Carlsbad F'eld Office **OCD** Artesia

Form 3160-3 (March 2012)

NM OIL CONSERVATION ARTESIA DISTRICT

Alig 17 2010

FORM APPROVED OMB No. 1004-0137 Expires October 31, 2014

UNITED STATES

DEPARTMENT OF THE BUREAU OF LAND MAN	NMNM054289 6. If Indian, Allotee or Tribe Name				
APPLICATION FOR PERMIT TO					
la. Type of work: ✓ DRIŁL REENTER				7 If Unit or CA Agre	eement, Name and No.
Ib. Type of Well: ☐ Oil Well ☐ Gas Well ☐ Other ☐ Single Zone ☐ Multiple Zone			8. Lease Name and GARRETT FED CO	Well No.	
2. Name of Operator MATADOR PRODUCTION COMPANY	1	2289	37	9. API Well No. 30 - 0	15-45/83
· · · · · · · · · · · · · · · · · · ·		one No. (include area code))371-5200		10. Field and Pool, or Exploratory PURPLE-SAGE WOLFCAMP GAS	
4. Location of Well (Report location clearly and in accordance with any State requirements.*) At surface SWNW / 2372 FNL / 584 FWL / LAT 32.1746147 / LONG -104.0132281			:e	11. Sec., T. R. M. or Blk. and Survey or Area SEC 32 / T24S / R29E / NMP	
At proposed prod. zone SENE / 2323 FNL / 240 FEL / LAT 14. Distance in miles and direction from nearest town or post office* 5 miles	32.1740007	LONG - 103.99000		12. County or Parish EDDY	13. State NM
15. Distance from proposed* location to nearest 584 feet property or lease line, ft. (Also to nearest drig. unit line, if any)	16. No. of a 80	cres in lease	17. Spacii 320	ng Unit dedicated to this	well
18. Distance from proposed location* to nearest well, drilling, completed, 30 feet applied for, on this lease, ft.	77. Troposed Depth			M/BIA Bond No. on file NMB001079	
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 22. App. 2920 feet 03/01.		mate date work will sta 8	vill start* 23. Estimated duration 90 days		on
	24. Attac				
The following, completed in accordance with the requirements of Onsho	ore Oil and Gas	Order No.1, must be a	ttached to tl	his form:	
 Well plat certified by a registered surveyor. A Drilling Plan. A Surface Use Plan (if the location is on National Forest System SUPO must be filed with the appropriate Forest Service Office). 	Lands, the	Item 20 above). 5. Operator certific	cation		s may be required by the
25. Signature (Electronic Submission)		(Printed Typed) Wood / Ph: (505)4	66-8120		Date 01/31/2018
Title President					
Approved by (Signature) Name		Name (Printed'Typed) Cody Layton / Ph: (575)234-5959			Date 07/16/2018
Title Assistant Field Manager Lands & Minerals Application approval does not warrant or certify that the applicant hol		LSBAD	nts in the su	bject lease which would	entitle the applicant to
conduct operations thereon. Conditions of approval, if any, are attached.					
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a States any false, fictitious or fraudulent statements or representations as	crime for any p s to any matter v	erson knowingly and vithin its jurisdiction.	willfully to	make to any department	or agency of the United

(Continued on page 2)

*(Instructions on page 2)



INSTRUCTIONS

GENERAL: This form is designed for submitting proposals to perform certain well operations, as indicated on Federal and Indian lands and leases for action by appropriate Federal agencies, pursuant to applicable Federal laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from local Federal offices.

ITEM 1: If the proposal is to redrill to the same reservoir at a different subsurface location or to a new reservoir, use this form with appropriate notations. Consult applicable Federal regulations concerning subsequent work proposals or reports on the well.

ITEM 4: Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local Federal offices for specific instructions.

ITEM 14: Needed only when location of well cannot readily be found by road from the land or lease description. A plat, or plats, separate or on the reverse side, showing the roads to, and the surveyed location of, the well, and any other required information, should be furnished when required by Federal agency offices.

ITEMS 15 AND 18: If well is to be, or has been directionally drilled, give distances for subsurface location of hole in any present or objective productive zone.

ITEM 22: Consult applicable Federal regulations, or appropriate officials, concerning approval of the proposal before operations are started.

NOTICES

The Privacy Act of 1974 and regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 25 U.S.C. 396; 43 CFR 3160

PRINCIPAL PURPOSES: The information will be used to: (1) process and evaluate your application for a permit to drill a new oil, gas, or service well or to reenter a plugged and abandoned well; and (2) document, for administrative use, information for the management, disposal and use of National Resource Lands and resources including (a) analyzing your proposal to discover and extract the Federal or Indian resources encountered; (b) reviewing procedures and equipment and the projected impact on the land involved; and (c) evaluating the effects of the proposed operation on the surface and subsurface water and other environmental impacts. ROUTINE USE: Information from the record and/or the record will be transferred to appropriate Federal, State, and local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecution, in connection with congressional inquiries and for regulatory responsibilities.

EFFECT OF NOT PROVIDING INFORMATION: Filing of this application and disclosure of the information is mandatory only if you elect to initiate a drilling or reentry operation on an oil and gas lease.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM collects this information to allow evaluation of the technical, safety, and environmental factors involved with drilling for oil and/or gas on Federal and Indian oil and gas leases. This information will be used to analyze and approve applications. Response to this request is mandatory only if the operator elects to initiate drilling or reentry operations on an oil and gas lease. The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Collection Clearance Officer (WO-630), 1849 C Street, N.W., Mail Stop 401 LS, Washington, D.C. 20240.

(Continued on page 3) (Form 3160-3, page 2)

Additional Operator Remarks

Location of Well

1. SHL: SWNW / 2372 FNL / 584 FWL / TWSP: 24S / RANGE: 29E / SECTION: 32 / LAT: 32.1746147 / LONG: -104.0132281 (TVD: 0 feet, MD: 0 feet)
PPP: SWNE / 2328 FNL / 2460 FEL / TWSP: 24S / RANGE: 29E / SECTION: 32 / LAT: 32.17471 / LONG: -104.00656 (TVD: 10955 feet, MD: 13336 feet)
PPP: SENW / 2328 FNL / 1320 FWL / TWSP: 24S / RANGE: 29E / SECTION: 32 / LAT: 32.17473 / LONG: -104.010822 (TVD: 10955 feet, MD: 12022 feet)
PPP: SWNW / 2372 FNL / 584 FWL / TWSP: 24S / RANGE: 29E / SECTION: 32 / LAT: 32.1746147 / LONG: -104.0132281 (TVD: 0 feet, MD: 0 feet)
BHL: SENE / 2323 FNL / 240 FEL / TWSP: 24S / RANGE: 29E / SECTION: 32 / LAT: 32.174688 / LONG: -103.998856 (TVD: 10955 feet, MD: 15720 feet)

BLM Point of Contact

Name: Judith Yeager

Title: Legal Instruments Examiner

Phone: 5752345936 Email: jyeager@blm.gov

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Review and Appeal Rights

A person contesting a decision shall request a State Director review. This request must be filed within 20 working days of receipt of the Notice with the appropriate State Director (see 43 CFR 3165.3). The State Director review decision may be appealed to the Interior Board of Land Appeals, 801 North Quincy Street, Suite 300, Arlington, VA 22203 (see 43 CFR 3165.4). Contact the above listed Bureau of Land Management office for further information.

(Form 3160-3, page 4)

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: | Matador Production Company

LEASE NO.: | NMNM-054289

WELL NAME & NO.: | Garrett Fed Com 226H SURFACE HOLE FOOTAGE: | 2372' FNL & 0584' FWL BOTTOM HOLE FOOTAGE | 2323' FNL & 0240' FEL

LOCATION: | Section 24, T. 29 S., R 32 E., NMPM

COUNTY: | County, New Mexico

Communitization Agreement

The operator will submit a Communitization Agreement to the Carlsbad Field Office, 620 E Greene St. Carlsbad, New Mexico 88220, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.

If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.

In addition, the well sign shall include the surface and bottom hole lease numbers. When the Communitization Agreement number is known, it shall also be on the sign.

A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

☐ Eddy County

Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822

- 1. Although Hydrogen Sulfide has not been reported in the area, it is always a potential hazard. If Hydrogen Sulfide is encountered, report measured amounts and formations to the BLM.
- 2. Hydrogen Sulfide has been reported as a hazard, but no measurements have been recorded. It is recommended that monitoring equipment be onsite for potential Hydrogen Sulfide. If Hydrogen Sulfide is encountered, report measurements and formations to the BLM.
- 3. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval an Incident of Non-Compliance will be written and will be a "Major" violation.
- 4. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.
- 5. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

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Wait on cement (WOC) for Water Basin:

After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements.

Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Medium Cave/Karst

Possibility of water flows in the Castile and Salado.

Possibility of lost circulation in the Rustler, Red Beds, and Delaware.

Abnormal pressure maybe encountered when penetrating the 3rd Bone Spring Sandstone and all subsequent formations.

- 1. The 13-3/8 inch surface casing shall be set at approximately 610 feet (in a competent bed below the Magenta Dolomite, which is a Member of the Rustler, and if salt is encountered, set casing at least 25 feet above the salt) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

2.	The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:
_	Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.
	cement does not circulate to surface on the intermediate casing, the cement on the $5/8 \times 7$ casing must come to surface.
3.	The minimum required fill of cement behind the 7-5/8 X 7 inch intermediate casing is:
_	Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.
Te po pr	rmation below the 9-5/8" shoe to be tested according to Onshore Order 2.III.B.1.i. st to be done as a mud equivalency test using the mud weight necessary for the re pressure of the formation below the shoe (not the mud weight required to event dissolving the salt formation) and the mud weight for the bottom of the le. Report results to BLM office.
	entralizers required on horizontal leg, must be type for horizontal service and a nimum of one every other joint.
4.	The minimum required fill of cement behind the 5-1/2 X 4-1/2 inch production casing is:
	Cement as proposed by operator. Operator shall provide method of verification.
5.	If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
C.	PRESSURE CONTROL
1.	All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API 53.

2. Variance approved to use flex line from BOP to choke manifold. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor. If the BLM inspector questions the straightness of the hose, a BLM engineer will be contacted and will review in the field or via picture supplied by inspector to determine if changes are required (operator shall expect delays if this occurs).

BOP Option #1:

- 3. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be psi.
 - a. For surface casing only: If the BOP/BOPE is to be tested against casing, the wait on cement (WOC) time for that casing is to be met (see WOC statement at start of casing section). Independent service company required.
- 4. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 9-5/8 1st intermediate casing shoe shall be psi.
- 5. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 7-5/8 X 7 intermediate casing shoe shall be psi. 5M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

BOP Option #2:

Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. Operator shall perform the 9-5/8" and 7-5/8 X 7" casing integrity tests to 70% of the casing burst. This will test the multi-bowl seals.
- e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 7-5/8 X 7 casing shoe shall be psi.

- a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

5M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

6. The appropriate BLM office shall be notified a minimum of hours in advance for a representative to witness the tests.

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- a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- a. The tests shall be done by an independent service company utilizing a test plug **not a cup or J-packer**.
- b. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
- c. The results of the test shall be reported to the appropriate BLM office.
- d. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- e. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- f. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the **Wolfcamp** formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

D. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the **Wolfcamp** formation, and shall be used until production casing is run and cemented.

E. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

F. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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PECOS DISTRICT SURFACE USE CONDITIONS OF APPROVAL

OPERATOR'S NAME: Matador Production Company
LEASE NO.: NMNM054289
WELL NAME & NO.: Garrett Fed Com 226H
SURFACE HOLE FOOTAGE: 2372'/N & 584'/W
BOTTOM HOLE FOOTAGE LOCATION: Section 32, T.24 S., R.29 E., NMPM
COUNTY: Eddy County, New Mexico

TABLE OF CONTENTS

Standard Conditions of Approval (COA) apply to this APD. If any deviations to these standards exist or special COAs are required, the section with the deviation or requirement will be checked below.

General Provisions
Permit Expiration
Archaeology, Paleontology, and Historical Sites
Noxious Weeds
Special Requirements
Hydrology
Cave/Karst
Range
☐ Construction
Notification
Topsoil
Closed Loop System
Federal Mineral Material Pits
Well Pads
Roads
☐ Road Section Diagram
☐ Production (Post Drilling)
Well Structures & Facilities
Pipelines
☐ Interim Reclamation
Final Abandonment & Reclamation

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I. GENERAL PROVISIONS

The approval of the Application For Permit To Drill (APD) is in compliance with all applicable laws and regulations: 43 Code of Federal Regulations 3160, the lease terms, Onshore Oil and Gas Orders, Notices To Lessees, New Mexico Oil Conservation Division (NMOCD) Rules, National Historical Preservation Act As Amended, and instructions and orders of the Authorized Officer. Any request for a variance shall be submitted to the Authorized Officer on Form 3160-5, Sundry Notices and Report on Wells.

II. PERMIT EXPIRATION

If the permit terminates prior to drilling and drilling cannot be commenced within 60 days after expiration, an operator is required to submit Form 3160-5, Sundry Notices and Reports on Wells, requesting surface reclamation requirements for any surface disturbance. However, if the operator will be able to initiate drilling within 60 days after the expiration of the permit, the operator must have set the conductor pipe in order to allow for an extension of 60 days beyond the expiration date of the APD. (Filing of a Sundry Notice is required for this 60 day extension.)

III. ARCHAEOLOGICAL, PALEONTOLOGY & HISTORICAL SITES

Any cultural and/or paleontological resource discovered by the operator or by any person working on the operator's behalf shall immediately report such findings to the Authorized Officer. The operator is fully accountable for the actions of their contractors and subcontractors. The operator shall suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Authorized Officer. An evaluation of the discovery shall be made by the Authorized Officer to determine the appropriate actions that shall be required to prevent the loss of significant cultural or scientific values of the discovery. The operator shall be held responsible for the cost of the proper mitigation measures that the Authorized Officer assesses after consultation with the operator on the evaluation and decisions of the discovery. Any unauthorized collection or disturbance of cultural or paleontological resources may result in a shutdown order by the Authorized Officer.

IV. NOXIOUS WEEDS

The operator shall be held responsible if noxious weeds become established within the areas of operations. Weed control shall be required on the disturbed land where noxious weeds exist, which includes the roads, pads, associated pipeline corridor, and adjacent land affected by the establishment of weeds due to this action. The operator shall consult with the Authorized Officer for acceptable weed control methods, which include following EPA and BLM requirements and policies.

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V. SPECIAL REQUIREMENT(S)

Cave/Karst Surface Mitigation

The following stipulations will be applied to minimize impacts during construction, drilling and production:

Construction:

In the advent that any underground voids are opened up during construction activities, construction activities will be halted and the BLM will be notified immediately.

No Blasting:

No blasting will be utilized for pad construction. The pad will be constructed and leveled by adding the necessary fill and caliche.

Pad Berming:

- The entire perimeter of the well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad.
- The compacted berm shall be constructed at a minimum of 12 inches high with impermeable mineral material (e.g., caliche).
- No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad.
- The topsoil stockpile shall be located outside the bermed well pad.
- Topsoil, either from the well pad or surrounding area, shall not be used to construct the berm.
- No storm drains, tubing or openings shall be placed in the berm.
- If fluid collects within the bermed area, the fluid must be vacuumed into a safe container and disposed of properly at a state approved facility.
- The integrity of the berm shall be maintained around the surfaced pad throughout the life of the well and around the downsized pad after interim reclamation has been completed.
- Any access road entering the well pad shall be constructed so that the integrity of the berm height surrounding the well pad is not compromised. (Any access road crossing the berm cannot be lower than the berm height.)
- Following a rain event, all fluids will vacuumed off of the pad and hauled off-site and disposed at a proper disposal facility.

Tank Battery Liners and Berms:

Tank battery locations and all facilities will be lined and bermed. A 20 mil permanent liner will be installed with a 4 oz. felt backing, or equivalent, to prevent tears or punctures. Tank battery berms must be large enough to contain 1 ½ times the content of the largest tank.

Leak Detection System:

A method of detecting leaks is required. The method could incorporate gauges to measure loss, situating values and lines so they can be visually inspected, or installing electronic sensors to alarm when a leak is present. Leak detection plan will be submitted to BLM for approval.

Automatic Shut-off Systems:

Automatic shut off, check values, or similar systems will be installed for pipelines and tanks to minimize the effects of catastrophic line failures used in production or drilling.

Cave/Karst Subsurface Mitigation

The following stipulations will be applied to protect cave/karst and ground water concerns:

Rotary Drilling with Fresh Water:

Fresh water will be used as a circulating medium in zones where caves or karst features are expected. SEE ALSO: Drilling COAs for this well.

Directional Drilling:

Kick off for directional drilling will occur at least 100 feet below the bottom of the cave occurrence zone. SEE ALSO: Drilling COAs for this well.

Lost Circulation:

ALL lost circulation zones from the surface to the base of the cave occurrence zone will be logged and reported in the drilling report.

Regardless of the type of drilling machinery used, if a void of four feet or more and circulation losses greater than 70 percent occur simultaneously while drilling in any cavebearing zone, the BLM will be notified immediately by the operator. The BLM will assess the situation and work with the operator on corrective actions to resolve the problem.

Abandonment Cementing:

Upon well abandonment in cave karst areas additional plugging conditions of approval may be required. The BLM will assess the situation and work with the operator to ensure proper plugging of the wellbore.

Pressure Testing:

The operator will perform annual pressure monitoring on all casing annuli and reported in a sundry notice. If the test results indicated a casing failure has occurred, remedial action will be undertaken to correct the problem to the BLM's approval.

Hydrology:

The entire well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad. Topsoil shall not be used to construct the berm. No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad. The berm shall be maintained through the life of the well and after interim reclamation has been completed. Any water erosion that may occur due to the construction of the well pad during the life of the well will be quickly corrected and proper measures will be taken to prevent future erosion.

Tank battery locations will be lined and bermed. A 20 mil permanent liner will be installed with a 4 oz. felt backing to prevent tears or punctures. Tank battery berms must be large enough to contain 1 ½ times the content of the largest tank or 24 hour production, whichever is greater. Automatic shut off, check valves, or similar systems will be installed for tanks to minimize the effects of catastrophic line failures used in production or drilling.

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Following proper procedures for crossing fence lines including bracing and tying off on both sides of road passageways through fences with H-braces prior to cutting the fence, would mitigate the impacts to fence. The operator would notify the New Mexico State Land Office private surface landowners, and grazing allotment holders prior to crossing any fences.

Any damage to fences, cattle guards, windmills, and pipelines or structures that provide water to livestock during construction, throughout the life of the project, and caused by its operation, must be immediately corrected by the Applicant. The Applicant must notify the New Mexico State Land Office, grazing allottee or the private surface landowner and the BLM-CFO (575-234-5972) if any damage occurs to windmills, tanks, pipelines or structures that provide water to livestock.

VI. CONSTRUCTION

A. NOTIFICATION

The BLM shall administer compliance and monitor construction of the access road and well pad. Notify the Carlsbad Field Office at (575) 234-5909 at least 3 working days prior to commencing construction of the access road and/or well pad.

When construction operations are being conducted on this well, the operator shall have the approved APD and Conditions of Approval (COA) on the well site and they shall be made available upon request by the Authorized Officer.

B. TOPSOIL

The operator shall strip the top portion of the soil (root zone) from the entire well pad area and stockpile the topsoil along the edge of the well pad as depicted in the APD. The root zone is typically six (6) inches in depth. All the stockpiled topsoil will be redistributed over the interim reclamation areas. Topsoil shall not be used for berming the pad or facilities. For final reclamation, the topsoil shall be spread over the entire pad area for seeding preparation.

Other subsoil (below six inches) stockpiles must be completely segregated from the topsoil stockpile. Large rocks or subsoil clods (not evident in the surrounding terrain) must be buried within the approved area for interim and final reclamation.

C. CLOSED LOOP SYSTEM

Tanks are required for drilling operations: No Pits.

The operator shall properly dispose of drilling contents at an authorized disposal site.

D. FEDERAL MINERAL MATERIALS PIT

Payment shall be made to the BLM prior to removal of any federal mineral materials. Call the Carlsbad Field Office at (575) 234-5972.

E. WELL PAD SURFACING

Surfacing of the well pad is not required.

If the operator elects to surface the well pad, the surfacing material may be required to be removed at the time of reclamation. The well pad shall be constructed in a manner which creates the smallest possible surface disturbance, consistent with safety and operational needs.

F. EXCLOSURE FENCING (CELLARS & PITS)

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Exclosure Fencing

The operator will install and maintain exclosure fencing for all open well cellars to prevent access to public, livestock, and large forms of wildlife before and after drilling operations until the pit is free of fluids and the operator initiates backfilling. (For examples of exclosure fencing design, refer to BLM's Oil and Gas Gold Book, Exclosure Fence Illustrations, Figure 1, Page 18.)

G. ON LEASE ACCESS ROADS

Road Width

The access road shall have a driving surface that creates the smallest possible surface disturbance and does not exceed fourteen (14) feet in width. The maximum width of surface disturbance, when constructing the access road, shall not exceed twenty-five (25) feet.

Surfacing

Surfacing material is not required on the new access road driving surface. If the operator elects to surface the new access road or pad, the surfacing material may be required to be removed at the time of reclamation.

Where possible, no improvements should be made on the unsurfaced access road other than to remove vegetation as necessary, road irregularities, safety issues, or to fill low areas that may sustain standing water.

The Authorized Officer reserves the right to require surfacing of any portion of the access road at any time deemed necessary. Surfacing may be required in the event the road deteriorates, erodes, road traffic increases, or it is determined to be beneficial for future field development. The surfacing depth and type of material will be determined at the time of notification.

Crowning

Crowning shall be done on the access road driving surface. The road crown shall have a grade of approximately 2% (i.e., a 1" crown on a 14' wide road). The road shall conform to Figure 1; cross section and plans for typical road construction.

Ditching

Ditching shall be required on both sides of the road.

Turnouts

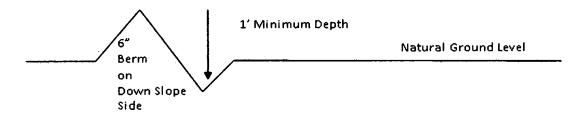
Vehicle turnouts shall be constructed on the road. Turnouts shall be intervisible with interval spacing distance less than 1000 feet. Turnouts shall conform to Figure 1; cross section and plans for typical road construction.

Drainage

Drainage control systems shall be constructed on the entire length of road (e.g. ditches, sidehill outsloping and insloping, lead-off ditches, culvert installation, and low water crossings).

A typical lead-off ditch has a minimum depth of 1 foot below and a berm of 6 inches above natural ground level. The berm shall be on the down-slope side of the lead-off ditch.

Cross Section of a Typical Lead-off Ditch



All lead-off ditches shall be graded to drain water with a 1 percent minimum to 3 percent maximum ditch slope. The spacing interval are variable for lead-off ditches and shall be determined according to the formula for spacing intervals of lead-off ditches, but may be amended depending upon existing soil types and centerline road slope (in %);

Formula for Spacing Interval of Lead-off Ditches

Example - On a 4% road slope that is 400 feet long, the water flow shall drain water into a lead-off ditch. Spacing interval shall be determined by the following formula:

400 foot road with 4% road slope:
$$\frac{400'}{4\%}$$
 + 100' = 200' lead-off ditch interval

Cattle guards

An appropriately sized cattle guard sufficient to carry out the project shall be installed and maintained at fence/road crossings. Any existing cattle guards on the access road route shall be repaired or replaced if they are damaged or have deteriorated beyond practical use. The operator shall be responsible for the condition of the existing cattle guards that are in place and are utilized during lease operations.

Fence Requirement

Where entry is granted across a fence line, the fence shall be braced and tied off on both sides of the passageway prior to cutting. The operator shall notify the private surface landowner or the grazing allotment holder prior to crossing any fences.

Public Access

Public access on this road shall not be restricted by the operator without specific written approval granted by the Authorized Officer.

Construction Steps

- 1. Salvage topsoil
- 3. Redistribute topsoil
- 2. Construct road 4. Revegetate slopes

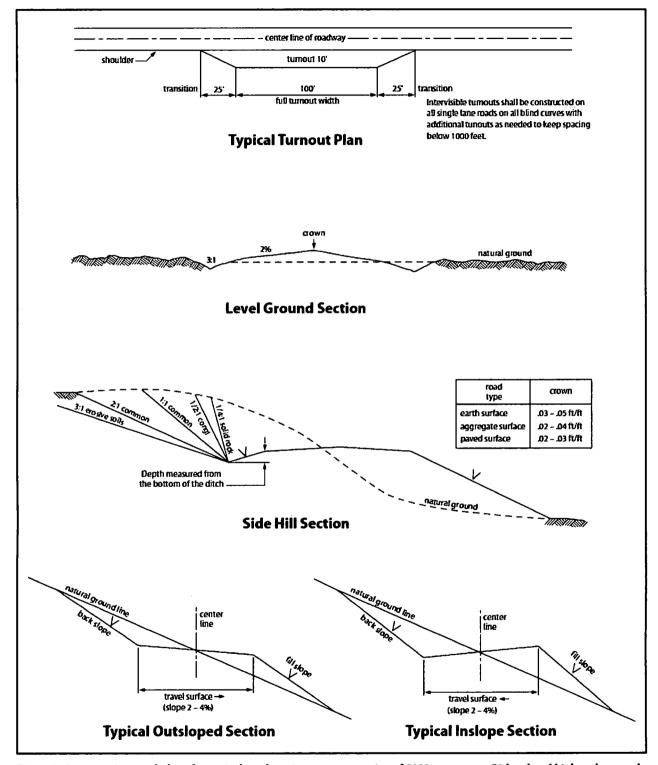


Figure 1. Cross-sections and plans for typical road sections representative of BLM resource or FS local and higher-class roads.

VII. PRODUCTION (POST DRILLING)

A. WELL STRUCTURES & FACILITIES

Placement of Production Facilities

Production facilities should be placed on the well pad to allow for maximum interim recontouring and revegetation of the well location.

Exclosure Netting (Open-top Tanks)

Immediately following active drilling or completion operations, the operator will take actions necessary to prevent wildlife and livestock access, including avian wildlife, to all open-topped tanks that contain or have the potential to contain salinity sufficient to cause harm to wildlife or livestock, hydrocarbons, or Resource Conservation and Recovery Act of 1976-exempt hazardous substances. At a minimum, the operator will net, screen, or cover open-topped tanks to exclude wildlife and livestock and prevent mortality. If the operator uses netting, the operator will cover and secure the open portion of the tank to prevent wildlife entry. The operator will net, screen, or cover the tanks until the operator removes the tanks from the location or the tanks no longer contain substances that could be harmful to wildlife or livestock. Use a maximum netting mesh size of 1 ½ inches. The netting must not be in contact with fluids and must not have holes or gaps.

Chemical and Fuel Secondary Containment and Exclosure Screening

The operator will prevent all hazardous, poisonous, flammable, and toxic substances from coming into contact with soil and water. At a minimum, the operator will install and maintain an impervious secondary containment system for any tank or barrel containing hazardous, poisonous, flammable, or toxic substances sufficient to contain the contents of the tank or barrel and any drips, leaks, and anticipated precipitation. The operator will dispose of fluids within the containment system that do not meet applicable state or U. S. Environmental Protection Agency livestock water standards in accordance with state law; the operator must not drain the fluids to the soil or ground. The operator will design, construct, and maintain all secondary containment systems to prevent wildlife and livestock exposure to harmful substances. At a minimum, the operator will install effective wildlife and livestock exclosure systems such as fencing, netting, expanded metal mesh, lids, and grate covers. Use a maximum netting mesh size of 1½ inches.

Open-Vent Exhaust Stack Exclosures

The operator will construct, modify, equip, and maintain all open-vent exhaust stacks on production equipment to prevent birds and bats from entering, and to discourage perching, roosting, and nesting. (Recommended exclosure structures on open-vent exhaust stacks are in the shape of a cone.) Production equipment includes, but may not be limited to, tanks, heater-treaters, separators, dehydrators, flare stacks, in-line units, and compressor mufflers.

Containment Structures

Proposed production facilities such as storage tanks and other vessels will have a secondary containment structure that is constructed to hold the capacity of 1.5 times the largest tank, plus freeboard to account for precipitation, unless more stringent protective requirements are deemed necessary.

Painting Requirement

All above-ground structures including meter housing that are not subject to safety requirements shall be painted a flat non-reflective paint color, **Shale Green** from the BLM Standard Environmental Color Chart (CC-001: June 2008).

B. PIPELINES

BURIED PIPELINE STIPULATIONS

A copy of the application (Grant, APD, or Sundry Notice) and attachments, including conditions of approval, survey plat and/or map, will be on location during construction. BLM personnel may request to you a copy of your permit during construction to ensure compliance with all stipulations.

Holder agrees to comply with the following stipulations to the satisfaction of the Authorized Officer:

- 1. The Holder shall indemnify the United States against any liability for damage to life or property arising from the occupancy or use of public lands under this grant.
- 2. The Holder shall comply with all applicable Federal laws and regulations existing or hereafter enacted or promulgated. In any event, the holder shall comply with the Toxic Substances Control Act of 1976 as amended, 15 USC 2601 et seq. (1982) with regards to any toxic substances that are used, generated by or stored on the right-of-way or on facilities authorized under this right-of-way grant. (See 40 CFR Part 702-799 and especially, provisions on polychlorinated biphenyls, 40 CFR 761.1-761.193.) Additionally, any release of toxic substances (leaks, spills, etc.) in excess of the reportable quantity established by 40 CFR Part 117 shall be reported as required by the Comprehensive Environmental Response, Compensation, and Liability Act, section 102b. A copy of any report required or requested by any Federal agency or State government as a result of a reportable release or spill of any toxic substances shall be furnished to the authorized officer concurrent with the filing of the reports to the involved Federal agency or State government.
- 3. The holder agrees to indemnify the United States against any liability arising from the release of any hazardous substance or hazardous waste (as these terms are defined in the Comprehensive Environmental Response, Compensation and Liability Act of 1980, 42 U.S.C. 9601, et seq. or the Resource Conservation and Recovery Act, 42 U.S.C.6901, et seq.) on the Right-of-Way (unless the release or threatened release is wholly unrelated to the Right-of-Way holder's activity on the Right-of-Way), or resulting from the activity of the Right-of-Way holder on the Right-of-Way. This agreement applies without regard to whether a release is caused by the holder, its agent, or unrelated third parties.

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4. If, during any phase of the construction, operation, maintenance, or termination of the pipeline, any oil or other pollutant should be discharged from the pipeline system, impacting Federal lands, the control and total removal, disposal, and cleaning up of such oil or other pollutant, wherever found, shall be the responsibility of holder, regardless of fault. Upon failure of holder to control, dispose of, or clean up such discharge on or affecting Federal lands, or to repair all damages resulting therefrom, on the Federal lands, the Authorized Officer may take such measures as he deems necessary to control and clean up the discharge and restore the area, including where appropriate, the aquatic environment and fish and wildlife habitats, at the full expense of the holder. Such action by the Authorized Officer shall not relieve holder of any responsibility as provided herein.

5. All construction and maintenance activity will be confined to the authorized right-of-way.			
6. The pipeline will be buried with a minimum cover of 36 inches between the top of the pipe and ground level.			
7. The maximum allowable disturbance for construction in this right-of-way will be 30 feet:			
• Blading of vegetation within the right-of-way will be allowed: maximum width of blading operations will not exceed 20 feet. The trench is included in this area. (Blading is defined as the complete removal of brush and ground vegetation.)			
• Clearing of brush species within the right-of-way will be allowed: maximum width of clearing operations will not exceed 30 feet. The trench and bladed area are included in this area. (Clearing is defined as the removal of brush while leaving ground vegetation (grasses, weeds, etc.) intact. Clearing is best accomplished by holding the blade 4 to 6 inches above the ground surface.)			
• The remaining area of the right-of-way (if any) shall only be disturbed by compressing the vegetation. (Compressing can be caused by vehicle tires, placement of equipment, etc.)			
8. The holder shall stockpile an adequate amount of topsoil where blading is allowed. The topsoil to be stripped is approximately6 inches in depth. The topsoil will be segregated from other spoil piles from trench construction. The topsoil will be evenly distributed over the bladed area for the preparation of seeding.			
9. The holder shall minimize disturbance to existing fences and other improvements on public lands. The holder is required to promptly repair improvements to at least their former state. Functional use of these improvements will be maintained at all times. The holder will contact the owner of any improvements prior to disturbing them. When necessary to pass through a fence line, the fence shall be braced on both sides of the passageway prior to cutting of the fence. No permanent gates will be allowed unless approved by the Authorized Officer.			
10. Vegetation, soil, and rocks left as a result of construction or maintenance activity will be randomly scattered on this right-of-way and will not be left in rows, piles, or berms, unless otherwise approved by the Authorized Officer. The entire right-of-way shall be recontoured to match the surrounding landscape. The backfilled soil shall be compacted and a 6 inch berm will be left over the ditch line to allow for settling back to grade.			
11. In those areas where erosion control structures are required to stabilize soil conditions, the holder will install such structures as are suitable for the specific soil conditions being encountered			

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and which are in accordance with sound resource management practices.

	holder will reseed all disturbed areas requirements, using the following sec	s. Seeding will be done according to the attached ed mix.
	(X) seed mixture 1	() seed mixture 3
	() seed mixture 2	() seed mixture 4
	() seed mixture 2/LPC	() Aplomado Falcon Mixture
to blend	with the natural color of the landscap	o safety requirements shall be painted by the holder be. The paint used shall be color which simulates reen, Munsell Soil Color No. 5Y 4/2.
way and number,	at all road crossings. At a minimum and the product being transported. A	t the point of origin and completion of the right-of- , signs will state the holder's name, BLM serial All signs and information thereon will be posted in a maintained in a legible condition for the life of the
maintena before ma pipeline i	ance as determined necessary by the anintenance begins. The holder will troute is not used as a roadway. As d	e as a road for purposes other than routine Authorized Officer in consultation with the holder ake whatever steps are necessary to ensure that the etermined necessary during the life of the pipeline, construct temporary deterrence structures.
discovere immediat immediat Authorize determine holder wi	ed by the holder, or any person work tely reported to the Authorized Office te area of such discovery until written ed Officer. An evaluation of the disc e appropriate actions to prevent the lill be responsible for the cost of eval-	arces (historic or prehistoric site or object) ing on his behalf, on public or Federal land shall be er. Holder shall suspend all operations in the n authorization to proceed is issued by the covery will be made by the Authorized Officer to oss of significant cultural or scientific values. The uation and any decision as to proper mitigation ficer after consulting with the holder.
of operation of weeds	ions. Weed control shall be required cludes associated roads, pipeline condue to this action. The operator shall	noxious weeds become established within the areas on the disturbed land where noxious weeds exist, ridor and adjacent land affected by the establishment I consult with the Authorized Officer for acceptable ng EPA and BLM requirements and policies.
		uct and maintain pipeline/utility trenches that are not ent livestock, wildlife, and humans from becoming

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Approval Date: 07/16/2018

entrapped. At a minimum, the operator will construct and maintain escape ramps, ladders, or

other methods of avian and terrestrial wildlife escape in the trenches according to the following criteria:

- a. Any trench left open for eight (8) hours or less is not required to have escape ramps; however, before the trench is backfilled, the contractor/operator shall inspect the trench for wildlife, remove all trapped wildlife, and release them at least 100 yards from the trench
- b. For trenches left open for eight (8) hours or more, earthen escape ramps (built at no more than a 30 degree slope and spaced no more than 500 feet apart) shall be placed in the trench.

VIII. INTERIM RECLAMATION

During the life of the development, all disturbed areas not needed for active support of production operations should undergo interim reclamation in order to minimize the environmental impacts of development on other resources and uses.

Within six (6) months of well completion, operators should work with BLM surface management specialists (Jim Amos: 575-234-5909) to devise the best strategies to reduce the size of the location. Interim reclamation should allow for remedial well operations, as well as safe and efficient removal of oil and gas.

During reclamation, the removal of caliche is important to increasing the success of revegetating the site. Removed caliche that is free of contaminants may be used for road repairs, fire walls or for building other roads and locations. In order to operate the well or complete workover operations, it may be necessary to drive, park and operate on restored interim vegetation within the previously disturbed area. Disturbing revegetated areas for production or workover operations will be allowed. If there is significant disturbance and loss of vegetation, the area will need to be revegetated. Communicate with the appropriate BLM office for any exceptions/exemptions if needed.

All disturbed areas after they have been satisfactorily prepared need to be reseeded with the seed mixture provided below.

Upon completion of interim reclamation, the operator shall submit a Sundry Notices and Reports on Wells, Subsequent Report of Reclamation (Form 3160-5).

IX. FINAL ABANDONMENT & RECLAMATION

At final abandonment, well locations, production facilities, and access roads must undergo "final" reclamation so that the character and productivity of the land are restored.

Earthwork for final reclamation must be completed within six (6) months of well plugging. All pads, pits, facility locations and roads must be reclaimed to a satisfactory revegetated, safe, and stable condition, unless an agreement is made with the landowner or BLM to keep the road and/or pad intact.

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After all disturbed areas have been satisfactorily prepared, these areas need to be revegetated with the seed mixture provided below. Seeding should be accomplished by drilling on the contour whenever practical or by other approved methods. Seeding may need to be repeated until revegetation is successful, as determined by the BLM.

Operators shall contact a BLM surface protection specialist prior to surface abandonment operations for site specific objectives (Jim Amos: 575-234-5909).

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Seed Mixture 1 for Loamy Sites

Holder shall seed all disturbed areas with the seed mixture listed below. The seed mixture shall be planted in the amounts specified in pounds of pure live seed (PLS)* per acre. There shall be no primary or secondary noxious weeds in the seed mixture. Seed shall be tested and the viability testing of seed will be done in accordance with State law(s) and within nine (9) months prior to purchase. Commercial seed shall be either certified or registered seed. The seed container shall be tagged in accordance with State law(s) and available for inspection by the Authorized Officer.

Seed shall be planted using a drill equipped with a depth regulator to ensure proper depth regulator to ensure proper depth of planting where drilling is possible. The seed mixture shall be evenly and uniformly planted over the disturbed area (small/heavier seeds have a tendency to drop the bottom of the drill and are planted first). Holder shall take appropriate measures to ensure this does not occur. Where drilling is not possible, seed shall be broadcast and the area shall be raked or chained to cover the seed. When broadcasting the seed, the pounds per acre shall be doubled. The seeding shall be repeated until a satisfactory stand is established as determined by the Authorized Officer. Evaluation of growth may not be made before completion of at least one full growing season after seeding.

Species to be planted in pounds of pure live seed* per acre:

<u>lb/acre</u>
0.5
1.0
5.0
2.0

^{*}Pounds of pure live seed:

Pounds of seed x percent purity x percent germination = pounds pure live seed

PECOS DISTRICT SURFACE USE CONDITIONS OF APPROVAL

OPERATOR'S NAME:
LEASE NO.:
WELL NAME & NO.:
SURFACE HOLE FOOTAGE:
BOTTOM HOLE FOOTAGE
LOCATION:
COUNTY:
Matador Production Company
NMNM054289
Garrett Fed Com 226H
2372'/N & 584'/W
2323'/N & 240'/E
Section 32, T.24 S., R.29 E., NMPM
Eddy County, New Mexico

TABLE OF CONTENTS

Standard Conditions of Approval (COA) apply to this APD. If any deviations to these standards exist or special COAs are required, the section with the deviation or requirement will be checked below.

☐ General Provisions
Permit Expiration
Archaeology, Paleontology, and Historical Sites
Noxious Weeds
Special Requirements
Hydrology
Cave/Karst
Range
☐ Construction
Notification
Topsoil
Closed Loop System
Federal Mineral Material Pits
Well Pads
Roads
Road Section Diagram
Well Structures & Facilities
Pipelines
☐ Interim Reclamation
Final Ahandonment & Reclamation

I. GENERAL PROVISIONS

The approval of the Application For Permit To Drill (APD) is in compliance with all applicable laws and regulations: 43 Code of Federal Regulations 3160, the lease terms, Onshore Oil and Gas Orders, Notices To Lessees, New Mexico Oil Conservation Division (NMOCD) Rules, National Historical Preservation Act As Amended, and instructions and orders of the Authorized Officer. Any request for a variance shall be submitted to the Authorized Officer on Form 3160-5, Sundry Notices and Report on Wells.

II. PERMIT EXPIRATION

If the permit terminates prior to drilling and drilling cannot be commenced within 60 days after expiration, an operator is required to submit Form 3160-5, Sundry Notices and Reports on Wells, requesting surface reclamation requirements for any surface disturbance. However, if the operator will be able to initiate drilling within 60 days after the expiration of the permit, the operator must have set the conductor pipe in order to allow for an extension of 60 days beyond the expiration date of the APD. (Filing of a Sundry Notice is required for this 60 day extension.)

III. ARCHAEOLOGICAL, PALEONTOLOGY & HISTORICAL SITES

Any cultural and/or paleontological resource discovered by the operator or by any person working on the operator's behalf shall immediately report such findings to the Authorized Officer. The operator is fully accountable for the actions of their contractors and subcontractors. The operator shall suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Authorized Officer. An evaluation of the discovery shall be made by the Authorized Officer to determine the appropriate actions that shall be required to prevent the loss of significant cultural or scientific values of the discovery. The operator shall be held responsible for the cost of the proper mitigation measures that the Authorized Officer assesses after consultation with the operator on the evaluation and decisions of the discovery. Any unauthorized collection or disturbance of cultural or paleontological resources may result in a shutdown order by the Authorized Officer.

IV. NOXIOUS WEEDS

The operator shall be held responsible if noxious weeds become established within the areas of operations. Weed control shall be required on the disturbed land where noxious weeds exist, which includes the roads, pads, associated pipeline corridor, and adjacent land affected by the establishment of weeds due to this action. The operator shall consult with the Authorized Officer for acceptable weed control methods, which include following EPA and BLM requirements and policies.

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V. SPECIAL REQUIREMENT(S)

Cave/Karst Surface Mitigation

The following stipulations will be applied to minimize impacts during construction, drilling and production:

Construction:

In the advent that any underground voids are opened up during construction activities, construction activities will be halted and the BLM will be notified immediately.

No Blasting:

No blasting will be utilized for pad construction. The pad will be constructed and leveled by adding the necessary fill and caliche.

Pad Berming:

- The entire perimeter of the well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad.
- The compacted berm shall be constructed at a minimum of 12 inches high with impermeable mineral material (e.g., caliche).
- No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad.
- The topsoil stockpile shall be located outside the bermed well pad.
- Topsoil, either from the well pad or surrounding area, shall not be used to construct the berm.
- No storm drains, tubing or openings shall be placed in the berm.
- If fluid collects within the bermed area, the fluid must be vacuumed into a safe container and disposed of properly at a state approved facility.
- The integrity of the berm shall be maintained around the surfaced pad throughout the life of the well and around the downsized pad after interim reclamation has been completed.
- Any access road entering the well pad shall be constructed so that the integrity of the berm height surrounding the well pad is not compromised. (Any access road crossing the berm cannot be lower than the berm height.)
- Following a rain event, all fluids will vacuumed off of the pad and hauled off-site and disposed at a proper disposal facility.

Tank Battery Liners and Berms:

Tank battery locations and all facilities will be lined and bermed. A 20 mil permanent liner will be installed with a 4 oz. felt backing, or equivalent, to prevent tears or punctures. Tank battery berms must be large enough to contain 1 ½ times the content of the largest tank.

Leak Detection System:

A method of detecting leaks is required. The method could incorporate gauges to measure loss, situating values and lines so they can be visually inspected, or installing electronic sensors to alarm when a leak is present. Leak detection plan will be submitted to BLM for approval.

Automatic Shut-off Systems:

Automatic shut off, check values, or similar systems will be installed for pipelines and tanks to minimize the effects of catastrophic line failures used in production or drilling.

Cave/Karst Subsurface Mitigation

The following stipulations will be applied to protect cave/karst and ground water concerns:

Rotary Drilling with Fresh Water:

Fresh water will be used as a circulating medium in zones where caves or karst features are expected. SEE ALSO: Drilling COAs for this well.

Directional Drilling:

Kick off for directional drilling will occur at least 100 feet below the bottom of the cave occurrence zone. SEE ALSO: Drilling COAs for this well.

Lost Circulation:

ALL lost circulation zones from the surface to the base of the cave occurrence zone will be logged and reported in the drilling report.

Regardless of the type of drilling machinery used, if a void of four feet or more and circulation losses greater than 70 percent occur simultaneously while drilling in any cavebearing zone, the BLM will be notified immediately by the operator. The BLM will assess the situation and work with the operator on corrective actions to resolve the problem.

Abandonment Cementing:

Upon well abandonment in cave karst areas additional plugging conditions of approval may be required. The BLM will assess the situation and work with the operator to ensure proper plugging of the wellbore.

Pressure Testing:

The operator will perform annual pressure monitoring on all casing annuli and reported in a sundry notice. If the test results indicated a casing failure has occurred, remedial action will be undertaken to correct the problem to the BLM's approval.

Hydrology:

The entire well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad. Topsoil shall not be used to construct the berm. No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad. The berm shall be maintained through the life of the well and after interim reclamation has been completed. Any water erosion that may occur due to the construction of the well pad during the life of the well will be quickly corrected and proper measures will be taken to prevent future erosion.

Tank battery locations will be lined and bermed. A 20 mil permanent liner will be installed with a 4 oz. felt backing to prevent tears or punctures. Tank battery berms must be large enough to contain 1 ½ times the content of the largest tank or 24 hour production, whichever is greater. Automatic shut off, check valves, or similar systems will be installed for tanks to minimize the effects of catastrophic line failures used in production or drilling.

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Following proper procedures for crossing fence lines including bracing and tying off on both sides of road passageways through fences with H-braces prior to cutting the fence, would mitigate the impacts to fence. The operator would notify the New Mexico State Land Office private surface landowners, and grazing allotment holders prior to crossing any fences.

Any damage to fences, cattle guards, windmills, and pipelines or structures that provide water to livestock during construction, throughout the life of the project, and caused by its operation, must be immediately corrected by the Applicant. The Applicant must notify the New Mexico State Land Office, grazing allottee or the private surface landowner and the BLM-CFO (575-234-5972) if any damage occurs to windmills, tanks, pipelines or structures that provide water to livestock.

VI. CONSTRUCTION

A. NOTIFICATION

The BLM shall administer compliance and monitor construction of the access road and well pad. Notify the Carlsbad Field Office at (575) 234-5909 at least 3 working days prior to commencing construction of the access road and/or well pad.

When construction operations are being conducted on this well, the operator shall have the approved APD and Conditions of Approval (COA) on the well site and they shall be made available upon request by the Authorized Officer.

B. TOPSOIL

The operator shall strip the top portion of the soil (root zone) from the entire well pad area and stockpile the topsoil along the edge of the well pad as depicted in the APD. The root zone is typically six (6) inches in depth. All the stockpiled topsoil will be redistributed over the interim reclamation areas. Topsoil shall not be used for berming the pad or facilities. For final reclamation, the topsoil shall be spread over the entire pad area for seeding preparation.

Other subsoil (below six inches) stockpiles must be completely segregated from the topsoil stockpile. Large rocks or subsoil clods (not evident in the surrounding terrain) must be buried within the approved area for interim and final reclamation.

C. CLOSED LOOP SYSTEM

Tanks are required for drilling operations: No Pits.

The operator shall properly dispose of drilling contents at an authorized disposal site.

D. FEDERAL MINERAL MATERIALS PIT

Payment shall be made to the BLM prior to removal of any federal mineral materials. Call the Carlsbad Field Office at (575) 234-5972.

E. WELL PAD SURFACING

Surfacing of the well pad is not required.

If the operator elects to surface the well pad, the surfacing material may be required to be removed at the time of reclamation. The well pad shall be constructed in a manner which creates the smallest possible surface disturbance, consistent with safety and operational needs.

F. EXCLOSURE FENCING (CELLARS & PITS)

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Exclosure Fencing

The operator will install and maintain exclosure fencing for all open well cellars to prevent access to public, livestock, and large forms of wildlife before and after drilling operations until the pit is free of fluids and the operator initiates backfilling. (For examples of exclosure fencing design, refer to BLM's Oil and Gas Gold Book, Exclosure Fence Illustrations, Figure 1, Page 18.)

G. ON LEASE ACCESS ROADS

Road Width

The access road shall have a driving surface that creates the smallest possible surface disturbance and does not exceed fourteen (14) feet in width. The maximum width of surface disturbance, when constructing the access road, shall not exceed twenty-five (25) feet.

Surfacing

Surfacing material is not required on the new access road driving surface. If the operator elects to surface the new access road or pad, the surfacing material may be required to be removed at the time of reclamation.

Where possible, no improvements should be made on the unsurfaced access road other than to remove vegetation as necessary, road irregularities, safety issues, or to fill low areas that may sustain standing water.

The Authorized Officer reserves the right to require surfacing of any portion of the access road at any time deemed necessary. Surfacing may be required in the event the road deteriorates, erodes, road traffic increases, or it is determined to be beneficial for future field development. The surfacing depth and type of material will be determined at the time of notification.

Crowning

Crowning shall be done on the access road driving surface. The road crown shall have a grade of approximately 2% (i.e., a 1" crown on a 14' wide road). The road shall conform to Figure 1; cross section and plans for typical road construction.

Ditching

Ditching shall be required on both sides of the road.

Turnouts

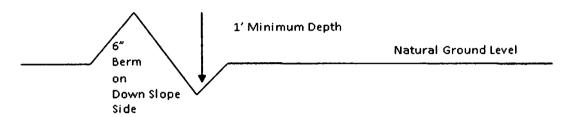
Vehicle turnouts shall be constructed on the road. Turnouts shall be intervisible with interval spacing distance less than 1000 feet. Turnouts shall conform to Figure 1; cross section and plans for typical road construction.

Drainage

Drainage control systems shall be constructed on the entire length of road (e.g. ditches, sidehill outsloping and insloping, lead-off ditches, culvert installation, and low water crossings).

A typical lead-off ditch has a minimum depth of 1 foot below and a berm of 6 inches above natural ground level. The berm shall be on the down-slope side of the lead-off ditch.

Cross Section of a Typical Lead-off Ditch



All lead-off ditches shall be graded to drain water with a 1 percent minimum to 3 percent maximum ditch slope. The spacing interval are variable for lead-off ditches and shall be determined according to the formula for spacing intervals of lead-off ditches, but may be amended depending upon existing soil types and centerline road slope (in %);

Formula for Spacing Interval of Lead-off Ditches

Example - On a 4% road slope that is 400 feet long, the water flow shall drain water into a lead-off ditch. Spacing interval shall be determined by the following formula:

400 foot road with 4% road slope:
$$\frac{400'}{4\%}$$
 + 100' = 200' lead-off ditch interval

Cattle guards

An appropriately sized cattle guard sufficient to carry out the project shall be installed and maintained at fence/road crossings. Any existing cattle guards on the access road route shall be repaired or replaced if they are damaged or have deteriorated beyond practical use. The operator shall be responsible for the condition of the existing cattle guards that are in place and are utilized during lease operations.

Fence Requirement

Where entry is granted across a fence line, the fence shall be braced and tied off on both sides of the passageway prior to cutting. The operator shall notify the private surface landowner or the grazing allotment holder prior to crossing any fences.

Public Access

Public access on this road shall not be restricted by the operator without specific written approval granted by the Authorized Officer.

Construction Steps

- 1. Salvage topsoil
- 3. Redistribute topsoil
- 2. Construct road
- 4. Revegetate slopes

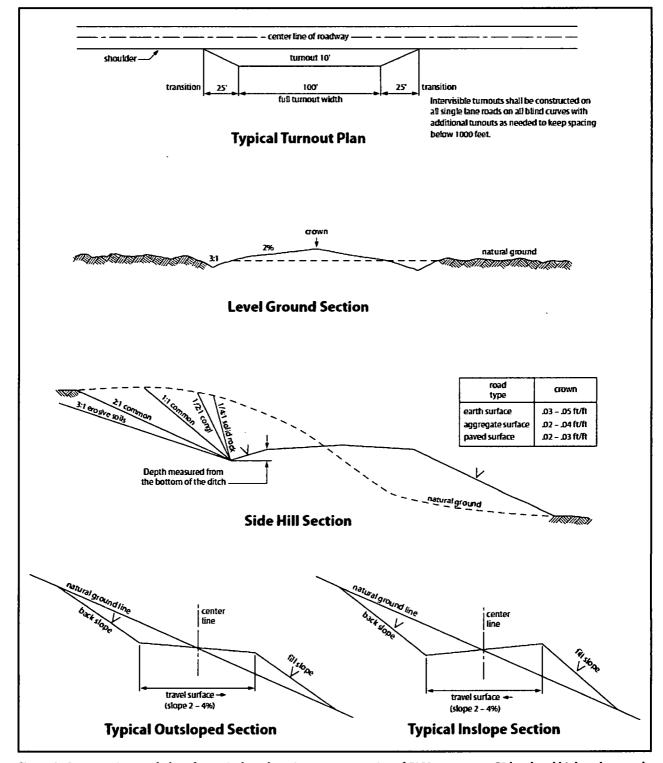


Figure 1. Cross-sections and plans for typical road sections representative of BLM resource or FS local and higher-class roads.

VII. PRODUCTION (POST DRILLING)

A. WELL STRUCTURES & FACILITIES

Placement of Production Facilities

Production facilities should be placed on the well pad to allow for maximum interim recontouring and revegetation of the well location.

Exclosure Netting (Open-top Tanks)

Immediately following active drilling or completion operations, the operator will take actions necessary to prevent wildlife and livestock access, including avian wildlife, to all open-topped tanks that contain or have the potential to contain salinity sufficient to cause harm to wildlife or livestock, hydrocarbons, or Resource Conservation and Recovery Act of 1976-exempt hazardous substances. At a minimum, the operator will net, screen, or cover open-topped tanks to exclude wildlife and livestock and prevent mortality. If the operator uses netting, the operator will cover and secure the open portion of the tank to prevent wildlife entry. The operator will net, screen, or cover the tanks until the operator removes the tanks from the location or the tanks no longer contain substances that could be harmful to wildlife or livestock. Use a maximum netting mesh size of 1 ½ inches. The netting must not be in contact with fluids and must not have holes or gaps.

Chemical and Fuel Secondary Containment and Exclosure Screening

The operator will prevent all hazardous, poisonous, flammable, and toxic substances from coming into contact with soil and water. At a minimum, the operator will install and maintain an impervious secondary containment system for any tank or barrel containing hazardous, poisonous, flammable, or toxic substances sufficient to contain the contents of the tank or barrel and any drips, leaks, and anticipated precipitation. The operator will dispose of fluids within the containment system that do not meet applicable state or U. S. Environmental Protection Agency livestock water standards in accordance with state law; the operator must not drain the fluids to the soil or ground. The operator will design, construct, and maintain all secondary containment systems to prevent wildlife and livestock exposure to harmful substances. At a minimum, the operator will install effective wildlife and livestock exclosure systems such as fencing, netting, expanded metal mesh, lids, and grate covers. Use a maximum netting mesh size of 1 ½ inches.

Open-Vent Exhaust Stack Exclosures

The operator will construct, modify, equip, and maintain all open-vent exhaust stacks on production equipment to prevent birds and bats from entering, and to discourage perching, roosting, and nesting. (Recommended exclosure structures on open-vent exhaust stacks are in the shape of a cone.) Production equipment includes, but may not be limited to, tanks, heater-treaters, separators, dehydrators, flare stacks, in-line units, and compressor mufflers.

Containment Structures

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Proposed production facilities such as storage tanks and other vessels will have a secondary containment structure that is constructed to hold the capacity of 1.5 times the largest tank, plus freeboard to account for precipitation, unless more stringent protective requirements are deemed necessary.

Painting Requirement

All above-ground structures including meter housing that are not subject to safety requirements shall be painted a flat non-reflective paint color, **Shale Green** from the BLM Standard Environmental Color Chart (CC-001: June 2008).

B. PIPELINES

BURIED PIPELINE STIPULATIONS

A copy of the application (Grant, APD, or Sundry Notice) and attachments, including conditions of approval, survey plat and/or map, will be on location during construction. BLM personnel may request to you a copy of your permit during construction to ensure compliance with all stipulations.

Holder agrees to comply with the following stipulations to the satisfaction of the Authorized Officer:

- 1. The Holder shall indemnify the United States against any liability for damage to life or property arising from the occupancy or use of public lands under this grant.
- 2. The Holder shall comply with all applicable Federal laws and regulations existing or hereafter enacted or promulgated. In any event, the holder shall comply with the Toxic Substances Control Act of 1976 as amended, 15 USC 2601 et seq. (1982) with regards to any toxic substances that are used, generated by or stored on the right-of-way or on facilities authorized under this right-of-way grant. (See 40 CFR Part 702-799 and especially, provisions on polychlorinated biphenyls, 40 CFR 761.1-761.193.) Additionally, any release of toxic substances (leaks, spills, etc.) in excess of the reportable quantity established by 40 CFR Part 117 shall be reported as required by the Comprehensive Environmental Response, Compensation, and Liability Act, section 102b. A copy of any report required or requested by any Federal agency or State government as a result of a reportable release or spill of any toxic substances shall be furnished to the authorized officer concurrent with the filing of the reports to the involved Federal agency or State government.
- 3. The holder agrees to indemnify the United States against any liability arising from the release of any hazardous substance or hazardous waste (as these terms are defined in the Comprehensive Environmental Response, Compensation and Liability Act of 1980, 42 U.S.C. 9601, et seq. or the Resource Conservation and Recovery Act, 42 U.S.C.6901, et seq.) on the Right-of-Way (unless the release or threatened release is wholly unrelated to the Right-of-Way holder's activity on the Right-of-Way), or resulting from the activity of the Right-of-Way holder on the Right-of-Way. This agreement applies without regard to whether a release is caused by the holder, its agent, or unrelated third parties.

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4. If, during any phase of the construction, operation, maintenance, or termination of the pipeline, any oil or other pollutant should be discharged from the pipeline system, impacting Federal lands, the control and total removal, disposal, and cleaning up of such oil or other pollutant, wherever found, shall be the responsibility of holder, regardless of fault. Upon failure of holder to control, dispose of, or clean up such discharge on or affecting Federal lands, or to repair all damages resulting therefrom, on the Federal lands, the Authorized Officer may take such measures as he deems necessary to control and clean up the discharge and restore the area, including where appropriate, the aquatic environment and fish and wildlife habitats, at the full expense of the holder. Such action by the Authorized Officer shall not relieve holder of any responsibility as provided herein.

5. All construction and maintenance activity will be confined to the authorized right-of-way.
6. The pipeline will be buried with a minimum cover of <u>36</u> inches between the top of the pipe and ground level.
7. The maximum allowable disturbance for construction in this right-of-way will be <u>30</u> feet:
• Blading of vegetation within the right-of-way will be allowed: maximum width of blading operations will not exceed 20 feet. The trench is included in this area. (Blading is defined as the complete removal of brush and ground vegetation.)
• Clearing of brush species within the right-of-way will be allowed: maximum width of clearing operations will not exceed 30 feet. The trench and bladed area are included in this area. (Clearing is defined as the removal of brush while leaving ground vegetation (grasses, weeds, etc.) intact. Clearing is best accomplished by holding the blade 4 to 6 inches above the ground surface.)
• The remaining area of the right-of-way (if any) shall only be disturbed by compressing the vegetation. (Compressing can be caused by vehicle tires, placement of equipment, etc.)
8. The holder shall stockpile an adequate amount of topsoil where blading is allowed. The topsoil to be stripped is approximately6 inches in depth. The topsoil will be segregated from other spoil piles from trench construction. The topsoil will be evenly distributed over the bladed area for the preparation of seeding.
9. The holder shall minimize disturbance to existing fences and other improvements on public lands. The holder is required to promptly repair improvements to at least their former state. Functional use of these improvements will be maintained at all times. The holder will contact the owner of any improvements prior to disturbing them. When necessary to pass through a fence line, the fence shall be braced on both sides of the passageway prior to cutting of the fence. No permanent gates will be allowed unless approved by the Authorized Officer.
10. Vegetation, soil, and rocks left as a result of construction or maintenance activity will be randomly scattered on this right-of-way and will not be left in rows, piles, or berms, unless otherwise approved by the Authorized Officer. The entire right-of-way shall be recontoured to match the surrounding landscape. The backfilled soil shall be compacted and a 6 inch berm will be left over the ditch line to allow for settling back to grade.
11. In those areas where erosion control structures are required to stabilize soil conditions, the holder will install such structures as are suitable for the specific soil conditions being encountered and which are in accordance with sound resource management practices.

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	nents, using the following seed	mix.	
((X) seed mixture 1	() seed mixture 3	
(() seed mixture 2	() seed mixture 4	
(() seed mixture 2/LPC	() Aplomado Falcon Mixture	
to blend with the	natural color of the landscape.	safety requirements shall be painted by the holder. The paint used shall be color which simulates en, Munsell Soil Color No. 5Y 4/2.	er
way and at all ro number, and the	ad crossings. At a minimum, s product being transported. All	he point of origin and completion of the right-of igns will state the holder's name, BLM serial signs and information thereon will be posted in a legible condition for the life of the	a
maintenance as of before maintenant pipeline route is	determined necessary by the Aunce begins. The holder will tak not used as a roadway. As determined the control of the control	as a road for purposes other than routine athorized Officer in consultation with the holder the whatever steps are necessary to ensure that the termined necessary during the life of the pipeline construct temporary deterrence structures.	e
discovered by the immediately repointmediate area of Authorized Office determine appropholder will be real.	e holder, or any person working orted to the Authorized Officer of such discovery until written a cer. An evaluation of the disco- priate actions to prevent the los sponsible for the cost of evalua	ces (historic or prehistoric site or object) g on his behalf, on public or Federal land shall be. Holder shall suspend all operations in the authorization to proceed is issued by the very will be made by the Authorized Officer to as of significant cultural or scientific values. The stion and any decision as to proper mitigation er after consulting with the holder.	
of operations. W which includes a of weeds due to	eed control shall be required or issociated roads, pipeline corridates this action. The operator shall controls the controls of the control of the cont	exious weeds become established within the area in the disturbed land where noxious weeds exist, dor and adjacent land affected by the establishm consult with the Authorized Officer for acceptable EPA and BLM requirements and policies.	ent

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18. <u>Escape Ramps</u> - The operator will construct and maintain pipeline/utility trenches that are not otherwise fenced, screened, or netted to prevent livestock, wildlife, and humans from becoming entrapped. At a minimum, the operator will construct and maintain escape ramps, ladders, or

other methods of avian and terrestrial wildlife escape in the trenches according to the following criteria:

- a. Any trench left open for eight (8) hours or less is not required to have escape ramps; however, before the trench is backfilled, the contractor/operator shall inspect the trench for wildlife, remove all trapped wildlife, and release them at least 100 yards from the trench
- b. For trenches left open for eight (8) hours or more, earthen escape ramps (built at no more than a 30 degree slope and spaced no more than 500 feet apart) shall be placed in the trench.

VIII. INTERIM RECLAMATION

During the life of the development, all disturbed areas not needed for active support of production operations should undergo interim reclamation in order to minimize the environmental impacts of development on other resources and uses.

Within six (6) months of well completion, operators should work with BLM surface management specialists (Jim Amos: 575-234-5909) to devise the best strategies to reduce the size of the location. Interim reclamation should allow for remedial well operations, as well as safe and efficient removal of oil and gas.

During reclamation, the removal of caliche is important to increasing the success of revegetating the site. Removed caliche that is free of contaminants may be used for road repairs, fire walls or for building other roads and locations. In order to operate the well or complete workover operations, it may be necessary to drive, park and operate on restored interim vegetation within the previously disturbed area. Disturbing revegetated areas for production or workover operations will be allowed. If there is significant disturbance and loss of vegetation, the area will need to be revegetated. Communicate with the appropriate BLM office for any exceptions/exemptions if needed.

All disturbed areas after they have been satisfactorily prepared need to be reseeded with the seed mixture provided below.

Upon completion of interim reclamation, the operator shall submit a Sundry Notices and Reports on Wells, Subsequent Report of Reclamation (Form 3160-5).

IX. FINAL ABANDONMENT & RECLAMATION

At final abandonment, well locations, production facilities, and access roads must undergo "final" reclamation so that the character and productivity of the land are restored.

Earthwork for final reclamation must be completed within six (6) months of well plugging. All pads, pits, facility locations and roads must be reclaimed to a satisfactory revegetated, safe, and stable condition, unless an agreement is made with the landowner or BLM to keep the road and/or pad intact.

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After all disturbed areas have been satisfactorily prepared, these areas need to be revegetated with the seed mixture provided below. Seeding should be accomplished by drilling on the contour whenever practical or by other approved methods. Seeding may need to be repeated until revegetation is successful, as determined by the BLM.

Operators shall contact a BLM surface protection specialist prior to surface abandonment operations for site specific objectives (Jim Amos: 575-234-5909).

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Seed Mixture 1 for Loamy Sites

Holder shall seed all disturbed areas with the seed mixture listed below. The seed mixture shall be planted in the amounts specified in pounds of pure live seed (PLS)* per acre. There shall be no primary or secondary noxious weeds in the seed mixture. Seed shall be tested and the viability testing of seed will be done in accordance with State law(s) and within nine (9) months prior to purchase. Commercial seed shall be either certified or registered seed. The seed container shall be tagged in accordance with State law(s) and available for inspection by the Authorized Officer.

Seed shall be planted using a drill equipped with a depth regulator to ensure proper depth regulator to ensure proper depth of planting where drilling is possible. The seed mixture shall be evenly and uniformly planted over the disturbed area (small/heavier seeds have a tendency to drop the bottom of the drill and are planted first). Holder shall take appropriate measures to ensure this does not occur. Where drilling is not possible, seed shall be broadcast and the area shall be raked or chained to cover the seed. When broadcasting the seed, the pounds per acre shall be doubled. The seeding shall be repeated until a satisfactory stand is established as determined by the Authorized Officer. Evaluation of growth may not be made before completion of at least one full growing season after seeding.

Species to be planted in pounds of pure live seed* per acre:

Species	
	<u>lb/acre</u>
Plains lovegrass (Eragrostis intermedia)	0.5
Sand dropseed (Sporobolus cryptandrus)	1.0
Sideoats grama (Bouteloua curtipendula)	5.0
Plains bristlegrass (Setaria macrostachya)	2.0

^{*}Pounds of pure live seed:

Pounds of seed x percent purity x percent germination = pounds pure live seed



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT



Operator Certification

I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

NAME: Brian Wood Signed on: 01/31/2018

Title: President

Street Address: 37 Verano Loop

City: Santa Fe State: NM Zip: 87508

Phone: (505)466-8120

Email address: afmss@permitswest.com

Field Representative

Representative Name: Sam Pryor

Street Address: 5400 LBJ Freeway, Suite 1500

City: Dallas State: TX Zip: 75240

Phone: (972)371-5241

Email address:



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT



APD ID: 10400026769 Submission Date: 01/31/2018

Operator Name: MATADOR PRODUCTION COMPANY

Well Name: GARRETT FED COM Well Number: 226H

Well Type: CONVENTIONAL GAS WELL Well Work Type: Drill

lighlighted data eflects the most recent changes

Show Final Text

Section 1 - General

APD ID: 10400026769 Tie to previous NOS?

Submission Date: 01/31/2018

BLM Office: CARLSBAD

User: Brian Wood

Title: President

Federal/Indian APD: FED

Is the first lease penetrated for production Federal or Indian? FED

Lease number: NMNM054289

Lease Acres: 80

Surface access agreement in place?

Allotted?

Reservation:

Agreement in place? NO

Federal or Indian agreement:

Agreement number:

Agreement name:

Keep application confidential? NO

Permitting Agent? YES

APD Operator: MATADOR PRODUCTION COMPANY

Operator letter of designation:

Operator Info

Operator Organization Name: MATADOR PRODUCTION COMPANY

Operator Address: 5400 LBJ Freeway, Suite 1500

Zip: 75240

Operator PO Box:

Operator City: Dallas

State: TX

Operator Phone: (972)371-5200

Operator Internet Address: amonroe@matadorresources.com

Section 2 - Well Information

Well in Master Development Plan? NO

Mater Development Plan name:

Well in Master SUPO? NO

Master SUPO name:

Well in Master Drilling Plan? NO

Master Drilling Plan name:

Well Name: GARRETT FED COM

Well Number: 226H

Well API Number:

Field/Pool or Exploratory? Field and Pool

Field Name: PURPLE-SAGE

Pool Name:

WOLFCAMP GAS

Is the proposed well in an area containing other mineral resources? USEABLE WATER, NATURAL GAS, OIL

Well Name: GARRETT FED COM Well Number: 226H

Describe other minerals:

Is the proposed well in a Helium production area? N Use Existing Well Pad? NO New surface disturbance?

Type of Well Pad: MULTIPLE WELL

Multiple Well Pad Name: Number: 122H

GARRETT FED COM Well Class: HORIZONTAL

Number of Legs: 1

Well Work Type: Drill

Well Type: CONVENTIONAL GAS WELL

Describe Well Type: Well sub-Type: INFILL

Describe sub-type:

Distance to lease line: 584 FT Distance to town: 5 Miles Distance to nearest well: 30 FT

Reservoir well spacing assigned acres Measurement: 320 Acres

Garrett_226H_Plat_20180131083959.pdf Well plat:

Well work start Date: 03/01/2018 **Duration: 90 DAYS**

Section 3 - Well Location Table

Survey Type: RECTANGULAR

Describe Survey Type:

Vertical Datum: NAVD88 Datum: NAD83

Survey number: 18329

	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	αντ
SHL Leg #1	237 2	FNL	584	FWL	248	29E	32	Aliquot SWN W	32.17461 47	- 104.0132 281	EDD Y		NEW MEXI CO	S	STATE	292 0	0	0
KOP Leg #1	237 2	FNL	584	FWL	248	29E	32	Aliquot SWN W	32.17461 47	- 104.0132 281	EDD Y		NEW MEXI CO	s	STATE	- 745 6	104 12	103 76
PPP Leg #1	237 2	FNL	584	FWL	24S	29E	32	Aliquot SWN W	32.17461 47	- 104.0132 281	EDD Y		NEW MEXI CO	s	STATE	292 0	0	0

Well Name: GARRETT FED COM Well Number: 226H

	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	ΔΛΤ
PPP Leg #1	232 8	FNL	132 0	FWL	248	29E	32	Aliquot SENW	32.17473	- 104.0108 22	EDD Y	l .	NEW MEXI CO	F	NMNM 054289	- 803 5	120 22	109 55
PPP Leg #1	232 8	FNL	246 0	FEL	24S	29E	32	Aliquot SWNE	32.17471	- 104.0065 6	EDD Y		NEW MEXI CO	F	FEE	- 803 5	133 36	109 55
EXIT Leg #1	232 3	FNL	240	FEL	248	29E	32	Aliquot SENE	32.17468 8	- 103.9988 56	EDD Y		NEW MEXI CO	F	FEE	- 803 5	157 20	109 55
BHL Leg #1	232 3	FNL	240	FEL	248	29E	32	Aliquot SENE	32.17468 8	- 103.9988 56	EDD Y	1	NEW MEXI CO	F	FEE	- 803 5	157 20	109 55

Alternatives to Reduce Flaring

Below are alternatives considered from a conceptual standpoint, but determined to be impractical, to reduce the amount of gas flared.

- Power Generation On lease
 - o Operating a generator will only utilize a portion of the produced gas and the remainder of gas would still need to be flared.
 - o Power generation also requires an agreement with a power company that is willing to purchase the gas. The terms of any such agreement typically require a long-term commitment from the operator at certain and steady deliverables. With gas decline rates and the unpredictability of markets, it is impracticable for the operator to agree to a long-term commitment because as the wells decline the operator would be burdened with penalties for failure to meet the deliverables.
- Compressed Natural Gas On lease
 - Compressed Natural Gas is likely to be uneconomic to operate when the gas volume declines.
- NGL Removal On lease
 - o NGL Removal requires a plant and is expensive on such a small scale rendering it uneconomic and still requires residue gas to be flared.



U.S. Department of the Interior **BUREAU OF LAND MANAGEMENT**

Drilling Plan Data Report 07/19/2018

APD ID: 10400026769

Submission Date: 01/31/2018

Highlighted data reflects the most

Operator Name: MATADOR PRODUCTION COMPANY

Well Number: 226H

recent changes

Well Name: GARRETT FED COM

Well Type: CONVENTIONAL GAS WELL

Well Work Type: Drill

Show Final Text

Section 1 - Geologic Formations

Formation ID	Formation Name	Flavotion	True Vertical	1	1		Producing
1	Formation Name	Elevation	Depth	Depth	Lithologies	Mineral Resources	
1	QUATERNARY	2921	0	0	OTHER : CALICHE	USEABLE WATER	No
2	RUSTLER ANHYDRITE	2892	29	29		USEABLE WATER	No
3	TOP SALT	2521	400	400		NONE	No
4	CASTILE	1699	1222	1225	ANHYDRITE	NONE	No
5	BASE OF SALT	126	2795	2813		NONE	No
6	BELL CANYON	72	2849	2868	SANDSTONE	NATURAL GAS,OIL	No
7	CHERRY CANYON	-840	3761	3788	SANDSTONE	NATURAL GAS,OIL	No
8	BRUSHY CANYON	-2007	4928	4963	SANDSTONE	NATURAL GAS,OIL	No
9	BONE SPRING	-3648	6569	6615	LIMESTONE	NATURAL GAS,OIL	No
10	BONE SPRING 1ST	-4436	7357	7393	OTHER : CARBONATE	NATURAL GAS,OIL	No
11	BONE SPRING 1ST	-4603	7524	7560	LIMESTONE,SANDSTO NE	NATURAL GAS,OIL	No
12	BONE SPRING 2ND	-4869	7790	7826	OTHER : CARBONATE	NATURAL GAS,OIL	No
13	BONE SPRING 2ND	-5373	8294	8330	SANDSTONE	NATURAL GAS,OIL	Yes
14	BONE SPRING 3RD	-5719	8640	8676	OTHER : Carbonate	NATURAL GAS,CO2,OIL	No
15	BONE SPRING 3RD	-6461	9382	9418	SANDSTONE	NATURAL GAS,CO2,OIL	No
16	WOLFCAMP	-6822	9743	9779	OTHER : A Carbonate	NATURAL GAS,CO2,OIL	No
17	WOLFCAMP	-7282	10203	10239	OTHER : B Carbonate	NATURAL GAS,CO2,OIL	Yes

Well Name: GARRETT FED COM Well Number: 226H

Section 2 - Blowout Prevention

Pressure Rating (PSI): 5M

Rating Depth: 12000

Equipment: A 12,000' 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and 1 annular preventer will be used below surface casing to TD. See attached BOP, choke manifold, co-flex hose, and speed head diagrams. An accumulator complying with Onshore Order 2 requirements for the BOP stack pressure rating will be present. Rotating head will be installed as needed.

Requesting Variance? YES

Variance request: Matador requests a variance to have the option of running a speed head for setting the intermediate 1 and 2 strings. In the case of running a speed head with landing mandrel for 9.625" and 7" casing, a minimum 3M BOPE system will be installed after surface casing is set. BOP test pressures will be 250 psi low and 3000 psi high. Annular will be tested to 250 psi low and 2500 psi high before drilling below the surface shoe. After 7" casing is set in the speed head, the BOP will then be lifted to install another casing head section for setting the production casing. Matador will nipple up the casing head and BOP and a minimum 5M BOPE system will be installed. Pressure tests will be made to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high. A diagram of the speed head is attached. Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. Manufacturer does not require the hose to be anchored. If the specific hose is not available, then one of equal or higher rating will be used.

Testing Procedure: Pressure tests will be conducted before drilling out from under all casing strings. BOP will be inspected and operated as required in Onshore Order 2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position. A third-party company will test the BOPs. After setting the surface casing, and before drilling the surface casing shoe, a minimum 2M BOPE system will be installed. It will be tested to 250 psi low and 2000 psi high. Annular will be tested to 250 psi low and 1000 psi high. After setting intermediate 1 casing, a minimum 3M BOPE system will be installed and tested to 250 psi low and 3000 psi high. Annular will be tested to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high.

Choke Diagram Attachment:

Garrett 226H Choke_20180131090253.pdf

BOP Diagram Attachment:

Garrett_226H_BOP_20180131090308.pdf

Section 3 - Casing

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	17.5	13.375	NEW	API	N	0	610	0	610	2920		610	J-55		OTHER - BTC	1.12 5	1.12 5	DRY	1.8	DRY	1.8
2	INTERMED IATE	8.75	7.625	NEW	API	Y	0	2600	0	2584			2600	P- 110		OTHER - BTC	1.12 5	1.12 5	DRY	1.8	DRY	1.8

Well Name: GARRETT FED COM Well Number: 226H

ω Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
4	INTERMED IATE	5	9.625	NEW	API	N	0	2900	U	2881			2900	J-55	l	OTHER - BTC	1.12 5	1.12 5	DRY	1.8	DRY	1.8
4	PRODUCTI ON	6.12 5	5.5	NEW	API	Υ	o	10200	0	10164			10200	P- 110		OTHER - BTC/TXP	l_	1.12 5	DRY	1.8	DRY	1.8
	INTERMED IATE	8.75	7.625	NEW	API	Υ	2600	10300	2584	10264				P- 110			1.12 5	1.12 5	DRY	1.8	DRY	1.8
	INTERMED IATE	8.75	7.0	NEW	API	Y	10300	11212	10264	10940				P- 110	ŀ	OTHER - BTC	1.12 5	1.12 5	DRY	1.8	DRY	1.8
7	PRODUCTI ON	6.12 5	4.5	NEW	API	Y	10200	15720	10164	10955				P- 110	I	OTHER - BTC/TXP	_	1.12 5	DRY	1.8	DRY	1.8

Casing Attachments

Casing	ID:	1

String Type: SURFACE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Garrett_226H_Casing_Design_Assumptions_20180131090833.pdf

Casing ID: 2

String Type: INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Garrett_226H_Casing_Design_Assumptions_20180131091921.pdf

Casing Design Assumptions and Worksheet(s):

Garrett_226H_Casing_Design_Assumptions_20180131091315.pdf

Well Name: GARRETT FED COM Well Number: 226H

Casing Attachments Casing ID: 3 String Type: INTERMEDIATE **Inspection Document: Spec Document: Tapered String Spec:** Casing Design Assumptions and Worksheet(s): Garrett_226H_Casing_Design_Assumptions_20180131091207.pdf Casing ID: 4 String Type: PRODUCTION **Inspection Document: Spec Document: Tapered String Spec:** Garrett_226H_5.5in_Specs_20180131092007.pdf Casing Design Assumptions and Worksheet(s): Garrett 226H Casing Design Assumptions_20180131092031.pdf

Casing ID: 5 String Type: INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Garrett_226H_7.625in_Specs_20180131091524.pdf

Casing Design Assumptions and Worksheet(s):

Garrett_226H_Casing_Design_Assumptions_20180131091541.pdf

Well Name: GARRETT FED COM Well Number: 226H

Casing Attachments

Casing ID: 6

String Type: INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Garrett_226H_Casing_Design_Assumptions_20180131091832.pdf

Casing Design Assumptions and Worksheet(s):

Garrett_226H_Casing_Design_Assumptions_20180131092150.pdf

Casing ID: 7

String Type: PRODUCTION

Inspection Document:

Spec Document:

Tapered String Spec:

Garrett_226H_4.5in_Specs_20180131092110.pdf

Casing Design Assumptions and Worksheet(s):

Garrett_226H_Casing_Design_Assumptions_20180131092127.pdf

Section 4 - Cement

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	610	268	1.82	12.8	487	100	CLASS C	BENTONITE + 2% CaCl2 + 3% NaCl + LCM
SURFACE	Tail		0	610	352	1.38	14.8	485	100	CLASS C	5% NaCl + LCM
INTERMEDIATE	Lead		0	2600	700	2.13	12.6	1491	60	TXI	fluid loss + dispersant + retarder + LCM
INTERMEDIATE	Tail		0	2600	225	1.38	14.8	310	60	TXI	fluid loss + dispersant + retarder + LCM
INTERMEDIATE	Lead		0	2900	638	2.13	12.6	1358	100	CLASS C	BENTONITE + 1% CaCl2 + 8% NaCl +

Well Name: GARRETT FED COM

Well Number: 226H

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
											LCM
INTERMEDIATE	Tail		0	2900	202	1.38	14.8	278	100	CLASS C	5% NaCl + LCM
PRODUCTION	Lead		0	1020 0	530	1.17	15.8	620	25	Class H	FLUID LOSS + DISPERSANT + RETARDER + LCM
PRODUCTION	Tail		0	1020 0	530	1.17	15.8	620	25	Class H	FLUID LOSS + DISPERSANT + RETARDER + LCM
INTERMEDIATE	Lead		2600	1030 0	700	2.13	12.6	1491	60	TXI	fluid loss + dispersant + retarder + LCM
INTERMEDIATE	Tail		2600	1030 0	225	1.38	14.8	310	60	TXI	fluid loss + dispersant + retarder + LCM
INTERMEDIATE	Lead		1030 0	1121 2	700	2.13	12.6	1491	60	TXI	fluid loss + dispersant + retarder + LCM
INTERMEDIATE	Tail		1030 0	1121 2	225	1.38	14.8	310	60	TXI	fluid loss + dispersant + retarder + LCM
PRODUCTION	Lead		1020 0	1572 0	530	1.17	15.8	620	25	Class H	fluid loss + dispersant + retarder + LCM
PRODUCTION	Tail		1020 0	1572 0	530	1.17	15.8	620	25	Class H	fluid loss + dispersant + retarder + LCM

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

Describe what will be on location to control well or mitigate other conditions: All necessary mud products (barite, bentonite, LCM) for weight addition and fluid loss control will be on location at all times.

Describe the mud monitoring system utilized: An electronic Pason mud monitoring system complying with Onshore Order 1 will be used.

Circulating Medium Table

Well Name: GARRETT FED COM Well Number: 226H

Top Depth	Bottom Depth	Mud Type	Min Weight (Ibs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	Н	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
1121 2	1572 0	OIL-BASED MUD	12.5	12.5							
610	2900	OTHER : BRINE WATER	10	10							
0	610	SPUD MUD	8.3	8.3							
2900	1121 2	OTHER : FRESH WATER + CUT BRINE	9	9							

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures:

A 2-person mud logging program will be used from 11,200 MD to TD.

No electric logs are planned at this time. GR will be collected through the MWD tools from intermediate casing to TD. CBL with CCL will be run as far as gravity will let it fall to TOC.

List of open and cased hole logs run in the well:

CBL,GR,MWD

Coring operation description for the well:

No core is planned.

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 7000

Anticipated Surface Pressure: 4589.89

Anticipated Bottom Hole Temperature(F): 170

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards attachment:

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations plan:

Well Name: GARRETT FED COM Well Number: 226H

Garrett_226H_H2S_Plan_20180131093056.pdf

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

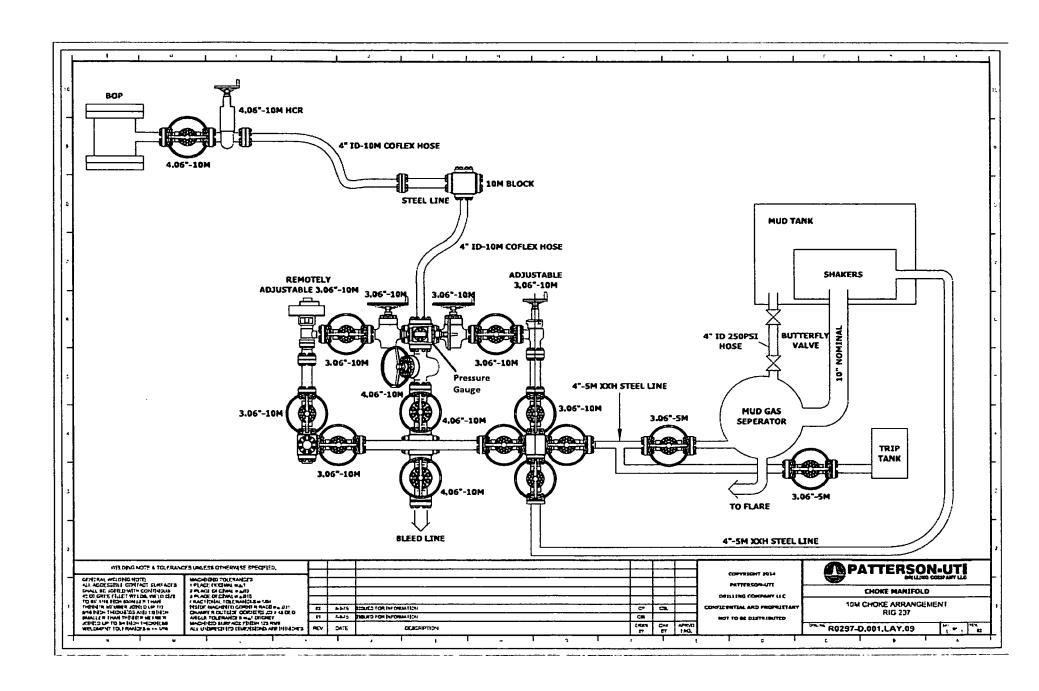
Garrett_226H_Horizontal_Drill_Plan_20180131093125.pdf

Other proposed operations facets description:

Other proposed operations facets attachment:

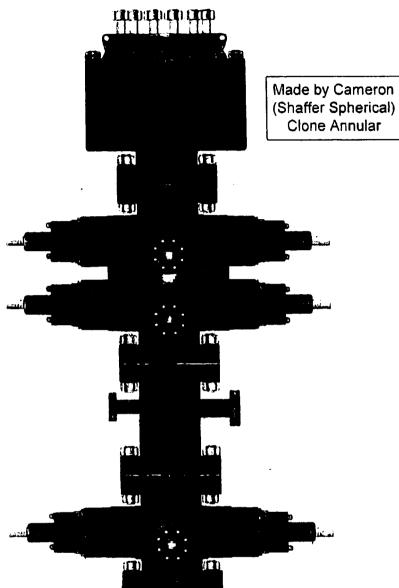
Garrett_226H_Speedhead_Specs_20180131093146.pdf Garrett_226H_General_Drill_Plan_20180517082047.pdf

Other Variance attachment:









PATTERSON-UTI # ______PS2-628

STYLE: New Shaffer Spherical

BORE ______13 5/8" ______PRESSURE ______5,000

HEIGHT: ______48 ½" ______WEIGHT: ______13,800 lbs

PATTERSON-UTI # PC2-128

STYLE: New Cameron Type U

BORE 13 5/8" PRESSURE 10,000

RAMS: TOP 5" Pipe BTM Blinds

HEIGHT: 66 5/8" WEIGHT: 24,000 lbs

Length 40" Outlets 4" 10M

DSA 4" 10M x 2" 10M

PATTERSON-UTI # PC2-228

STYLE: New Cameron Type U

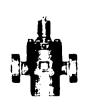
BORE 13 5/8" PRESSURE 10,000

RAMS: 5" Pipe

HEIGHT: 41 5/8" WEIGHT: 13,000 lbs

WING VALVES













2" Check Valve

2" Manual Valve

2" Manual Valve

4" Manual Valve

4" Hydraulic Valve

Midwest Hose

& Specialty, Inc.

Internal Hydrostatic Test Graph

Customer: Patterson

Pick Ticket #: 284918

Hose Specifications

Hose Type Ck LD. 3"

3"
Working Pressure
10000 PSI

Length 10' O.D. 4.79" Burst Pressure

Standard Safety Multiplier Applies

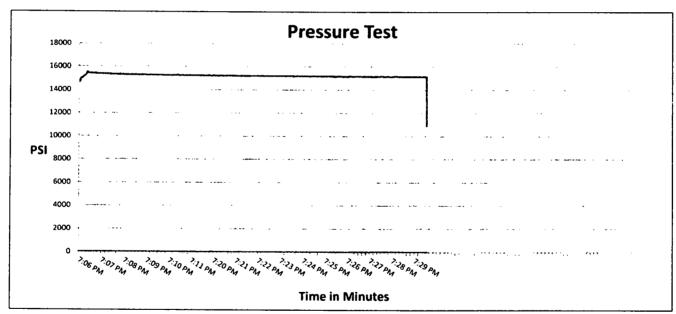
<u>Verification</u>

Type of Fitting
4-1/16 10K
Die Size
5.37"
Hose Serial #

10490

Coupling Method
Swage
Final O.D.
5.37"
Hose Assembly Serial #

284918-2



Test Pressure 15000 PSI Time Held at Test Pressure
15 2/4 Minutes

Actual Burst Pressure

Peak Pressure 15732 PSI

Comments: Hose assembly pressure tested with water at ambient temperature.

Tested By://Tyler His

Approved By: Ryan Adams



Midwest Hose & Specialty, Inc.

Inter	rnal Hydrosto	itic Test Certificate	
General Inform	nation	Hose Speci	fications
Customer	PATTERSON B&E	Hose Assembly Type	Choke & Kill
MWH Sales Representative	AMY WHITE	Certification	API 7K
Date Assembled	12/8/2014	Hose Grade	MUD
Location Assembled	ОКС	Hose Working Pressure	10000
Sales Order #	236404	Hose Lot # and Date Code	10490-01/13
Customer Purchase Order #	260471	Hose I.D. (Inches)	3"
Assembly Serial # (Pick Ticket #)	287918-2	Hose O.D. (Inches)	5.30"
Hose Assembly Length	10'	Armor (yes/no)	YES
	Fit	tings	
End A		End I	3
Stem (Port and Revision #)	R3.0X64WB	Stem (Part and Revision #)	R3.0X64WB
Stem (Heat #)	91996	Stem (Heat #)	91996
Ferrule (Part and Revision #)	RF3.0	Ferrule (Part and Revision #)	RF3.0
Ferrule (Heat #)	37DA5631	Ferrule (Heat #)	37DA5631
Connection (Part #)	4 1/16 10K	Connection (Part #)	4 1/16 10K
Connection (Heat #)		Connection (Heat #)	
Dies Used	5.3	7 Dies Used	5.37
	Hydrostatic Te	st Requirements	
Test Pressure (psi)	15,000	Hose assembly was tested	d with ambient water
Test Pressure Hold Time (minutes)	15 1/2	temperature.	



Midwest Hose & Specialty, Inc.

Customer:	PATTERSON B&E	Customer P.O.# 260471
Sales Order #	236404	Date Assembled: 12/8/2014

Hose Assembly Type:	Choke & Kill		
Assembly Serial #	287918-2	Hose Lot # and Date Code	10490-01/13
Hose Working Pressure (psi)	10000	Test Pressure (psi)	15000

We hereby certify that the above material supplied for the referenced purchase order to be true according to the requirements of the purchase order and current industry standards.

Supplier:

Midwest Hose & Specialty, Inc.

3312 S I-35 Service Rd

Oklahoma City, OK 73129

Comments:

Approved By	Date
12/11	12/9/2014
Fran Alama	

December 9, 2014



Internal Hydrostatic Test Graph

Customer: Patterson

Pick Ticket #: 284918

Verification

Hose Specifications

Hose Type
Ck
LD.
3"
Working Pressure

10000 PSI

Length
20'
O.D.
4.77"
Burst Pressure
Standard Safety Multiplier Applies

Type of Fitting
4-1/16 10K
Die Size
5.37"
Hose Serial #
10490

Coupling Method
Swage
Final O.D.
5.40"
Hose Assembly Serial #
284918-1

Test Pressure 15000 PSI Time Held at Test Pressure 15 2/4 Minutes **Actual Burst Pressure**

Peak Pressure 15893 PSI

Comments: Hose assembly pressure tested with water at ambient temperature.

Tested By: Tyler Hill

Approved By: Ryan Adams



Midwest Hose & Specialty, Inc.

Internal Hydrostatic Test Certificate

General Infor	mation	Hose Specifi	cations
Customer	PATTERSON B&E	Hose Assembly Type	Choke & Kill
MWH Sales Representative	AMY WHITE	Certification	API 7K
Date Assembled	12/8/2014	Hose Grade	MUD
Location Assembled	ОКС	Hose Working Pressure	10000
Sales Order #	236404	Hose Lot # and Date Code	10490-01/13
Customer Purchase Order #	260471	Hose I.D. (inches)	3"
Assembly Serial # (Pick Ticket #)	287918-1	Hose O.D. (Inches)	5.30"
Hose Assembly Length	20'	Armor (yes/no)	YES
	Fit	tings	
End A		End B	
Stem (Part and Revision #)	R3.0X64WB	Stem (Part and Revision #)	R3.0X64WB
Stem (Heat #)	A141420	Stem (Heat #)	A141420
Ferrule (Part and Revision #)	RF3.0	Ferrule (Part and Revision #)	RF3.0
Ferrule (Heat #)	37DA5631	Ferrule (Heat #)	37DA5631
Connection (Part #)	4 1/16 10K	Connection (Part #)	4 1/16 10K
Connection (Heat #)	V3579	Connection (Heat #)	V3579
Dies Used	5.3	7 Dies Used	5.3
	Hydrostatic Te	st Requirements	
Test Pressure (psi)	15,000	Hose assembly was tested	with ambient water
Test Pressure Hold Time (minutes)	15 1/2	temperature.	



Midwest Hose & Specialty, Inc.

Customer: PATTERSON B&E		Customer P.O.# 260471	
Sales Order # 236404		Date Assembled: 12/8/2014	
	Sne	ifications	
Hose Assembly Type:	Choke & Kill		
	•	Hose Lot # and Date Code	10490-01/13

We hereby certify that the above material supplied for the referenced purchase order to be true according to the requirements of the purchase order and current industry standards.

Supplier:

Midwest Hose & Specialty, Inc.

3312 S I-35 Service Rd

Oklahoma City, OK 73129

Comments:

Approved By	Date
Fan Alama	12/9/2014



Internal Hydrostatic Test Graph

Customer: Patterson

Pick Ticket #: 284918

Hose Specifications

Hose Type Mud I.D. 3"

Working Pressure 10000 PSI

Length 70' O.D. 4.79"

Burst Pressure Standard Safety Multiplier Applies

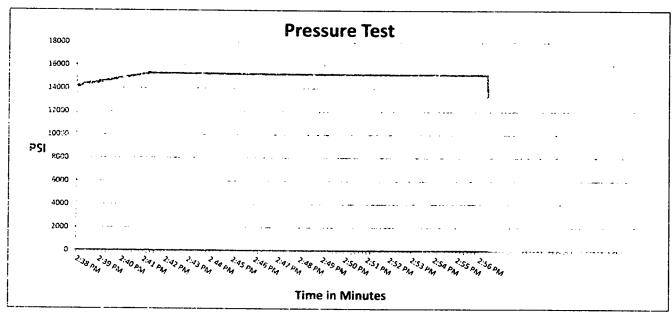
Verification

Type of Fitting 4 1/16 10K Die Size 5.37"

Hose Serial# 10490

Coupling Method Swage Final O.D. 5.37" Hose Assembly Serial #

284918-3



Test Pressure 15000 PSI

Time Held at Test Pressure 16 3/4 Minutes

Actual Burst Pressure

Peak Pressure 15410 PSI

Comments: Hose assembly pressure tested with water at ambient temperature.

Tested By: Ayler Hill

Approved By: Ryan Agams



Midwest Hose & Specialty, Inc.

General Inform	nation	Hose Specif	ications
Customer	PATTERSON B&E	Hose Assembly Type	Choke & Kill
MWH Sales Representative	AMY WHITE	Certification	API 7K
Date Assembled	12/8/2014	Hose Grade	MUD
Location Assembled	ОКС	Hose Working Pressure	10000
Sales Order #	236404	Hose Lot # and Date Code	10490-01/13
Customer Purchase Order#	260471	Hose I.D. (Inches)	3"
Assembly Serial # (Pick Ticket #)	287918-3	Hose O.D. (Inches)	5.23"
Hose Assembly Length	70'	Armor (yes/no)	YES
	Fit	tings	
End A		End B	
Stem (Part and Revision #)	R3.0X64WB	Stem (Part and Revision #)	R3.0X64WB
Stem (Heat #)	A141420	Stem (Heat #)	A141420
Ferrule (Part and Revision #)	RF3.0	Ferrule (Part and Revision #)	RF3.0
Ferrule (Heat #)	37DA5631	Ferrule (Heat #)	37DA5631
Connection (Part #)	4 1/16 10K	Connection (Part #)	4 1/16 10K
Connection (Heat #)		Connection (Heat #)	
Dies Used	5.3	7 Dies Used	5.3
	Hydrostatic Te	st Requirements	
Test Pressure (psi)	15,000	Hose assembly was tested	with ambient water
Test Pressure Hold Time (minutes)	16 3/4	temperature.	



Midwest Hose & Specialty, Inc.

Customer:	PATTERSON I	B&E	Customer P.O.# 260471	
Sales Order # 236404		Date Assembled: 12/8/2014		
		Spec	ifications	
<u> 214.0004833, 0.43, 00.4003</u> ,	48411, 1888, 888 - 18, 1969 (N. 6248			
Hose Assei	nbly Type:	Choke & Kill		
Hose Asser		Choke & Kill 287918-3	Hose Lot # and Date Code	10490-01/13

We hereby certify that the above material supplied for the referenced purchase order to be true according to the requirements of the purchase order and current industry standards.

Supplier:

Midwest Hose & Specialty, Inc.

3312 S I-35 Service Rd

Oklahoma City, OK 73129

Comments:

Approved By	Date
Fan Alaua	12/9/2014

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an
 internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

• Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at
 setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force
 will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative
 backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing
 will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

• Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at
 setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force
 will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative
 backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_c=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at
 setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force
 will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative
 backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

December 31 2015



Connection: TenarisXP® BTC

Casing/Tubing: CAS

Coupling Option: REGULAR

Size: 4.500 in. Wall: 0.290 in.

Weight: 13.50 lbs/ft

Grade: P110-ICY

Min. Wall Thickness: 87.5 %

Nominal OD	4.500 in.	Nominal Weight	13.50 lbs/ft	Standard Drift Diameter	3.795 in.	
Nominal ID	3.920 in.	Wall Thickness	0.290 in.	Special Drift Diameter	N/A	
Plain End Weight	13.05 lbs/ft	<u> </u>				
Body Yield Strength	479 x 1000 lbs	Internal Yield	14100 psi	SMYS	125000 psi	
Collapse	11 620 psi					
Critical Section Area	3.836 sq. in.	Threads per in.	5.00	Make-Up Loss`	4.016 in.	
Connection OD Critical Section Area	5.000 in. 3.836 sq. in.	Coupling Length Threads per in.	9.075 in. 5.00	Connection ID Make-Up Loss	3.908 in. 4.016 in.	
·····				T		
Tension Efficiency	100 %	Joint Yield Strength	479 x 1000 lbs	Internal Pressure Capacity ⁽¹⁾	14100 psi	
		Structural	479 x 1000 lbs	Structural	1071/100	
Structural	100 %			- 11 (2)	127 ' /100 f	
Structural Compression Efficiency	100 %	Compression Strength	473 N 1000 103	Bending ⁽²⁾		
Compression	100 % 11620 psi	Compression Strength	477 x 1000 ibs	Bending¹≛/		
Compression Efficiency External Pressure				Bending 127		
Compression Efficiency External Pressure		Compression Strength Optimum	7720 ft-lbs	Bending ¹	8490 ft-lbs	

For the latest performance data, always visit our website: www.tenaris.com

July 15 2015



Size: 5.500 in. Wall: 0.361 in.

Weight: 20.00 lbs/ft Grade: P110-IC

Min. Wall Thickness: 87.5 %

Connection: TenarisXP™ BTC Casing/Tubing: CAS

Coupling Option: REGULAR

-		GEOMET	ry			
Nominal OD	5.500 in.				4.653 in.	
Nominal ID	4.778 in.	Wall Thickness	Wall Thickness 0.361 in.		N/A	
Plain End Weight	19.83 lbs/ft					
		PERFORM	ANCE			
Body Yield Strength	641 x 1000 lbs	Internal Yleid	12630 psi	SMYS	110000 psi	
Collapse	12100 psi					
	TEI	NARISXP™ BTC CO		ATA		
		GEOMET	TRY	· · · · · · · · · · · · · · · · · · · 		
Connection OD	6.100 in.	Coupling Length	9.450 in.	Connection ID	4.766 in.	
Critical Section Area	5.828 sq. in.	Threads per in.	5.00	Make-Up Loss	4.204 in.	
		PERFORM	ANCE			
Tension Efficiency	100 %	Joint Yield Strength	641 x 1000 lbs	Internal Pressure Capacity ⁽¹⁾	12630 psi	
Structural Compression Efficiency	100 %	Structural Compression Strength	641 x 1000 lbs	Structural 92 °/1 Bending(2)		
External Pressure Capacity	12100 psi					
	Ε	STIMATED MAKE-	JP TORQUES ⁽	3)		
Minimum	11270 ft-lbs	Optimum	12520 ft-lbs	Maximum	13770 ft-li	
		OPERATIONAL LIN	IT TORQUES			
Operating Torque	21500 ft-lbs	Yield Torque	23900 ft-lbs	T		

BLANKING DIMENSIONS

Blanking Dimensions

- (1) Internal Pressure Capacity related to structural resistance only. Internal pressure leak resistance as per section 10.3 API 5C3 / ISO 10400 2007.
- (2) Structural rating, pure bending to yield (i.e no other loads applied)
- (3) Torque values calculated for API Modified thread compounds with Friction Factor=1. For other thread compounds please contact us at licens@es@oilfield.tenaris.com. Torque values may be further reviewed. For additional information, please contact us at contact-tenarishydril@tenaris.com

Issued on: 12 Janv. 2017 by T. DELBOSCO

VRCC 16-1177 Rev02 for Houston Field Service

DATA ARE INFORMATIVE ONLY. BASED ON SI_PD-101836 P&B



OD	Weight	Wall Th.	Grade	API Drift	Connection
7 5/8 in.	29.70 lb/ft	0.375 in.	P110 EC	6.750 in.	VAM® HTF NR

PIPE PROPE	RTIES
Nominal OD	7.625 in,
Nominal ID	6.875 in.
Nominal Cross Section Area	8.541 sqin.
Grade Type	Enhanced API
Min. Yield Strength	125 ksi
Max. Yield Strength	140 ksi
Min. Ultimate Tensile Strength	135 ksi
Tensile Yield Strength	1 068 klb
Internal Yield Pressure	10 760 psi
Collapse pressure	7 360 psi

CONNECTION PROPERTIES								
Connection Type	Premium Integral Flush							
Connection OD (nom)	7.701 in.							
Connection ID (nom)	6.782 in.							
Make-Up Loss	4.657 In.							
Critical Cross Section	4.971 sqin.							
Tension Efficiency	58 % of pipe							
Compression Efficiency	72.7 % of pipe							
Compression Efficiency with Sealability	34.8 % of pipe							
Internal Pressure Efficiency	100 % of pipe							
External Pressure Efficiency	100 % of pipe							

CONNECTION PERFORMANCES					
Tensile Yield Strength	619 klb				
Compression Resistance	778 kib				
Compression with Sealability	372 klb				
Internal Yield Pressure	10 760 psi				
External Pressure Resistance	7 360 psi				
Max. Bending	44 º/100ft				
Max. Bending with Sealability	17 º/100ft				

TORQUE VALUES								
Min. Make-up torque	9 600 ft.lb							
Opti. Make-up torque	11 300 ft.lb							
Max. Make-up torque	13 000 ft.lb							
Max. Torque with Sealability	58 500 ft.lb							
Max. Torsional Value	73 000 ft.lb							

VAMs HTFr (High Torque Flush) is a flush OD integral connection providing maximum clearance along with torque strength for challenging applications such as extended reach and slim hole wells, drilling liner / casing, liner rotation to achieve better cementation in highly deviated and critical High Pressure / High Temperature wells.

Looking ahea on the outcoming testing industry standards, VAM® decided to create an upgraded design and launch on the market the VAM® HTF-NR as the new standard version of VAM® extreme high torque flush connection. The VAM® HTF-NR has extensive tests as per API RP 5C5:2015 CAL II which include the gas sealability having load points with bending, internal pressure and high temperature at 135°C.

Do you need help on this product? - Remember no one knows VAM® like VAM®

canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com

china@vamfieldservice.com baku@vamfieldservice.com singapore@vamfieldservice.com australia@vamfieldservice.com

Over 180 VAM® Specialists available worldwide 24/7 for Rig Site Assistance

Other Connection Data Sheets are available at www.vamservices.com

Vallourec Group



Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_c=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing
 will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud
 gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient
 of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft
 with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a
 more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at
 setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force
 will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative
 backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

• Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing
 will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at
 setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force
 will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative
 backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

• Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DFh=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DFh=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud
 gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient
 of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing
 will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Surface Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore
pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at
 setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force
 will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative
 backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_c=1.125

Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mudgradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud
 gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore
 pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst
 pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick
 with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that
 (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft),
 which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).



Hydrogen Sulfide Drilling Operations Plan

1 H2S safety instructions covering:

- Characteristics of H2S
- Physical effects & hazards
- Principal and operation of H2S detectors, warning system, and briefing areas
- Evacuation procedures, routes, and first aid
- Proper use of safety equipment & life support systems
- Essential personnel meeting medical evaluation criteria will receive additional training on the proper use of 30-minute pressure demand air packs

2 H2S Detection and Alarm Systems:

- H2S sensor/detectors will be located on the drilling rig floor, in the base of the sub structure / cellar area, and on the mud pits in the shale shaker area. Additional H2S detectors may be placed as deemed necessary.
- An audio alarm system will be installed on the derrick floor and in the doghouse.

3 Windsocks and / Wind Streamers:

- Windsocks at mud pit area will be high enough to be visible.
- Windsocks on the rig floor and top of doghouse will be high enough to be visible.

4 Condition Flags and Signs:

- Warning sign on access road to location
- Flags to be displayed on sign at entrance to location
 - o Green Flag Normal Safe Operation Condition
 - Yellow Flag Potential Pressure and Danger
 - o Red Flag Danger (H2S present in dangerous concentrations) Only H2S trained personnel admitted on location

5 Well Control Equipment:

See APD

6 Communications:

- While working under masks, chalkboards will be used for communications.
- Hand signals will be used where chalk board is inappropriate.
- Two-way radio will be used to communicate off location in case of emergency help is required. In most cases cellular telephones will be available at drilling foreman's trailer or living quarters.



7 Drill Stem Testing:

• No DST or cores are planned at this time.

8 Drilling contractor supervisor will be required to be familiar with the effects H2S has on tubulars good and other mechanical equipment.

9 If H2S is encountered, mud system will be altered if necessary to maintain control of formation. A mud gas separator will be brought into service along with H2S scavengers if necessary.

11 Emergency Contacts

• See next page

H2S Contingency Plan Emergency Contacts Matador Production Company Garrett Fed Com wells, Eddy County, NM

Company Office			
Matador Production Company	(972)-371-5200		
Key Personnel			-
Name	Title	Office	Mobile
Billy Goodwin	Vice President Drilling	972-371-5210	817-522-2928
Gary Martin	Drilling Superintendent		601-669-1774
Dee Smith	Drilling Superintendent	972-371-5447	972-822-1010
Adam Lange	Drilling Engineer	972-371-5247	214-458-0788
A			
Artesia Ambulance		911	
State Police		575-746-2703	
		575-746-2703	
City Police Sheriff's Office		575-746-9888	
Fire Department		575-746-2701	
Local Emergency Planning Committe	20	575-746-2122	
New Mexico Oil Conservation Division		575-748-1283	
Carlsbad	<u></u>	3/3 / 40 1203	-
Ambulance		911	
State Police		575-885-3137	
Loving City Police		575-745-3511	:
Sheriff's Office		575-887-7551	
Malaga Fire Department		575-745-2317	
Local Emergency Planning Committe	2e	575-885-3581	
Santa Fe		······································	
New Mexico Emergency Response C	Commission (Santa Fe)	505-476-9600	
New Mexico Emergency Response C		505-827-9126	
New Mexico State Emergency Opera		505-476-9635	
National			
Carlsbad BLM		575-234-5972	
National Emergency Response Cent	er (Washington, D.C.)	800-424-8802	1
Medical			
Flight for Life- 4000 24th St.; Lubboo	k, TX	806-743-9911	
Aerocare- R3, Box 49F; Lubbock, TX		806-747-8923	
Med Flight Air Amb- 2301 Yale Blvd	S.E., D3; Albuquerque, NM	505-842-4433	
SB Air Med Service- 2505 Clark Carr	Loop S.E.; Albuquerque, NM	505-842-4949	
Other			
Boots & Coots IWC		800-256-9688	or 281-931-8884
Cudd Pressure Control		432-699-0139	or 432-563-3356
Halliburton		575-746-2757	
B.J. Services		575-746-3569	

H2S Rig Diagram

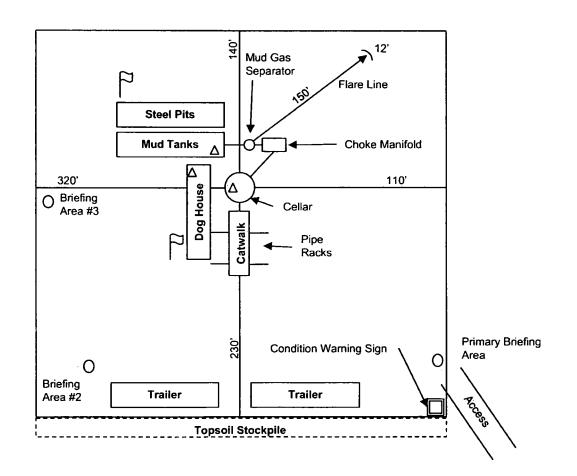
Garrett Fed Com 226H SHL 2372' FNL & 584' FWL 32-24S-29E Eddy County, NM (not to scale)

Wind Direction Indicator

↑ H2S Monitors

O Briefing Areas

Prevailing
Winds → North



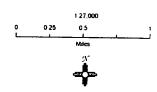


Matador Production Company

Garrett Fed Com #226H H₂S Contingency Plan: 2 Mile Radius Map

Section 32, Township 24S, Range 29E Eddy County, New Mexico

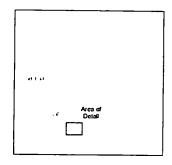
Surface Hole Location

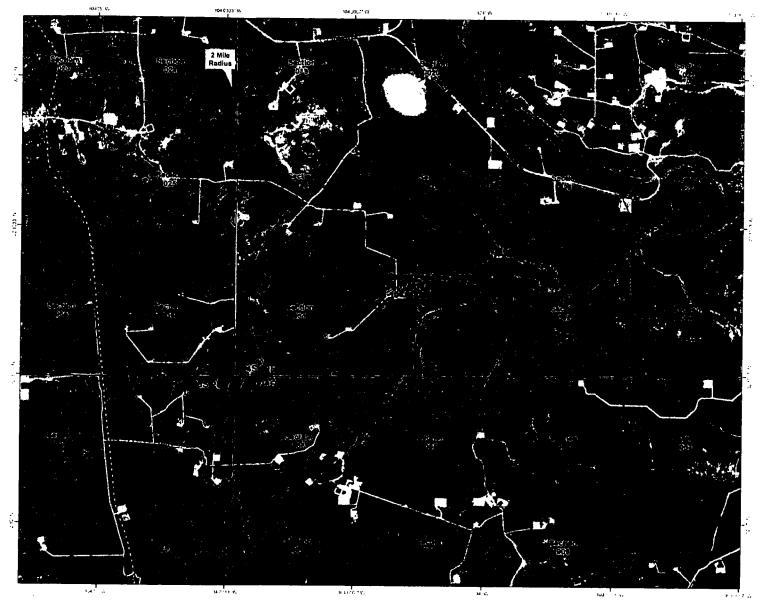


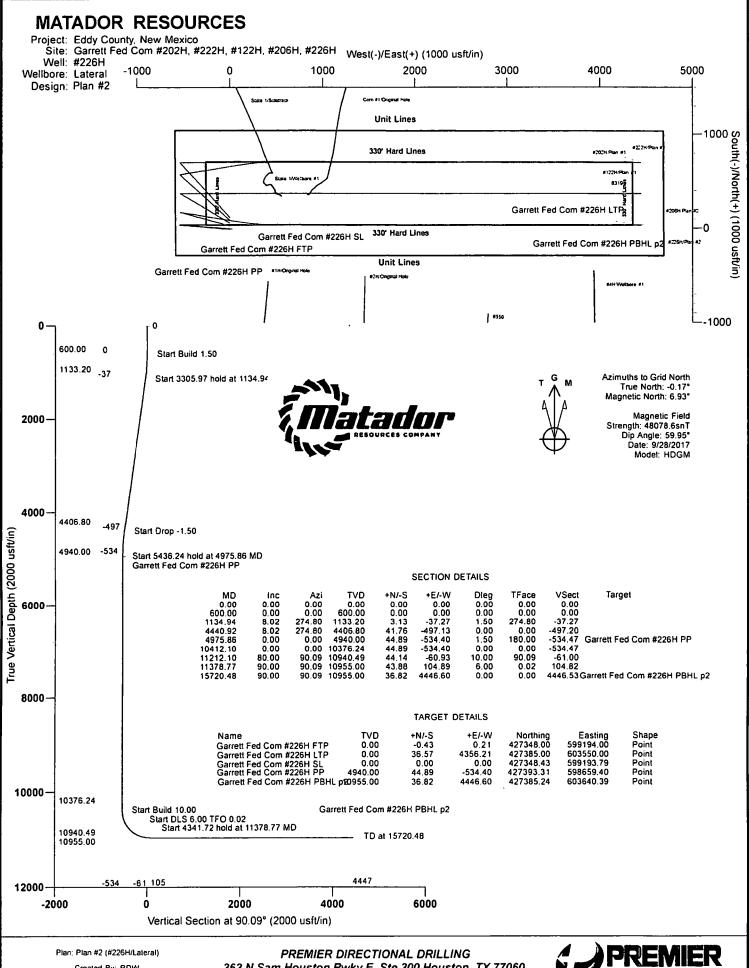
NAD 1983 New Mexico State Plane East FIPS 3001 Feet

PERMITS WEST ...

Prepared by Pormsts West, Inc., December 15, 2017 for Matador Production Company







Created By: RDW Date: 13:44, October 04 2017

363 N Sam Houston Pwky E, Ste 300 Houston, TX 77060 Phone: 281-673-4000



MATADOR RESOURCES Project: Eddy County, New Mexico Site: Garrett Fed Com #202H, #222H, #122H, #206H, #226H Azimuths to Grid North G M Well: #226H Т True North: -0.17° Wellbore: Lateral Magnetic North: 6.93° Design: Plan #2 **SLOTS** Magnetic Field +N/-S +E/-W Northing Strength: 48078.6snT Slot Name Easting #122H 60.08 -0.04 427408.51 599193.75 Dip Angle: 59.95° #202H 120.01 0.00 427468.43 599193.79 Date: 9/28/2017 #206H 29.97 -0.02 427378.40 599193.77 Model: HDGM 90.01 #222H -0.04 427438.43 599193.76 #226H 0.00 0.00 427348.43 599193.79 1000-State 1/Sidetrack 800 #202H/Plan #1 330' Hard Lines #222H/Plan #2 000 5000 600 10000 5000 Hard Lines 7000 State 1 000 TO 600 #122H/Plan #1 South(-)/North(+) (200 usft/in) 7000 30. 400-6000 2000 00 State 1/Wellbore #1 200 9(0Q 500ξ #202H #222H #206H/Plan #2 10**0**00 2000/2C 330' Hard Lines 0 #226H/Plan #2 Carrett Fed Com #226H PP -200· **Unit Lines** -400 -800 -600 -400 -200 200 400 600 West(-)/East(+) (200 usft/in)



PDD

Planning Report

Database:

EDM 5000 14 Multi User

Company: Project:

MATADOR RESOURCES Eddy County, New Mexico

Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Well: Wellbore: #226H Lateral Plan #2 Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference: MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference: Grid

Survey Calculation Method:

Minimum Curvature

Mean Sea Level

Design: Project

Site

Eddy County, New Mexico

Map System:

Geo Datum:

US State Plane 1927 (Exact solution)

Map Zone:

NAD 1927 (NADCON CONUS)

New Mexico East 3001

Garrett Fed Com #202H, #222H, #122H, #206H, #226H

Site Position: From:

Northing:

427,468.43 usft

System Datum:

Latitude:

Longitude:

32° 10' 29.36 N 104° 0' 45.86 W

Position Uncertainty:

Мар

Easting:

13.200 in

599.193.80 usft

0.00 usft Slot Radius:

Grid Convergence:

0.17 °

Well

#226H - Slot #226H

Well Position

+N/-S +E/-W

-120.01 usft 0.00 usft Northing:

427,348.43 usft 599,193.80 usft Latitude: Longitude: 32° 10' 28.17 N

Position Uncertainty

0.00 usft

Easting: Wellhead Elevation:

Ground Level:

104° 0' 45.86 W 2,920.00 usft

Wellbore

Lateral

Magnetics

Model Name

Sample Date

Declination (°)

Dip Angle (°)

Field Strength

(nT)

HDGM

9/28/2017

7.10

59.95

48,079

Design

Plan #2

Audit Notes:

Version:

Phase:

PLAN

Tie On Depth:

0.00

Vertical Section:

Depth From (TVD) (usft)

+N/-S (usft) 0.00

+E/-W (usft) 0.00

Direction (°)

90.09

0.00

Date 10/4/2017

Depth From

Plan Survey Tool Program

Depth To

(usft)

Survey (Wellbore)

Tool Name

Remarks

(usft) 0.00

15,720.48 Plan #2 (Lateral)

MWD+HDGM

OWSG MWD + HDGM

Planning Report

Database:

EDM 5000 14 Multi User

Company: Project: Eddy County, New Mexico

Site:

Design:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Well: Wellbore: #226H Lateral Plan #2

MATADOR RESOURCES

TVD Reference: MD Reference:

Well #226H - Slot #226H Local Co-ordinate Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Measured			Vertical			Dogleg	Build	Turn		
Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Rate (°/100ft)	Rate (°/100ft)	Rate (°/100ft)	TFO (°)	Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00	
1,134.94	8.02	274.80	1,133.20	3.13	-37.27	1.50	1.50	0.00	274.80	
4,440.92	8.02	274.80	4,406.80	41.76	-497.13	0.00	0.00	0.00	0.00	
4,975.86	0.00	0.00	4,940.00	44.89	-534.40	1.50	-1.50	0.00	180.00	Garrett Fed Com #
10,412.10	0.00	0.00	10,376.24	44.89	-534.40	0.00	0.00	0.00	0.00	
11,212.10	80.00	90.09	10,940.49	44.14	-60.93	10.00	10.00	0.00	90.09	
11,378.77	90.00	90.09	10,955.00	43.88	104.89	6.00	6.00	0.00	0.02	
15,720.48	90.00	90.09	10,955.00	36.82	4,446,60	0.00	0.00	0.00	0.00	Garrett Fed Com #

Planning Report

Database:

EDM 5000 14 Multi User

Company: Project:

MATADOR RESOURCES Eddy County, New Mexico

Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Well: Wellbore: Lateral

#226H

Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference: MD Reference:

North Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

Grid

Survey Calculation Method:

Minimum Curvature

Design:	Plan #2								
Planned Survey		* *** *****							
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00 500.00 600.00 700.00 800.00	0.00 0.00 0.00 1.50	0.00 0.00 0.00 274.80	400.00 500.00 600.00 699.99	0.00 0.00 0.00 0.11	0.00 0.00 0.00 -1.30	0.00 0.00 0.00 -1.30	0.00 0.00 0.00 1.50	0.00 0.00 0.00 1.50	0.00 0.00 0.00 0.00
900.00	3.00 4.50 6.00	274.80 274.80 274.80	799.91 899.69 999.27	0.44 0.99 1.75	-5.22 -11.73 -20.85	-5.22 -11.74 -20.85	1.50 1.50 1.50	1.50 1.50	0.00 0.00
1,100.00 1,134.94 1,200.00 1,300.00	7.50 8.02 8.02 8.02	274.80 274.80 274.80 274.80	1,098.57 1,133.20 1,197.62 1,296.64	2.74 3.13 3.89 5.06	-32.56 -37.27 -46.32 -60.23	-32.57 -37.27 -46.32 -60.23	1.50 1.50 1.50 0.00 0.00	1.50 1.50 1.50 0.00 0.00	0.00 0.00 0.00 0.00 0.00
1,400.00	8.02	274.80	1,395.66	6.23	-74.14	-74.15	0.00	0.00	0.00
1,500.00	8.02	274.80	1,494.68	7.40	-88.05	-88.06	0.00	0.00	0.00
1,600.00	8.02	274.80	1,593.70	8.56	-101.96	-101.97	0.00	0.00	0.00
1,700.00	8.02	274.80	1,692.72	9.73	-115.87	-115.88	0.00	0.00	0.00
1,800.00	8.02	274.80	1,791.74	10.90	-129.78	-129.79	0.00	0.00	0.00
1,900.00	8.02	274.80	1,890.76	12.07	-143.69	-143.71	0.00	0.00	0.00
2,000.00	8.02	274.80	1,989.78	13.24	-157.60	-157.62	0.00	0.00	0.00
2,100.00	8.02	274.80	2,088.80	14.41	-171.51	-171.53	0.00	0.00	0.00
2,200.00	8.02	274.80	2,187.83	15.57	-185.42	-185.44	0.00	0.00	0.00
2,300.00	8.02	274.80	2,286.85	16.74	-199.33	-199.35	0.00	0.00	0.00
2,400.00	8.02	274.80	2,385.87	17.91	-213.24	-213.27	0.00	0.00	0.00
2,500.00	8.02	274.80	2,484.89	19.08	-227.15	-227.18	0.00	0.00	0.00
2,600.00	8.02	274.80	2,583.91	20.25	-241.06	-241.09	0.00	0.00	0.00
2,700.00	8.02	274.80	2,682.93	21.42	-254.97	-255.00	0.00	0.00	0.00
2,800.00	8.02	274.80	2,781.95	22.58	-268.88	-268.91	0.00	0.00	0.00
2,900.00	8.02	274.80	2,880.97	23.75	-282.79	-282.82	0.00	0.00	0.00
3,000.00	8.02	274.80	2,979.99	24.92	-296.70	-296.74	0.00	0.00	0.00
3,100.00	8.02	274.80	3,079.01	26.09	-310.61	-310.65	0.00	0.00	0.00
3,200.00	8.02	274.80	3,178.03	27.26	-324.52	-324.56	0.00	0.00	0.00
3,300.00	8.02	274.80	3,277.06	28.43	-338.43	-338.47	0.00	0.00	0.00
3,400.00	8.02	274.80	3,376.08	29.59	-352.34	-352.38	0.00	0.00	0.00
3,500.00	8.02	274.80	3,475.10	30.76	-366.25	-366.30	0.00	0.00	0.00
3,600.00	8.02	274.80	3,574.12	31.93	-380.16	-380.21	0.00	0.00	0.00
3,700.00	8.02	274.80	3,673.14	33.10	-394.07	-394.12	0.00	0.00	0.00
3,800.00	8.02	274.80	3,772.16	34.27	-407.98	-408.03	0.00	0.00	0.00
3,900.00	8.02	274.80	3,871.18	35.44	-421.89	-421.94	0.00	0.00	0.00
4,000.00	8.02	274.80	3,970.20	36.60	-435.80	-435.86	0.00	0.00	0.00
4,100.00	8.02	274.80	4,069.22	37.77	-449.71	-449.77	0.00	0.00	0.00
4,200.00	8.02	274.80	4,168.24	38.94	-463.62	-463.68	0.00	0.00	0.00
4,300.00	8.02	274.80	4,267.26	40.11	-477.53	-477.59	0.00	0.00	0.00
4,400.00	8.02	274.80	4,366.29	41.28	-491.44	-491.50	0.00	0.00	0.00
4,440.92	8.02	274.80	4,406.80	41.76	-497.13	-497.20	0.00	0.00	0.00
4,500.00	7.14	274.80	4,465.37	42.41	-504.90	-504.96	1.50	-1.50	0.00
4,600.00	5.64	274.80	4,564.74	43.34	-515.99	-516.05	1.50	-1.50	0.00
4,700.00	4.14	274.80	4,664.38	44.05	-524.48	-524.54	1.50	-1.50	0.00
4,800.00	2.64	274.80	4,764.20	44.55	-530.36	-530.43	1.50	-1.50	0.00
4,900.00	1.14	274.80	4,864.14	44.82	-533.65	-533.72	1.50	-1.50	0.00
4,975.86	0.00	0.00	4,940.00	44.89	-534.40	-534.47	1.50	-1.50	0.00

PDD

Planning Report

Database: Company: EDM 5000 14 Multi User MATADOR RESOURCES Eddy County, New Mexico

Project: Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Well: Wellbore: #226H Lateral Local Co-ordinate Reference:

TVD Reference: MD Reference:

North Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

Grid

Survey Calculation Method:

Minimum Curvature

Wellbore: Design:	Lateral Plan #2								
Planned Survey					 .				
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
5,000.00	0.00	0.00	4,964.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,100.00	0.00	0.00	5,064.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,200.00	0.00	0.00	5,164.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,300.00	0.00	0.00	5,264.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,400.00	0.00	0.00	5,364.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,500.00	0.00	0.00	5,464.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,600.00	0.00	0.00	5,564.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,700.00	0.00	0.00	5,664.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,800.00	0.00	0.00	5,764.14	44.89	-534.40	-534.47	0.00	0.00	0.00
5,900.00	0.00	0.00	5,864.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,000.00	0.00	0.00	5,964.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,100.00		0.00	6,064.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,200.00	0.00	0.00	6,164.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,300.00	0.00	0.00	6,264.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,400.00	0.00	0.00	6,364.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,500.00	0.00	0.00	6,464.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,600.00	0.00	0.00	6,564.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,700.00	0.00	0.00	6,664.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,800.00	0.00	0.00	6,764.14	44.89	-534.40	-534.47	0.00	0.00	0.00
6,900.00	0.00	0.00	6,864.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,000.00	0.00	0.00	6,964.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,100.00	0.00	0.00	7,064.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,200.00	0.00	0.00	7,164.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,300.00	0.00	0.00	7,264.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,400.00	0.00	0.00	7,364.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,500.00	0.00	0.00	7,464.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,600.00	0.00	0.00	7,564.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,700.00	0.00	0.00	7,664.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,800.00	0.00	0.00	7,764.14	44.89	-534.40	-534.47	0.00	0.00	0.00
7,900.00	0.00	0.00	7,864.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,000.00	0.00	0.00	7,964.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,100.00	0.00	0.00	8,064.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,200.00	0.00	0.00	8,164.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,300.00	0.00	0.00	8,264.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,400.00	0.00	0.00	8,364.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,500.00	0.00	0.00	8,464.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,600.00	0.00	0.00	8,564.14	44.89	-534.40	-534.47	0.00	0.00	0.00
8,700.00 8,800.00 8,900.00 9,000.00 9,100.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	8,664.14 8,764.14 8,864.14 8,964.14 9,064.14	44.89 44.89 44.89 44.89 44.89	-534.40 -534.40 -534.40 -534.40	-534.47 -534.47 -534.47 -534.47	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
9,200.00 9,300.00 9,400.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	9,164.14 9,264.14 9,364.14	44.89 44.89 44.89	-534.40 -534.40 -534.40 -534.40	-534.47 -534.47 -534.47 -534.47	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00
9,500.00 9,600.00	0.00 0.00	0.00 0.00	9,464.14 9,564.14	44.89 44.89	-534.40 -534.40	-534.47 -534.47	0.00 0.00	0.00 0.00	0.00 0.00 0.00
9,700.00	0.00	0.00	9,664.14	44.89	-534.40	-534.47	0.00	0.00	0.00
9,800.00	0.00	0.00	9,764.14	44.89	-534.40	-534.47	0.00	0.00	0.00
9,900.00	0.00	0.00	9,864.14	44.89	-534.40	-534.47	0.00	0.00	0.00
10,000.00	0.00	0.00	9,964.14	44.89	-534.40	-534.47	0.00	0.00	0.00
10,100.00	0.00	0.00	10,064.14	44.89	-534.40	-534.47	0.00	0.00	0.00
10,200.00	0.00	0.00	10,164.14	44.89	<u>-534.40</u>	-534.47	0.00	<u>0.0</u> 0	0.00

Planning Report

TVD Reference:

Database: Company: EDM 5000 14 Multi User MATADOR RESOURCES

Project:

Design:

Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Well: Wellbore: #226H Lateral Plan #2

Eddy County, New Mexico

MD Reference: North Reference: Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

Grid

Survey Calculation Method:

Local Co-ordinate Reference:

Minimum Curvature

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
10,300.00	0.00	0.00	10,264.14	44.89	-534.40	-534.47	0.00	0.00	0.00
10,400.00	0.00	0.00	10,364.14	44.89	-534.40	-534.47	0.00	0.00	0.00
10,412.10	0.00	0.00	10,376.24	44.89	-534.40	-534.47	0.00	0.00	0.00
10,450.00	3.79	90.09	10,414.11	44.88	-533.14	-533.21	10.00	10.00	0.00
10,500.00	8.79	90.09	10,463.79	44.87	-527.67	-527.74	10.00	10.00	0.00
10,550.00	13.79	90.09	10,512.81	44.86	-517.88	-517.95	10.00	10.00	0.00
10,600.00	18.79	90.09	10,560.79	44.84	-503.86	-503.93	10.00	10.00	0.00
10,650.00	23.79	90.09	10,607.36	44.81	-485.71	-485.78	10.00	10.00	0.00
10,700.00	28.79	90.09	10,652.18	44.77	-463.58	-463.65	10.00	10.00	0.00
10,750.00	33.79	90.09	10,694.89	44.73	-437.62	-437.69	10.00	10.00	0.00
10,800.00	38.79	90.09	10,735.18	44.69	-408.03	-408.10	10.00	10.00	0.00
10,850.00	43.79	90.09	10,772.74	44.63	-375.05	-375.12	10.00	10.00	0.00
10,900.00	48.79	90.09	10,807.27	44.58	-338.92	-338.99	10.00	10.00	0.00
10,950.00	53.79	90.09	10,838.53	44.52	-299.91	-299.98	10.00	10.00	0.00
11,000.00	58.79	90.09	10,866.27	44.45	-258.33	-258.40	10.00	10.00	0.00
11,050.00	63.79	90.09	10,890.29	44.38	-214.50	-214.56	10.00	10.00	0.00
11,100.00	68.79	90.09	10,910.39	44.31	-168.73	-168.80	10.00	10.00	0.00
11,150.00	73.79	90.09	10,926.42	44.24	-121.39	-121.46	10.00	10.00	0.00
11,200.00	78.79	90.09	10,938.27	44.16	-72.83	-72.90	10.00	10.00	0.00
11,212.10	80.00	90.09	10,940.49	44.14	-60.93	-61.00	10.00	10.00	0.00
11,250.00	82.27	90.09	10,946.33	44.08	-23.49	-23.56	6.00	6.00	0.00
11,300.00	85.27	90.09	10,951.75	44.00	26.21	26.14	6.00	6.00	0.00
11,350.00	88.27	90.09	10,954.57	43.92	76.12	76.06	6.00	6.00	0.00
11,378.77	90.00	90.09	10,955.00	43.88	104.89	104.82	6.00	6.00	0.00
11,400.00	90.00	90.09	10,955.00	43.84	126.12	126.05	0.00	0.00	0.00
11,500.00	90.00	90.09	10,955.00	43.68	226.12	226.05	0.00	0.00	0.00
11,600.00	90.00	90.09	10,955.00	43.52	326.12	326.05	0.00	0.00	0.00
11,700.00	90.00	90.09	10,955.00	43.35	426.12	426.05	0.00	0.00	0.00
11,800.00	90.00	90.09	10,955.00	43.19	526.12	526.05	0.00	0.00	0.00
11,900.00	90.00	90.09	10,955.00	43.03	626.12	626.05	0.00	0.00	0.00
12,000.00	90.00	90.09	10,955.00	42.87	726.12	726.05	0.00	0.00	0.00
12,100.00	90.00	90.09	10,955.00	42.70	826.12	826.05	0.00	0.00	0.00
12,200.00	90.00	90.09	10,955.00	42.54	926.12	926.05	0.00	0.00	0.00
12,300.00	90.00	90.09	10,955.00	42.38	1,026.12	1,026.05	0.00	0.00	0.00
12,400.00	90.00	90.09	10,955.00	42.22	1,126.12	1,126.05	0.00	0.00	0.00
12,500.00	90.00	90.09	10,955.00	42.05	1,226.12	1,226.05	0.00	0.00	0.00
12,600.00	90.00	90.09	10,955.00	41.89	1,326.12	1,326.05	0.00	0.00	0.00
12,700.00	90.00	90.09	10,955.00	41.73	1,426.12	1,426.05	0.00	0.00	0.00
12,800.00	90.00	90.09	10,955.00	41.57	1,526.12	1,526.05	0.00	0.00	0.00
12,900.00 13,000.00 13,100.00 13,200.00 13,300.00	90.00 90.00 90.00 90.00 90.00	90.09 90.09 90.09 90.09 90.09	10,955.00 10,955.00 10,955.00 10,955.00 10,955.00	41.40 41.24 41.08 40.91 40.75	1,626.12 1,726.12 1,826.12 1,926.12 2,026.12	1,626.05 1,726.05 1,826.05 1,926.05 2,026.05	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
13,400.00 13,500.00 13,600.00 13,700.00 13,800.00	90.00 90.00 90.00 90.00 90.00	90.09 90.09 90.09 90.09 90.09	10,955.00 10,955.00 10,955.00 10,955.00 10,955.00	40.73 40.59 40.43 40.26 40.10 39.94	2,126.12 2,226.12 2,326.12 2,426.12 2,526.12	2,126.05 2,226.05 2,326.05 2,426.05 2,526.05	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00
13,900.00	90.00	90.09	10,955.00	39.78	2,626.12	2,626.05	0.00	0.00	0.00
14,000.00	90.00	90.09	10,955.00	39.61	2,726.12	2,726.05	0.00	0.00	0.00
14,100.00	90.00	90.09	10,955.00	39.45	2,826.12	2,826.05	0.00	0.00	0.00
14,200.00	90.00	90.09	10,955.00	39.29	2,926.12	2,926.05	0.00	0.00	0.00

Planning Report

Database:

EDM 5000 14 Multi User

Company: Project:

MATADOR RESOURCES

Site:

Eddy County, New Mexico Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Well: Wellbore: Design:

#226H Lateral Plan #2 Local Co-ordinate Reference:

TVD Reference:

MD Reference:

North Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

Grid

Survey Calculation Method:

Minimum Curvature

Planned Survey
•

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
14,300:00	90.00	90.09	10,955.00	39.13	3,026.12	3,026.05	0.00	0.00	0.00
14,400.00	90.00	90.09	10,955.00	38.96	3,126.12	3,126.05	0.00	0.00	0.00
14,500.00	90.00	90.09	10,955.00	38.80	3,226.12	3,226.05	0.00	0.00	0.00
14,600.00	90.00	90.09	10,955.00	38.64	3,326.12	3,326.05	0.00	0.00	0.00
14,700.00	90.00	90.09	10,955.00	38.48	3,426.12	3,426.05	0.00	0.00	0.00
14,800.00	90.00	90.09	10,955.00	38.31	3,526.12	3,526.05	0.00	0.00	0.00
14,900.00	90.00	90.09	10,955.00	38.15	3,626.12	3,626.05	0.00	0.00	0.00
15,000.00	90.00	90.09	10,955.00	37.99	3,726.12	3,726.05	0.00	0.00	0.00
15,100.00	90.00	90.09	10,955.00	37.82	3,826.12	3,826.05	0.00	0.00	0.00
15,200.00	90.00	90.09	10,955.00	37.66	3,926.12	3,926.05	0.00	0.00	0.00
15,300.00	90.00	90.09	10.955.00	37.50	4,026.11	4,026.05	0.00	0.00	0.00
15,400.00	90.00	90.09	10,955.00	37.34	4,126.11	4,126.05	0.00	0.00	0.00
15,500.00	90.00	90.09	10,955.00	37.17	4,226.11	4,226.05	0.00	0.00	0.00
15,600.00	90.00	90.09	10,955.00	37.01	4,326.11	4,326.05	0.00	0.00	0.00
15,700.00	90.00	90.09	10,955.00	36.85	4,426.11	4,426.05	0.00	0.00	0.00
15,720.48	90.00	90.09	10,955.00	36.82	4,446.60	4.446.53	0.00	0.00	0.00

PDD

Anticollision Report

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H

0.00 usft

Reference Wellbore Lateral Reference Design: Plan #2 Local Co-ordinate Reference:

TVD Reference:

MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

2.00 sigma

Grid

Output errors are at

Database: Offset TVD Reference: EDM 5000 14 Multi User

Reference Datum

Minimum Curvature

Reference

Plan #2

Filter type:

NO GLOBAL FILTER: Using user defined selection & filtering criteria

Interpolation Method: Stations Depth Range:

Unlimited

Maximum center-center distance of 1,000.00 us

Scan Method: Error Surface:

Error Model:

ISCWSA

Closest Approach 3D Pedal Curve

Results Limited by: Warning Levels Evaluated at:

Casing Method:

Not applied

Survey Tool Program

Date 10/4/2017

2.00 Sigma

From (usft)

Summary

To

(usft) Survey (Wellbore)

Tool Name

Description

0.00

15,720.48 Plan #2 (Lateral)

MWD+HDGM

OWSG MWD + HDGM

	Reference	Offset	Dista	nce		
Site Name Offset Well - Wellbore - Design	Measured Depth (usft)	Measured Depth (usft)	Between Centres (usft)	Between Ellipses (usft)	Separation Factor	Warning
Amethyst State #1 (OFFSET)						
State 1 - Sidetrack - Sidetrack State 1 - Sidetrack - Sidetrack State 1 - Sidetrack - Sidetrack State 1 - Wellbore #1 - Wellbore #1	100.00 600.00 3,500.00 11,785.69	71.90 568.60 3,442.84 10,941.67	609.67 610.71 994.49 331.92	609.42 606.95 969.70 247.24	162.180 40.120 3.920	ES SF CC, ES
State 1 - Wellbore #1 - Wellbore #1	11,800.00	10,942.03	332.23	247.36	3.914	Sr.
Corral Canyon Fed Com Pad (OFFSET) #1H - Original Hole - Original Hole #2H - Original Hole - Original Hole #3H - Original Hole - Original Hole #4H - Wellbore #1 - Wellbore #1						Out of range Out of range Out of range Out of range
Emerald State Com #1 (OFFSET)						
Com #1 - Original Hole - Original Hole Com #1 - Original Hole - Original Hole Com #1 - Original Hole - Original Hole	333.65 500.00 1,300.00	331.17 492.28 1,271.24	916.27 916.70 988.81	914.30 913.55 980.07	463.813 291.011 113.112	ES
Garrett Fed Com #202H, #222H, #122H, #206H, #226H						
#122H - Lateral - Plan #1 #122H - Lateral - Plan #1 #122H - Lateral - Plan #1	600.00 700.00 8.000.00	600.00 699.21 7.996.94	60.08 60.63 332.16	56.24 56.09 273.81	15.643 13.344 5.692	ES
#202H - Lateral - Plan #1 #202H - Lateral - Plan #1	600.00 9.600.00	600.00 9,594.12	120.01 664.16	116.17 594.58		CC, ES
#206H - Lateral - Plan #2	600.00	600.00	29.97	26.13	7.804	
#206H - Lateral - Plan #2 #206H - Lateral - Plan #2	700.00	699.79	30.21	25.66	6.648	
#200H - Lateral - Plan #2 #222H - Lateral - Plan #2	9,456.06 600.00	9,458.42 600.00	128.36 90.01	60.07 86.17	1.880 23.433	CC. ES
#222H - Lateral - Plan #2	15,720.48	15,711.79	660.33	375.44	2.318	

Offset D	Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State 1 - Sidetrack - Sidetrack - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Sidetrack - Offset Design Amethyst State #1 (OFFSET) - Offset Design Amethyst State #1 (OFFSET) - Offset Design Amethyst State #1 (OFFSET) - Offset State #1													
Survey Pro	gram: 10	0-MWD STAN	IDARD										Offset Well Error:	0.00 usft
Refer	rence	Offs	et	Semi Majo	r Axis									
Measured	Vertical	Measured	Vertical	Reference	Offset	Highside	Highside Offset Wellbore Centre		Between	Between	Minimum	Separation	Warning	
Depth	Depth	Depth	Depth			Toolface	+N/-S	+E/-W	Centres	Ellipses	Separation	Factor	_	
(usft)	(usfl)	(usft)	(usft)	(usft)	(usft)	(*)	(usft)	(usft)	(usfl)	(usft)	(usft)			

Anticollision Report

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H, #206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Design: Plan #2

Reference Wellbore Lateral

Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference: MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Survey Pro	ogram: 100	HMWD STAN	DARD										Offset Well Error:	0.00 us
Refer	rence	Offs	et	Semi Major	Axis				Dist	ance				0.00
leasured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (*)	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
0.00	0.00	0.00	27.50	0.00	0.00	36.26	491.60	360.54	610.26					
100.00	100.00	71.90	99,40	0.13	0.13	36.25	491.66	360.51	609.67	609.42	0.26	2,371.357 C	c	
200.00	200.00	171,89	199.39	0.49	0.44	36.23	491.86	360.44	609.79	608.87	0.92	660.270		
300.00	300.00	271,91	299.41	0.85	0.79	36.22	492,01	360.39	609.88	608.24	1.64	372.076		
400.00	400.00	370.81	398.31	1.20	1.15	36.22	492.15	360.47	610.04	607.70	2.35	259.707		
500.00	500.00	471.00	498.50	1.56	1.50	36,22	492.37	360.68	610.35	607.28	3.06	199.352		
600.00	600.00	568.60	596.10	1.92	1,85	36.23	492.59	360.98	610.71	606.95	3.77	162.180 E	s	
700.00	699.99	685.26	692.75	2.27	2.19	121.53	493.21	361.64	612.32	607.86	4.46	137,262	•	
800.00	799.91	760.56	788.04	2.62	2.53	121,79	494.31	362,58	615.89	610.74	5.15	119.607		
900.00	899.69	856.95	884.40	2.97	2.88	122.19	496.19	363.71	621.63	615.78	5.85	106.321		
1,000.00	999.27	955.21	982.63	3.33	3.23	122.76	498.43	364.94	629.13	622.58	6.56	95.962		
1,100.00	1,098.57	1,053.40	1,080.79	3.70	3.58	123.48	500.78	366.26	638.30	631.03	7.27	87.790		
1,134.94	1,133.20	1,087.56	1,114.93	3.83	3.70	123.46	501.63	366.74	641.91		7.52	85.338		
1,134,54	1,197.62	1,148.73	1,176.08	4.08	3.92	124.36	503.39	367.53	649.02	641.04	7.98	81.329		
1,300.00		1,243.75	1,271.01	4.46	4.26	125.15	507.33	368.28	660.72	652.03	8.69	76.034		
1,400.00		1,334.72	1,361.84	4.85	4.59	125.77	512.26	368.36	673.06	663,67	9 39	71.714		
	*													
1,500.00	1,494.68	1,417.64	1,444.55	5.24	4 89	126.32	518.08	369.57	687.55	677.51	10.05	68.436		
1,600.00	1,593.70	1,504.61	1,531.18	5.63	5.21	126.91	525.13	372.28	704 02	693 30	10.72	65.653		
1,700.00	1,692.72	1,594.64	1,620.78	6.03	5.54	127.53	533.00	376.27	721.93	710.51	11.41	63.255		
1,800.00	1,791.74	1,689.88	1,715.50	6.42	5.90	128.19	541.60	381.25	740.68	728.55	12.13	61.072		
1,900.00	1,890.76	1,784.16	1.809 24	6.82	6.25	128.83	550.15	386.66	759.90	747.06	12.84	59.189		
2,000.00	1,989.78	1,878.07	1,902.57	7.22	6.61	129.51	558.38	392.97	779.69	766.14	13.55	57.558		
2,100.00	2,088.80	1,985.63	2,009.51	7.62	7.02	130.34	566.69	401.00	799.42	785.09	14.32	55.808		
2,200.00	2,187.83	2,098.55	2,121.97	8.02	7.44	131.18	573.94	408.11	817.55	802.42	15,13	54.042		
2,300.00	2,286.85	2,200.24	2,223.35	8.42	7.82	131.89	579.74	413.58	834.66	818.78	15.88	52.577		
2,400.00	2,385.87	2,293.73	2,316,55	8.82	8.17	132.55	584.76	418.97	851.94	835.36	16.58	51.381		
2,500.00	2,484.89	2,390.97	2,413.45	9.23	8.53	133.30	589.29	425.58	869.66	852.35	17.30	50.262		
2,600.00	2,583.91	2,506.64	2.528.76	9.63	8.95	134.28	592.41	434.03	886.65	868.54	18,11	48.959		
2,700.00	2,682.93	2,626.46	2.648.36	10.04	9.38	135.32	593.02	441.38	901.57	882.64	18.93	47.639		
2.800.00	2,781.95	2,744.49	2,766.30	10.44	9.79	136.25	592.50	445.84	914.26	894.54	19.72	46 356		
2,900.00	2,880.97	2,851.34	2,873.13	10.84	10,16	136.99	592.01	447.78	925.58	905.11	20.47	45.213		
0.000.00	2.979.99	2 040 05	0.074.70		40.40									
3,000.00		2,949,95	2,971.73	11.25	10.49	137.64	591.61	449.07	936.69	915,50	21 19	44,206		
3,100 00	3,079.01	3,048.09	3,069.86	11.65	10.83	138.26	591.40	450.43	948.08	926.17	21 91	43.279		
3,200.00	3,178.03	3,147 43	3,169.19	12.06	11.18	138.86	591.30	451.63	959.50	936.87	22.63	42.400		
3,300.00	3,277.06	3,246 14	3,267.90	12,47	11.52	139.46	591.13	452.91	971.05	947.70	23.35	41,587		
3,400.00	3,376.08	3,344.78	3,366.53	12.87	11.86	140.04	590.91	454.19	982.68	958.61	24.07	40.827	•	
3,500.00	3,475.10	3,442.84	3,464.58	13.28	12,21	140.59	590.84	455,47	994.49	969.70	24.79	40.120 S	c	

Anticollision Report

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Wellbore Lateral Reference Design: Plan #2 Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference: MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Offset D	esian	Ameth	yst State	#1 (OFFS	ET) - St	ate 1 - We	llbore #1 - W	ellbore #1			•		Offset Site Error:	0.00 usft
		HWD STAI		•	,								Offset Well Error:	0.00 usft
Refer	rence	Offs	set	Semi Major	Axis				Dist	ance				
Measured		Measured	Vertical	Reference	Offset	Highside	Offset Wellbo		Between	Between		Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (*)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
1										,,	(,			
100.00	0.00 100.00	0.00 72.19	27.50 99.69	0.00 0.13	0.00 0.13	36.26 36.25	491.60 491.62	360.54 360.54	610.26 609.66	609.40	0.26	2,365.590		
200.00	200.00	171.76	199.26	0.49	0.13	36.25	491.73	360.54	609.74	608.95	0.79			
300.00	300.00	271.34	298.84	0.85	0.49	36.24	491.92	360.54	609.90		1.33	458.047		
400.00	400.00	370.91	398.41	1.20	0.66	36.22	492.20	360.54	610.12		1.87	326.546		
500.00	500.00	470.48	497.98	1.56	0.84	36.20	492.57	360.54	610.42	608.01	2.41	253.779		
600.00	600.00	569.39	596.89	4.00	1.14	26.24	402.93	360 85	610 82	607.76	3.06	199.676		
600.00 700.00	699.99	670.01	697.49	1 92 2.27	1.49	36.21 121.61	492.83 492.53	362.12	612 02		3.76	162.683		
800.00	799.91	771.40	798.87	2.62	1.85	122.05	491,79	363.60	614.38	609.91	4.46	137.612		
900.00	899.69	872.58	900.03	2.97	2.20	122.71	490.63	365,23	617.94	612.77	5.17	119,499		
1,000.00	999.27	973.45		3.33	2.55	123.58	489.04	366.99	622.80	616.92	5.88	105.889		
1,100.00		1,073.94		3.70	2.91	124.65	487.04	368.90	629 07	622.48	6.60	95.365		
1,134.94 1,200.00	1,133.20 1,197.62	1,108.95 1,173.70		3.83 4.08	3.03 3.26	125.07 125.94	486.25 484.54	369.60 371.08	631.62 636.60		6.85 7.32	92.235 86.938		
1,200.00		1,273.04		4.46	3.62	127.32	481.27	371.00	644.42		8.05	80.033		
1,400.00		1,372.07		4.85	3.98	128.75	477.23	377.43	652.51		8.78	74.295		
1,500.00		1,470.78	-	5.24	4.34	130.23	472.44	381.60	660.94	651.43	9.51	69.474		
1,600.00 1,700.00	1,593.70	1,569.13		5.63	4.69 4.95	131,75 132,81	466.90	386.41	669.76 680.48	659.52 669.62	10.24 10.86	65.385 62.669		
1,800.00	1,692.72 1,791.74	1,638.89 1,722.82		6.03 6.42	5.25	133.81	463.58 464.48	390.41 396.63	696.18	684.66	11.52	60.421		
1,900.00	1,890.76	1,822.33		6.82		135.11	463.55	404.73	711.62	699.37	12.26	58.059		
1,202,000														
2,000.00	1,989.78	1,906.56		7.22	5.93	136.12	463.79	411.88	728.45	715.53	12.92	56.401		
2,100.00	2,088.80	2,001.91		7.62	6.27	136.94	467.79	418.85	746.91		13.62	54.839		
2,200.00 2,300.00	2,187.83 2,286.85	2,107.72	2,132.53 2,239.52	8.02 8.42	6.66 7.06	137.93 139.06	470.55 470.56	427.32 435.97	765.19 782.17	750.81 767.01	14.38 15.15	53.209 51.618		
2,400.00			2,335.48	8.82	7.41	140.04	470.17	443.37	798.88	783.01	15.87	50.338		
2,500.00		2,459.81		9.23	7.96	141.61	465.84	452.83	813.62	796.79	16.82	48,359		
2,600.00	2,583.91	2,568.36 2,667.75	2,591.91	9.63	8.34 8,68	142.74 143.50	459.68 456.83	455.68 456.32	823.78	806.21	17.57 18.29	46,875 45,611		
2,700.00 2,800.00		2,767.81		10.04 10.44	9.02	144.03	456 82 456.83	455.09	834.01 844.27	815.73 825.27	19.00	44,430		ļ
2,900.00	2,880.97	2,865.78		10.84	9.35	144.38	458.76	452.72	854.56	834.85	19.71	43.356		
3,000.00		2,962.73		11.25	9.68	144.76	460,18	450.94	865.13	844.72	20.41	42.382		
3,100.00	3,079.01	3,059.51		11.65	10.01	145.19	461.00	449.82	876 02	854.91	21,11	41,490		
3,200.00 3,300.00	3,178.03 3,277.06	3,156,11 3,338,64		12.06 12.47	10.34 10.96	145.66 146.17	461.20 460.87	449,36 449,49	887.25 898.79	865.43 875.98	21.81 22.81	40.675 39.404		1
3,400.00		3,350.24		12.47	11.00	146,73	459.88	450.32	910.72	887.50	23.22	39.221		ł
-,														
3,500.00		3,449,13		13.28	11.35	147.29	458.89	451.15	922.74	898.80	23.94	38.543		
3,600.00	3,574.12	3,548.01		13.68	11.70	147.83	457.90	451.98	934.83	910.17	24.66	37.909		
3,700.00	3,673.14	3,646.89		14.09	12.05	148.35	456.91	452.81	947.01	921.63	25.38	37.314		
3,800.00	3,772.16	3,745.78	3,769.14	14.50	12.40	148.86	455.92	453.65	959.27	933.17	26.10	36.754		
3,900.00	3,871 18	3,844.87	3,868 22	14 90	12 75	149.36	454.94	454.47	971.59	944.77	26.82	36.227		
4,000.00	3,970.20	3,944.20	3,967.55	15.31	13.11	149.84	454.08	455.19	983.95	956.41	27.54	35.726		
	4,069.22		4,066.92	15.72	13.46	150.30	453.34	455.81	996.32	968.06	28.26	35.251		
	10,694.89		10,689.89	38.43	36.82	-22.91	375 57	505,77	999 73	925.21	74.52	13.416		
	10,735.18		10,716.30	38.57	36.91	-24.68	375.95	506.06	972.45	897.76	74.69	13.019		1
10,850.00	10,772.74	10,727.10	10,748 39	38.71	37.02	-27.03	376.38	506.79	942.49	867.60	74.89	12.585		
10.900.00	10,807.27	10,762 74	10.784.02	38.87	37.15	-30.13	376 83	507.60	909.69	834.58	75.11	12.112		
	10,838.53			39.04	37.27	-34.04	377.06	508.41	874.31	798.99	75.32	11.608		
•	10,866.27			39.24	37.37	-38.91	377.02	509,19	836,68	761 17	75.51			
		10,852.64		39.46	37.47	-44.92	376.78	509.91	797.20	721.50	75.70	10.531		
11,100 00	10,910.39	10,875.09	10,896.32	39.72	37.55	-52.18	376.45	510.56	756.27	680.38	75.88	9.966		
								·						

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Wellbore Lateral Reference Design: Plan #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference:

Offset D		Ameth ∧ATS GWM⊢		#1 (OFFS	E⊺) - St	ate 1 - We	libore #1 - W	ellbore #1					Offset Site Error: Offset Well Error:	0.00 ust
Refer	_	Offs		Semi Major	Axis				Dist	ance		,	Unset Well Error:	U.00 US
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (*)	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
11,150.00	10,926.42	10,894.00	10,915.22	40.01	37.62	-60.65	376.08	511.10	714.35	638.27	76 08	9 390		
11,200.00	10,938.27	10,908.32	10,929.53	40.34	37.67	-69.84	375.79	511.50	671.93	595.65	76.28	8 809		
11,212.10	10,940.49	10,911.08	10,932.29	40.43	37.68	-72.10	375.73	511.57	661.65	585.32	76.33	8 668		
11,250.00	10,946.33	10,918.45	10,939.66	40.71	37.70	-76.71	375.57	511.77	629.63	553.12	76 51	8 229		
11,300.00	10,951.75	10,925.66	10,946.86	41.12	37.73	-82.31	375.41	511.95	588.05	511 26	76.78	7.658		
11,350.00	10,954.57	10,930.02	10.951.22	41.56	37.75	-87.16	375.32	512.06	547.61	470.48	77.13	7.100		
11,378.77	10,955.00	10,931.25	10,952.45	41.83	37.75	-89.56	375.29	512.09	525.03	447.67	77.36	6 787		
11,400.00	10,955.00	10,931.82	10,953.02	42.03	37.75	-89.66	375.27	512.10	508 76	431.21	77.55	6.560		
11,500.00	10,955.00	10,934.44	10,955.64	43.10	37.76	-90.11	375.21	512.17	437.88	359.08	78.80	5.557		
11,600.00	10,955.00	10,937.01	10,958.21	44.33	37 77	-90.55	375.15	512.23	380.31	299.62	80.68	4.714		
11,700.00	10,955.00	10,939.54	10,960.74	45.70	37 78	-90.99	375.10	512.29	342.80	259.80	83.00	4.130		
11,785.69	10,955.00	10,941.67	10,962.87	46.99	37 79	-91.36	375.04	512.35	331,92	247.24	84.68	3.920 C	C. ES	
11,800.00	10,955,00	10,942.03	10,963.22	47.21	37.79	-91.42	375.04	512.35	332.23	247.36	84.87	3.914 SF	:	
11,900.00	10,955.00	10,944.47	10,965.66	48.83	37.80	-91.84	374.98	512.41	351.05	265.60	85.44	4.108		
12,000.00	10,955.00	10,946.86	10,968.06	50.56	37.81	-92.25	374.92	512.47	395.07	310.21	84.85	4.656		
12,100.00	10.955.00	10,949.22	10,970.41	52.38	37.81	-92.66	374.86	512.52	457.07	373.26	83.81	5.454		
12,200.00	10,955.00	10,951.53	10,972.72	54.29	37.82	-93.06	374,81	512.58	530.78	448.02	82,76	6.413		
12,300.00	10,955.00	10,953.81	10.975.00	56.29	37.83	-93.45	374.75	512.63	612.00	530.11	81.89	7.474		
12,400 00	10,955.00	10,956.05	10,977.23	58.35	37.84	-93.84	374.70	512.68	698.10	616.91	81.19	8.598		
12,500.00	10,955.00	10,958.25	10,979.43	60.47	37.85	-94.22	374.64	512 73	787.49	706.84	80.64	9.765		
12,600.00	10,955.00	10,960.41	10,981.59	62.65	37.86	-94 59	374 59	512.78	879.16	798.95	80.21	10 961		
12,700.00	10,955.00	10,962.54	10,983.72	64.89	37.86	-94.95	374.53	512.83	972.46	892.60	79.87	12.176		

PDD

Anticollision Report

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Wellbore Lateral Reference Design:

Plan #2

Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference:

2920+28.50 @ 2948.50usft (Patterson 282)

MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Output errors are at Database:

Minimum Curvature

2.00 sigma

EDM 5000 14 Multi User

Offset TVD Reference:

Refer	ence	NATS GWM- efiO		Semi Major	Axis				Dista	ance			Offset Well Error:	0.00 us
leasured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)		Between	Minimum Separation (usft)	Separation Factor	Warning	
0.00	0.00	0.00	2.50	0.00	0.00	66.48	365.72	840.49	916.62					
100,00	100.00	97.75	100.25	0.13	0.18	66.51	365.35	840.64	916.60	916,30	0.30	3,019 133		
200.00	200.00	199.88	202.38	0.49	0.54	66.58	364.28	840.94	916.46	915.43	1.02	894.271		
300.00	300.00	298.30	300.79	0.85	0.89	66.65	363.13	841.26	916.29	914.55	1,74	527.570		
333.65	333.65	331.17	333.65	0.97	1.01	66.68	362.78	841.40	916.27	914.30	1.98	463.813 C	С	
400.00	400.00	395.94	398.42	1.20	1.24	66.73	361.94	841.82	916.33	913.88	2.45	374.611		
500.00	500 00	492.28	494.74	1.56	1.59	66.83	360.74	842.72	916.70	913.55	3.15	291.011E	S	
600.00	600.00	585.73	588.19	1.92	1.92	66.90	360.03	843.96	917.62	913.78	3.84	239.013		
700.00	699.99	678.89	681.33	2.27	2.25	152.16	359.88	845.70	920.43	915.91	4.52	203,648		
800.00	799.91	774.82	777.23	2.62	2.59	152.27	360.12	847.97	926.18	920.97	5.21	177.923		
900.00	899.69	872.08	874.45	2.97	2.93	152.45	360.37	850.59	934.55	928.65	5.90	158.388		
1,000.00	999.27	969.25	971.59	3 33	3.27	152.66	360.81	853.37	945.49	938.89	6.60	143.296		
1,100.00	1,098.57	1,067.25	1,069.54	3 70	3.62	152.90	361.74	856.16	958.93	951.63	7.30	131.342		
1,134.94	1,133.20	1,101.74	1,104.01	3.83	3,74	153.00	362.05	857.16	964.20	956.65	7.55	127.709		
1,200.00	1,197.62	1,172.03	1,174.28	4.08	3.99	153.27	362.58	859.00	974.07	966.03	8.03	121.275		
1,300.00	1,296.64	1,271.24	1.273.46	4.46	4.35	153.65	363.22	861.15	988.81	980.07	8.74	113,112 SF	=	

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Design: Plan #2

Reference Wellbore Lateral

North Reference: **Survey Calculation Method:**

Local Co-ordinate Reference:

Output errors are at

TVD Reference:

MD Reference:

Database:

Minimum Curvature

2.00 sigma

EDM 5000 14 Multi User

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

Reference Datum Offset TVD Reference:

Offse	t Design	Garret	t Fed Co	m #202H, #	#222H, #	#122H, #20	06H, #226H -	#122H - I	_ateral - F	lan #1			Offset Site Error:	0.00 usft
	Program: 0-1												Offset Well Error:	0.00 usft
	eference ed Vertical	Offs Measured	set Vertical	Semi Major Reference		Highside	Offset Wellbo	ro Contro		ence	Minimum	Separation		
Depth (usft)	Depth	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (*)	+N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Ellipses (usft)	Separation (usft)	Factor	Warning	
0	.00 0.00	0.00	0.00	0.00	0.00	-0.04	60.08	-0.04	60.08					
100			100.00	0.13	0.00	-0.04	60.08	-0.04	60.08	59.83	0.26	234.421		
200			200.00	0,49	0.49	-0.04	60.08	-0.04	60.08	59.11	0.97	61.735		
300	.00 300.00	300.00	300.00	0.85	0.85	-0.04	60.08	-0.04	60.08	58.39	1.69	35.549		
400	.00 400.00	400.00	400.00	1.20	1.20	-0.04	60.08	-0.04	60.08	57.68	2.41	24.961		
500	.00 500.00	500.00	500.00	1.56	1.56	-0.04	60,08	-0.04	60.08	56.96	3.12	19.233		
600	.00 600.00	600.00	600.00	1.92	1.92	-0.04	60.08	-0.04	60.08	56.24	3.84	15.643 C	:C	
700			699.19	2.27	2.27	85.32	60.74	-1.15	60.63	56.09	4.54	13.344 E	S	
800			798.30	2.62	2.62	85.80	62.69	-4.49	62.28	57.04	5.24	11.883		
900			897.24	2.97	2.98	86.54	65.95	-10.03	65.03	59.08	5.95	10.936		
1,000	.00 999.27	996.63	995.92	3.33	3.34	87.47	70,50	-17,79	68.90	62.24	6.66	10.342		
1,100			1,094.25	3 70	3.70	88.52	76.34	-27.74	73.89	66.50	7.39	9.997		
1,134			1,128.49	3.83	3.85	88.90	78.68	-31.72	75.90	68.23	7.67	9.894		
1,200			1,192.80	4.08	4.11	89.61	83.26	-39.51	79.80	71.63	8.18	9.759		
1,300			1,291.63	4.46 4.85	4.49	90.58	90.29	-51.49	85.82	76.88	8.94	9.599		
1,400.	.00 1,395.66	1,405.25	1,390.47	4.85	4.88	91.41	97.32	-63,46	91.86	82.15	9.71	9.458		
1,500.		•	1,489.31	5.24	5.27	92.15	104.35	-75,43	97.92	87.43	10.49	9.334		
1,600.			1,588,15	5.63	5.66	92.80	111.38	-87.41	103.99	92.71	11.27	9.225		
1,700.			1,686.99	6.03	6.06	93.37	118.41	-99.38	110.07	98.01		9.128		
1,800.			1,785.83	6.42	6.45	93.89	125.44	-111.35	116.16	103.31		9.041		
1,900.	00 1,890.76	1,906.21	1,884.67	6.82	6.85	94.35	132.47	-123.32	122.26	108.62	13.64	8.963		
2,000.		2,006.40	1,983.50	7.22	7.25	94.77	139.50	-135.30	128.37	113.93	14.43	8.893		
2,100.			2,082.34	7.62	7.65	95.16	146.53	-147.27	134.48	119.25	15.23	8.830		
2,200.	-		2,181.18	8.02	8.05	95.50	153.56	-159.24	140.60	124.57	16.03	8.772		
2,300.			2,280.02	8.42	8.45 8.79	95.82	160.59	-171.22	146.72	129.90	16.83	8.7.19		
2,400.	VU 2,305.87	2,392.84	2,378.86	8.82	0.79	96.12	167.61	-183,19	152.85	135.28	17.57	8.699		
2,500.			2,477.70	9.23	9.25	96.39	174.64	-195.16	158.98	140.55	18.43	8.627		
2,600.			2,576.54	9.63	9 65	96 64	181.67	-207.14	165.12	145.89	19,23	8.586		
2,700.			2,675,38	10,04	10.06	96,88	188,70	-219.11	171.26	151.22		8.549		
2,800.			2,774.21	10.44	10.46	97.09	195.73	-231.08	177.40	156.56	20.84	8.514		
2,900.	00 2,880.97	2,891.88	2,873.05	10.84	10.80	97.30	202.76	-243,06	183.54	161.96	21.58	8.507		
3,000.		3,008.31	2,971.89	11.25	11.27	97.48	209.79	-255.03	189.68	167.24	22.45	8.451		ľ
3,100.			3,070.73	11.65	11.67	97.66	216.82	-267.00	195.83	172.58	23.25	8.423		
3,200.			3,169.57	12.06	12.07	97.83	223.85	-278.98	201.98	177.92	24.06	8.396		
3,300. 3,400.			3,268.41 3,367.25	12.47 12.87	12.40 12.88	97.99 98.13	230.88 237.91	-290.95 -302.92	208.13 214.28	183.34 188.61	24.79 25.67	8.396 8.348		İ
								-302,32	214.20	100.01		0.340		1
3,500.			3,466.08	13.28	13.28	98.27	244.94	-314.90	220.44	193.96	26.47	8.326		1
3,600.			3,564.92	13.68	13.69	98.41	251 97	-326.87	226.59	199.31		8.306		-
3,700.		3,709 64 3,809 84	3,663.76	14.09	14.09	98.53 98.65	259 00	-338.84 -350.83	232.75	204.66	28.09	8 286		1
	00 3,772.16 00 3,871.18		3,762.60 3,861.44	14.50 14.90	14.50 14.82	98 65 98.76	266.03 273.06	-350,82 -362.79	238.90 245.06	210.01 215.44	28 90 29.62	8.268 8.273		
												J.21 J		
1	00 3,970.20		3,960.28	15.31	15.23	98.87	280 09	-374.76	251.22	220.79	30.43	8.256		
	00 4.069.22		4,059.12	15.72	15.63	98.97	287 12	-386.73	257.38	226.14	31.23	8.240		
	00 4,168,24	4,189.40	4,157.96	16.12	16.03	99 07	294.15	-398.71	263.54	231.50	32 04	8.225		ļ
4,300. 4,400.			4,256.79 4,355.63	16.53 16.94	16.44 16.84	99.16 99.25	301.18 308.21	-410.68 -422.65	269.70	236.85	32.85	8.211		}
4,400.	uu 4,300.29	4.309.02	4,333.03	16.94	16.84	99 25	308 21	-422.65	275.86	242.20	33.65	8.197		ľ
4,440.		4,429.86	4,396.08	17.10	17.01	99 29	311.09	-427.55	278.38	244.40	33.98	8.191		
4,500.		4,488.83	4,454.48	17.34	17.24	99.30	315.24	-434.63	281.95	247.49	34,46	8.182		
4,600.		4,588.64	4,553.31	17.73	17.65	98.90	322.27	-446.60	287.66	252.41	35.25	8.161		
4,700.		4,688.37	4,652.07	18.11	18.05	98.02	329.29	-458:56 470.51	293.02	256.99	36.02	8.134		
4,800.	00 4,764.20	4,787.96	4,750.70	18.46	18.45	96.67	336.31	-470,51	298,14	261,36	36,78	8,106		

PDD

Anticollision Report

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H

Reference Design: Plan #2

Reference Wellbore Lateral

0.00 usft

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature 2.00 sigma

Output errors are at

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Offset D	esign	Garret	t Fed Cor	n #202H, #	‡222H,	#122H, #20	6H, #226H -	#122H - I	Lateral - F	lan #1			Offset Site Error:	0 00 usft
	-	TWD+HDGM											Offset Well Error:	0.00 usft
Refer		Offs Measured	et Vertical	Semi Major Reference		Highside	Offset Wellbo	C	Dist			C		
Depth	Depth	Depth	Depth	Reference	Onset	Toolface	+N/-S	+E/-W	Between Centres	Between Ellipses	Minimum Separation	Separation Factor	Warning	
(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	(*)	(usft)	(usft)	(usft)	(usft)	(usft)			
4,900.00	4,864,14	4,887.35	4,849.12	18.81	18.86	94.88	343.31	-482.43	303.22	265.71	37.51	8.083		
4,975.86	4,940.00	4,962.56	4,923.60	19.06	19.16	8.05	348.61	-491.46	307.18	269.13	38.05	8.072		
5,000.00	4,964.14	4,986.47	4,947.27	19.14	19.26	7.48	350.29	-494.32	308.48	270.26	38.22	8.071		
5,100.00		5,086.11	131	19.45	19.66	5.15	357.29	-506.24	314.20	275.28				
5,200.00	5,164.14	5,189.19	5,148.27	19.78	20.07	3.12	363.61	-517.02	319.60	279.98	39.62			
5,300.00	5,264.14	5,292.87	5,251.48	20.10	20.46	1.58	368.56	-525.45	324.05	283.73	40.32	8.038		
5,400.00	5,364.14	5,397.01	5,355 39	20.42	20.84	0.51	372.11	-531.48	327.35	286.35	41.00	7.984		
5,500.00	5,464.14	5,501.46	5,459.74	20.74	21.20	-0.12	374.22	-535.07	329.36	287.69	41.67	7.904		
5,600.00	5,564.14	5,606.05	5,564.33	21.07	21,55	-0.31	374.88	-536.21	330.00	287.67	42.33	7.796		
5,607.06	5,571.20	5,613.44	5,571.71	21.09	21.57	-0.31	374.87	-536.19	329.99	287.62	42.38	7.787		
5,700.00	5,664.14	5,705.86	5,664.14	21.40	21.87	-0.31	374.88	-536.21	330.00	287.02	42.98	7.677		
5,800.00	5,764.14	5,805.86	5,764.14	21,72	22 19	-0.31	374.88	-536.21	330.00	286.36	43.64	7.562		
5,900.00	5,864.14	5,905 86	5,864.14	22.05	22.52	-0.31	374.88	-536.21	330.00	285.70	44.30	7.450		
6,000.00	5,964.14	6,005.86	5,964.14	22.38	22.84	-0.31	374.88	-536.21	330.00	285.05	44.96	7.341		
6,100.00	6,064.14	6,105.86	6,064.14	22.71	23.17	-0.31	374.88	-536.21	330.00	284.38	45.62	7.234		
6,200.00	6,164.14	6,205.86	6,164.14	23.04	23.50	-0.31	374.88	-536.21	330.00	283.72	46.28	7.130		
6,300,00	6,264,14	6,305.86	6.264.14	23.38	23.83	-0 31	374.88	-536.21	330.00	283.06	46.95	7.030		
6,400.00	6,364.14	6,405.86	6,364,14	23.71	24.16	-0.31	374.88	-536.21	330.00	282.39	47.61	6.931		
6,500.00	6,464.14	6,505.86	6,464.14	24 04	24.49	-0.31	374.88	-536.21	330.00	281.72	48 28	6.835	•	
6,600.00	6,564.14	6,605.86	6,564.14	24.38	24.82	-0.31	374.88	-536.21	330.00	281.05	48.95	6.742		
6,700.00	6,664,14	6,705.86	6,664.14	24.71	25.15	-0.31	374.88	-536.21	330.00	280.38	49.62	6.651		
6,800.00	6,764.14	6,805.86	6,764.14	25.05	25.49	-0.31	374.88	-536,21	330.00	279.71	50.29	6.562		
6,900.00	6,864.14	6,905.86	6,864.14	25,38	25.82	-0.31	374.88	-536.21	330.00	279.04	50.96	6.475		
7,000.00	6,964.14	7,005.86	6,964.14	25.72	26.15	-0.31	374.88	-536.21	330.00	278.37	51.64	6.391		
7,100.00	7,064.14	7,105.86	7,064.14	26.06	26.49	-0.31	374.88	-536.21	330.00	277.69	52.31	6.308		
7,200.00	7,164.14	7,205.86	7,164.14	26.39	26.83	-0.31	374.88	-536.21	330,00	277.01	52.99	6.228		
7,300.00	7,264,14	7,305.86	7,264.14	26.73	27.16	-0.31	374 88	-536.21	330.00	276.34	53 66	6,149		
7,400.00	7,364.14	7,405.86	7,364.14	27.07	27.50	-0.31	374 88	-536.21	330.00	275.66	54.34	6.073		
7,500.00	7,464.14	7,505.86	7,464.14	27.41	27.84	-0.31	374.88	-536.21	330.00	274.98	55.02	5.998		
7,600.00	7,564.14	7,605.86	7,564.14	27.75	28.17	-0.31	374.88	-536.21	330.00	274.30	55 70	5.924		
7,700.00	7,664.14	7,705.86	7.664.14	28,09	28.51	-0.31	374 88	-536.21	330.00	273.62	56.38	5.853		
7,800.00	7,764.14	7,805.93	7,764.20	28.43	28.85	-0.26	374.88	-535.92	330.00	272.94	57.06	5.783		
7,833.69	7,797.83		7,797.83	28.55	28.95	0.09	374.88	-533,86	329.99	272.71	57.00	5.760		
7,900.00	7.864.14	7,904.70	7.862.16	28.77	29.13	1.75	374.86	-524 32	330.14	272.41	57 73	5.719		
8,000.00	7,964.14	7,996.94		29.11	29.37	6.22	374.82	-498.45	332.16	273.81	58.36	5.692 \$	iF.	
8,100.00	8,064.14	8,079.15	8,025.02	29.46	29.57	12.10	374.76	-463.70	339.63	280.94	58.69	5.787		ļ
8,200.00	8,164.14	8,150.00	8,084.62	29.80	29 73	18 28	374.70	-425.46	356.33	298.01	58.32	6.110		
8,300.00	8,264.14	8,130.00 8,210.15	8,131.19	30.14	29.88	24.02	374.70 374.64	-425.46 -387.44	384.72	327.71	58.32 57.01	6.110		
8,400.00	8,364.14	8,260.64	8,167 03	30.49	30.01	28 97	374.54 374.58	-351.90	425.27	370 39	54 88	7 749		
8,500.00	8,464.14	B.300.00	8,192.72	30.83	30.13	32.78	374.53	-322.08	476.88	424.66	52.23	9.131		
8,600.00	8,564 14	8,338 81	8,215.98	31.17	30.27	36.44	374.48	291.03	537.66	487.89	49.77	10.802		
. 700 00	0.00	0.000 - 7	B 000 07	s	ac									į
8,700.00	8,664.14	8,369.15	8,232.67	31.52	30.39	39.19	374.44	-265.70	605.78	558.39	47.40	12.781		
8,800.00	8,764.14	8,400.00 8,417.30	8,248.24	31.86	30.53	41.87	374 40	-239,07	679.67	634.19	45.48	14.943		į
8,900.00 9,000.00	8,864 14 8,964.14	8,417.39	8,256.38	32.21	30.62	43.32	374.38	-223.70	757.94	714.37	43.57	17.397		
9,000.00	9,064.14	8,436.76 8,450.00	8,264.89 8,270.37	32.55 32.90	30.72 30.79	44.88 45 92	374.35 374.33	-206.30 -194.25	839.73	797.61	42.11 40.83	19.940		1
3, 100.00	3,004 14	3,430.00	0,21031	32.30	30 79	40 32	3/4.33	-134.23	924.29	883.45	40.83	22.636		
													-	

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error:

0.00 usft

Reference Well: Well Error:

Reference Design: Plan #2

#226H 0.00 usft

Reference Wellbore Lateral

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

	esign oram: 0-M	IWD+HDGM		m #202H, #			,	20211-1		iuii ir i			Offset Site Error:	0 00 us
Refer	ence	Offs		Semi Major					Dist	ance			Offset Well Error:	0.00 us
easured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (*)	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
0.00	0.00	0.00	0.00	0.00	0.00	0.00	120.01	0.00	120.01					
100.00	100.00	100.00	100.00	0.13	0.13	0.00	120.01	0.00	120.01	119.75	0.26	468.213		
200.00	200.00	200.00	200.00	0.49	0,49	0.00	120.01	0.00	120.01	119.03	0.97	123.305		
300.00	300.00	300.00	300.00	0.85	0.85	0.00	120.01	0.00	120.01	118.32	1.69	71.002		
400,00	400.00	400.00	400.00	1.20	1.20	0.00	120.01	0.00	120.01	117.60	2.41	49 854		
500.00	500.00	500.00	500.00	1.56	1.56	0.00	120.01	0.00	120.01	116.88	3.12	38,413		
600.00	600.00	600.00	600.00	1.92	1.92	0.00	120.01	0.00	120.01	116,17	3.84	31,243 (CC, ES	
700.00	699.99	697.73	697.72	2.27	2.27	85.39	120.93	-0.85	120.84	116.30	4.54	26.615		
800.00	799.91	795.41	795.33	2.62	2.62	85.94	123.68	-3.39	123 34	118.11	5.23	23.565		
900.00	899.69	892.99	892.71	2.97	2.97	86,82	128.27	-7.61	127.55	121.61	5.93	21.494		
1,000.00	999.27	990.42	989.75	3.33	3.32	87.95	134.68	-13.50	133.47	126.83	6.64	20.098		
1,100.00	1,098.57	1,087.66	1,086.33	3.70	3.68	89.25	142.89	-21.05	141 15	133.80	7.36	19.183		
1,134.94	1,133,20	1,121.58	1,119.96	3 83	3.80	89.73	146.17	-24.07	144.26	136.65	7.61	18.953		
1,200.00	1,197.62		1,183.76	4.08	4.05	90.65	152.76	-30.13	150.39	142.29	8.10			
1,300.00	1,296.64	1,285.49	1,282.28	4.46	4.42	91.93	162.95	-39.50	159.89	151.04	8.85	18.065		
1,400.00	1,395.66	1,384.98	.1,380.80	4.85	4.81	93.07	173.13	-48.87	169.46	159 85	9.61	17.628		
1,500.00	1,494.68	1,484.47	1,479.32	5.24	5.19	94.08	183.32	-58.25	179.09	168.71	10.38	17.251		
1,600.00	1,593.70	1,583.96	1,577.84	5.63	5.58	94.99	193.51	-67.62	188.77	177,62	11.15	16.924		
1,700.00	1,692.72	1,683.44	1,676.36	6.03	5.97	95.81	203.70	-76.99	198.50	186.57	11.93	16.638		
1,800.00	1,791.74	1,782.93	1,774.88	6.42	6.36	96.56	213.89	-86.36	208.26	195.55	12.71	16.386		
1,900.00	1,890.76	1,882.42	1,873.40	6.82	6.75	97.23	224.07	-95.73	218.05	204.56	13.49	16.162		
2,000.00	1,989.78	1,981.91	1.971.92	7.22	7.15	97.85	234.26	-105.10	227.87	213.60	14.28	15.963		
2,100.00	2,088.80	2,081.39	2,070.44	7.62	7.54	98.42	244.45	-114.48	237.72	222.66	15.06	15.784		
2,200.00	2,187.83	2,180.88	2,168.96	8.02	7.94	98. 94	254.64	-123,85	247.58	231.74	15.85	15.622		
2,300.00		2,280.37	2,267.48	8.42	8.33	99.43	264.82	-133.22	257.47	240.83	16.64	15.476		
2,400.00	2,385.87	2,379.86	2,366.00	8.82	8.73	99.87	275.01	-142.59	267.37	249.94	17.43	15.343		
2,500.00	2,484.89	2,479.35	2,464.52	9.23	9.13	100.29	285.20	-151.96	277.29	259.07	18.22	15.221		
2,600.00	2,583.91	2,578.83	2,563.04	9.63	9.52	100.68	295.39	-161.33	287.22	268.21	19.01	15.110		
2,700.00	2,682.93	2,678.32	2,661.56	10,04	9,92	101.04	305.58	-170.71	297 16	277.36	19.80	15.008		
2,800.00	2,781.95	2,777.81	2,760.08	10.44	10.32	101.38	315 76	-180.08	307.11	286.52	20.59	14.913		
2,900.00	2,880.97	2,877.30	2,858.60	10.84	10.72	101.69	325.95	-189,45	317 08	295.69	21.39	14.826		
3,000.00	2,979.99	2,976.78	2,957.12	11,25	11.12	101.99	336 14	-198.82	327 05	304,87	22.18	14.745		
3,100.00	3.079.01	3,076.27	3,055.64	11.65	11.51	102.27	346.33	-208.19	337 03	314.05	22.97	14.670		
3,200.00	3,178.03	3,175.76	3,154.16	12.06	11.91	102.53	356.51	-217 56	347 02	323.25	23.77	14.599		
3,300.00	3,277.06 3,376.08	3,275.25 3,374.73	3,252.68 3,351.20	12.47 12.87	12.31 12.71	102.78 103.01	366.70 376.89	-226.94 -236.31	357.01 367.01	332.45 341.65	24.56 25.36	14.534 14.472		
				12.07	12.71	103,01	370.09	-235.31	367.01	341.03	25.36	14,472		
3,500.00	3,475.10	3,474.22	3,449.72	13.28	13,11	103.24	387.08	-245.68	377.02	350.86	26.16	14,415		
3,600.00	3,574.12	3,573.71	3,548.24	13.68	13.51	103.45	397.27	-255.05	387.03	360.08	26.95	14.360		
3,700.00	3,673.14	3,673.20	3,646.76	14.09	13.91	103.65	407.45	-264.42	397.05	369.30	27.75	14,309		
3,800.00	3,772.16 3,871.18	3,772.69 3,872.17	3,745.28 3,843.80	14.50 14.90	14 31 14.71	103.84 104.02	417.64 427.83	-273,79 -283,17	407.07 417.09	378.52 387.75	28.54 29.34	14.261 14.216		
4,000.00	3,970.20 4,069.22	3,971.66 4,071.15	3,942.32 4,040.84	15.31 15.72	15.11 15.51	104,19 104,36	438.02	-292.54	427.12	396.99	30.14	14.173		
4,200.00	4,069.22	4,170.64	4,139.36	16.12	15.51	104.52	448.21	-301.91	437.16	406.22	30.93	14.132		
4,300.00	4,166.24	4,170.64	4,139.36	16,12	16,31		458.39 468.58	-311.28	447.19	415.46	31.73	14.093		
4,400.00	4.366.29	4,369.61	4,336.40	16.53	16.71	104.67 104.81	468.58 478.77	-320.65 -330 02	457.23 467.28	424.70 433.95	32.53 33.33	14.056 14.021		
4,440.92	4,406.80	4,410.32	4,376.71	17.10	16,88	104.87	482.94	-333.86	471.39	437 73				
4,500.00	4,465.37	4,469.11	4,434.93	17.34	17.11	104.98	488.96	-339.40	477.20	437 73	33.65 34.12	14.008 13.986		
4,600.00	4,564.74	4,568.66	4,434.93	17.73	17,11	104.98	466.96 499.15	-339.40 -348.77	477.20	443.08 451.62	34.12 34.90			
.,000.00		4,668.20										13.939		
4,700.00	4,664,38	4 008 /11	4,632.08	18.11	17.92	104.57	509.35	-358,15	495.18	459.51	35.67	13.883		

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Wellbore Lateral Reference Design: Plan #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

Offset TVD Reference:

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset D	esian	Garrett	Fed Cor	n #202H. #	#222H, #	#122H, #20	6H, #226H -	#202H - I	_ateral - F	Plan #1			Offset Site Error:	0.00 usft
		IWD+HDGM		·				•					Offset Well Error:	0.00 usft
Refer	rence	Offs		Semi Major					Dist			_		
Measured		Measured	Vertical	Reference	Offset	Highside	Offset Wellbo		Between	Between			Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (*)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
4,900.00		4.866.96	4,828.92	18,81	18.72	103.04	529.70	-376 87	510 81	473.65	37.15	13.749		
4,975.86		4,942.16	4,903.38	19.06	19.02	16.99	537.40	-383.96	516.28		37.70	13.696		
5,000.00		4,966.06	4,927.05	19.14	19.12	16.67	539.85	-386.21	518.00		37.87	13.680		
5,100.00		5,065.09	5,025.12	19.45	19.52	15.37	549.99	-395.54	525.29	486.73	38.57	13.620		
5,200.00	5,164.14	5,164.12	5,123.18	19.78	19.91	14,11	560.13	-404.87	532.85	493.58	39.27	13 570		
5,300.00	5,264.14	5,263.15	5,221.24	20.10	20.31	12.89	570.27	-414.19	540.66	500.70	39.97	13 527		
5,400.00	5,364.14	5,362.17	5,319.31	20.42	20 71	11.70	580.41	-423.52	548.72	508.05	40.67	13,493		
5,500.00		5,461.20	5,417.37	20.74	21.11	10.54	590.55	-432.85	557.00		41.36	13.466		
5,600.00		5,560.23	5,515.44	21.07	21.51	9.42	600.69	-442.18	565.51		42.06	13.445		
5,700.00		5,659.26	5,613.50	21.40	21.91	8.33	610.83	-451.51	574.22	531.47	42.75	13 431		
5,800.00	5,764.14	5,758.28	5,711.56	21.72	22 31	7.28	620 97	-460.84	583.14	539.69	43.45	13.421		
	5.004.44	5 057 04	£ 000 00	22.05	22.74	C 2C	c24.44	470.46	500.05	640.11	44.44	42.447		
5,900.00		5,857.31 5,956.34	5,809.63 5,907.69	22.05 22.38	22.71 23.11	6.25 5.26	631 11 641.25	-470.16 -479.49	592.25 601.54	548,11 556,71		13,417 13,416		
6,000.00		6.055.36	6,005.76	22.71	23.11	4.30	651 39	-479.49 -488.82	611.01			13.410		
6,200.00		6,154.39	6,103.82	23.04	23.91	3.36	661.54	-498.15	620.65			13.427		
6,300.00		6,253.42	6,201.88	23.38	24.31	2.46	671.68	-507.48	630.45			13.438		
6,400.00		6,358.19	6,305.68	23 71	24.73	1.55	682.19	-517,15	640.21			13.437		
6,500.00		6,471 39	6,418.16	24 04	25 17	0 77	691.53	-525.74	. 648.33			13.391		
6,600.00 6,700.00		6,585.26 6,699.59	6,531.63 6,645.80	24.38 24.71	25.59 25.99	0 20 -0.15	698.44 702.87	-532.10 -536.18	654.37 658.25	605.20 608.36	49.16 49.89	13.310 13.194		
6,800.00		6,814.17	6,760.35	25.05	26.38	-0.13	704.79	-537.94	659.93		50.59	13.046		
0,000.00	3,731.11	3,511,77	0,7 00.00	25.55	20.00	0.01		001.01	555.55	000.01	00.00	70.010		
6,900.00	6,864.14	6,917.96	6,864.14	25 38	26.71	-0.31	704.88	-538.02	660.00		51.26	12.876		
7,000.00		7,017.96	6,964.14	25 72	27.04	-0.31	704.88	-538.02	660.00		51.93	12.710		
7,100.00		7,117.96	7,064.14	26 06	27.36	-0.31	704 88	-538 02	660 00			12.547		
	7,164.14	7,217.96	7,164.14	26.39	27.69	-0.31	704.88	-538.02	660.00		53.27	12.389		
7,300.00	7,264.14	7,317.96	7,264.14	26 73	28.01	-0.31	704.88	-538.02	660.00	606.05	53.95	12.234		
7,400.00	7,364.14	7,417.96	7,364.14	27 07	28.34	-0.31	704.88	-538.02	660.00	605.38	54.62	12.082		
7,500.00	7,464.14	7,517.96	7,464.14	27.41	28.67	-0.31	704.88	-538.02	660.00	604.70	55.30	11.935		
1	7,564,14	7,617.96	7,564.14	27.75	29.00	-0.31	704.88	-538.02	660.00		55.98	11.790		
	7,664.14	7.717.96	7,664.14	28.09	29.33	0.31	704.88	-538.02	660.00			11.649		
7,800 00	7,764.14	7,817.95	7,764.14	28 43	29.66	-0.31	704.88	-538.02	660.00	602.67	57.34	11.511		
7,900.00	7,864.14	7,917.95	7,864.14	28.77	29.99	-0 31	704.88	-538.02	660.00	601.99	58.02	11.376		
8,000.00		8,017.95	7,964.14	29.11	30.32	-0.31	704.88	-538.02	660.00		58.70	11.244		
8,100.00		8,117.96	8,064.14	29.46	30.65	-0.31	704.88	-538.02	660.00			11.115		
8,200 00		8,217.96	8,164 14	29.80	30.98	-0.31	704 88	-538.02	660.00	599.94	60.06	10.988		
8,300.00	8,264.14	8,317.96	8,264.14	30.14	31.32	-0.31	704.88	-538.02	660.00	599.26	60,75	10.865		
8,400.00	8,364,14	8,417.96	8,364.14	30.49	31.65	-0.31	704 88	-538 02	660.00	598.57	61,43	10 744		
8,500.00		8,517.96	8,464.14	30.49	31.98	-0.31	704.88	-538.02	660.00	597.89	62.12	10.625		
8,600.00	8,564.14	8,617.96	8,564.14	31.17	32.32	-0.31	704.88	-538 02	660.00			10.509		
8,700.00	8,664.14	8,717.96	8,664.14	31.52	32.65	-0.31	704.88	-538 02	660.00	596.51	63,49	10.396		
8,800.00	8,764.14	8,817 96	8,764.14	31.86	32.99	-0.31	704 88	-538 02	660.00	595.83	64.18	10.284		
8,900.00		8,917.96	8,864.14	32.21	33 33	-0 31	704 88	-538 02	660.00	595.14	64.86	10.175		
9,000.00 9,100.00		9,017.96	8,964.14	32.55	33.66	-0.31 0.31	704 88	-538 02 538 03	660 00	594.45 593.76	65.55 66.24	10.068 9.964		
9,100.00		9,117.96 9,217.96	9,064.14 9,164.14	32.90 33.24	34.00 34.34	-0.31 -0.31	704.88 704.88	-538 02 -538.02	660.00 660.00	593.76 593.07	66.24 66.93	9.964 9.861		
9,200.00		9,217.90	9,164.14	33.59	34.54	-0.31 -0.31	704.88	-537.93	660.00	593.07	67.62	9.661		
3,300.00	3,204 14	5,510 04	J,204,22	33.33	54.01	-0.51	704.00	-551.55	500.00	552.50	U7.U2	3,01		
9,363.27	9,327.41	9,381 43	9,327.41	33 81	34 87	0.09	704.87	-533.33	659 99	591.94	68.05	9.699		
9,400.00		9,417.52	9,363.03	33.93	34.97	0.59	704.86	-527 60	660.01	591.72	68.30	9.664		
9,500.00		9,510.79	9,452.76	34.28	35.21	2.76	704.82	-502.53	660 80	591.84	68.97	9.582	_	
		9,594.12		34.63	35.40	5.74	704.77	-468.08	664 16	594.58	69.57	9.546 9	iF	
9,700.00	9,664.14	9,666.10	9,589.42	34.97	35.55	9.01	704.70	-429.75	672 23	602.25	69.98	9.605		

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error:

0.00 usft

Well Error:

Reference Well: #226H 0.00 usft Reference Wellbore Lateral

Reference Design: Plan #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference:

Offset D	_	IWD+HDGM	1 64 66	11 #20211, 1	r22211, n	12211, #20	16H, #226H -	#20211 - 1	-aleiai - r	1411#1			Offset Site Error:	0.00 ust
Refer	-	Offs	et	Semi Major	Axis				Dist	элсе			Offset Well Error:	0.00 ust
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (*)	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
9,800.00	9,764.14	9,727.07	9,636.89	35.32	35.67	12.22	704.64	-391.51	686.94	616.91	70.03	9.809		
9,900.00	9,864.14	9,778.30	9,673.44	35.67	35.77	15.16	704.58	-355.64	709.59	639.98	69.61	10.194		
10,000.00	9,964.14	9,821.29	9,701.54	36.02	35.86	17.76	704.53	-323.12	740.76	672.07	68.69	10.784		
10,100.00	10,064.14	9,850.00	9,718.91	36,36	35.92	19.54	704.49	-300.27	780,44	713.22	67.22	11,610		
10,200.00	10,164.14	9,888.20	9,740.21	35.71	36.02	21.95	704.44	-268.57	827.89	762.13	65.76	12.590		
10,300.00	10,264.14	9,914.40	9,753.57	37.06	36.10	23.62	704.41	-246.04	882.49	818.48	64.01	13.786		
10,400.00	10,364.14	9,936.94	9,764.24	37.41	36.17	25.05	704.37	-226.18	943.29	881.05	62.25	15,154		
10,412.10	10,376.24	9,950.00	9,770.06	37.45	36.21	25.88	704.35	-214.49	951.16	888.91	62.24			
10,450.00	10,414.11	9,950.00	9,770.06	37.58	36.21	-61.42	704.35	-214.49	975.32	913.89	61.43	15,878		

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error:

0.00 usft

Reference Well: Well Error:

#226H

Reference Wellbore Lateral Reference Design: Plan #2

0.00 usft

Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference: MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Offset D	esign	Garret	t Fed Cor	m #202H, #	‡222H, ‡	#122H, #20	6H, #226H -	#206H - I	_ateral - F	Plan #2			Offset Site Error:	0.00 usft
1 .	_	MD+HDGM											Offset Well Error:	0.00 usft
Refer Measured		Offs Measured	et Vertical	Semi Major Reference		Minheida	Offices Wiellho	en Camten	Dist			C		
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Highside Toolface (*)	Offset Wellbo +N/-S (usft)	+E/-W	Between Centres (usft)	Between Ellipses (usft)	Separation (usft)	Separation Factor	Warning	
								(usft)		(ask)	(03.17)			
0.00 100.00		0.00 100.00	0,00 100,00	0.00 0.13	0.00 0.13	-0.05 -0.05	29,97 29.97	-0.02	29.97	20.72	0.26	146 045		
200.00		200.00	200.00	0.13	0.13	-0.05	29.97 29.97	-0.02 -0.02	29.97 29.97	29.72 29.00	0.26 0.97	116.945 30,798		
300.00		300.00	300.00	0.85	0.85	-0.05	29.97	-0.02	29.97	28.28	1.69	17,734		
400.00		400.00	400.00	1.20	1.20	-0.05	29.97	-0.02	29.97	27.57	2.41	12.452		
500.00		500.00	500.00	1.56	1.56	-0.05	29.97	-0.02	29.97	26.85	3.12	9.594		
600.00	600.00	600.00	600.00	1.92	1.92	-0.05	29.97	-0.02	29.97	26.13	3.84	7.804 C	ic.	
700.00	699.99	699.79	699.78	2.27	2.27	85.23	30.32	-1.28	30.21	25.66	4.54	6.648 E		
800.00	799.91	799,58	799.49	2.62	2.62	85.46	31.34	-5.06	30.90	25.66	5.24	5.897		
900.00	899.69	899.37	899.06	2.97	2.98	85.83	33 04	-11.34	32.07	26.12	5.95	5.392		
1,000.00	999.27	999.14	998.42	3.33	3.34	86.29	35.43	-20,13	33.70	27.03	6.67	5.055		
1,100.00	1,098.57	1,098.91	1,097.49	3.70	3.70	86.82	38.49	-31.42	35 79	28.39	7.40	4.836		
1,134.94	1,133.20	1,133.78	1,132.05	3.83	3.83	87.04	39.72	-35.95	36.63	28.97	7.66	4.781		
1,200.00		1,201.18	1,196 47	4.08	4.09	87.66	42.05	-44.53	38.22	30.05	8.16	4.682		
1,300.00		1,301.21	1,295.50	4.46	4,47	88.51	45.63	-57.73	40.66	31.73	8.93	4.554		
1,400.00	1,395.66	1,401.24	1,394.53	4.85	4.86	89.27	49.21	-70.92	43.12	33,41	9.70	4.444		
1,500.00	1,494.68	1,501.28	1,493.56	5 24	5.25	89.95	52.79	-84,12	45.58	35.09	10.48	4.349		
1,600.00	1,593.70	1,601.31	1,592.59	5.63	5.64	90.56	56.37	-97 31	48.04	36.78	11.26	4.265		
1,700.00	1,692.72	1,701.34	1,691 62	6.03	6.03	91.11	59.95	-110.50	50.51	38.46	12.05	4.191		
1,800.00	1,791.74	1,801.37	1,790.65	6.42	6.43	91.61	63.52	-123.70	52.99	40.14	12.84	4 126		
1,900.00	1,890.76	1,901.40	1,889.68	6.82	6.82	92.06	67.10	-136.89	55.46	41.83	13.64	4.067		
2,000.00	1,989.78	2,001.43	1,988.71	7.22	7.22	92.47	70.68	-150.09	57.95	43.51	14.43	4.015		
2,100.00	2,088.80	2,101.47	2,087.74	7.62	7.62	92.85	74.26	-163.28	60.43	45.20	15.23	3.968		
2,200.00	2,187.83	2,201.50	2,186.77	8.02	8.02	93.20	77.84	-176,47	62.92	46 89	16.03	3.925		
2,300.00		2,301.53	2,285.80	8.42	8.42	93.53	81.42	-189.67	65.41	48.57	16.83	3.886		
2,400.00	2,385.87	2,401.56	2,384 82	8 82	8 82	93.83	85.00	-202.86	67.90	50.26	17.63	3.851		
2,500.00		2,501.59	2,483.85	9.23	9.22	94.11	88 58	-216.06	70.39	51.95	18.44	3.818		
2,600.00	2,583.91	2,601.62	2,582.88	9.63	9.62	94.37	92 16	-229.25	72.88	53.64	19.24	3.788		
2,700.00		2,701.66	2,681.91	10,04	10.02	94.61	95.74	-242.45	75. 38	55.34	20,04	3.761		
2,800.00	2,781.95	2,801.69	2,780.94	10.44	10.42	94.84	99.32	-255.64	77.88	57.03	20.85	3.735		
2,900.00	2,880.97	2,901.72	2,879.97	10.84	10.82	95.05	102.90	-268.83	80.37	58.72	21.65	3.712		
3,000.00	2,979.99	3,001.75	2,979.00	11.25	11,23	95.25	106.48	-282.03	82.87	60.41	22.46	3.690		
3,100.00	3,079.01	3,101.78	3,078.03	11.65	11.63	95.44	110.06	-295.22	85.37	62.11	23.27	3.669		
3,200.00	3,178.03	3,201 81	3,177.06	12.06	12.03	95.61	113.64	-308.42	87.87	63.80	24.07	3.650		
3,300.00	3,277.06	3,301.85	3,276.09	12.47	12,44	95.78	117 22	-321.61	90.37	65.49	24.88	3.632		1
3,400.00	3,376.08	3,401.88	3,375,12	12.87	12.84	95.94	120.80	-334.80	92.88	67.19	25.69	3.616		
3,500.00	3,475.10	3,501.91	3,474.15	13.28	13.24	96 09	124.37	-348.00	95.38	68.88	26.50	3.600		
3,600.00	3,574.12	3,601.94	3,573.17	13 68	13.65	96 23	127.95	-361.19	97.88	70.58	27.30	3.585		
3,700.00	3,673.14	3,701.97	3,672.20	14.09	14.05	96 37	131.53	-374.39	100.39	72.28	28 11	3 571		1
3,800.00	3,772.16	3,802.00	3,771.23	14.50	14.45	96.50	135.11	-387.58	102.89	73.97	28,92	3.558		
3,900.00	3,871.18	3,902.03	3,870.26	14.90	14.86	96.62	138.69	-400.78	105.40	75.67	29.73	3 545		
4,000.00	3,970.20	4,002.07	3,969.29	15.31	15.26	96.74	142.27	-413.97	107,90	77 36	30,54	3 533		
	4,069.22	4,102.10		15.72	15.67	96 85	145.85	-427.16	110,41	79 0 6	31 35	3.522		
4,200.00		4,202.13	4,167.35	16.12	16 07	96.96	149.43	-440.36	112.92	80.76	32.16	3.511		
4,300.00			4,266.38	16,53	16.47	97.06	153.01	-453.55	115.42	82.46	32.97	3.501		1
4,400.00	4,366.29	4,402.19	4,365.41	16.94	16.88	97.16	156.59	-466.75	117.93	84 15	33.78	3.492		
4,440 92	4,406.80	4,438.71	4,405.93	17.10	17.03	97.19	158.05	-472.15	118.96	84.87	34 09	3.490		
4,500.00	4,465.37	4,502.22	4.464.44	17.34	17.28	97.06	160.17	-479.94	120.38	85 80	34 58	3.481		
4,600.00	4,564.74	4.602.29		17.73	17.69	95,86	163.75	-493.13	122.57	87.18	35.39	3.464		
4,700.00	4,664.38	4,697.76		18.11	18.07	93.66	167.24	-506.00	124.58	88.42	36.15	3,446		
4,800.00	4,764.20	4,798.06	4,762.28	18,46	18,46	91.37	170.14	-516.69	126.35	89.44	36.91	3.423		
<u> </u>														

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft #226H

0.00 usft

Well Error:

Reference Wellbore Lateral Reference Design: Plan #2 Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Jurvey Pro	ogram: 0-M	IWD+HDGM											Offset Well Error:	0.00 us
Refer	-	Offs	et	Semi Major	Axis				Dista	ance			Onset Well Error;	U.UU U
leasured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (*)	Offset Wellbo: +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
4,900.00		4,898.51		18.81	18.84	89.13	172.35	-524.85	127.85	90.22		3.398		
4,975.86	4,940.00	4,974.81	4,938.52	19.06	19.11	2.24	173.57	-529.36	128.80	90 66		3.377		
5,000.00		4,999.11		19.14	19.20	1.74	173.88	-530.48	129.06	90,76		3.370		
5,100.00	5,064.14	5,099.90	5,063.53	19.45	19.55	0.37	174.71	-533.56	129.83	90.88		3.333		
5,200.00	5,164.14		5,164.14	19.78	19.87	0.09	174.89	-534 19	130.00	90.40		3.283		
5,300.00		5,300.51		20.10	20.20	0.09	174.89	-534.19	130.00	89.75		3.230		
5,400.00	5,364.14	5,400.51	5,364.14	20.42	20.52	0.09	174.89	-534.19	130.00	89.11	40.89	3,179		
5,500.00	5,464.14	5,500.51	5,464.14	20.74	20.85	0.09	174.89	534.19	130.00	88.46	41.54	3.129		
5,600.00	5,564.14	5,600.51	5,564.14	21.07	21.17	0.09	174.89	-534.19	130.00	87.81	42.19	3.081		
5,700.00	5,664.14	5,700.51	5,664.14	21.40	21.50	0.09	174.89	-534.19	130.00	87.15	42.85	3.034		
5,800.00	5,764.14	5,800.51	5,764.14	21.72	21.83	0.09	174.89	-534.19	130.00	86.50	43.50	2.988		
5,900.00	5,864.14	5,900.51	5,864.14	22.05	22.15	0.09	174.89	-534.19	130.00	85.84	44 16	2.944		
6,000.00			5,964 14	22.38	22.48	0.09	174.89	-534.19	130.00	85.18	44.82	2.900		
6.100.00		6,100.51	6,064.14	22.71	22.81	0.09	174.89	-534.19	130.00	84.52		2.858		
6,200.00			6,164.14	23.04	23.15	0.09	174.89	-534.19	130.00	83.85	46,15	2.817		
6,300.00	6,264.14	6,300.51		23.38	23.48	0.09	174 89	-534.19	130.00	83.19	46 81	2.777		
6,400.00	6.364.14	6,400.51	6,364.14	. 23.71	23.81	0.09	174.89	-534.19	130.00	82.52	47.48	2.738	•	
6,500.00	6,464.14	6,500.51	6,464 14	24,04	24,14	0.09	174.89	-534.19	130.00	81.86		2.700		
6,600.00	6,564.14	6,600 51	6,564.14	24.38	24.48	0.09	174,89	-534.19	130.00	81.19	48.81	2.663		
6,700.00	6,664,14	6,700,51		24.71	24.81	0.09	174.89	-534.19	130.00	80 52	49.48	2.627		
6,800.00	6,764.14	6,800.51	6.764.14	25.05	25.15	0.09	174.89	-534.19	130.00	79.84	50,16	2.592		
6,900.00	6,864.14	6,900.51	6,864.14	25.38	25.49	0.09	174.89	-534,19	130.00	79.17	50.83	2.558		
7,000.00	6,964.14	7,000.51	6,964.14	25.72	25.82	0.09	174.89	-534.19	130.00	78.50	51.50	2.524		
7,100.00	7,064,14	7.100.51	7,064,14	26.06	26.16	0.09	174.89	-534.19	130.00	77.82	52.18	2.492		
7,200.00	7,164,14	7,200.51	7,164.14	26.39	26,50	0.09	174.89	-534.19	130.00	77.15	52.85	2.460		
7,300.00	7,264.14	7,300.51	7,264.14	26.73	26.84	0.09	174.89	-534.19	130.00	76.47	53.53	2.429		
7,400.00	7,364.14	7,400.51	7,364.14	27.07	27.18	0.09	174.89	-534.19	130.00	75.79	54.21	2.398		
7,500.00	7,464.14	7,500.51	7,464.14	27.41	27.52	0 09	174,89	-534.19	130.00	75.11	54.89	2.368		
7,600.00	7,564,14	7,600.51	7,564.14	27.75	27.86	0.09	174.89	-534,19	130.00	74.43	55.57	2.339		
7,700.00	7,664.14	7,700.51		28.09	28.20	0.09	174.89	-534.19	130.00	73.75	56.25	2 31 1		
7,800.00	7,764.14	7,800.51	7.764.14	28.43	28.54	0.09	174.89	-534.19	130.00	73.07	56.93	2.283		
7,900.00	7,864.14	7,900.51	7,864.14	28.77	28.88	0.09	174.89	-534.19	130.00	72.39	57.61	2.256		
8,000.00	7,964.14	8,000.51	7,964.14	29.11	29.22	0.09	174.89	-534.19	130.00	71.70	58.30	2.230		
8,100.00	8,064.14	8,100.51	8.064.14	29.46	29.56	0.09	174.89	-534.19	130.00	71.02	58.98	2.204		
8,200.00	8,164.14	8,200.51	8,164.14	29.80	29.90	0.09	174.89	-534.19	130.00	70.33	59.67	2.179		
8,300.00	8,264.14	8,300.51	8,264.14	30.14	30.25	0.09	174.89	-534.19	130.00	69.65	60.35	2.154		
8,400.00	8,364.14	8,400.51	8,364.14	30.49	30.59	0 09	174.89	-534.19	130.00	68.96	61.04	2.130		
8,500.00	8,464.14	8,500.51	8,464,14	30.83	30.93	0.09	174,89	-534.19	130.00	68.27	61.73	2.106		
8,600.00	8.564.14	8,600.51	8,564.14	31.17	31.28	0.09	174.89	-534.19	130 00	67 58	62 42	2 083		
8,700.00	B,664.14	8,700.51	8,664.14	31.52	31.62	0.09	174.89	-534.19	130.00	66.89	63.11	2.060		
8,800.00	8,764.14	8,800.51	8,764.14	31.86	31 97	0.09	174.89	-534.19	130.00	66.21	63.79	2.038		
8,900.00	8,864.14	8,900.51	8,864.14	32.21	32.31	0.09	174.89	-534.19	130.00	65.52	64.48	2.016		
9,000.00	8,964.14	9,000.51	8.964.14	32.55	32.66	0.09	174.89	-534.19	130 00	64 82	65.18	1.995		
9,100.00	9,064.14	9,100,51	9,064 14	32.90	33 00	0.09	174.89	-534.19	130.00	64 13	65.87	1.974		
9,200.00	9,164.14	9,200.51	9,164.14	33.24	33.35	0.09	174.89	-534.19	130.00	63 44	66.56	1 953		
9,300.00	9,264.14	9,300.51	9,264.14	33.59	33.69	0.09	174.89	-534.19	130.00	62 75	67.25	1 933		
9,400.00	9,364.14	9,403.11	9,366.24	33.93	34.02	3.82	173.53	-525.82	128.95	61.02	67.92	1.898		
9,456.06	9,420.20	9,458.42	9,420.20	34 13	34.17	9 20	171 60	-513.88	128.36	60 07	68.29	1.880 S	F	
9,500.00	9.464.14	9,499.87	9,459.72	34.28	34.29	14.74	169,61	-501.59	129.04	60 55	68 49	1.884		
9,600.00	9,564.14	9.586 35	9.538.73	34 63	34.51	29.47	164.02	-467.08	139.17	71.30	67.87	2.051		
	9,664.14	9,660 85	0.004.00	34 97	34.70	43.26	157.72	-428.23	166.96	102.04	64.92	2.572		

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error:

0.00 usft

Reference Well: Well Error:

#226H 0.00 usft

Reference Wellbore Lateral

Reference Design: Plan #2

Local Co-ordinate Reference:

TVD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Output errors are at

Offset TVD Reference:

Database:

Minimum Curvature

2.00 sigma

EDM 5000 14 Multi User

Refer		IWD+HDGM Offs	et	Semi Major	Axis				Dista	псе			Offset Well Error:	0.00 us
fleasured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (")	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
9,800.00	9,764,14	9,723.68	9,650.88	35.32	34.88	53.69	151.43	-389.39	212.62	151.88	60.74	3.501		
9,900.00	9,864.14	9,776.21	9,688,29	35,67	35.03	60.97	145.54	-353.03	271.94	215.14	56.79	4.788		
10,000.00	9,964.14	9,820.08	9,716.85	36.02	35.18	66.01	140.22	-320.17	340.79	287.22	53.57	6.362		
10,100.00	10,064.14	9,850.00	9,734.83	36.36	35.29	68 95	136,40	-296.56	416.40	365.82	50.58	8.233		
10,200.00	10,164.14	9,887.90	9,755.77	36.71	35.45	72.18	131.35	-265.39	496,60	447.47	49.13	10.108		
10,300.00	10,264,14	9,914.31	9,769.10	37.06	35.57	74.14	127.71	-242.89	580.43	532.78	47.65	12.180		
10,400.00	10,364.14	9,936.95	9,779.69	37.41	35.67	75.65	124.51	-223.13	666.94	620.40	46.53	14.332		
10,412.10	10,376.24	9,950.00	9,785.43	37.45	35.74	76.46	122.63	-211.56	677,74	630.88	46.86	14.464		
10,450.00	10,414 11	9,950.00	9,785.43	37.58	35,74	-12.19	122.63	-211.56	710.42	664.27	46.15	15.394		
10,500.00	10,463.79	9,950.00	9,785.43	37.73	35.74	-10.65	122.63	-211.56	752.43	707.19	45.24	16.633		
10,550,00	10,512.81	9,971.41	9,794.26	37.88	35.86	-8 .77	119,51	-192.31	792.39	747.33	45.06	17.587		
10,500.00	10,560.79	9,984,44	9,799.28	38 02	35 93	-7.57	117.59	-180.45	830.54	785.99	44.55	18.643		
10,650.00	10,607.36	10,000.00	9,804.91	38.16	36.02	-6.57	115.27	-166,12	866.62	822 52	44.10	19.652		
10,700.00	10,652.18	10,000.00	9,804.91	38.30	36.02	-6.06	115.27	-166 12	900.72	857,48	43.25	20.826		
10,750.00	10,694.89	10,026.88	9,813,70	38.43	36.19	-5,19	111.21	-141.05	932.13	889.05	43.08	21.638		
10,800.00	10,735.18	10,054.41	9,821.46	38.57	36.37	-4.48	106.99	-114,99	961.58	918.69	42.89	22.421		
10,850.00	10.772.74	10,054,41	9.821.46	38.71	36.37	-4.24	106.99	-114,99	988.15	945.99	42.16	23 438		

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well: 0.00 usft

Well Error:

#226H 0.00 usft

Reference Wellbore Lateral

Reference Design: Plan #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Offset D	esign	Garrett	Fed Cor	n #202H, #	‡222H, #	#122H, #20	6H, #226H -	#222H - I	_ateral - P	Plan #2			Offset Site Error:	0.00 usft
		WD+HDGM				•							Offset Well Error:	0 00 usft
Refer	ence	Offs		Semi Major				_		ance		_		
Measured		Measured	Vertical	Reference	Offset	Highside	Offset Wellbo			Between		Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (*)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
										/				
0.00	0.00	0.00 100.00	0.00	0.00 0.13	0.00 0.13	-0.02 -0.02	90.01 90.01	-0.04 -0.04	90.01 90.01	89.75	0.26	351,165		
100.00	100.00 200.00	200.00	100.00 200.00	0.13	0.13	-0.02 -0.02	90.01	-0.04 -0.04	90.01			92.480		
300.00	300.00	300.00	300.00	0.45	0.45	-0.02	90.01	-0.04	90.01			53.252		
400.00	400.00	400.00	400.00	1.20	1.20	-0.02	90.01	-0.04	90.01					
500.00	500.00	500.00	500.00	1.56	1.56	-0.02	90.01	-0.04	90.01					
600.00	600.00	600.00	600.00	1.92	1.92	-0.02	90.01	-0.04	90.01			23.433 (CC, ES	
700.00 800.00	699,99 799,91	698.44 796.84	698.43 796.75	2.27 2.62	2.27 2.62	85,38 85.97	90.86 93.40	-0.98 -3.80	90.76 93.03	86.22 87.79		19.981 17.759		
900.00	899.69	895.16	894.87	2.02	2.02	86.90	97.64	-8.51	96.82	90.88		16.298		
1,000.00	999 27	993.37	992.67	3 33	3.33	88.07	103.55	-15.07	102.18	95.53		15.361		
1,000.00	000 27		552,5.											
1,100.00	1,098.57	1,108.18	1,090.47	3.70	3.75	89.43	111.12	-23.47	109.07	101,63		14.666		
1,134.94	1,133.20	1,126.64	1,125.03	3.83	3.82	90.08	113.97	-26,64	111.65			14.621		
1,200.00	1,197.62	1,208.54	1,189.36	4.08	4.13	91.43	119.28	-32.53	116.50			14.231		
1,300.00	1,296.64	1,291.10	1,288.25	4.46	4,44	93.28	127.43	-41.58 50.63	124.07	115.19		13.976		
1,400.00	1,395.66	1,409.27	1,387.14	4.85	4.89	94.93	135.59	-50.63	131.76	122.05	9.71	13.570		
1,500.00	1,494.68	1,509.63	1,486.03	5.24	5.27	96.39	143.75	-59.69	139.54	129.06	10.48	13.316		
1,600.00	1,593.70	1,609.99	1,584.92	5 63	5.66	97.69	151.90	-68.74	147.40	136.15	11.25	13.099		
1,700.00	1,692,72	1,689.64	1,683.81	6.03	5.96	98.87	160.06	-77.79	155.33			12.998		
1,800.00	1,791.74	1,789.28	1,782.70	6.42	6.35	99.93	168.21	-86.84	163.32					
1,900.00	1,890.76	1,888.92	1,881.59	6.82	6.73	100.89	176.37	-95.90	171.36	157.85	13.50	12.690		
2,000.00	1,989.78	1,988.56	1,980.48	7.22	7.12	101.76	184.52	-104.95	179.44	165.15	14.28	12.563		
2,100.00	2,088.80	2,088.19	2,079.37	7.62	7.51	102.56	192.68	-114.00	187.56					
2,200.00	2.187.83	2,187.83	2,178.26	8.02	7.89	103.29	200.84	-123.05	195.71			12.351		
2,300.00	2,286.85	2,287.47	2,277.14	8.42	8.28	103.97	208.99	-132.11	203 89	187.26	16.63	12.261		
2,400.00	2,385.87	2,387.10	2,376.03	8.82	8.67	104.59	217.15	-141.16	212.10	194.69	17.41	12.181		
0.500.00	0.404.00	0.400.74	2 474 02	0.22	0.05	105 16	225 20	150.21	220.22	202.14	+0.30	12 100		
2,500.00 2,600.00	2,484.89 2,583.91	2,486.74 2,586.38	2,474.92 2,573.81	9.23 9.63	9.06 9.45	105.16 105.70	225.30 233.46	-150.21 -1 5 9.26	220.33 228.59					
2,700.00	2,682.93	2,686.02	2,672.70	10.04	9.84	106.19	241.61	-168.32	236,86			11.982		
2,800.00	2,781.95	2,785.65	2,771.59	10.44	10.23	106.66	249.77	-177.37	245.14	224.59				
2,900.00	2,880.97	2,885.29	2.870.48	10.84	10.62	107,09	257.93	-186.42	253.44	232.10				
3,000.00	2,979.99	2,984.93	2.969.37	11.25	11 01	107.49	266.08	-195.48	261.76					
3,100.00	3,079.01	3,084.56	3,068.26	11.65	11.40	107.87	274.24	-204.53 -213.58	270.09					,
3,200.00 3,300.00	3,178.03 3,277.06	3,184.20 3,283.84	3,167.15 3,266.04	12.06 12.47	11.79 12.18	108.23 108.57	282.39 290.55	-213.58 -222.63	278.42 286.77					
3,400.00	3,376.08	3,283.48	3,364.93	12.47	12.16	108.89	290.55	-222.63	295.13			11.677		
3, 100.00	5,575,00	5,250.40	2,004.00	12.07		. 30.00	2550	_000	200.10	_00.00	20.27			
3,500.00		3,483.11	3,463.82	13.28	12.95	109.19	306.86	-240.74	303.50					
3,600.00	3,574.12	3,582.75	3,562.71	13.68	13.35	109.47	315.02	-249.79	311.87	285.02				
3,700.00	3,673.14	3,682.39	3,661.59	14.09	13.74	109.74	323.17	-258.84	320.25					
3,800.00	3,772.16	3.782.02	3,760.48 3,859.37	14.50	14,13	109.99	331.33	-267.90 -276.95	328.64	300.22 307.82				
3,900.00	3,871.18	3,881.66	3,009.37	14.90	14.52	110.24	339.48	-276.95	337.03	301.02	29.21	11.55/		
4.000.00	3,970.20	3,981.30	3,958.26	15.31	14.91	110.47	347.64	-286.00	345.43	315.43	30.00	11.514		
4,100.00		4,080.94	4,057.15	15.72	15.31	110.69	355.79	-295.05	353.84					
4,200.00		4,180.57	4,156.04	16.12	15.70	110.90	363.95	-304.11	362.25		31.58	11.472		
4,300.00		4,280.21	4,254.93	16.53	16.09	111.10	372.11	-313.16	370.66		32.37			
4,400.00	4,366.29	4,379.85	4,353 82	16.94	16.48	111.29	380.26	-322.21	379.08	345.93	33.15	11.434		
4440.00	4 400 00	4,420.62	4 204 20	47.40	16.64	111 27	383.60	-325.92	382.53	349.05	33,48	11.427		
4,440.92	4,406.80 4,465.37	4,420.62 4,479.50	4,452.73	17.10 17.34	16.64 16.87	111.37 111.48	388.42	-325.92 -331.27	382.53 387.34					
4,600.00		4,479.30	4,452.73	17.34	17.26	111.37	396.58	-340.33	394.72					
4,700.00		4,678.93		18.11	17.66	110.91	404 74	-349.39	401.18					
4,800.00		4,778.58		18.46	18.05	110.11	412.90	-358.44	406.76					
L											<u> </u>	_		
						· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·							

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error:

0.00 usft

Reference Well: Well Error:

#226H 0.00 usft

Reference Wellbore Lateral

Reference Design: Plan #2

Local Co-ordinate Reference:

TVD Reference: MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

Offset TVD Reference:

2.00 sigma

Database:

EDM 5000 14 Multi User

	esign	Garret	t Fed Co	m #202H, #	#222H, #	#122H, #20)6H, #226H -	#222H -	Lateral - F	Plan #2			Offset Site Error:	0.00 u
-	_	IWD+HDGM											Offset Well Error:	0.00 u
Refer	rence Vertical	Offs		Semi Major				_		ance				
Depth	Depth	Measured Depth	Vertical Depth	Reference	Offset	Highside	Offset Wellbo			Between		Separation	Warning	
(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	Toolface (*)	+N/-S	+E/-W	Centres	Ellipses	Separation	Factor		
				(2011)	(4514)	٠,	(usft)	(usft)	(usft)	(usft)	(usft)			
4,900.00		4.878.09	4,848.33	18.81	18.44	108.98	421.05	-367.48	411 59	374.60	36,99	11.128		
4,975.86		4,953.45	4,923.12	19.06	18.74	22.72	427.21	-374.33	414 83	377.29	37.54	11.051		
5,000.00		4,977.41	4,946.90	19,14	18,83	22.34	429.18	-376.50	415.82	378,11	37.71	11.027		
5,100.00		5,076.66	5,045.40	19.45	19.22	20.78	437.30	-385.52	420 12	381.70	38.43	10.933		
,200.00	•	5,175.91	5,143.91	19.78	19.61	19.25	445.42	-394.54	424.74	385.60	39.14	10 852		
5,300.00	5,264.14	5,275.16	5,242.41	20.10	20.00	17.75	453.55	-403.56	429.65	389.80	39.85	10.782		
5,400.00	5,364.14	5,374,41	5,340.92	20.42	20.20	46.00								
5,500.00		5,473.66	5,439,42	20.42	20.39	16.29	461.67	-412.57	434.85	394.29	40.56	10,721		
5,600.00				20.74	20.78	14.87	469.80	-421.59	440.32	399.06	41.27	10.671		
5,700.00		5,572.91		21.07	21.17	13.48	477,92	-430 61	446.07	404.10	41.97	10.628		
5,800.00		5,672.16	5,636.43	21.40	21.56	12.12	486.04	439.63	452.07	409.40	42.67	10.594		
5,800.00	5,764.14	5,771.41	5,734.93	21.72	21.95	10.81	494.17	-448.64	458 32	414.95	43.37	10.567		
5,900.00	5,864.14	5,870.66	5,833.44	22.05	22.34	9.52	502.29	-457.66	ACA DA	420.74	44.07	40 5 - 7		
3,000.00		5,969.91		22.38	22.34	8.28	510.42	-457.66 -466.68	464.81	420.74	44,07	10.547		•
5,100.00		6,069.16	6,030.45	22.71	23 12	7.06			471.53	426.76	44.77	10.532		
5,200.00		6,168.40	6,128.95	23.04	23.51	7.06 5.89	518.54 526.66	-475 70	478.47	433.00	45.47	10.523		
5,300.CO		6,267.65	6,227.46	23.38	23.91	4.75	526.66 534.70	-484.71 403.73	485.61	439.45	46.16	10.520		
_,,	U,447.17	5,251.00	J,EE7.70	23.30	23.31	4.73	534.79	-493.73	492.95	446.10	46.86	10.520		
6,400.00	6,364.14	6,366.90	6,325.96	23.71	24.30	3.64	542.91	-502.75	500.49	452.94	47.55	10,525		
5,500.00	6,464.14	6,466.15	6,424.47	24.04	24.69	2.56	551.04	-511,77	508.21	459.96	48.25	10.534		
,600.00	6,564.14	6,569,50	6,527.07	24.38	25.09	1.50	559.31	-520.95	515.93	466.97	48.96	10.537		
,700.00	6,664.14	6,678.80	6,635.87	24.71	25.51	0.62	566.33	-528.74	522.24	472.53	49.71	10.506		
.800 00		6,788.62	6,745.43	25.05	25.91	0.02	571.28	-534.24	526.73					
		-1	-,, ,-,, ,-	25.00	20.51	0.02	37 1.20	7334.24	320.73	476.29	50.43	10,444		
5,900.00	6,864.14	6,898.78	6,855.50	25,38	26.29	-0.32	574.13	-537,40	529.32	478,18	51,14	10.350		
.000.000	6,964.14	7,007.42	6,964.14	25.72	26.66	-0.41	574.88	-538.23	530 01	478.18	51.82	10.227		
,100.00	7,064.14	7,107,42	7,064.14	26.06	26.98	-0.41	574.88	-538.23	530.01	477.51	52.50	10.096		
,200.00	7,164.14	7,207.42	7,164.14	26.39	27.31	-0.41	574.88	-538.23	530.01	476.84	53.17	9.968		
300.00	7,264.14	7,307.42	7,264.14	26.73	27.64	-0.41	574.88	-538.23	530.01	476.16	53.85	9,843		
								***************************************	200.01	470.10	00.00	5,043		
,400.00	7,364,14	7,407.42		27.07	27.98	-0.41	574.88	-538,23	530 01	475.48	54.52	9.721		
,500.00	7,464.14	7,507.42		27,41	28,31	-0.41	574.88	-538.23	530.01	474.81	55.20	9.602		
,600.00	7,564.14	7,607.42	7,564.14	27.75	28.64	-0.41	574.88	-538.23	530.01	474.13	55.88	9.485		
,700.00		7,707.42	7,664.14	28,09	28.97	-0.41	574.88	-538.23	530.01	473.45	56.56	9.371		
,800.00	7,764.14	7.807.42	7,764.14	28.43	29.31	-0,41	574.88	-538.23	530.01	472.77	57.24	9.260		
000.00	7.004.44	7.007.40												
,900.00	7,864.14	7,907.42	7,864.14	28.77	29.64	-0.41	574.88	-538.23	530.01	472.09	57.92	9 151		
000.00	7,964.14	8,007.42	7,964.14	29.11	29.97	-0.41	574.88	-538.23	530.01	471.41	58.60	9.044		
100.00	8,064.14	8,107.42	8,064.14	29.46	30.31	-0.41	574.88	-538.23	530.01	470.72	59.28	8.940		
,200.00	8,164.14	8,207.42	8,164.14	29.80	30.64	-0.41	574.88	-538.23	530.01	470.04	59.97	8.838		
,300.00	8,264.14	8,307 42	8,264.14	30.14	30.98	-0.41	574.88	-538,23	530.01	469.36	60.65	8.739		
400.00	8,364,14	9 407 43	0.264.44	20.40	24.00	.								
	-	8,407.42	8,364.14	30.49	31.32	-0.41	574 88	-538.23	530.01	468.67	61.34	8.641		
500.00	8,464.14	8,507.42	8,464.14	30.83	31.65	-0.41	574 88	-538.23	530.01	467.99	62.02	8.546		
600 00	8,564.14	8,607.42	8,564.14	31,17	31.99	-0.41	574.88	-538.23	530.01	467.30	62.71	8.452		
	8,664.14	8,707.42		31.52	32.33	-0.41	574.88	-538.23	530.01	466.61	63.40	8.360		
800.00	8,764.14	8,807.42	8,764.14	31.86	32.67	-0.41	574 88	-538.23	530 01	465,92	64.08	8.271		
000.00	0.004.44	B 007 40	0.00444	20.01	22.5-	٠.٠								
	8,864 14	8,907.42		32.21	33.01	-0.41	574.88	-538.23	530 01	465.24	64.77	8.183		
	8,964.14	9,007.42		32.55	33,35	-0.41	574.88	-538.23	530 01	464 55	65.46	8.097		
	9,064,14	9,107.42		32.90	33.6 9	-0.41	574.88	-538.23	530.01	463.86	66.15	8.012		
	9,164.14	9,207,42		33.24	34.03	-0.41	574.88	-538.23	530.01	463,17	66.84	7.929		
300.00	9,264.14	9,307.42	9,264.14	33.59	34,37	-0.41	574.88	-538.23	530.01	462.48	67.53	7.848		
100.00	0.754.44	0.407.43	0.004.4.4	22.22	24									
	9,364.14	9,407.42	-	33.93	34.71	-0.41	574.88	-538.23	530.01	461.79	68.22	7.769		
	9,464.14	9,507.42		34.28	35.05	-0.41	574 88	-538.23	530.01	461.09	68.91	7.691		
	9,564.14	9,607.42		34.63	35.39	-0.41	574.88	-538.23	530.01	460.40	69.61	7.614		
	9,654.14	9.707.42		34.97	35 73	-0.41	574.88	-538,23	530.01	459.71	70.30	7.539		
800.00	9,764,14	9,807.42	9.764.14	35 32	36 08	-0.41	574.88	-538.23	530.01	459.01	70.99	7.466		

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H,

#206H, #226H

Site Error: Reference Well:

Well Error:

#226H

Reference Wellbore Lateral Reference Design: Plan #2

0.00 usft

0.00 usft

Local Co-ordinate Reference:

Well #226H - Slot #226H

TVD Reference: MD Reference:

2920+28.50 @ 2948.50usft (Patterson 282) 2920+28.50 @ 2948.50usft (Patterson 282)

North Reference:

Survey Calculation Method:

Minimum Curvature

Output errors are at

2.00 sigma

Database:

EDM 5000 14 Multi User

Offset TVD Reference: Reference Datum

Offset D	esign	Garret	t Fed Cor	n #202H, #	#222H,	#122H, #206	SH, #226H -	#222H - 1	_ateral - F	lan #2			Offset Site Error:	0 00 usft
		/WD+HDGM				•	•						Offset Well Error:	0 00 usft
Refer		Offs		Semi Major				_	Dist			_		
Measured		Measured	Vertical	Reference	Offset		Offset Wellbo		Between	Between		Separation	Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (*)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
9,900.00	9.864.14	9,907.42	9,864,14	35.67	36.42		574.88	-538.23	530.01	458.32	71,69	7.393		
10,000.00			9,964.14	36.02	36.76		574.88	-538.23	530.01	457.63	72.38	7.323		i
	10,064.14		10,064.14	36.36	37.10		574.88	-538.23	530.01	456.93	73.07	7.253		
	10,164.14			36,71	37.45		574.88	-538.23	530,01	456.24	73,77	7.185		
10,300.00	10,264.14			37.06	37.79		574.88	-538.23	530.01	455 54	74.47	7.118		
10,310.27	10,274.41	10,317.70	10,274.41	37,10	37.83	-0.41	574.88	-538,23	530,01	455.47	74.54	7,111		
10 400 00	10 364 14	10,405.47	10 362 18	37,41	38.13	-0.40	574.91	-538.06	530.04	454.88	75.16	7.052		
	10,376.24			37.45	38.16		574,96	-537.70	530.10	454.86	75.24	7.046		
		10,449.30		37.58	38.26		575.34	-535.33	530.52	455.04		7.029		
10,500.00	10,463.79	10,493.01	10,449.19	37.73	38.40	-90.03	576.29	-529,34	531,61	455.84	75.78	7.016		
10,550.00	10,512.81	10,536.64	10,491.80	37.88	38.52	-89.78	577,74	-520.12	533.30	457.25	76.05	7.013		
40.600.00	10 560 70	10 600 20	10 522 51	28.02	29.64	90.54	670 70	507.76	525 57	450 27	76 30	7.010		
	10,560.79		10,533.51 10,574.10	38.02 38.16	38.64 38.75		579.70 582.14	-507.76 -492.31	535.57 538.40	459 27 461.86		7 019 7.034	,	
	10,652.18			38.30	38.86		585.06	-473.88	541.77	465.01		7.057		
ı	10,694.89			38.43	38.96		588.43	-452.56	545.66	468.67	76.99			
	10,735.18		10,687.16	38 57	39.05		592.25	-428.45	550.04	472.83				
							F==			:-	••			
	10,772.74			38.71	39 14		596.48	-401.68	554.88	477.43				
	10,807.27	10,841,49	10,753 30	38.87 39.04	39.23 39.32		601.12 606.14	-372.35 -340.61	560.15 565.83	482.45 487.83				
	10,838.53			39.24	39.42		611.52	-306.60	571 86	493.54				,
	10,890.29			39.46	39.53		617.24	-270.45	578.23	499.52			•	
1,200.00	, 5,555.25	. 5, 5, 6, 10	. 5,550.00	556	35.50									
		11,017.79		39.72	39.66		623.27	-232.33	584.89	505.74				
		11,062.45		40.01	39.82		629.59	-192.40	591.81	512.15				
-		11,107.44		40,34	40.00		636.17	-150.83	598.93	518.71				
		11,118.38 11,153.17		40.43 40.71	40.06 40.24		637.80 643.03	-140.54 -107 45	600.69 606.25	520 32 525,40				
11,230.00	10,340.33	11,133,17	10,504.40	4U, / I	40.24	-97.12	U+13.U3	-107 43	300,23	323,40	00.03	,,450		
11,300.00	10,951.75	11,200.24	10,914.95	41.12	40.52	-87.23	650.20	-62.14	613.70	532.14	81.56	7.524		
	10,954.57			41.56	40.85		657.48	-16.13	621.24	538.91				
		11,274.89		41.83	41.05		661.71	10.63	625.61	542.80				
	10,955.00			42.03	41.21		664.86	30.51	628.86	545.68				
11,500.00	10,955.00	11,391.52	10,934.00	43.10	42.05	-88.11	679.89	125.54	644.45	559.38	85.07	7.575		
11,600.00	10,955.00	11,542.09	10,934.00	44.33	43.67	7 -88.16	697.52	275.03	656.33	568.33	88.00	7.458		
	10,955.00			45.70	45.64		703.32	427.36	660.30	569.03				
	10,955.00			45.74	45.70	-88.18	703.30	431.36	660.29	568,94				
		11,805.60		47.21	47.29		703.15	527.19	660.30	565.89				
11,900.00	10,955.00	11,905.60	10,934 00	48.83	48.89	-88.18	702. 9 9	627.19	660.30	562.68	97.62	6.764		
12 000 00	10 955 00	12,005.60	10 934 00	50.56	50.60	-88.18	702.83	727.19	660.30	559.25	101.05	6.534		
-	10,955.00			52.38	52.40		702.67	827.19	660,30	555.62				
	10,955.00			54.29	54.30		702.51	927.19	660.30	551.82				
		12,305.60		56.29	56.27		702.34	1,027.19	660.30	547.85				
12,400.00	10,955.00	12,405 60	10,934.00	58.35	58.31	1 -88,18	702.18	1,127.19	660.30	543.75	116.55	5.665		
40 500 0-	40.022.52	40 505 00	40.00 : 00				700.00	4 007		620.60	400	c .c=		
		12,505.60		60.47	60.42		702.02	1,227.19	660.30	539.52 535.18				
	10,955.00	12,605.60 12,705.60		62.65 64.89	62.59 64.80		701.86 701.70	1,327.19 1,427.19	660.30 660.30	535.18 530.73				
		12,705,60		67.16	67.07		701.70	1,527.19	660 30	526.19				
		12,905.60		69.48	69.37		701.33	1,627.19	660.30					
12,500.00	.0,000.00	. 2,300.00	. 5,557.00	05.40	35.31	30.10	, 51.51	.,521.15	300.00	521.50	,,,,,,	7.,00		
13,000.00	10,955.00	13,005 60	10,934 00	71.84	71.72		701.21	1,727.19	660.31	516.87	143.44	4.603		
	10,955.00			74.23	74 09		701.05	1,827.19	660.31					
		13,205.60		76.65	76,50	and the second s	700.89	1,927.19	660.31					
		13,305.60		79.10	78.94		700 72	2,027.19	660.31					
13,400,00	10,955.00	13,405 60	10,934.00	81.57	81.41	-88.18	700 56	2,127.19	660.31	497.45	162.86	4.054		
L						·								

PDD

Anticollision Report

Company:

MATADOR RESOURCES

Project:

Eddy County, New Mexico

Reference Site:

Garrett Fed Com #202H, #222H, #122H.

#206H, #226H

Site Error:

0.00 usft

Reference Well: Well Error:

Local Co-ordinate Reference:

TVD Reference:

MD Reference:

Well #226H - Slot #226H

2920+28.50 @ 2948.50usft (Patterson 282)

2920+28.50 @ 2948.50usft (Patterson 282)

#226H

0.00 usft

Reference Wellbore Lateral

Reference Design: Plan #2

North Reference:

Survey Calculation Method:

Output errors are at

Offset TVD Reference:

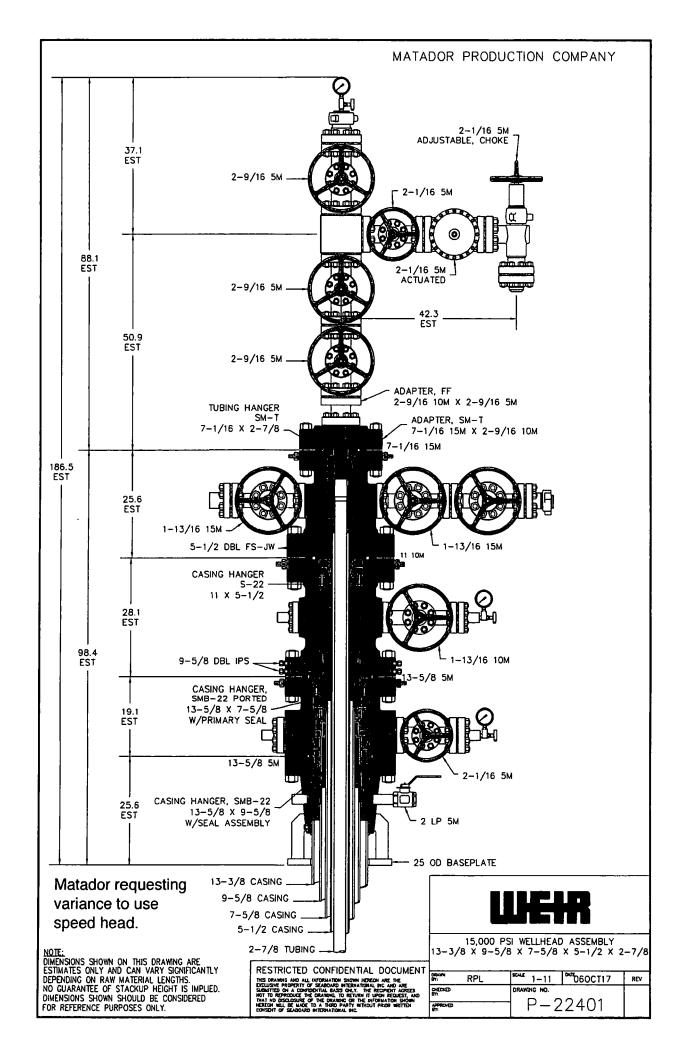
Database:

Minimum Curvature

2.00 sigma

EDM 5000 14 Multi User

Offset D	-		t Fed Co	m #202H, i	#222H, #	*122H, #20)6H, #226H -	#222H - I	Lateral - F	lan #2			Offset Site Error:	0.00 us
Survey Pro Refei		fWD+HDGM		0									Offset Well Error:	0.00 us
Reiei Measured	Vertical	Offs		Semi Major		10-1-14-			Dist			_		
Depth (usft)	Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	(usft)	Highside Toolface (*)	Offset Wellbo +N/-S (usft)	re Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning	
13,500.00	10,955.00	13,505.60	10,934,00	84.07	83.89	-88.18	700.40	2,227.19	660.31	492.46	167.85	3.934		
13,600.00	10,955.00	13,605.60	10,934.00	86.59	86.40	-88.18	700.24	2,327.19	660.31	487.44	172.87	3.820		
13,700.00	10,955.00	13,705.60	10.934.00	89.13	88.93	-88, 18	700.08	2,427.19	660.31	482.37	177.94	3,711		
13,800.00	10,955.00	13,805.60	10,934.00	91.68	91.48	-88.18	699.91	2,527.19	660.31	477.27	183.04	3.607		
13,900.00	10,955.00	13,905.60	10,934.00	94.25	94.04	-88.18	699.75	2,627 19	660,31	472.14	188.18	3.509		
14,000.00	10,955.00	14,005.60	10,934.00	96.84	96,62	-88.18	699.59	2,727 19	660.31	466.97	193.34	3.415		
14,100.00	10,955.00	14,105.60	10,934.00	99,44	99.21	-88.18	699.43	2,827.19	660.31	461.78	198.53	3.326		
14,200.00	10,955.00	14,205.60	10,934.00	102.05	101.82	-88,18	699.27	2,927.19	660.31	456.56	203.75	3.241		
14,300 00	10,955.00	14,305.60	10,934.00	104.68	104.44	-88.18	699,10	3,027.19	660.31	451.32	208.99	3.159		
14,400.00	10,955.00	14,405.60	10,934.00	107.31	107.07	-88.18	698.94	3,127.19	660,31	446.06	214.26	3.082		
14,500.00	10,955.00	14,505.60	10,934.00	109.96	109.71	-88.18	698.78	3,227.19	660.31	440.77	219,54	3.008		
14,600.00	10,955.00			112.61	112.36	-88.18	698.62	3,327.19	660,31	435.47	224.85	2.937		
-	10,955.00	14,705.60	10,934.00	115.28	115.02	-88.18	698.46	3,427.19	660.31	430,15	230.17	2.869		
14,800.00	10,955.00	14,805.60	10,934.00	117.95	117.68	-88.18	698.29	3,527 19	660 32	424.81	235.51	2.804		
-	10,955.00	14,905.60	10,934.00	120.63	120.36	-88.18	698.13	3,627.18	660 32	419.46	240.86	2.741		
15,000.00	10,955.00	15,005.60	10,934.00	123.31	123.04	-88.18	697.97	3,727 18	660 32	414.09	246.23	2.682		
	10,955.00		10,934.00	126 01	125.73	-88.18	697.81	3,827.18	660 32	408.71	251.61	2.624		
15,200.00	10,955.00	15,205.60	10,934.00	128 71	128.43	-88.18	697.64	3,927.18	660.32	403.31	257.00	2.569		
15,300.00	10,955,00	15,305.60	10,934.00	131.41	131.13	-88,18	697.48	4.027.18	660.32	397.91	262.41	2.516		
15,400,00	10,955.00	15,405.60	10,934,00	134,12	133.83	-88,18	697.32	4,127.18	660 32	392.49	267.83	2.465		
15.500.00	10,955.00	15,505,60	10,934.00	136.84	136.55	-88.18	697.16	4,227.18	660.32	387.07	273.25	2.417		
	10,955.00			139.56	139.26	-88.18	697.00	4,327.18	660.32	381.63	278.69	2.369		
-	10,955.00			142.29	141.68	-88.18	696.83	4,427.18	660.32	376.49	283.83	2.326		
	10,955.00			142.32	141.71	-88.18	696.83	4,428 23	660.32	376.43	283.89	2.326		
15,720,48	10,955.00	15,711.79	10,934.00	142.85	142.16	-88.18	696.81	4,444.58	660.33	375,44	284.88	2.318 S	F	



VRCC 16-1177 Rev02 for Houston Field Service

DATA ARE INFORMATIVE ONLY. BASED ON SI_PD-101836 P&B



OD	Weight	Wall Th.	Grade	API Drift	Connection
7 5/8 in.	29.70 lb/ft	0.375 in.	P110 EC	6.750 in.	VAM® HTF NR

PIPE PROPER	TIES	
Nominal OD	7.625	łn.
Nominal ID	6.875	in.
Nominal Cross Section Area	8.541	sqın.
Grade Type	Enhanced API	
Min. Yleid Strength	125	ksi
Max. Yield Strength	140	ksi
Min. Ultimate Tensile Strength	135	ksi
Tensile Yield Strength	1 068	kib
Internal Yield Pressure	10 760	psi
Collapse pressure	7 360	psi

CONNECTION PROPERTIES									
Connection Type	Premium Integral Flush								
Connection OD (nom)	7.701 in.								
Connection ID (nom)	6.782 in.								
Make-Up Loss	4.657 in.								
Critical Cross Section	4.971 sqin.								
Tension Efficiency	58 % of pipe								
Compression Efficiency	72.7 % of pipe								
Compression Efficiency with Sealability	34.8 % of pipe								
Internal Pressure Efficiency	100 % of pipe								
External Pressure Efficiency	100 % of pipe								

CONNECTION PERFORMANCES								
Tensile Yield Strength	619 klb							
Compression Resistance	778 klb							
Compression with Sealability	372 klb							
Internal Yield Pressure	10 760 psi							
External Pressure Resistance	7 360 psi							
Max. Bending	44 °/100ft							
Max. Bending with Sealability	17 °/100ft							

TORQUE VALUES									
Min. Make-up torque	9 600 ft.lb								
Opti. Make-up torque	11 300 ft.lb								
Max. Make-up torque	13 000 ft.lb								
Max. Torque with Sealability	58 500 ft.lb								
Max. Torsional Value	73 000 ft.lb								

VAMP HTF" (High Torque Flush) is a flush OD integral connection providing maximum clearance along with torque strength for challenging applications such as extended reach and slim hole wells, drilling liner / casing, liner rotation to acheive better cementation in highly deviated and critical High Pressure / High Temperature wells.

Looking ahea on the outcoming testing industry standards, VAM® decided to create an upgraded design and launch on the market the VAM® HTF-NR as the new standard version of VAM® extreme high torque flush connection. The VAM® HTF-NR has extensive tests as per API RP 5C5:2015 CAL II which include the gas sealability having load points with bending, internal pressure and high temperature at 135°C.

Do you need help on this product? - Remember no one knows VAM® like VAM®

canada@vamfieldservice.com usa@vamfieldservice.com mexico@vamfieldservice.com brazil@vamfieldservice.com

uk@vamfieldservice.com dubai@vamfieldservice.com nigeria@vamfieldservice.com angola@vamfieldservice.com china@vamfieldservice.com baku@vamfieldservice.com singapore@vamfieldservice.com australia@vamfieldservice.com

Over 180 VAM® Specialists available worldwide 24/7 for Rig Site Assistance

Other Connection Data Sheets are available at www.vamservices.com

Vallourec Group



For the latest performance data, always visit our website: www.tenaris.com

July 15 2015



Size: 5.500 in. Wall: 0.361 in.

Weight: 20.00 lbs/ft

Grade: P110-IC

Min. Wall Thickness: 87.5 %

Tenaris	
----------------	--

Casing/Tubing: CAS

Connection: TenarisXP™ BTC

Coupling Option: REGULAR

		PIPE BODY	DATA								
		GEOMET	RY								
Nominal OD	5.500 in.	Nominal Welght	20.00 lbs/ft	Standard Drift Diameter	4.653 in.						
Nominal ID	4.778 in.	Wall Thickness	0.361 in.	Special Drift Diameter	N/A						
Plain End Weight	19.83 lbs/ft										
		PERFORM	ANCE								
Body Yield Strength	641 x 1000 lbs	Internal Yleld	12630 psi	SMYS	110000 psi						
Collapse	12100 psi										
		LA DICYDIM DIC CO	NAISCETANI D	A T A							
TENARISXP™ BTC CONNECTION DATA GEOMETRY											
		1			4.766 :-						
Connection OD	6.100 in.	Coupling Length	9.450 in.	Connection ID	4.766 in.						
Critical Section Area	5.828 sq. in.	Threads per in.	5.00	Make-Up Loss	4.204 in.						
PERFORMANCE											
Tension Efficiency	100 %	Joint Yield Strength	641 x 1000 lbs	Internal Pressure Capacity ⁽¹⁾	12630 psi						
Structural Compression Efficiency	100 %	Structural Compression Strength	641 x 1000 lbs	Structural Bending ⁽²⁾	92 °/100 ft						
External Pressure Capacity	12100 psi										
	E	STIMATED MAKE-	UP TORQUES	(3)							
Minimum	11270 ft-lbs	Optimum	12520 ft-lbs	Maximum	13770 ft-lb						
OPERATIONAL LIMIT TORQUES											
Operating Torque	21500 ft-lbs	Yield Torque	23900 ft-lbs								

BLANKING DIMENSIONS

Blanking Dimensions

- (1) Internal Pressure Capacity related to structural resistance only. Internal pressure leak resistance as per section 10.3 API 5C3 / ISO 10400 - 2007.
- (2) Structural rating, pure bending to yield (i.e no other loads applied)
- (3) Torque values calculated for API Modified thread compounds with Friction Factor=1. For other thread compounds please contact us at licensees@oilfield.tenaris.com. Torque values may be further reviewed. For additional information, please contact us at contact-tenarishydril@tenaris.com

Matador Production Company Garrett Fed Com 226H SHL 2372' FNL & 584' FWL BHL 2323' FNL & 240' FEL Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

Drilling Program

1. ESTIMATED TOPS

Formation Name	TVD	MD	Bearing
Quaternary	0′	0′	water
Rustler anhydrite	29′	29'	N/A
Salado salt	400'	400'	N/A
Castile anhydrite	1222'	1225'	N/A
Base salt	2795'	2813'	N/A
Bell Canyon sandstone	2849'	2868'	hydrocarbons
Cherry Canyon sandstone	3761'	3788′	hydrocarbons
Brushy Canyon sandstone	4928'	4963'	hydrocarbons
Bone Spring limestone	6569'	6615'	hydrocarbons
1 st Bone Spring carbonate	7357′	7393'	hydrocarbons
1 st Bone Spring sandstone	7524'	7560'	hydrocarbons
2 nd Bone Spring carbonate	7790'	7826'	hydrocarbons
2nd Bone Spring sandstone	8294'	8330'	hydrocarbons
3 rd Bone Spring carbonate	8640'	8676'	hydrocarbon
3 rd Bone Spring sandstone	9382'	9418'	hydrocarbon
Wolfcamp A carbonate	9743'	9779'	hydrocarbon
Wolfcamp B carbonate (Goal)	10203'	10239'	hydrocarbons
(КОР	10376'	10412'	hydrocarbons)
TD	10955'	15720'	hydrocarbons

2. NOTABLE ZONES

Wolfcamp B is the goal. Hole will extend east of the last perforation point to allow for pump installation. All perforations will be \geq 330' from the dedication perimeter. Closest water well (C 00856) is 4792' northwest. Depth to water was not reported in this 380' deep well.

3. PRESSURE CONTROL

Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

A 12,000' 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and 1 annular preventer will be used below surface casing to TD. See attached BOP, choke manifold, co-flex hose, and speed head diagrams.

An accumulator complying with Onshore Order 2 requirements for the BOP stack pressure rating will be present. Rotating head will be installed as needed.

Pressure tests will be conducted before drilling out from under all casing strings. BOP will be inspected and operated as required in Onshore Order 2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position.

A third-party company will test the BOPs.

After setting the surface casing, and before drilling the surface casing shoe, a minimum 2M BOPE system will be installed. It will be tested to 250 psi low and 2000 psi high. Annular will be tested to 250 psi low and 1000 psi high.

After setting intermediate 1 casing, a minimum 3M BOPE system will be installed and tested to 250 psi low and 3000 psi high. Annular will be tested to 250 psi low and 2500 psi high.

After setting intermediate 2 casing, a minimum 5M BOPE system will be installed and tested to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high.

Matador requests a variance to have the option of running a speed head for setting the intermediate 1 and 2 strings. In the case of running a speed head with landing mandrel for 9.625" and 7" casing, a minimum 3M BOPE system will be installed after surface casing is set. BOP test pressures will be 250 psi low and 3000 psi high. Annular will be tested to 250 psi low and 2500 psi high before drilling below the surface shoe. After 7" casing is set in the speed head, the BOP will then be lifted to install another casing head section for setting the production casing. Matador will nipple up the casing head and BOP and a minimum 5M BOPE system will be installed. Pressure tests will be made to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high. A diagram of the speed head is attached.

Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. Manufacturer does not require the hose to be anchored. If the specific hose is not available, then one of equal or higher rating will be used.

Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

4. CASING & CEMENT

All casing will be API and new. See attached casing assumption worksheet.

Hole O. D.	Set MD	Set TVD	Casing O. D.	Weight (lb/ft)	Grade	Joint	Collapse	Burst	Tension
17.5"	0′ - 610'	0' - 610'	13.375" surface	54.5	J-55	втс	1.125	1.125	1.8
12.25"	0' - 2900'	0' - 2881'	9.625" inter. 1	40	J-55	втс	1.125	1.125	1.8
8.75"	0′ - 2600'	0' - 2584'	7.625" inter. 2 top	29	P-110	втс	1.125	1.125	1.8
8.75"	2600' - 10300'	2584' - 10264'	7.625" inter. 2 middle	29.7	P-110	VAM HTF-NR	1.125	1.125	1.8
8.75"	10300' - 11212'	10264' - 10940'	7.0" inter. 2 bottom	29.7	P-110	втс	1.125	1.125	1.8
6.125"	0' - 10200'	0' - 10164'	5.5" product. top	20	P-110	втс/тхр	1.125	1.125	1.8
6.125"	10200' - 15720'	10164' - 10955'	4.5" product. bottom	13.5	P-110	втс/тхр	1.125	1.125	1.8

Name	Type	Sacks	Yield	Cu. Ft.	Weight	Blend
Surface	Lead	268	1.82	487	12.8	Class C + bentonite + 2% CaCl ₂ + 3% NaCl + LCM
	Tail	352	1.38	485	14.8	Class C + 5% NaCl + LCM
TOC = Gl	-	1	00% Exce	ss	Centra	lizers per Onshore Order 2.III.B.1f
Intermediate 1	Lead	638	2.13	1358	12.6	Class C + bentonite + 1% CaCl ₂ + 8% NaCl + LCM
	Tail	202	1.38	278	14.8	Class C + 5% NaCl + LCM
TOC = GI	-	1	00% Exce	ss	2 on b	tm jt, 1 on 2nd jt, 1 every 4th jt to surface
Intermediate 2	Lead	700	2.13	1491	12.6	TXI + fluid loss + dispersant + retarder + LCM
	Tail	225	1.38	310	14.8	TXI + fluid loss + dispersant +

Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

						retarder + LCM
TOC = 260	0'	60% Excess			2 on btm jt, 1 on 2nd jt, 1 every other jt to top of tail cement (500' above TOC)	
Production	Tail	530	1.17	620	15.8	Class H + fluid loss + dispersant + retarder + LCM
TOC = 990	0'	25% Excess			2 on btm jt, 1 on 2nd jt, 1 every third jt to top of curve	

5. MUD PROGRAM

An electronic Pason mud monitoring system complying with Onshore Order 1 will be used. All necessary mud products (barite, bentonite, LCM) for weight addition and fluid loss control will be on location at all times. Mud program is subject to change due to hole conditions. A closed loop system will be used.

Туре	Interval (MD)	lb/gal	Viscosity	Fluid Loss
fresh water spud	0' - 610'	8.3	28	NC
brine water	610' - 2900'	10.0	30-32	NC
fresh water & cut brine	2900' - 11212'	9.0	30-31	NC
ОВМ	11212' - 15720'	12.5	50-60	<10

6. CORES, TESTS, & LOGS

No core or drill stem test is planned.

A 2-person mud logging program will be used from ≈11,200' MD to TD.

No electric logs are planned at this time. GR will be collected through the MWD tools from intermediate casing to TD. CBL with CCL will be run as far as gravity will let it fall to TOC.

7. DOWN HOLE CONDITIONS

No abnormal pressure or temperature is expected. Maximum expected bottom hole pressure is ≈7000 psi. Expected bottom hole temperature is ≈170° F.

Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

In accordance with Onshore Order 6, Matador does not anticipate that there will be enough H_2S from the surface to the Bone Spring to meet the BLM's minimum requirements for the submission of an " H_2S Drilling Operation Plan" or "Public Protection Plan" for drilling and completing this well. Since Matador has an H_2S safety package on all wells, an " H_2S Drilling Operations Plan" is attached. Adequate flare lines will be installed off the mud/gas separator where gas may be flared safely. All personnel will be familiar with all aspects of safe operation of equipment being used.

8. OTHER INFORMATION

Anticipated spud date is upon approval. It is expected it will take ≈3 months to drill and complete the well.



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Well Name: GARRETT FED COM

Well Type: CONVENTIONAL GAS WELL



APD ID: 10400026769

Submission Date: 01/31/2018

Operator Name: MATADOR PRODUCTION COMPANY

Well Number: 226H

Well Work Type: Drill

Show Final Text

Section 1 - Existing Roads

Will existing roads be used? YES

Existing Road Map:

Garrett 226H Road Map 20180131093204.pdf

Existing Road Purpose: ACCESS

Row(s) Exist? NO

ROW ID(s)

ID:

Do the existing roads need to be improved? NO

Existing Road Improvement Description:

Existing Road Improvement Attachment:

Section 2 - New or Reconstructed Access Roads

Will new roads be needed? YES

New Road Map:

Garrett 226H New Road Map 20180131093216.pdf

New road type: RESOURCE

Length: 764.14

Feet

Width (ft.): 30

Max slope (%): 0

Max grade (%): 4

Army Corp of Engineers (ACOE) permit required? NO

ACOE Permit Number(s):

New road travel width: 14

New road access erosion control: Detour borrow ditch will be frequently riprapped to slow discharge. If riprap is unavailable, then sand bags will be used. Straw wattles and geotextile fabric will not be used.

New road access plan or profile prepared? NO

New road access plan attachment:

Access road engineering design? NO

Access road engineering design attachment:

Well Name: GARRETT FED COM Well Number: 226H

Access surfacing type: OTHER

Access topsoil source: ONSITE

Access surfacing type description: CALICHE

Access onsite topsoil source depth: 6

Offsite topsoil source description:

Onsite topsoil removal process: Grader

Access other construction information: No new road is needed to access the pad. However, the pad will block the existing road that crosses the pad. That road provides access to Chevron and Judah oil wells in Section 31. A 764.14' permanent detour will be built north and west of Matador's pad. The 764.14' of new resource road will be crowned and ditched, have a 14' wide driving surface, and be surfaced with caliche. Maximum disturbed width = 30'. Maximum grade = 4%. Maximum cut or fill = 3'.

Access miscellaneous information:

Number of access turnouts:

Access turnout map:

Drainage Control

New road drainage crossing: OTHER

Drainage Control comments: New road will be crowned and ditched. No culvert, cattle guard, or vehicle turn out is needed.

Road Drainage Control Structures (DCS) description: ROAD WILL BE CROWNED AND DITCHED. NO FURTHER DRAINAGE CONSTRUCTION ANTICIPATED. Roads will be maintained as needed to Gold Book standards. This includes pulling ditches, preserving the crown, and cleaning culverts. This will be done at least once a year, and more often as needed

Road Drainage Control Structures (DCS) attachment:

Access Additional Attachments

Additional Attachment(s):

Section 3 - Location of Existing Wells

Existing Wells Map? YES

Attach Well map:

Garrett 226H Well Map 20180131093317.pdf

Existing Wells description:

Section 4 - Location of Existing and/or Proposed Production Facilities

Submit or defer a Proposed Production Facilities plan? SUBMIT

Production Facilities description: An existing tank battery on Matador's Garrett Fed Com 221H pad in NWNW 32-24s-29e will be used. Matador will bury 7 pipelines between the 122H pad and 221H pad. Five of the pipelines will be 3" O. D., X42 carbon steel, Schedule 80, MAOP 1440 psi, flow lines. Sixth pipeline will be a 2" O. D., X42 carbon steel, Schedule 80,

Well Name: GARRETT FED COM Well Number: 226H

MAOP 1440 psi, gas lift supply line. Seventh pipeline will be 8.625" O. D., steel, 1.232" WT SDR-7, MAOP 200 psi, produced water pipeline. No power line is needed given the gas lift supply line. Pipelines will be buried with >48" of cover in a 75' x 2,047.64' long corridor.

Production Facilities map:

Garrett_226H_Production_Facilities_20180131093354.pdf

Section 5 - Location and Types of Water Supply

Water Source Table

Water source use type: DUST CONTROL,

Water source type: GW WELL

INTERMEDIATE/PRODUCTION CASING, STIMULATION, SURFACE

CASING

Describe type:

Source longitude:

Source latitude:

Source datum:

Water source permit type: PRIVATE CONTRACT

Source land ownership: PRIVATE

Water source transport method: TRUCKING

Source transportation land ownership: PRIVATE

Water source volume (barrels): 20000 Source volume (acre-feet): 2.577862

Source volume (gal): 840000

Water source and transportation map:

Garrett 226H Water Source Map 20180131093431.pdf

Water source comments: Water will be trucked via existing roads from existing water well C 00464 on private land in NENW 13-24s-28e.

New water well? NO

New Water Well Info

Well latitude:

Well Longitude:

Well datum:

Well target aquifer:

Est. depth to top of aquifer(ft):

Est thickness of aquifer:

Aquifer comments:

Aguifer documentation:

Well depth (ft):

Well casing type:

Well casing outside diameter (in.):

Well casing inside diameter (in.):

New water well casing?

Used casing source:

Drilling method:

Drill material:

Well Name: GARRETT FED COM Well Number: 226H

Grout material:

Grout depth:

Casing length (ft.):

Casing top depth (ft.):

Well Production type:

Completion Method:

Water well additional information:

State appropriation permit:

Additional information attachment:

Section 6 - Construction Materials

Construction Materials description: NM One Call (811) will be notified before construction starts. Top 6" of soil and brush will be stockpiled east of the pad. V-door will face east. Closed loop drilling system will be used. Caliche will be hauled from an existing caliche pit on private (Calderon) land in NWNE 9-24s-28e. A berm will be built around the fill sides of the pad. Construction Materials source location attachment:

Garrett_226H_Construction_Methods_20180131093534.pdf

Section 7 - Methods for Handling Waste

Waste type: DRILLING

Waste content description: Contents (drill cuttings, mud, salts, and other chemicals) of the mud tanks will be hauled to a state approved disposal site, e. g., Petro Waste Environmental LP at Orla, Texas. (Texas Railroad Commission permit

number STF-0101, P012234, P012236.) **Amount of waste:** 2000 barrels

Waste disposal frequency: Daily

Safe containment description: Steel roll-off tanks

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE

FACILITY

Disposal type description:

Disposal location description: Petro Waste Environmental LP at Orla, Texas. (Texas Railroad Commission permit number

STF-0101, P012234, P012236.

Reserve Pit

Reserve Pit being used? NO

Temporary disposal of produced water into reserve pit?

Reserve pit length (ft.)

Reserve pit width (ft.)

Reserve pit depth (ft.)

Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

Well Name: GARRETT FED COM Well Number: 226H

Cuttings Area

Cuttings Area being used? NO

Are you storing cuttings on location? YES

Description of cuttings location Steel tanks

Cuttings area length (ft.)

Cuttings area width (ft.)

Cuttings area depth (ft.)

Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

WCuttings area liner

Cuttings area liner specifications and installation description

Section 8 - Ancillary Facilities

Are you requesting any Ancillary Facilities?: NO

Ancillary Facilities attachment:

Comments:

Section 9 - Well Site Layout

Well Site Layout Diagram:

Garrett_226H_Well_Site_Layout_20180131093618.pdf

Comments:

Section 10 - Plans for Surface Reclamation

Type of disturbance: New Surface Disturbance Multiple Well Pad Name: GARRETT FED COM

Multiple Well Pad Number: 122H

Recontouring attachment:

Garrett_226H_Recontour_Plat_20180131093635.pdf

Garrett_226H_Interim_Reclamation_Diagram_20180131093646.pdf

Drainage/Erosion control construction: Crowned and ditched

Drainage/Erosion control reclamation: Harrowed on the contour

Well Name: GARRETT FED COM Well Number: 226H

Well pad proposed disturbance

(acres): 3.65

Road proposed disturbance (acres):

0.53

Powerline proposed disturbance

(acres): 0

Pipeline proposed disturbance

(acres): 3.53

Other proposed disturbance (acres): 0

Total proposed disturbance: 7.71

Well pad interim reclamation (acres): Well pad long term disturbance (acres): 1.74

Road interim reclamation (acres): 0.01 Road long term disturbance (acres):

Powerline interim reclamation (acres): Powerline long term disturbance

Pipeline interim reclamation (acres):

3.53

Other interim reclamation (acres): 0

Total interim reclamation: 5.45

Pipeline long term disturbance

(acres): 0

(acres): 0

Other long term disturbance (acres): 0

Total long term disturbance: 2.26

Disturbance Comments:

Reconstruction method: Interim reclamation will be completed within 6 months of completing the well. Interim reclamation will consist of shrinking the pad 52% (1.91 acre) by removing caliche and reclaiming the west (10'), south (100'), and east (100') sides. A 20' dead end road on the west side of the pad will also be reclaimed. This will leave 1.74 acres for producing 5 wells and tractor-trailer turn around.

Topsoil redistribution: Enough stockpiled topsoil will be retained to cover the remainder of the pad when the well is plugged. Once the last well is plugged, then the rest of the pad and 764.14' of new road will be similarly reclaimed within 6 months of plugging. The old road will be re-opened. Noxious weeds will be controlled. Soil and brush will be evenly spread over disturbed areas and harrowed on the contour. Disturbed areas will be seeded in accordance with the State Land Office's requirements.

Soil treatment: None

Existing Vegetation at the well pad:

Existing Vegetation at the well pad attachment:

Existing Vegetation Community at the road:

Existing Vegetation Community at the road attachment:

Existing Vegetation Community at the pipeline:

Existing Vegetation Community at the pipeline attachment:

Existing Vegetation Community at other disturbances:

Existing Vegetation Community at other disturbances attachment:

Non native seed used? NO

Non native seed description:

Seedling transplant description:

Will seedlings be transplanted for this project? NO

Seedling transplant description attachment:

Will seed be harvested for use in site reclamation? NO

Seed harvest description:

Operator Name: MATADOR PRODUCTION COMPANY

Well Name: GARRETT FED COM

Well Number: 226H

Seed harvest description attachment:

Seed Managemen	nt	
Seed Table		
Seed type:		Seed source:
Seed name:		
Source name:		Source address:
Source phone:	•	
Seed cultivar:		
Seed use location:		
PLS pounds per acre:		Proposed seeding season:
Seed S	ummary	Total pounds/Acre:
Seed Type	Pounds/Acre]

Seed reclamation attachment:

Operator Contact/Responsible Official Contact Info

First Name:

Last Name:

Phone:

Email:

Seedbed prep:

Seed BMP:

Seed method:

Existing invasive species? NO

Existing invasive species treatment description:

Existing invasive species treatment attachment:

Weed treatment plan description: The operator shall consult with the Authorized Officer for acceptable weed control methods, which include following NMSLO requirements and policies.

Weed treatment plan attachment:

Monitoring plan description: According to NMSLO requirements

Monitoring plan attachment:

Success standards: According to NMSLO requirements

Pit closure description: No pit

Pit closure attachment:

Well Name: GARRETT FED COM Well Number: 226H

_	
S	ection 11 - Surface Ownership
Distu	rbance type: WELL PAD
Desc	ribe:
Surfa	ce Owner: STATE GOVERNMENT
Othe	r surface owner description:
BIA L	ocal Office:
BOR	Local Office:
COE	Local Office:
DOD	Local Office:
NPS	Local Office:
Siate	Flood Office the Wilh a single plant drived
Milita	ry Local Office:
USFV	NS Local Office:
Othe	r Local Office:
USFS	S Region:
USFS	Forest/Grassland:
	rbance type: NEW ACCESS ROAD
Desc	
	r surface owner description:
	ocal Office:
	Local Office:
	Local Office: Local Office:
	Local Oπice: Local Office:
NP3	ьосаі Опісе:

State Local Officer WPM MEXAGO ETANELAND OFFICE - SANTA FE

Military Local Office:

Well Name: GARRETT FED COM

Well Number: 226H

USFWS Local Office:

Other Local Office:

USFS Region:

USFS Forest/Grassland:

USFS Ranger District:

Section 12 - Other Information

Right of Way needed? NO

Use APD as ROW?

ROW Type(s):

ROW Applications

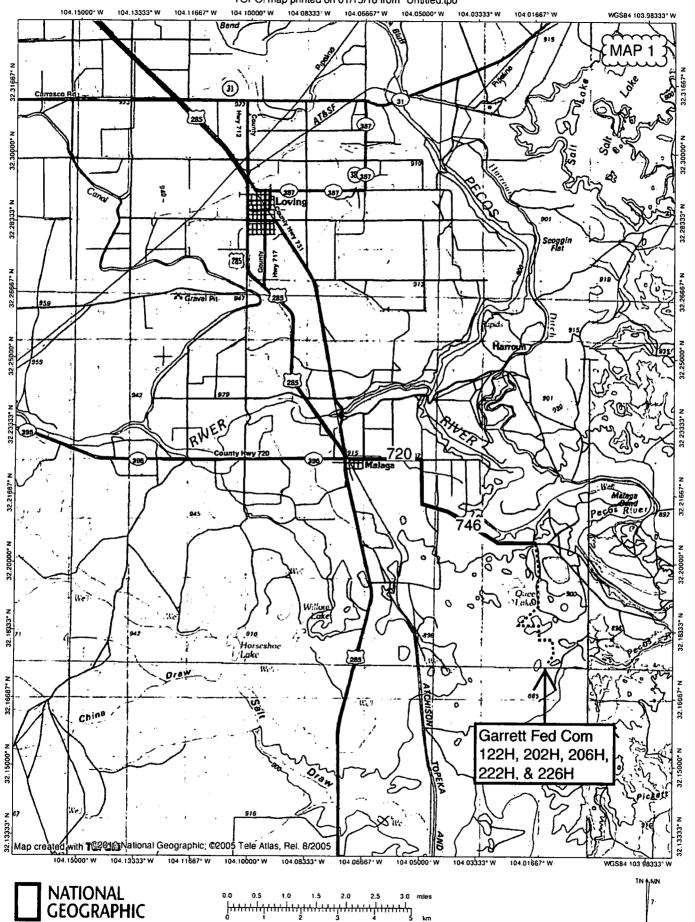
SUPO Additional Information:

Use a previously conducted onsite? YES

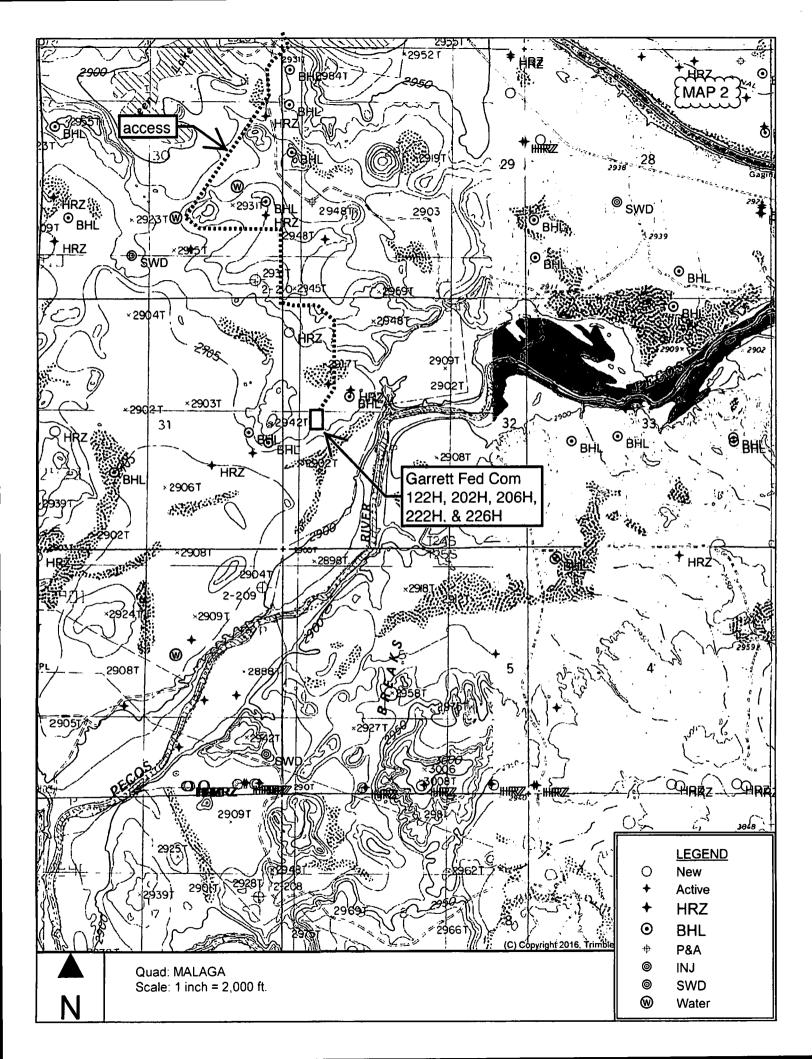
Previous Onsite information: On-site inspection was held with Jim Goodbar, Vance Wolf, et al (BLM) on August 24, 2017.

Other SUPO Attachment

Garrett_226H_General_SUPO_20180131093825.pdf
Garrett_226H_Surface_Use_Agreement_20180131093835.pdf



01/15/18



to CR 746

Garrett Fed Com 122H, 202H, 206H, 222H, 226H

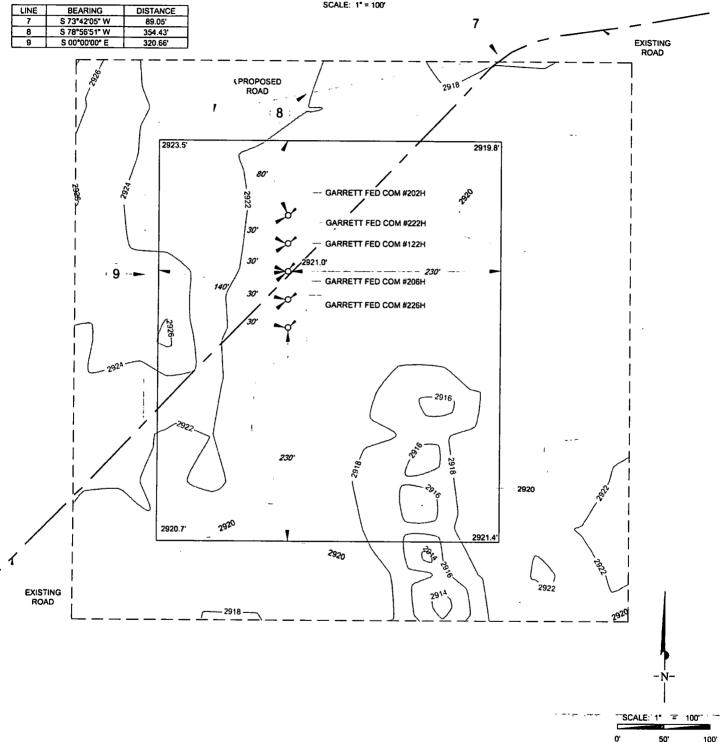


MAP 4

SECTION 32, TOWNSHIP 24S, RANGE 29-E, N.M.P.M. EDDY COUNTY, NEW MEXICO

PROPOSED ROAD LINE TABLE

DETAIL VIEW SCALE: 1° = 100°



ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO STATE PLANE COORDINATE SYSTEM, EAST ZONE OF THE NORTH AMERICAN DATUM 1983, U.S. SURVEY FEET

THIS PROPOSED PAD SITE LOCATION SHOWN HEREON HAS BEEN SURVEYED ON THE GROUND UNDER MY SUPERVISION AND PREPARED ACCORDING TO THE EVIDENCE FOUND AT THE TIME OF SURVEY, AND DATA PROVIDED BY MATADOR PRODUCTION COMPANY. THIS CERTIFICATION IS MADE AND LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE. THIS SURVEY IS CERTIFIED FOR THIS TRANSACTION ONLY.



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TELEPHONE: (817) 744-7512 • FAX (817) 744-7548

2803 NORTH BIG SPRING • MIDLAND, TEXAS 78705

TELEPHONE: (432) 582-1653 OR (800) 767-1653 • FAX (432) 582-1743

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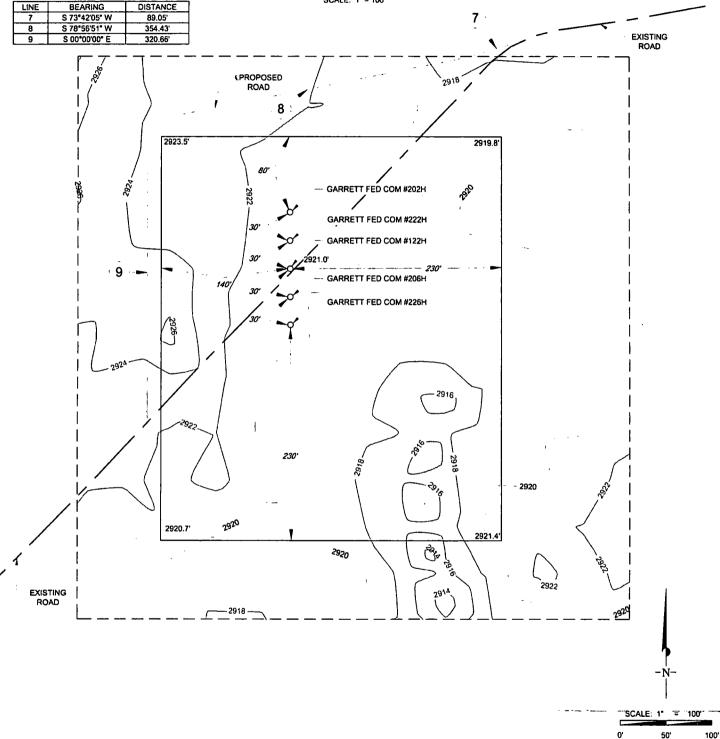




SECTION 32, TOWNSHIP 24S, RANGE 29-E, N.M.P.M. EDDY COUNTY, NEW MEXICO

PROPOSED ROAD LINE TABLE

DETAIL VIEW SCALE: 1" = 100'



ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO STATE PLANE COORDINATE SYSTEM, EAST ZONE OF THE NORTH AMERICAN DATUM 1983, U.S. SURVEY FEET

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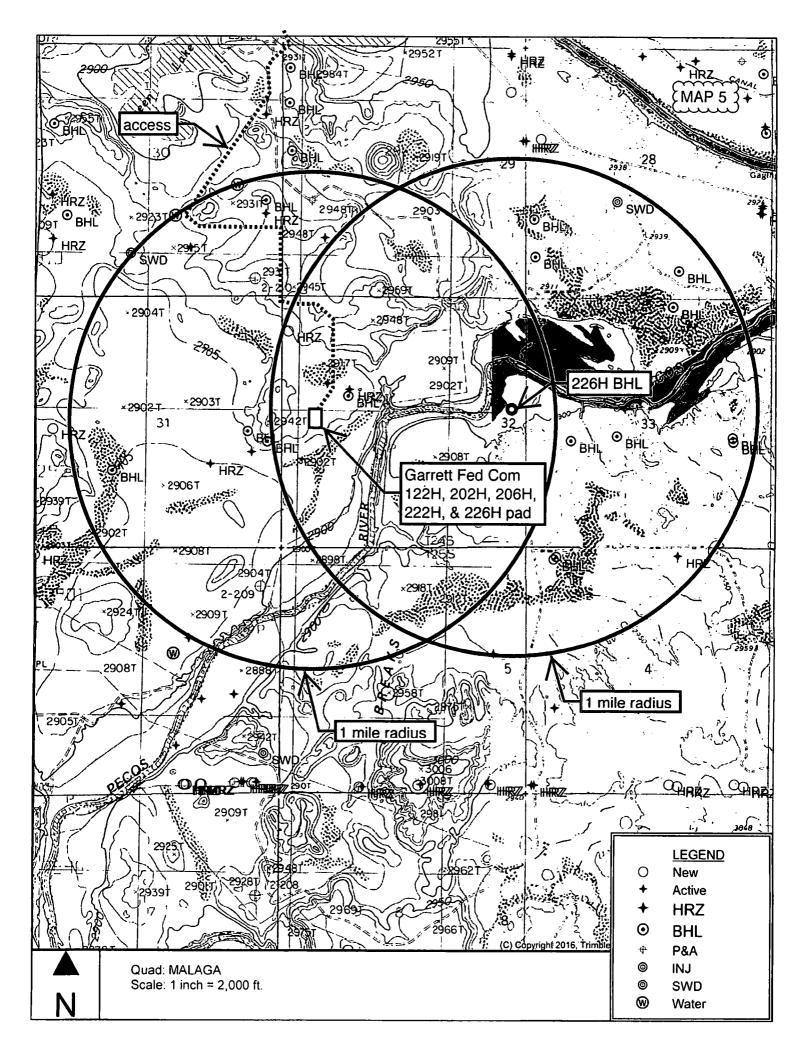
1400 EVERMAN PARKWAY, Ste. 197 • FT, WORTH, TEXAS 76140

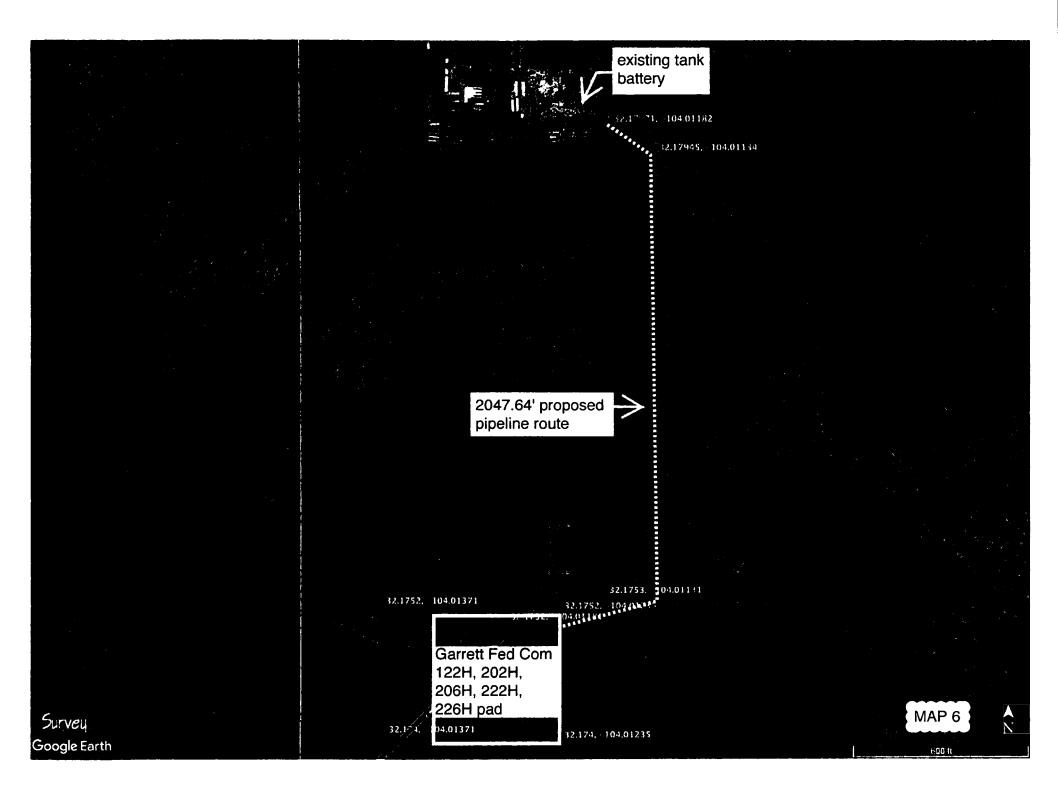
TELEPHONE: (817) 744-7512 • FAX (817) 744-7548

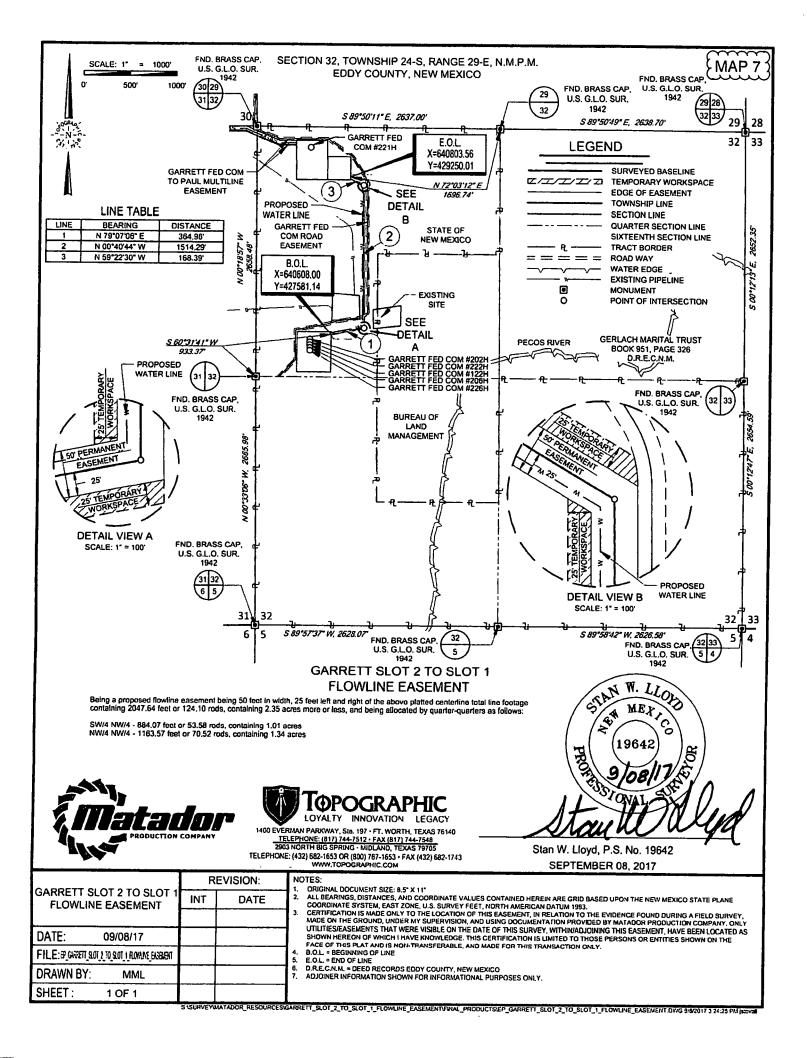
2903 NORTH BIG SPRING • MIDLAND, TEXAS 79705

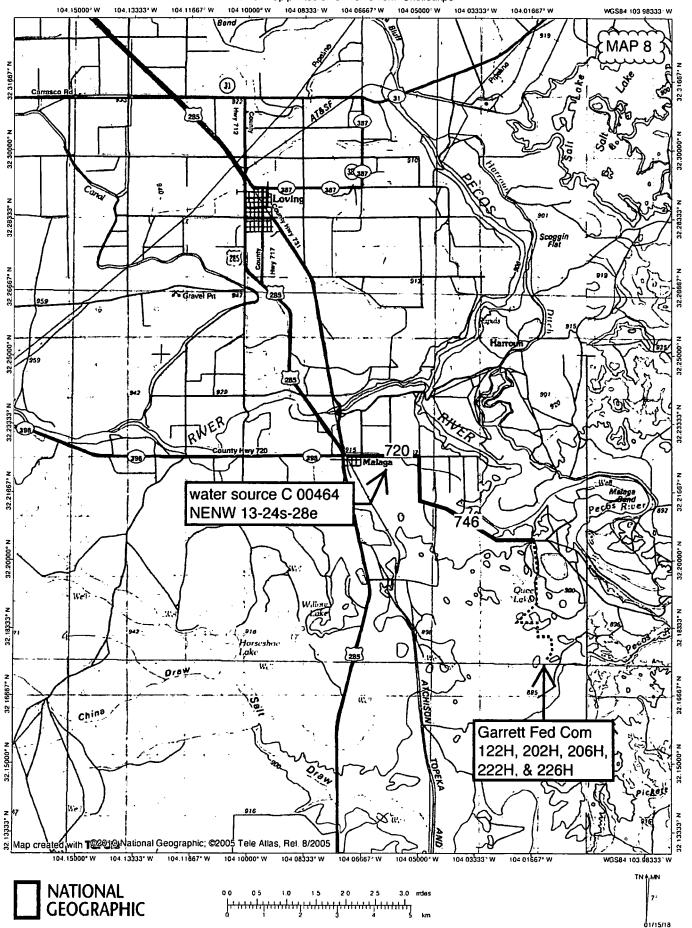
TELEPHONE: (432) 682-1653 OR (800) 767-1653 • FAX (432) 682-1743

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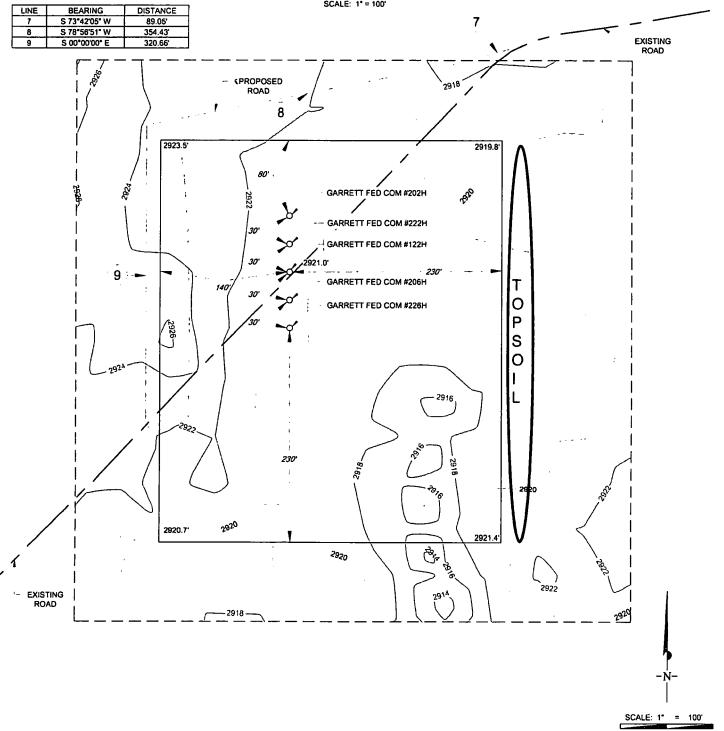


EMAP 9

SECTION 32, TOWNSHIP 24S, RANGE 29-E, N.M.P.M. EDDY COUNTY, NEW MEXICO

PROPOSED ROAD LINE TABLE

DETAIL VIEW SCALE: 1° = 100°



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100

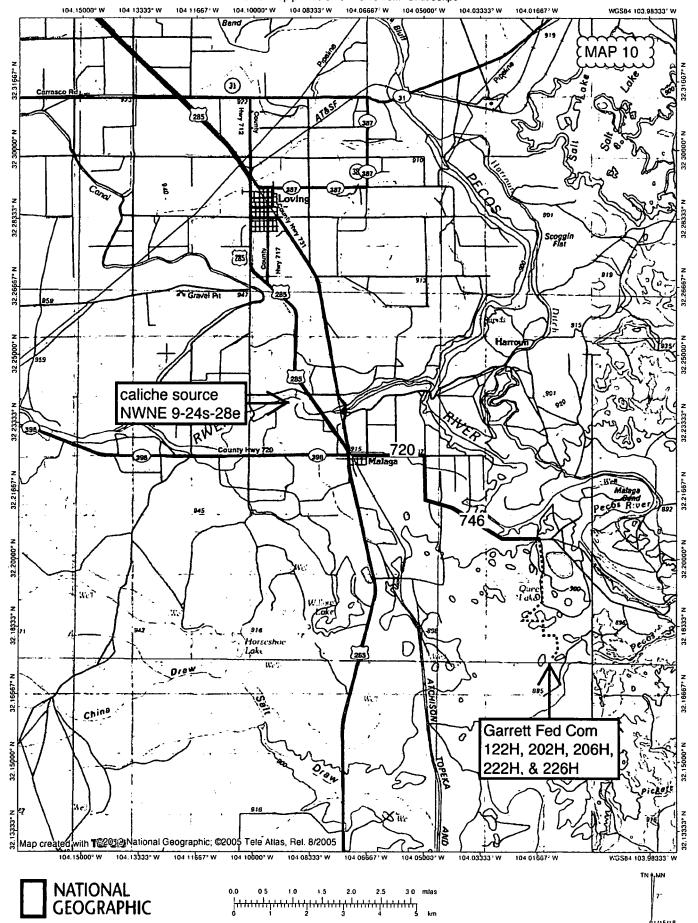
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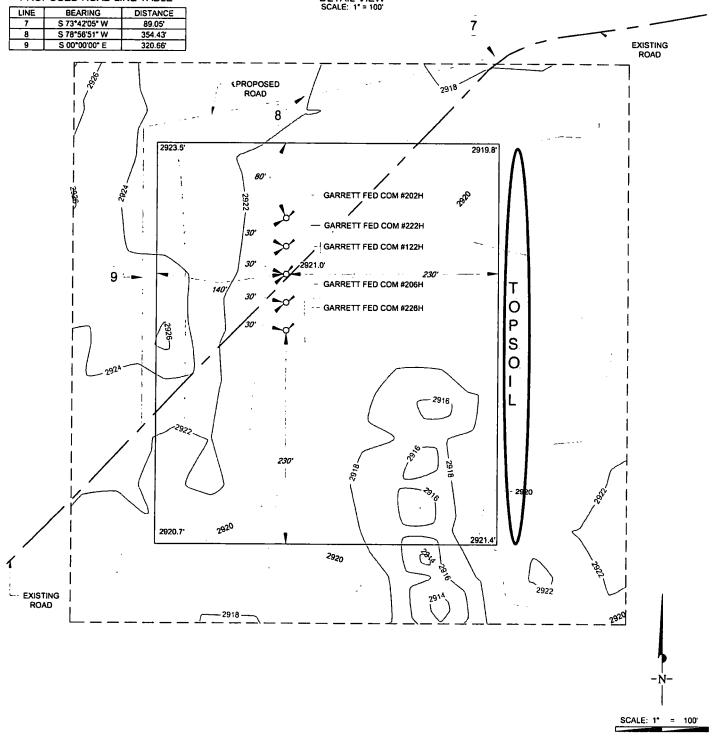




SECTION 32, TOWNSHIP 24S, RANGE 29-E, N.M.P.M. EDDY COUNTY, NEW MEXICO

PROPOSED ROAD LINE TABLE

DETAIL VIEW SCALE: 1" = 100"



ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO STATE PLANE COORDINATE SYSTEM, EAST ZONE OF THE NORTH AMERICAN DATUM 1883, U.S. SURVEY FEET

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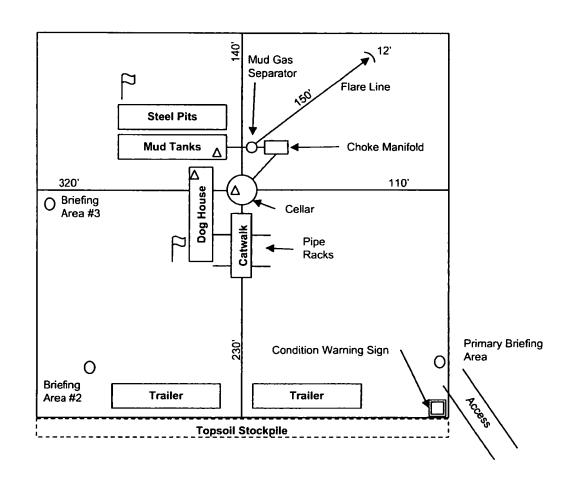
Rig Diagram

Garrett Fed Com 226H SHL 2372' FNL & 584' FWL 32-24S-29E Eddy County, NM (not to scale)

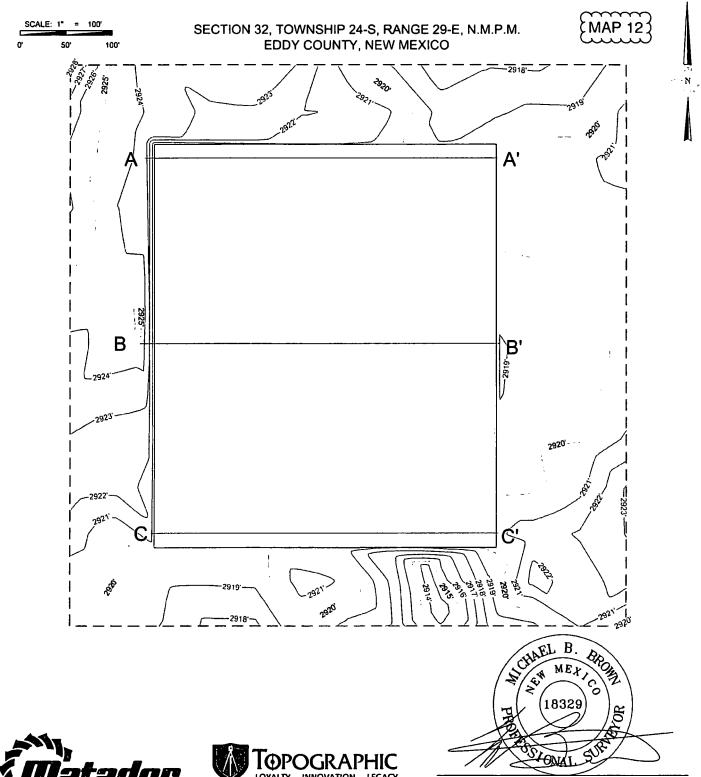
Wind Direction Indicator

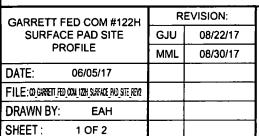
O Briefing Areas

Prevailing
Winds North











1400 EVERMAN PARKWAY, SI6. 197 - FT. WORTH, TEXAS 76140 TELEPHONE: (817) 744-7512 - FAX (817) 744-7548 TEXAS FIRM REGISTRATION NO. 10042504 WWW.TOPOGRAPHIC COM

Michael Blake Brown, P.S. No. 18329 **SEPTEMBER 01, 2017**

Field note description of even date accompanies this plat.

ORIGINAL DOCUMENT SIZE: 8.5" X 11"

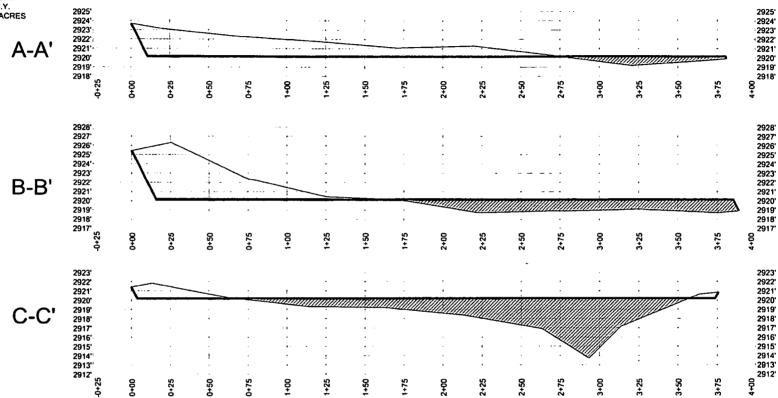
ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREIN ARE GRID BASED UPON THE NEW MEXICO STATE PLANE
COORDINATE SYSTEM, EAST ZONE, U.S. SURVEY FEET, NORTH AMERICAN DATUM ISON THE PLANE
CORDINATE SYSTEM, EAST ZONE, U.S. SURVEY FEET, NORTH AMERICAN DATUM ISON THE EVIDENCE FOUND DURING A FIELD SURVEY,
MADE ON THE GROUND, UNDER MY SUPERVISION, AND USING DOCUMENTATION PROVIDED BY MATADOR PRODUCTION COMPANY. ONLY
UTILITIES/EASEMENTS THAT WERE VISIBLE ON THE DATE OF THIS SURVEY, WITHIN/ADJOINING THE SEASEMENT, HAVE BEEN LOCATED AS
SHOWN HEREON OF WHICH I HAVE KNOWLEDGE. THIS CERTIFICATION IS LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE
FACE OF THIS PLAT AND IS NON-TRANSFERABLE, AND MADE FOR THIS TRANSACTION ONLY.

TOP OF PAD ELEVATION: 2920.1540 CUT SLOPE: 33.33% 3.000:1 18.43° FILL SLOPE: 33.33% 3.000:1 18.43° BALANCE TOLERANCE (C.Y.): 0.00 CUT SWELL FACTOR: 1.00 FILL SHRINK FACTOR: 1.00

SECTION 32, TOWNSHIP 24-S, RANGE 29-E, N.M.P.M. EDDY COUNTY: NEW MEXICO



PAD EARTHWORK VOLUMES CUT: 124,788.4 C.F., 4,621.79 C.Y. FILL: 124,788.4 C.F., 4,621.79 C.Y. AREA: 167540.1 SQ.FT., 3,846 ACRES



TOPOGRAPHIC LOYALTY INNOVATION LEGACY

Horizontal Scale = 1:60 Vertical Scale = 1:5

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	REVISION:		NOTES: 1. ORIGINAL DOCUMENT SIZE: 8.5" X 11"
GARRETT FED COM #122H SURFACE PAD SITE PROFILE	GJU	08/22/17	 ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREIN ARE GRID BASED UPON THE NEW MEXICO STATE PLANE COORDINATE SYSTEM, EAST ZONE, U.S.
	MML	08/30/17	SURVEY FEET, NORTH AMERICAN DATUM 1983. 3. CERTIFICATION IS MADE ONLY TO THE LOCATION OF THIS EASEMENT, IN RELATION TO THE
			EVIDENCE FOUND DURING A FIELD SURVEY, MADE ON THE GROUND, UNDER MY SUPERVISION, AND USING DOCUMENTATION PROVIDED BY MATADOR PRODUCTION COMPANY, ONLY UTILITIES/EASEMENTS THAT WERE VISIBLE ON THE DATE OF THIS
DATE: 06/05/17			SURVEY, WITHIN/ADJOINING THIS EASEMENT, HAVE BEEN LOCATED AS SHOWN HEREON OF WHICH I HAVE KNOWLEDGE. THIS CERTIFICATION IS LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE, AND MADE FOR THIS TRANSACTION ONLY.
FILE:OD_GARRETT_FED_COM_122H_SURFACE_PAD_SITE_REV			
DRAWN BY: EAH			
SHEET: 2 OF 2			



MAP 13

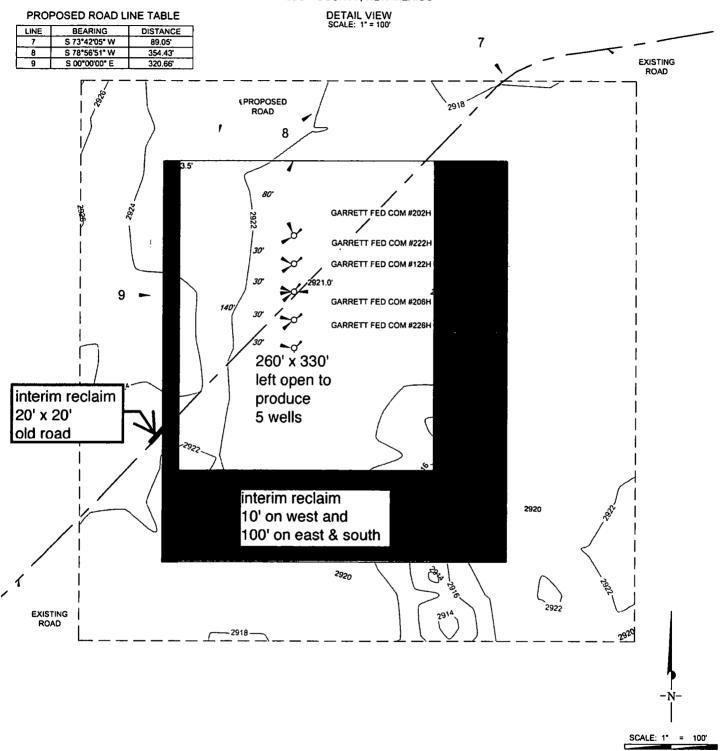
Michael Blake Brown, P.S. No. 18329 SEPTEMBER 01, 2017 Field note description of even date accompanies this plat.

S:SURVEYMATADOR_RESOURCESIGARRETT_FED_COM_122H_SURFACE_PAD_SITE-FINAL_PRODUCTSICD_GARRETT_FED_COM_122H_SURFACE_PAD_SITE_REV2.DWG 8/1/2017 10:11 50 AM milewin





SECTION 32, TOWNSHIP 24S, RANGE 29-E, N.M.P.M. EDDY COUNTY, NEW MEXICO



ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO STATE PLANE COORDINATE SYSTEM, EAST ZONE OF THE NORTH AMERICAN DATUM 1983, U.S. SURVEY FEET

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1400 EVERMAN PARKWAY, SIB. 197 · FT. WORTH, TEXAS 76140 <u>TELEPHONE:</u> (817) 744-7512 · FAX (817) 744-7548 2903 NORTH BIG SPRING · MIDLAND, TEXAS 79705 TELEPHONE: (432) 682-1653 OR (800) 767-1653 · FAX (432) 682-1743 WWW.TOPOGRAPHIC.COM

Matador Production Company Garrett Fed Com 226H SHL 2372' FNL & 584' FWL BHL 2323' FNL & 240' FEL Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

Surface Use Plan

1. ROAD DIRECTIONS & DESCRIPTIONS (See MAPS 1 - 4)

From the junction of US 285 & NM 396 in Malaga, NM...

Go E 1-1/3 miles on paved County Road 720

Then turn right and go SE 2.9 miles on paved County Road 746

Then turn right and go SW 1.5 miles on a caliche road

Turn left after crossing a cattle guard

Then go E, SE, S, and SW 1.3 miles on a caliche road directly onto the pad

Non-county roads will be maintained as needed to Gold Book standards. This includes pulling ditches, preserving the crown, and cleaning culverts. This will be done at least once a year, and more often as needed.

2. ROAD TO BE BUILT OR UPGRADED (See MAP 4)

No new road is needed to access the pad. However, the pad will block the existing road that crosses the pad. That road provides access to Chevron and Judah oil wells in Section 31. A 764.14' permanent detour will be built north and west of Matador's pad. The 764.14' of new resource road will be crowned and ditched, have a 14' wide driving surface, and be surfaced with caliche. Maximum disturbed width = 30'. Maximum grade = 4%. Maximum cut or fill = 3'. No culvert, cattle guard, or vehicle turn out is needed.

Detour borrow ditch will be frequently riprapped to slow discharge. If riprap is unavailable, then sand bags will be used. Straw wattles and geotextile fabric will not be used.

Upgrading will consist of patching potholes with caliche along the quarter-mile of road south from Matador's existing well in NWNW Section 32.



Matador Production Company
Garrett Fed Com 226H
SHL 2372' FNL & 584' FWL
BHL 2323' FNL & 240' FEL
Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

3. EXISTING WELLS (See MAP 5)

Existing oil, gas, water, disposal, and P & A wells are within a mile. No injection well is within a mile radius.

4. PROPOSED PRODUCTION FACILITIES (See MAPS 6 & 7)

An existing tank battery on Matador's Garrett Fed Com 221H pad in NWNW 32-24s-29e will be used. Matador will bury 7 pipelines between the 202H pad and 221H pad. Five of the pipelines will be 3" O. D., X42 carbon steel, Schedule 80, MAOP 1440 psi, flow lines. Sixth pipeline will be a 2" O. D., X42 carbon steel, Schedule 80, MAOP 1440 psi, gas lift supply line. Seventh pipeline will be 8.625" O. D., steel, 1.232" WT SDR-7, MAOP 200 psi, produced water pipeline. No power line is needed given the gas lift supply line. Pipelines will be buried with \geq 48" of cover in a 75' x 2,047.64' long corridor.

5. WATER SUPPLY (See MAP 8)

Water will be trucked via existing roads from existing water well C 00464 on private land in NENW 13-24s-28e.

6. CONSTRUCTION MATERIALS & METHODS (See MAPS 9 & 10)

NM One Call (811) will be notified before construction starts. Top \approx 6" of soil and brush will be stockpiled east of the pad. V-door will face east. Closed loop drilling system will be used. Caliche will be hauled from an existing caliche pit on private (Calderon) land in NWNE 9-24s-28e. A berm will be built around the fill sides of the pad.



Matador Production Company
Garrett Fed Com 226H
SHL 2372' FNL & 584' FWL
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Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

7. WASTE DISPOSAL

All trash will be placed in a portable trash cage. It will be hauled to the Eddy County landfill. There will be no trash burning. Contents (drill cuttings, mud, salts, and other chemicals) of the mud tanks will be hauled to a state approved disposal site, e. g., Petro Waste Environmental LP at Orla, Texas. (Texas Railroad Commission permit number STF-0101, P012234, P012236.) Human waste will be disposed of in chemical toilets and hauled to the Carlsbad wastewater treatment plant.

8. ANCILLARY FACILITIES

There will be no airstrip or camp. Camper trailers will be on location for the company man, tool pusher, and mud logger.

9. WELL SITE LAYOUT (See MAP 9)

Also see Rig Layout diagram for depictions of the well pad, trash cage, access onto the location, parking, living facilities, and rig orientation.

10. RECLAMATION (See MAPS 11 - 13)

Interim reclamation will be completed within 6 months of completing the well. Interim reclamation will consist of shrinking the pad $\approx 52\%$ (1.91 acre) by removing caliche and reclaiming the west (10'), south (100'), and east (100') sides. A 20' dead end road on the west side of the pad will also be reclaimed. This will leave 1.74 acres for producing 5 wells and tractor-trailer turn around. Disturbed areas will be contoured to match pre-construction grades. Soil and brush will be evenly spread over disturbed areas and harrowed on the contour. Disturbed areas will be seeded in accordance with the State Land Office's requirements.



Matador Production Company Garrett Fed Com 226H SHL 2372' FNL & 584' FWL BHL 2323' FNL & 240' FEL Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

Enough stockpiled topsoil will be retained to cover the remainder of the pad when the well is plugged. Once the last well is plugged, then the rest of the pad and 764.14' of new road will be similarly reclaimed within 6 months of plugging. The old road will be re-opened. Noxious weeds will be controlled.

Land use:

75' x 2047.64' pipeline route = 3.53 acres
30' x 764.14' detour road = 0.53 acre
+ 370' x 430' pad = 3.65 acres
7.71 acres short term
- 75' x 2047.64' pipeline route = 3.53 acres
- 20' x 20' road = 0.01 acre
- 1.91 acre interim reclamation pad
2.26 acres long term (0.53 ac. road + 1.73 ac. pad)

11. SURFACE OWNER

All construction will be on NM State Land Office land. Their address is PO Box 1148, Santa Fe, NM 87504. Phone is 505 827-5760. APD approval by NMOCD will constitute surface use approval under the terms of NM State Land Office lease VB-0055-0000.

12. OTHER INFORMATION

On-site inspection was held with Jim Goodbar, Vance Wolf, et al (BLM) on August 24, 2017. Boone filed archaeology report NMCRIS-138845 on August 29, 2017.



Matador Production Company Garrett Fed Com 226H SHL 2372' FNL & 584' FWL BHL 2323' FNL & 240' FEL Sec. 32, T. 24 S., R. 29 E., Eddy County, NM

CERTIFICATION

I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U. S. C. 1001 for the filing of false statements. Executed this 21st day of January, 2018.

Brian Wood, Consultant

Permits West, Inc.

37 Verano Loop, Santa Fe, NM 87508

(505) 466-8120

FAX: (505) 466-9682

Cellular: (505) 699-2276

Field representative will be:

Sam Pryor, Senior Staff Landman Matador Production Company 5400 LBJ Freeway, Suite 1500

Dallas TX 75240

Phone: (972) 371-5241 FAX: (214) 866-4841



To Who It May Concern:

All (pad, road, pipelines) construction will be on NM State Land Office land. Their address is PO Box 1148, Santa Fe, NM 87504. Phone is 505 827-5760. In this situation where NMSLO oil and gas lease VB-0055-0000 will be communitized, then surface use is authorized when NMOCD approves the APD.

Brian Wood



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

PWD Data Report

Section 1 - General

Would you like to address long-term produced water disposal? NO

Section 2 - Lined Pits

Would you like to utilize Lined Pit PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

. .

Lined pit PWD on or off channel:

Lined pit PWD discharge volume (bbl/day):

Lined pit specifications:

Pit liner description:

Pit liner manufacturers information:

Precipitated solids disposal:

Decribe precipitated solids disposal:

Precipitated solids disposal permit:

Lined pit precipitated solids disposal schedule:

Lined pit precipitated solids disposal schedule attachment:

Lined pit reclamation description:

Lined pit reclamation attachment:

Leak detection system description:

Leak detection system attachment:

Lined pit Monitor description:

Lined pit Monitor attachment:

Lined pit: do you have a reclamation bond for the pit?

Is the reclamation bond a rider under the BLM bond?

Lined pit bond number:

Lined pit bond amount:

Additional bond information attachment:

PWD disturbance (acres):

Section 3 - Unlined Pits

Injection well mineral owner:

Would you like to utilize Unlined Pit PWD options? NO

Produced Water Disposal (PWD) Location:	
PWD surface owner:	PWD disturbance (acres):
Unlined pit PWD on or off channel:	·
Unlined pit PWD discharge volume (bbl/day):	
Unlined pit specifications:	
Precipitated solids disposal:	
Decribe precipitated solids disposal:	
Precipitated solids disposal permit:	
Unlined pit precipitated solids disposal schedule:	
Unlined pit precipitated solids disposal schedule attachment:	
Unlined pit reclamation description:	
Unlined pit reclamation attachment:	
Unlined pit Monitor description:	
Unlined pit Monitor attachment:	
Do you propose to put the produced water to beneficial use?	
Beneficial use user confirmation:	
Estimated depth of the shallowest aquifer (feet):	
Does the produced water have an annual average Total Dissolutation of the existing water to be protected?	lved Solids (TDS) concentration equal to or less than
TDS lab results:	
Geologic and hydrologic evidence:	
State authorization:	
Unlined Produced Water Pit Estimated percolation:	
Unlined pit: do you have a reclamation bond for the pit?	
Is the reclamation bond a rider under the BLM bond?	
Unlined pit bond number:	
Unlined pit bond amount:	
Additional bond information attachment:	
Section 4 - Injection	
Would you like to utilize Injection PWD options? NO	
Produced Water Disposal (PWD) Location:	
PWD surface owner:	PWD disturbance (acres):
Injection PWD discharge volume (bbl/day):	

Injection well type:	
Injection well number:	Injection well name:
Assigned injection well API number?	Injection well API number:
Injection well new surface disturbance (acres):	
Minerals protection information:	
Mineral protection attachment:	
Underground Injection Control (UIC) Permit?	
UIC Permit attachment:	
Section 5 - Surface Discharge	
Would you like to utilize Surface Discharge PWD options? NO	
Produced Water Disposal (PWD) Location:	
PWD surface owner:	PWD disturbance (acres):
Surface discharge PWD discharge volume (bbl/day):	
Surface Discharge NPDES Permit?	
Surface Discharge NPDES Permit attachment:	
Surface Discharge site facilities information:	
Surface discharge site facilities map:	·
Section 6 - Other	
Would you like to utilize Other PWD options? NO	
Produced Water Disposal (PWD) Location:	
PWD surface owner:	PWD disturbance (acres):
Other PWD discharge volume (bbl/day):	
Other PWD type description:	
Other PWD type attachment:	
Have other regulatory requirements been met?	
Other regulatory requirements attachment:	



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Bond Info Data Report

Bond Information

Federal/Indian APD: FED

BLM Bond number: NMB001079

BIA Bond number:

Do you have a reclamation bond? NO

Is the reclamation bond a rider under the BLM bond?

Is the reclamation bond BLM or Forest Service?

BLM reclamation bond number:

Forest Service reclamation bond number:

Forest Service reclamation bond attachment:

Reclamation bond number:

Reclamation bond amount:

Reclamation bond rider amount:

Additional reclamation bond information attachment: