5

Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

30-015-33381

Form C-122
Revised October, 1999

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SEP 1 6 2004
OCD-ARTESIA

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator	MEWBOURNE OIL				Lease or Unit Name	TOMBSTONE 7 FED COM			
Type Test: ☑ Initial ☐ Annual ☐ Special					Test Date: 8/19/04	Well No.: 1			
Completion Date: 7/29/04	Total Depth: 9700			Plug Back TD: 9654	Elevation: 3535	Unit Ltr - Sec - TWP - Rge: P 7 20S 25E			
Csg. Size: 5 1/2	Wt.: 17	d: 4.892	Set At: 9700	Perforations: From: 9414 To: 9504		County: EDDY			
Tbg. Size: 2 7/8	Wt.: 6.5	d: 2.441	Set At: 8897	Perforations: From: To:		Pool: CEMETARY MORROW			
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE				Packer Set At: 8883		Formation: MORROW			
Producing Thru: TUBING	Reservoir Temp.: 181	Mean Annual Temp.: 60		Baro. Press.-P_a: 13.2		Connection: SALES			
L: 11048	H: 11048	Gg: 0.7	%CO_2: 7.562	%N_2: 1.902	%H_2S:	Prover:	Meter Run: 3.067		Taps: FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					1233.2				
1	3.067 X 1.000	119	10.1	72	313.2				24 HRS.
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							1170
2	TOTAL	FLOW	METER				
3							
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2				
3	TOTAL	FLOW	METER	
4				
5				

Gas Liquid Hydrocarbon Ratio: N/A Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons: N/A Deg.
Specific Gravity Separator Gas: 0.595 XXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 677 P.S.I.A. P.S.I.A.
Critical Temperature: 349 R. R

P_c 1233.2 P_c^2 1520.8

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		344.5	118.7	1402.1
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.085 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.085

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.269

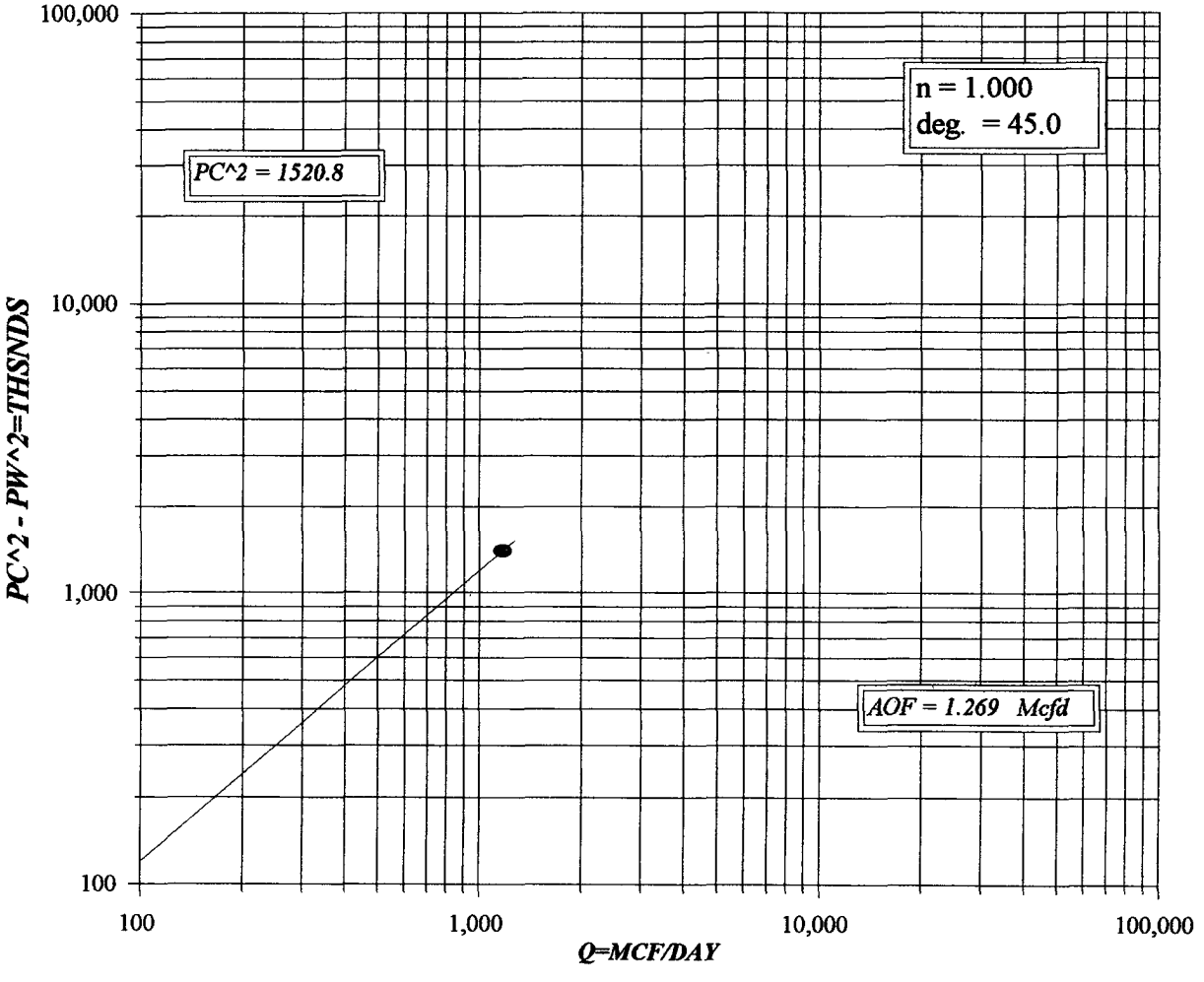
Absolute Open Flow: 1.269 Mcfd @ 15.025 | Angle of Slope (): 45 | Slope n: 1

Remarks: * NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	BM

MEWBOURNE OIL CO.

TOMBSTONE "7" FED COM #1



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	MEWBOURNE OIL CO.		LEASE :	TOMBSTONE 7 FED COMWELL NO.		:	2										
UNIT :	P		SECTION :	7		TOWNSHIP :	20S										
L :	8897	H :	8897	L/H :	1	G/GMIX :	0.595										
%C02 :	1.57	%N2 :	0.507	H2S :			DATE :	8/19/04									
d :	2.441	Fr :	0.010763	GH :	8197.0		RANGE :	25E									
VOL 1 :	1170	PSIA 1 :	313.2			RESV.TEMP	181.0										
VOL 2 :		PSIA 2 :															
VOL 3 :		PSIA 3 :				SHUT-IN PRE! =	1233.2										
VOL 4 :		PSIA 4 :															
				PCR :	677												
				TCR :	349												

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		`1ST	`2ND	`1ST	`2ND	`1ST	`2ND	`1ST	`2ND
1	QM	1.170	1.170	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	641.0	641.0	641.0	641.0	641.0	641.0	641.0	641.0
4	T	587.5	587.5	587.5	587.5	587.5	587.5	587.5	587.5
	PR (est)	0.46		0.00		0.00		0.00	
5	Z(est)	0.945	0.939	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	555.4	551.5	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	14.759	14.862	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.739	1.746	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.425	0.427	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	313.2	313.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	98.1	98.1	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.978	5.936	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	6.99	6.95	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)2	48.9	48.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	20.790345	20.610043	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	118.9	118.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	206.8	207.3	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	454.7	455.3	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	384.0	384.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	0.57	0.57	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.68	1.68	1.68	1.68	1.68	1.68	1.68	1.68
23	Z	0.939	0.939	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

Pc =	1233.2	Pc2 =	1520.8
Pt2 =	98.1	Pw =	344.5
	0.0		#DIV/0!
	0.0		#DIV/0!
	0.0		#DIV/0!
Pc2-Pw2=	1402.1	Pw2 =	118.7
	#DIV/0!		#DIV/0!
	#DIV/0!		#DIV/0!
	#DIV/0!		#DIV/0!
n =	1.000		
Pc2/(Pc2-Pw2) =	1.085		
	#DIV/0!		
	#DIV/0!		
	#DIV/0!		
[Pc2/Pc2-Pw2]n =	1.085		
	#DIV/0!		
	#DIV/0!		
	#DIV/0!		
AOF = Q	1.269		
	#DIV/0!		
	#DIV/0!		
	#DIV/0!		

FORM C122-D