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Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator	MEWBOURNE OIL CO.				Lease or Unit Name	ESPERANZA 19 FED COM			
Type Test: ☑ Initial ☐ Annual ☐ Special					Test Date: 4/14/04	Well No.: 1			
Completion Date: 2/15/04	Total Depth: 11670			Plug Back TD: 11624		Elevation: 3159	Unit Ltr - Sec - TWP - Rge: I 19 21S 27E		
Csg. Size: 5 1/2	Wt.: 17	d: 4.892	Set At: 11670	Perforations: From: 11286	To: 11334		County: EDDY		
Tbg. Size: 2 7/8	Wt.: 6.5	d: 2.441	Set At: 10507	Perforations: From:	To:		Pool: BURTON FLAT MORROW		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE				Packer Set At: 10485			Formation: MORROW		
Producing Thru: TUBING	Reservoir Temp.: 178	Mean Annual Temp.: 60		Baro. Press.-P_a: 13.2			Connection: SALES		
L: 10507	H: 10507	Gg: 0.602	%CO_2: 2.791	%N_2: 1.062	%H_2S:	Prover:	Meter Run: 3.067		Taps: FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					2860				
1	3.068 X 1.750	508	2.5	65	2620				1 HRS
2	3.068 X 1.750	508	10	66	2410				1 HRS
3	3.068 X 1.750	508	40	66	1845				1 HRS
4	3.068 X 1.750	508	75	65	1100				1 HRS
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							708
2	TOTAL	FLOW	METER				1417
3							2835
4							4129
5							

No.	P_r	Temp. R	T_r	Z
1				
2				
3	TOTAL	FLOW	METER	
4				
5				

Gas Liquid Hydrocarbon Ratio: N/A Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: N/A Deg.
Specific Gravity Separator Gas: 0.602 XXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 679 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 351 R. ____ R

P_c 2873.2 P_c^2 8255.3

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2634.4	6940.3	1315
2		2428.6	5898	2357.3
3		1885.8	3556.4	4698.9
4		1211.7	1468.3	6787
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.216 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.216

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 5.022

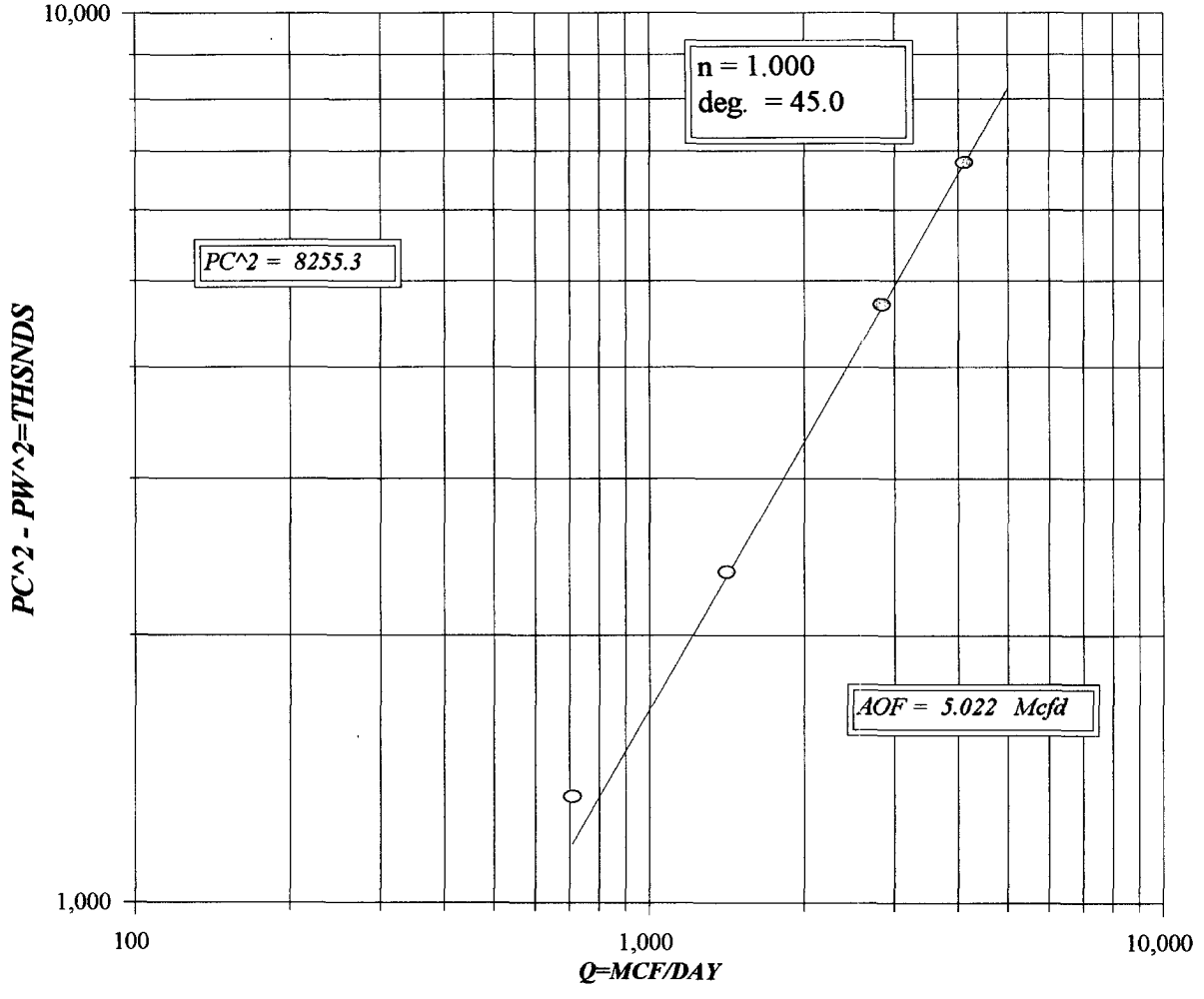
Absolute Open Flow: 5.022 Mcfd @ 15.025 | Angle of Slope (): 45 | Slope n: 1

Remarks: * NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	BM

MEWBOURNE OIL CO.

ESPERANZA "19" FED COM #1



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	MEWBOURNE OIL		LEASE :	ESPERANZA 19 FED COM	ELL NO. :	1					
UNIT :	I		SECTION :	19	TOWNSHIP :	21S					
L :	10507	H :	10507	L/H :	1	G/GMIX :	0.602				
%C02 :	2.791	%N2 :	1.062	H2S :		DATE :	4/14/04				
d :	2.441	Fr :	0.010763	GH :	8197.0	RANGE :	27E				
VOL 1 :	708	PSIA 1 :	2633.2			RESV.TEMP	178.0				
VOL 2 :	1417	PSIA 2 :	2423.2								
VOL 3 :	2835	PSIA 3 :	1858.2			SHUT-IN PRES =	2860				
VOL 4 :	4129	PSIA 4 :	1113.2								
				PCR :	679						
				TCR :	351						

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1	QM	0.708	0.708	1.417	1.417	2.835	2.835	4.129	4.129
2	TW	534	534	534	534	534	534	534	534
3	Ts	638.0	638.0	638.0	638.0	638.0	638.0	638.0	638.0
4	T	586.0	586.0	586.0	586.0	586.0	586.0	586.0	586.0
	PR (est)	3.88		3.57		2.74		1.64	
5	Z(est)	0.833	0.845	0.831	0.837	0.839	0.832	0.877	0.860
6	TZ	487.9	494.9	487.0	490.7	491.5	487.4	513.8	504.0
7	GH/TZ	16.799	16.562	16.833	16.706	16.678	16.819	15.954	16.265
8	eS	1.878	1.861	1.880	1.871	1.869	1.879	1.819	1.840
9	I-e-S	0.467	0.463	0.468	0.466	0.465	0.468	0.450	0.457
10	Pt	2633.2	2633.2	2423.2	2423.2	1858.2	1858.2	1113.2	1113.2
11	Pt2 /1000	6933.7	6933.7	5871.9	5871.9	3452.9	3452.9	1239.2	1239.2
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.252	5.327	5.241	5.281	5.290	5.245	5.530	5.424
14	FcQm	3.72	3.77	7.43	7.48	15.00	14.87	22.83	22.40
15	L/H(FcQm)2	13.8	14.2	55.2	56.0	224.9	221.1	521.4	501.6
16	Fw	6.4618072	6.5804596	25.817375	26.068661	104.5709	103.44809	234.73673	229.040186
17	Pw2	6940.2	6940.3	5897.7	5898.0	3557.5	3556.4	1474.0	1468.3
18	Ps2	13030.5	12915.4	11087.2	11035.1	6649.1	6682.3	2681.1	2702.0
19	Ps	3609.8	3593.8	3329.7	3321.9	2578.6	2585.0	1637.4	1643.8
20	P	3121.5	3113.5	2876.5	2872.6	2218.4	2221.6	1375.3	1378.5
21	Pr	4.60	4.59	4.24	4.23	3.27	3.27	2.03	2.03
22	Tr	1.67	1.67	1.67	1.67	1.67	1.67	1.67	1.67
23	Z	0.845	0.844	0.837	0.837	0.832	0.832	0.860	0.860

Pc =	2873.2	Pc2 =	8255.3
Pt2 =	6933.7	Pw =	2634.4
	5871.9		2428.6
	3452.9		1885.8
	1239.2		1211.7
Pc2-Pw2=	1315.0	Pw2 =	6940.3
	2357.3		5898.0
	4698.9		3556.4
	6787.0		1468.3
		n =	1.000
Pc2/(Pc2-Pw2) =			6.278
			3.502
			1.757
			1.216
[Pc2/Pc2-Pw2]n =			6.278
			3.502
			1.757
			1.216
	AOF= Q		4.445
			4.962
			4.981
			5.022

FORM C122-D