: G / Sec.: 27 / Twp.: 18 / Rge.: 35	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Singe		Packer Set At: 2164		County: Union	
Producing Thru: Tubing	Reservoir Temp. °F: 90 @ 2377	Mean Annual Temp. °F: 50	Baro. Press. – P_a: 12.25	State: New Mexico	

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
2377	2377	1.529	100	0	0		4.0	Flange

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size x Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					346				
1.	4.026 x 3.000	180.1	3	48	192.35	48			1.5
2.	4.026 x 3.000	150.1	6	49	162.35	49			1.5
3.	4.026 x 3.000	123.5	12	51	135.75	51			1.5
4.	4.026 x 3.000	98.5	14.5	51	110.75	51			1.5
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1							1400
2.							1570
3.							1726
4.							1768
5.							

NO.	P_t	Temp. °R	T_t	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio: 0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: 1.529 xxxxxxxxx
Specific Gravity Flowing Fluid: xxxxx
Critical Pressure: 1072 P.S.I.A. P.S.I.A.
Critical Temperature: 496 R R

P_c 358.2 P_c^2 128.307

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		192.4		91.289
2		162.4		101.933
3		135.8		109.865
4		110.8		116.163
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.09$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1939$

Absolute Open Flow: 1939 Mcfd @ 15.025 Angle of Slope θ: Slope, n: .97

Remarks:

Approved By Commission:	Conducted By:	Calculated By: Don Kimble	Checked By: