Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

30-015-33500

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: MEWBOURNE OIL		Lease or Unit Name: JUSTICE FED COM	
Type Test: ☑ Initial ☐ Annual ☐ Special		Test Date: 9/09/04	Well No.: 1
Completion Date: 9/9/2004	Total Depth: 11870	Plug Back TD: 11740	Elevation: 3194 GL
Unit Ltr - Sec - TWP - Rge: C 1 21S 27E			
Csg. Size: 5 1/2 / Wt.: 17 / d: 4.8 / Set At: 11870	Perforations: From: 11386 To: 11490	County: EDDY	
Tbg. Size: 2 7/8 / Wt.: 6.5 / d: 2.441 / Set At: 11133	Perforations: From: 11997 To: 12196	Pool: BURTON FLAT	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE	Packer Set At: 11114	Formation: MORROW	
Producing Thru: TUBING	Reservoir Temp.: 181	Mean Annual Temp.: 60	Baro. Press.-P_a: 13.2
Connection: SALES			

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
11133	11133	0.617	3.224	1.08	N/A	N/A	3.067	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					4013.2		PKR		24 HRS
1	3 X 1.125	85	12	45	554		"		24 HRS
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							170
2							
3	TOTAL	FLOW	METER				
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2	TOTAL	FLOW	METER	
3				
4				
5				

Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	DRY	Deg.
Specific Gravity Separator Gas	0.617	XXXXXXX
Specific Gravity Flowing Fluid	XXXXX	N/A
Critical Pressure	682 P.S.I.A.	N/A P.S.I.A.
Critical Temperature	350 R.	N/A R

P_c 4013.2 P_c^2 16105.8

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		567.5	322.1	15673.7
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.028 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.028

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 0.175

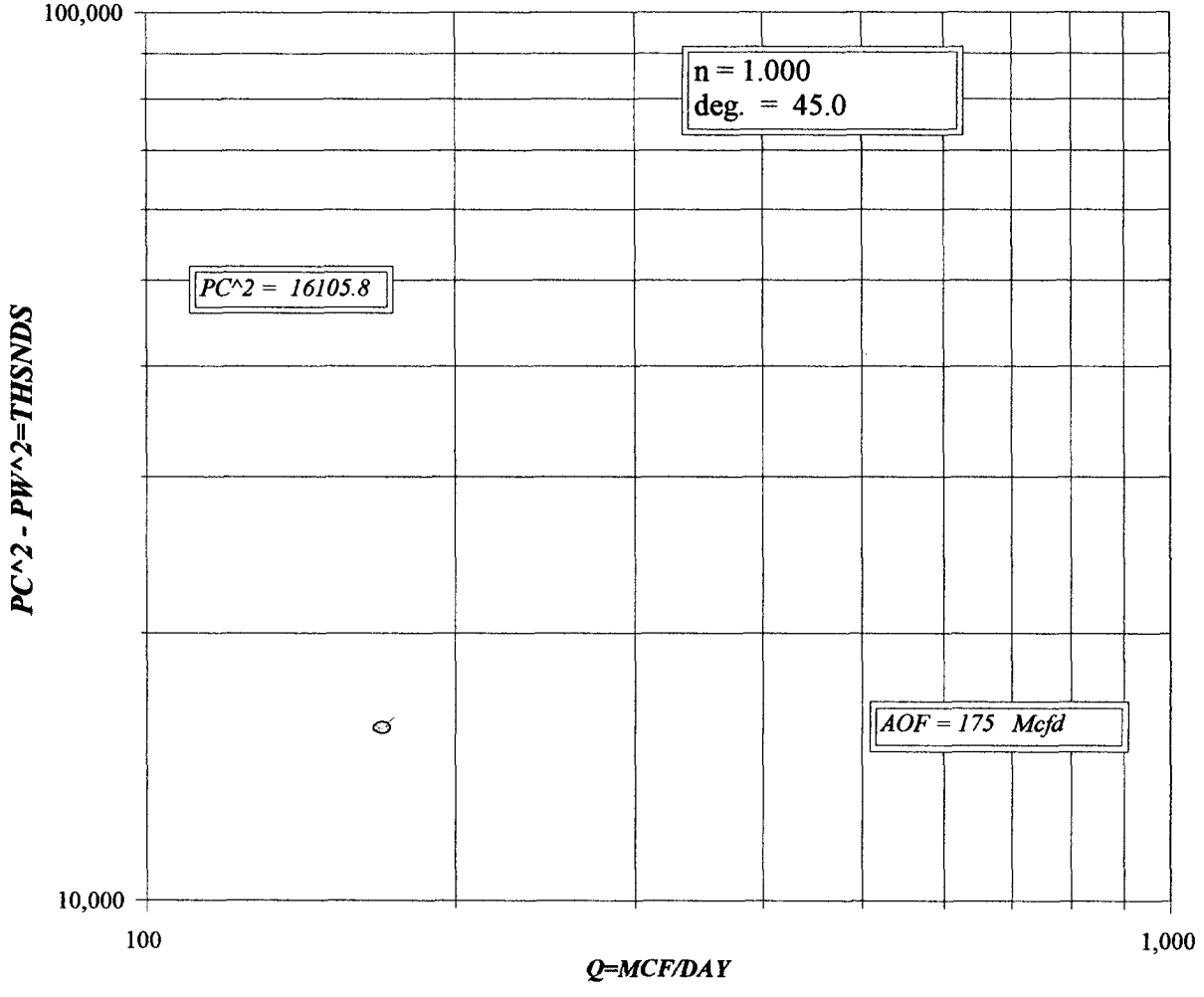
Absolute Open Flow 2,286 Mcfd @ 15.025 | Angle of Slope θ: 45 | Slope, n: 1.000

Remarks: NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	MEWBOURNE OIL	MERV BUECKER	BM

MEWBOURNE OIL

JUSTICE FED COM #1



COMPANY :	MEWBOUF	OIL		LEASE :	JUSTIS FED. COM		WELL NO. :	1			Pc =	4013.2		Pc2 =	16105.8				
UNIT :	C			SECTION :	1		TOWNSHIF :	21											
L :	11133	H :	11133	L/H :	1		G/GMIX :	0.617			Pt2 =	321.7		Pw =	567.5				
%CO2 :	3.224	%N2 :	1.083	H2S :				DATE :	9-9-04			0.0			#DIV/0!				
d :	2.441	Fr :	0.010763	GH :	6869.1			RANGE :	27			0.0			#DIV/0!				
												0.0			#DIV/0!				
VOL 1 :	170	PSIA 1 :	567.2				RESV.TEMP	185.3			Pc2-Pw2=			15673.7	Pw2 =	322.1			
VOL 2 :		PSIA 2 :										#DIV/0!			#DIV/0!				
VOL 3 :		PSIA 3 :					SHUT-IN PRI =	4013.2				#DIV/0!			#DIV/0!				
VOL 4 :		PSIA 4 :										#DIV/0!			#DIV/0!				
				PCR :	682							n =		1.000					
				TCR :	350														
											Pc2/(Pc2-Pw2) =			1.028					
														#DIV/0!					
LINE	RATE 1		RATE 2		RATE 3		RATE 4							#DIV/0!					
	`1ST	`2ND	`1ST	``2ND	`1ST	`2ND	`1ST	`2ND											
1 QM	0.170	0.170	0.000	0.000	0.000	0.000	0.000	0.000											
2 TW	534	534	534	534	534	534	534	534			[Pc2/Pc2-Pw2]n =			1.028					
3 Ts	645.3	645.3	645.3	645.3	645.3	645.3	645.3	645.3						#DIV/0!					
4 T	589.7	589.7	589.7	589.7	589.7	589.7	589.7	589.7						#DIV/0!					
PR (est)	0.83		0.00		0.00		0.00							#DIV/0!					
5 Z(est)	0.923	0.916	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
6 TZ	544.2	540.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!				AOF= Q		0.175					
7 GH/TZ	12.622	12.712	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!						#DIV/0!					
8 eS	1.605	1.611	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!						#DIV/0!					
9 I-e-S	0.377	0.379	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!						#DIV/0!					
10 Pt	567.2	567.2	0.0	0.0	0.0	0.0	0.0	0.0											
11 Pt2 /1000	321.7	321.7	0.0	0.0	0.0	0.0	0.0	0.0											
12 Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.0107631											
13 Fc=FrTZ	5.857	5.816	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
14 FcQm	1.00	0.99	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
15 L/H(FcQm)	1.0	1.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
16 Fw	0.373867	0.370671	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
17 Pw2	322.1	322.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
18 Ps2	517.1	518.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
19 Ps	719.1	720.3	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
20 P	643.1	643.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
21 Pr	0.94	0.94	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
22 Tr	1.68	1.68	1.68	1.68	1.68	1.68	1.68	1.68											
23 Z	0.916	0.916	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!						FORM C122-D					