m 3160-3 ne 2015) UNITED STATI DEPARTMENT OF THE BUREAU OF LAND MAN APPLICATION FOR PERMIT TO			ield Un	lice	APR 1	2 2019 Approv	· .	
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APPLICATION FOR PERMIT TO Type of work: Image: DRILL		~~~ ~		-	DISTRICT	ESAO	Cn	
APPLICATION FOR PERMIT TO Type of work: Image: DRILL		UK	T COIN		5. Lease Serial No.			
Type of work: DRILL	DRILL (ENT			NMNM:)70200			
		OR R	REENTER		6. If Indian, Allotee	e or Tribe l	Name	
	REENTER	٤			7. If Unit or CA Ag	reement, 1	Name and I	No.
Type of Well Oil Well 🖌 Gas Well	Other				8. Lease Name and	Well No.		
Type of Completion: Hydraulic Fracturing	Single Zor	ne	Multiple Zone		ASTEROID 20-29	FED CO	M WCA	
					2H 325	- 38:	5	
Name of Operator HISHOLM ENERGY OPERATING LLC			372 13	7	9. API Well No. 30-015	5-43	87	7
Address 1 Cherry St., Suite 1200 Unit 20 Fort Worth TX 76102). (include area code 04	e) [.]	10. Field and Pool, PURPLE SAGE /	-	-	982
Location of Well (Report location clearly and in accordance	e with any	State r	equirements.*)		11. Sec., T. R. M. c			Area
At surface LOT B / 120 FNL / 1330 FEL / LAT 32.296					SEC 20 / T23S / F	R26E / NN	ΛP	
At proposed prod. zone LOT P / 330 FSL / 400 FEL / L		87755	/ LONG -104.308	31808	. 			
Distance in miles and direction from nearest town or post o miles	office*				12. County or Paris EDDY	sh	13. State NM	
Distance from proposed* 120 feet	16. No	ofacr	es in lease	17. Spaci	ng Unit dedicated to	this well		
property or lease line, ft. (Also to nearest drig, unit line, if any)	320			640 .	,			
Distance from proposed location*	19. Pro	oposed	Depth	20. BLM	/BIA Bond No. in file	•		
to nearest well, drilling, completed, 30 feet applied for, on this lease, ft.	8635 f	eet / 1	9086 feet	FED: NN	/B001468			
Elevations (Show whether DF, KDB, RT, GL, etc.)		•	nate date work will	start*	23. Estimated dura	tion		<u> </u>
886 feet	01/01/2		ments		30 days			
e following, completed in accordance with the requirements applicable)				, and the l	lydraulic Fracturing	rule per 43	3 CFR 316.	2.3-3
Well plat certified by a registered surveyor. A Drilling Plan.			Item 20 above).		ns unless covered by a	an existing	bond on fil	ie (see
A Surface Use Plan (if the location is on National Forest Sys SUPO must be filed with the appropriate Forest Service Offi		, the	 Operator certific Such other site sp BLM. 		rmation and/or plans a	is may be r	equested by	/ the
Signature lectronic Submission)			Printed/Typed) r Elrod / Ph: (817))953-3728	3	Date 07/26/2	018	
e enior Regulatory Technician	I					-J		
proved by (Signature) lectronic Submission)			(Printed/Typed) ayton / Ph: (575)2	234-5959		Date 02/28/2	:019	
le		Office						
ssistant Field Manager Lands & Minerals plication approval does not warrant or certify that the applic plicant to conduct operations thereon. nditions of approval, if any, are attached.		egal or		iose rights	in the subject lease v	which wou	ld entitle th	ne
e 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, he United States any false, fictitious or fraudulent statement						any depar	tment or ag	gency
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(Continued on page 2)

APT DVapproval Date: 02/28/2019 *(Instructions on page 2)

Ruf 4-17-19.

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INSTRUCTIONS

GENERAL: This form is designed for submitting proposals to perform certain well operations, as indicated on Federal and Indian lands and leases for action by appropriate Federal agencies, pursuant to applicable Federal laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from local Federal offices.

ITEM I: If the proposal is to redrill to the same reservoir at a different subsurface location or to a new reservoir, use this form with appropriate notations. Consult applicable Federal regulations concerning subsequent work proposals or reports on the well.

ITEM 4: Locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local Federal offices for specific instructions.

ITEM 14: Needed only when location of well cannot readily be found by road from the land or lease description. A plat, or plats, separate or on the reverse side, showing the roads to, and the surveyed location of, the wen, and any other required information, should be furnished when required by Federal agency offices.

ITEMS 15 AND 18: If well is to be, or has been directionany drilled, give distances for subsurface location of hole in any present or objective productive zone.

ITEM 22: Consult applicable Federal regulations, or appropriate officials, concerning approval of the proposal before operations are started.

ITEM 24: If the proposal will involve hydraulic fracturing operations, you must comply with 43 CFR 3162.3-3, including providing information about the protection of usable water. Operators should provide the best available information about all formations containing water and their depths. This information could include data and interpretation of resistivity logs run on nearby wells. Information may also be obtained from state or tribal regulatory agencies and from local BLM offices.

NOTICES

The Privacy Act of 1974 and regulation in 43 CFR 2.48(d) provide that you be furnished the following information in connection with information required by this application.

AUTHORITY: 30 U.S.C. 181 et seq., 25 U.S.C. 396; 43 CFR 3160

PRINCIPAL PURPOSES: The information will be used to: (1) process and evaluate your application for a permit to drill a new oil, gas, or service wen or to reenter a plugged and abandoned well; and (2) document, for administrative use, information for the management, disposal and use of National Resource Lands and resources including (a) analyzing your proposal to discover and extract the Federal or Indian resources encountered; (b) reviewing procedures and equipment and the projected impact on the land involved; and (c) evaluating the effects of the proposed operation on the surface and subsurface water and other environmental impacts.

ROUTINE USE: Information from the record and/or the record win be transferred to appropriate Federal, State, and local or foreign agencies, when relevant to civil, criminal or regulatory investigations or prosecution, in connection with congressional inquiries and for regulatory responsibilities.

EFFECT OF NOT PROVIDING INFORMATION: Filing of this application and disclosure of the information is mandatory only if you elect to initiate a drilling or reentry operation on an oil and gas lease.

The Paperwork Reduction Act of 1995 requires us to inform you that:

The BLM conects this information to anow evaluation of the technical, safety, and environmental factors involved with drilling for oil and/or gas on Federal and Indian oil and gas leases. This information will be used to analyze and approve applications. Response to this request is mandatory only if the operator elects to initiate drilling or reentry operations on an oil and gas lease. The BLM would like you to know that you do not have to respond to this or any other Federal agency-sponsored information collection unless it displays a currently valid OMB control number.

BURDEN HOURS STATEMENT: Public reporting burden for this form is estimated to average 8 hours per response, including the time for reviewing instructions, gathering and maintaining data, and completing and reviewing the form. Direct comments regarding the burden estimate or any other aspect of this form to U.S. Department of the Interior, Bureau of Land Management (1004-0137), Bureau Information Conection Clearance Officer (WO-630), 1849 C Street, N.W., Mail Stop 401 LS, Washington, D.C. 20240.

(Continued on page 3)

Additional Operator Remarks

Location of Well

SHL: LOT B / 120 FNL / 1330 FEL / TWSP: 23S / RANGE: 26E / SECTION: 20 / LAT: 32.296558 / LONG: -104.3112731 (TVD: 0 feet, MD: 0 feet)
 PPP: LOT I / 330 FNL / 400 FEL / TWSP: 23S / RANGE: 26E / SECTION: 20 / LAT: 32.28963 / LONG: -104.308227 (TVD: 8669 feet, MD: 11843 feet)
 PPP: LOT A / 330 FNL / 400 FEL / TWSP: 23S / RANGE: 26E / SECTION: 20 / LAT: 32.2959852 / LONG: -104.3082611 (TVD: 8669 feet, MD: 9533 feet)
 BHL: LOT P / 330 FSL / 400 FEL / TWSP: 23S / RANGE: 26E / SECTION: 29 / LAT: 32.2687755 / LONG: -104.3081808 (TVD: 8635 feet, MD: 19086 feet)

BLM Point of Contact

Name: Katrina Ponder Title: Geologist

Phone: 5752345969

Email: kponder@blm.gov

Approval Date: 02/28/2019

(Form 3160-3, page 3)

Review and Appeal Rights

A person contesting a decision shall request a State Director review. This request must be filed within 20 working days of receipt of the Notice with the appropriate State Director (see 43 CFR 3165.3). The State Director review decision may be appealed to the Interior Board of Land Appeals, 801 North Quincy Street, Suite 300, Arlington, VA 22203 (see 43 CFR 3165.4). Contact the above listed Bureau of Land Management office for further information.

Approval Date: 02/28/2019

(Form 3160-3, page 4)

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	Chisholm Energy Operating, LLC
LEASE NO.:	NMNM-070200
WELL NAME & NO.:	Asteroid 20-29 Fed Com WCA 2H
SURFACE HOLE FOOTAGE:	0120' FNL & 1330' FEL
BOTTOM HOLE FOOTAGE	0330' FSL & 0400' FEL Sec. 29, T. 23 S., R 26 E.
LOCATION:	Section 20, T. 23 S., R 26 E., NMPM
COUNTY:	County, New Mexico

Communitization Agreement

The operator will submit a Communitization Agreement to the Carlsbad Field Office, 620 E Greene St. Carlsbad, New Mexico 88220, at least 90 days before the anticipated date of first production from a well subject to a spacing order issued by the New Mexico Oil Conservation Division. The Communitization Agreement will include the signatures of all working interest owners in all Federal and Indian leases subject to the Communitization Agreement (i.e., operating rights owners and lessees of record), or certification that the operator has obtained the written signatures of all such owners and will make those signatures available to the BLM immediately upon request.

If the operator does not comply with this condition of approval, the BLM may take enforcement actions that include, but are not limited to, those specified in 43 CFR 3163.1.

In addition, the well sign shall include the surface and bottom hole lease numbers. <u>When the Communitization Agreement number is known, it shall also be</u> on the sign.

A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

□ Eddy County

Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822

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- 1. Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.
- Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval – an Incident of Non-Compliance will be written and will be a "Major" violation.
- 3. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.
- 4. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

Wait on cement (WOC) for Water Basin:

After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements.

Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Medium Cave/Karst

Possible water flows in the Salado and Castile.

Possible lost circulation in the Rustler, Red Beds, and Delaware. Abnormal pressure may be encountered in the 3rd Bone Spring and all subsequent formations.

- 1. The 13-3/8 inch surface casing shall be set at approximately 420 feet (a minimum of 25 feet into the Rustler Anhydrite and above the salt) and cemented to the surface. If salt is encountered, set casing at least 25 feet above the salt.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

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Formation below the 13-3/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe and the mud weight for the bottom of the hole. Report results to BLM office.

2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is:

☐ Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst.

If cement does not circulate to surface on the intermediate casing, the cement on the production casing must come to surface.

Formation below the 9-5/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe (not the mud weight required to prevent dissolving the salt formation) and the mud weight for the bottom of the hole. Report results to BLM office.

Centralizers required on horizontal leg, must be type for horizontal service and a minimum of one every other joint.

3. The minimum required fill of cement behind the 5-1/2 inch production casing is:

☐ Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification. Excess calculates to 10% - Additional cement may be required.

4. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

C. **PRESSURE CONTROL**

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API 53.
- 2. Variance approved to use flex line from BOP to choke manifold. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor. If the BLM inspector questions the straightness of the hose, a BLM engineer will be contacted and will review in the field or via picture supplied by inspector to determine if changes are required (operator shall expect delays if this occurs).
- 3. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be psi.
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.

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- b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
- c. Manufacturer representative shall install the test plug for the initial BOP test.
- d. Operator shall perform the intermediate casing integrity test to 70% of the casing burst. This will test the multi-bowl seals.
- e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

5M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

4. The appropriate BLM office shall be notified a minimum of hours in advance for a representative to witness the tests.

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- a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
- a. The tests shall be done by an independent service company utilizing a test plug **not a cup or J-packer**.
- b. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall

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have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.

- c. The results of the test shall be reported to the appropriate BLM office.
- d. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
- e. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
- f. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the **Wolfcamp** formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

D. **DRILLING MUD**

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the **Wolfcamp** formation, and shall be used until production casing is run and cemented.

E. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

F. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and

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disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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PECOS DISTRICT SURFACE USE CONDITIONS OF APPROVAL

OPERATOR'S NAME:	Chisholm Energy Operating LLC
LEASE NO.:	NMNM070200
WELL NAME & NO.:	Asteroid 20-29 Fed Com WCA 2H
SURFACE HOLE FOOTAGE:	120'/N & 1330'/E
BOTTOM HOLE FOOTAGE	330'/S & 400'/E
LOCATION:	Section 20, T.23 S., R.26 E., NMPM
COUNTY:	Eddy County, New Mexico

TABLE OF CONTENTS

Standard Conditions of Approval (COA) apply to this APD. If any deviations to these standards exist or special COAs are required, the section with the deviation or requirement will be checked below.

General Provisions

Permit Expiration

Archaeology, Paleontology, and Historical Sites

Noxious Weeds

Special Requirements

Cave/Karst Watershed

Construction

Notification

Topsoil

Closed Loop System

Federal Mineral Material Pits

Well Pads

Roads

] Road Section Diagram

Production (Post Drilling)

Well Structures & Facilities

Interim Reclamation

Final Abandonment & Reclamation

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I. GENERAL PROVISIONS

The approval of the Application For Permit To Drill (APD) is in compliance with all applicable laws and regulations: 43 Code of Federal Regulations 3160, the lease terms, Onshore Oil and Gas Orders, Notices To Lessees, New Mexico Oil Conservation Division (NMOCD) Rules, National Historical Preservation Act As Amended, and instructions and orders of the Authorized Officer. Any request for a variance shall be submitted to the Authorized Officer on Form 3160-5, Sundry Notices and Report on Wells.

II. PERMIT EXPIRATION

If the permit terminates prior to drilling and drilling cannot be commenced within 60 days after expiration, an operator is required to submit Form 3160-5, Sundry Notices and Reports on Wells, requesting surface reclamation requirements for any surface disturbance. However, if the operator will be able to initiate drilling within 60 days after the expiration of the permit, the operator must have set the conductor pipe in order to allow for an extension of 60 days beyond the expiration date of the APD. (Filing of a Sundry Notice is required for this 60 day extension.)

III. ARCHAEOLOGICAL, PALEONTOLOGY & HISTORICAL SITES

Any cultural and/or paleontological resource discovered by the operator or by any person working on the operator's behalf shall immediately report such findings to the Authorized Officer. The operator is fully accountable for the actions of their contractors and subcontractors. The operator shall suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Authorized Officer. An evaluation of the discovery shall be made by the Authorized Officer to determine the appropriate actions that shall be required to prevent the loss of significant cultural or scientific values of the discovery. The operator shall be held responsible for the cost of the proper mitigation measures that the Authorized Officer assesses after consultation with the operator on the evaluation and decisions of the discovery. Any unauthorized collection or disturbance of cultural or paleontological resources may result in a shutdown order by the Authorized Officer.

IV. NOXIOUS WEEDS

The operator shall be held responsible if noxious weeds become established within the areas of operations. Weed control shall be required on the disturbed land where noxious weeds exist, which includes the roads, pads, associated pipeline corridor, and adjacent land affected by the establishment of weeds due to this action. The operator shall consult with the Authorized Officer for

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acceptable weed control methods, which include following EPA and BLM requirements and policies.

V. SPECIAL REQUIREMENT(S)

Karst

Cave/Karst Surface Mitigation

The following stipulations will be applied to minimize impacts during construction, drilling and production:

Construction:

In the advent that any underground voids are opened up during construction activities, construction activities will be halted and the BLM will be notified immediately.

No Blasting:

No blasting will be utilized for pad construction. The pad will be constructed and leveled by adding the necessary fill and caliche.

Pad Berming:

- The entire perimeter of the well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad.
- The compacted berm shall be constructed at a minimum of 12 inches high with impermeable mineral material (e.g., caliche).
- No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad.
- The topsoil stockpile shall be located outside the bermed well pad.
- Topsoil, either from the well pad or surrounding area, shall not be used to construct the berm.
- No storm drains, tubing or openings shall be placed in the berm.
- If fluid collects within the bermed area, the fluid must be vacuumed into a safe container and disposed of properly at a state approved facility.
- The integrity of the berm shall be maintained around the surfaced pad throughout the life of the well and around the downsized pad after interim reclamation has been completed.
- Any access road entering the well pad shall be constructed so that the integrity of the berm height surrounding the well pad is not compromised. (Any access road crossing the berm cannot be lower than the berm height.)
- Following a rain event, all fluids will vacuumed off of the pad and hauled off-site and disposed at a proper disposal facility.

Tank Battery Liners and Berms:

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Tank battery locations and all facilities will be lined and bermed. A 20 mil permanent liner will be installed with a 4 oz. felt backing, or equivalent, to prevent tears or punctures. Tank battery berms must be large enough to contain 1 $\frac{1}{2}$ times the content of the largest tank.

Leak Detection System:

A method of detecting leaks is required. The method could incorporate gauges to measure loss, situating values and lines so they can be visually inspected, or installing electronic sensors to alarm when a leak is present. Leak detection plan will be submitted to BLM for approval.

Automatic Shut-off Systems:

Automatic shut off, check values, or similar systems will be installed for pipelines and tanks to minimize the effects of catastrophic line failures used in production or drilling.

Cave/Karst Subsurface Mitigation

The following stipulations will be applied to protect cave/karst and ground water concerns:

Rotary Drilling with Fresh Water:

Fresh water will be used as a circulating medium in zones where caves or karst features are expected. SEE ALSO: Drilling COAs for this well.

Directional Drilling:

Kick off for directional drilling will occur at least 100 feet below the bottom of the cave occurrence zone. SEE ALSO: Drilling COAs for this well.

Lost Circulation:

ALL lost circulation zones from the surface to the base of the cave occurrence zone will be logged and reported in the drilling report.

Regardless of the type of drilling machinery used, if a void of four feet or more and circulation losses greater than 70 percent occur simultaneously while drilling in any cave-bearing zone, the BLM will be notified immediately by the operator. The BLM will assess the situation and work with the operator on corrective actions to resolve the problem.

Abandonment Cementing:

Upon well abandonment in cave karst areas additional plugging conditions of approval may be required. The BLM will assess the situation and work with the operator to ensure proper plugging of the wellbore.

Pressure Testing:

The operator will perform annual pressure monitoring on all casing annuli and reported in a sundry notice. If the test results indicated a casing failure has

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occurred, remedial action will be undertaken to correct the problem to the BLM's approval.

FLOWLINES (SURFACE):

- Flowlines will be routed around sinkholes and other karst features to avoid or lessen the possibility of encountering near surface voids and to minimize the possibility of leaks and spills from entering karst systems.
- If a void is encountered alignments may be rerouted to avoid the karst feature and lessen; the potential of subsidence or collapse of karst features, buildup of toxic or combustible gas, or other possible impacts to cave and karst resources from the buried pipeline.
- Regular monitoring is required to quickly identify leaks for their immediate and proper treatment.
- All spills or leaks will be reported to the BLM immediately for their immediate and proper treatment.

Watershed

1. Containment berms will be constructed around both tank battery production facilities designed to hold fluids. The containment berms will be constructed with compacted material capable of holding $1\frac{1}{2}$ time the capacity of the largest tank.

2. Topsoil will be stockpiled on the pads to enhance future reclamation. 3. The entire well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad. A water diversion ditch will placed along the south, west and northwest sides of the pad. Topsoil shall not be used to construct the berm. No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad. The berm shall be maintained through the life of the well and after interim reclamation has been completed. Any water erosion that may occur due to the construction of the well pad during the life of the well will be quickly corrected and proper measures will be taken to prevent future erosion.

4. A closed loop drilling system will be used.

5. The entire well pad will be bermed to prevent oil, salt, and other chemical contaminants from leaving the well pad. A water diversion ditch will placed along the south, west and northwest sides of the pad. Topsoil shall not be used to construct the berm. No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad. The berm shall be maintained through the life of the well and after interim reclamation has been completed.

6. Any water erosion that may occur due to the construction of the well pad during the life of the well will be quickly corrected and proper measures will be taken to prevent future erosion

7. Drainage turnouts shall have straw wattles installed.

8. <u>Surface Pipeline</u>: A leak detection plan will be submitted to the BLM Carlsbad Field Office for approval prior to pipeline installation. The method could incorporate gauges to detect pressure drops, situating values and lines so they

Page 5 of 14

can be visually inspected periodically or installing electronic sensors to alarm when a leak is present. The leak detection plan will incorporate an automatic shut off system that will be installed for proposed pipelines to minimize the effects of an undesirable event.

VI. CONSTRUCTION

A. NOTIFICATION

The BLM shall administer compliance and monitor construction of the access road and well pad. Notify the Carlsbad Field Office at (575) 234-5909 at least 3 working days prior to commencing construction of the access road and/or well pad.

When construction operations are being conducted on this well, the operator shall have the approved APD and Conditions of Approval (COA) on the well site and they shall be made available upon request by the Authorized Officer.

B. TOPSOIL

The operator shall strip the top portion of the soil (root zone) from the entire well pad area and stockpile the topsoil along the edge of the well pad as depicted in the APD. The root zone is typically six (6) inches in depth. All the stockpiled topsoil will be redistributed over the interim reclamation areas. Topsoil shall not be used for berming the pad or facilities. For final reclamation, the topsoil shall be spread over the entire pad area for seeding preparation.

Other subsoil (below six inches) stockpiles must be completely segregated from the topsoil stockpile. Large rocks or subsoil clods (not evident in the surrounding terrain) must be buried within the approved area for interim and final reclamation.

C. CLOSED LOOP SYSTEM

Tanks are required for drilling operations: No Pits.

The operator shall properly dispose of drilling contents at an authorized disposal site.

D. FEDERAL MINERAL MATERIALS PIT

Payment shall be made to the BLM prior to removal of any federal mineral materials. Call the Carlsbad Field Office at (575) 234-5972.

E. WELL PAD SURFACING

Page 6 of 14

Surfacing of the well pad is not required.

If the operator elects to surface the well pad, the surfacing material may be required to be removed at the time of reclamation. The well pad shall be constructed in a manner which creates the smallest possible surface disturbance, consistent with safety and operational needs.

F. EXCLOSURE FENCING (CELLARS & PITS)

Exclosure Fencing

The operator will install and maintain exclosure fencing for all open well cellars to prevent access to public, livestock, and large forms of wildlife before and after drilling operations until the pit is free of fluids and the operator initiates backfilling. (For examples of exclosure fencing design, refer to BLM's Oil and Gas Gold Book, Exclosure Fence Illustrations, Figure 1, Page 18.)

G. ON LEASE ACCESS ROADS

Road Width

The access road shall have a driving surface that creates the smallest possible surface disturbance and does not exceed fourteen (14) feet in width. The maximum width of surface disturbance, when constructing the access road, shall not exceed twenty-five (25) feet.

Surfacing

Surfacing material is not required on the new access road driving surface. If the operator elects to surface the new access road or pad, the surfacing material may be required to be removed at the time of reclamation.

Where possible, no improvements should be made on the unsurfaced access road other than to remove vegetation as necessary, road irregularities, safety issues, or to fill low areas that may sustain standing water.

The Authorized Officer reserves the right to require surfacing of any portion of the access road at any time deemed necessary. Surfacing may be required in the event the road deteriorates, erodes, road traffic increases, or it is determined to be beneficial for future field development. The surfacing depth and type of material will be determined at the time of notification.

Crowning

Crowning shall be done on the access road driving surface. The road crown shall have a grade of approximately 2% (i.e., a 1" crown on a 14' wide road). The road shall conform to Figure 1; cross section and plans for typical road construction.

Ditching

Ditching shall be required on both sides of the road.

Page 7 of 14

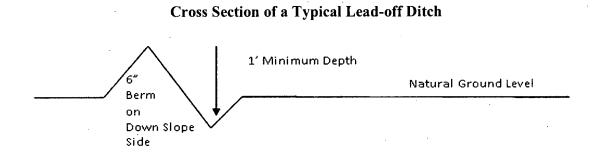
Turnouts

Vehicle turnouts shall be constructed on the road. Turnouts shall be intervisible with interval spacing distance less than 1000 feet. Turnouts shall conform to Figure 1; cross section and plans for typical road construction.

Drainage

Drainage control systems shall be constructed on the entire length of road (e.g. ditches, sidehill outsloping and insloping, lead-off ditches, culvert installation, and low water crossings).

A typical lead-off ditch has a minimum depth of 1 foot below and a berm of 6 inches above natural ground level. The berm shall be on the down-slope side of the lead-off ditch.



All lead-off ditches shall be graded to drain water with a 1 percent minimum to 3 percent maximum ditch slope. The spacing interval are variable for lead-off ditches and shall be determined according to the formula for spacing intervals of lead-off ditches, but may be amended depending upon existing soil types and centerline road slope (in %);

Formula for Spacing Interval of Lead-off Ditches

Example - On a 4% road slope that is 400 feet long, the water flow shall drain water into a lead-off ditch. Spacing interval shall be determined by the following formula:

400 foot road with 4% road slope: $\underline{400'} + 100' = 200'$ lead-off ditch interval 4%

Cattle guards

An appropriately sized cattle guard sufficient to carry out the project shall be installed and maintained at fence/road crossings. Any existing cattle guards on the access road route shall be repaired or replaced if they are damaged or have deteriorated beyond practical use. The operator shall be responsible for the condition of the existing cattle guards that are in place and are utilized during lease operations.

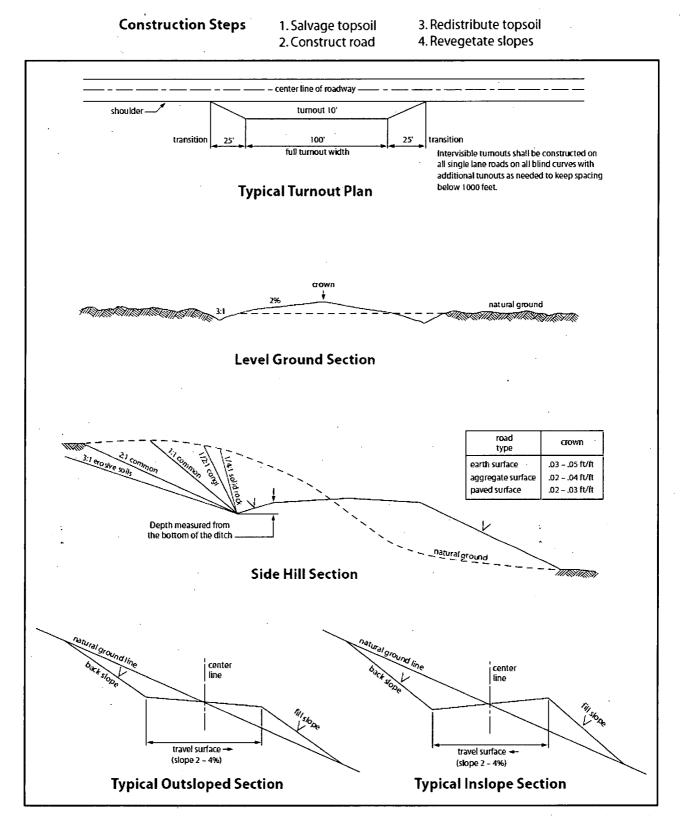
Page 8 of 14

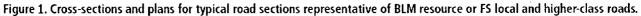
Fence Requirement

Where entry is granted across a fence line, the fence shall be braced and tied off on both sides of the passageway prior to cutting. The operator shall notify the private surface landowner or the grazing allotment holder prior to crossing any fences.

Public Access

Public access on this road shall not be restricted by the operator without specific written approval granted by the Authorized Officer.





Page 10 of 14

VII. PRODUCTION (POST DRILLING)

A. WELL STRUCTURES & FACILITIES

Placement of Production Facilities

Production facilities should be placed on the well pad to allow for maximum interim recontouring and revegetation of the well location.

Exclosure Netting (Open-top Tanks)

Immediately following active drilling or completion operations, the operator will take actions necessary to prevent wildlife and livestock access, including avian wildlife, to all open-topped tanks that contain or have the potential to contain salinity sufficient to cause harm to wildlife or livestock, hydrocarbons, or Resource Conservation and Recovery Act of 1976-exempt hazardous substances. At a minimum, the operator will net, screen, or cover open-topped tanks to exclude wildlife and livestock and prevent mortality. If the operator uses netting, the operator will cover and secure the open portion of the tank to prevent wildlife entry. The operator will net, screen, or cover the tanks until the operator removes the tanks from the location or the tanks no longer contain substances that could be harmful to wildlife or livestock. Use a maximum netting mesh size of 1 $\frac{1}{2}$ inches. The netting must not be in contact with fluids and must not have holes or gaps.

Chemical and Fuel Secondary Containment and Exclosure Screening

The operator will prevent all hazardous, poisonous, flammable, and toxic substances from coming into contact with soil and water. At a minimum, the operator will install and maintain an impervious secondary containment system for any tank or barrel containing hazardous, poisonous, flammable, or toxic substances sufficient to contain the contents of the tank or barrel and any drips, leaks, and anticipated precipitation. The operator will dispose of fluids within the containment system that do not meet applicable state or U. S. Environmental Protection Agency livestock water standards in accordance with state law; the operator must not drain the fluids to the soil or ground. The operator will design, construct, and maintain all secondary containment systems to prevent wildlife and livestock exclosure systems such as fencing, netting, expanded metal mesh, lids, and grate covers. Use a maximum netting mesh size of 1 ½ inches.

Open-Vent Exhaust Stack Exclosures

The operator will construct, modify, equip, and maintain all open-vent exhaust stacks on production equipment to prevent birds and bats from entering, and to discourage perching, roosting, and nesting. (*Recommended exclosure structures on open-vent exhaust stacks are in the shape of a cone.*) Production

equipment includes, but may not be limited to, tanks, heater-treaters, separators, dehydrators, flare stacks, in-line units, and compressor mufflers.

Containment Structures

Proposed production facilities such as storage tanks and other vessels will have a secondary containment structure that is constructed to hold the capacity of 1.5 times the largest tank, plus freeboard to account for precipitation, unless more stringent protective requirements are deemed necessary.

Painting Requirement

All above-ground structures including meter housing that are not subject to safety requirements shall be painted a flat non-reflective paint color, **Shale Green** from the BLM Standard Environmental Color Chart (CC-001: June 2008).

VIII. INTERIM RECLAMATION

During the life of the development, all disturbed areas not needed for active support of production operations should undergo interim reclamation in order to minimize the environmental impacts of development on other resources and uses.

Within six (6) months of well completion, operators should work with BLM surface management specialists (Jim Amos: 575-234-5909) to devise the best strategies to reduce the size of the location. Interim reclamation should allow for remedial well operations, as well as safe and efficient removal of oil and gas.

During reclamation, the removal of caliche is important to increasing the success of revegetating the site. Removed caliche that is free of contaminants may be used for road repairs, fire walls or for building other roads and locations. In order to operate the well or complete workover operations, it may be necessary to drive, park and operate on restored interim vegetation within the previously disturbed area. Disturbing revegetated areas for production or workover operations will be allowed. If there is significant disturbance and loss of vegetation, the area will need to be revegetated. Communicate with the appropriate BLM office for any exceptions/exemptions if needed.

All disturbed areas after they have been satisfactorily prepared need to be reseeded with the seed mixture provided below.

Upon completion of interim reclamation, the operator shall submit a Sundry Notices and Reports on Wells, Subsequent Report of Reclamation (Form 3160-5).

IX. FINAL ABANDONMENT & RECLAMATION

Page 12 of 14

At final abandonment, well locations, production facilities, and access roads must undergo "final" reclamation so that the character and productivity of the land are restored.

Earthwork for final reclamation must be completed within six (6) months of well plugging. All pads, pits, facility locations and roads must be reclaimed to a satisfactory revegetated, safe, and stable condition, unless an agreement is made with the landowner or BLM to keep the road and/or pad intact.

After all disturbed areas have been satisfactorily prepared, these areas need to be revegetated with the seed mixture provided below. Seeding should be accomplished by drilling on the contour whenever practical or by other approved methods. Seeding may need to be repeated until revegetation is successful, as determined by the BLM.

Operators shall contact a BLM surface protection specialist prior to surface abandonment operations for site specific objectives (Jim Amos: 575-234-5909).

Page 13 of 14

Seed Mixture 1 for Loamy Sites

Holder shall seed all disturbed areas with the seed mixture listed below. The seed mixture shall be planted in the amounts specified in pounds of pure live seed (PLS)* per acre. There shall be no primary or secondary noxious weeds in the seed mixture. Seed shall be tested and the viability testing of seed will be done in accordance with State law(s) and within nine (9) months prior to purchase. Commercial seed shall be either certified or registered seed. The seed container shall be tagged in accordance with State law(s) and available for inspection by the Authorized Officer.

Seed shall be planted using a drill equipped with a depth regulator to ensure proper depth regulator to ensure proper depth of planting where drilling is possible. The seed mixture shall be evenly and uniformly planted over the disturbed area (small/heavier seeds have a tendency to drop the bottom of the drill and are planted first). Holder shall take appropriate measures to ensure this does not occur. Where drilling is not possible, seed shall be broadcast and the area shall be raked or chained to cover the seed. When broadcasting the seed, the pounds per acre shall be doubled. The seeding shall be repeated until a satisfactory stand is established as determined by the Authorized Officer. Evaluation of growth may not be made before completion of at least one full growing season after seeding.

Species to be planted in pounds of pure live seed* per acre:

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		lb/acre
Plains lovegrass (Eragrostis intermedia)	0.5	
Sand dropseed (Sporobolus cryptandrus)	1.0	
Sideoats grama (Bouteloua curtipendula)	5.0	
Plains bristlegrass (Setaria macrostachya)	2.0	

*Pounds of pure live seed:

Pounds of seed x percent purity x percent germination = pounds pure live seed

FAFMSS

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Operator Certification

I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

NAME: Jennifer Elrod

Signed on: 07/26/2018

Operator Certification Data Report

04/02/2019

Title: Senior Regulatory Technician

Street Address: 801 CHERRY STREET, SUITE 1200-UNIT 20

City: Fort Worth

State: TX

State:

Zip: 76102

Zip:

Phone: (817)953-3728

Email address: jelrod@chisholmenergy.com

Field Representative

Representative Name:

Street Address:

City:

Phone:

Email address:

FAFMSS

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

APD ID: 10400032424

Operator Name: CHISHOLM ENERGY OPERATING LLC Well Name: ASTEROID 20-29 FED COM WCA Well Type: CONVENTIONAL GAS WELL

Submission Date: 07/26/2018

Application Data

Highlighted data reflects the most recent changes

kepori

04/02/2019

Show Final Text

Well Work Type: Drill

Well Number: 2H

Section 1 - General Submission Date: 07/26/2018 APD ID: 10400032424 Tie to previous NOS? 10400030146 Title: Senior Regulatory Technician BLM Office: CARLSBAD User: Jennifer Elrod Federal/Indian APD: FED Is the first lease penetrated for production Federal or Indian? FED Lease number: NMNM070200 Lease Acres: 320 Surface access agreement in place? Allotted? **Reservation:** Agreement in place? NO Federal or Indian agreement: Agreement number: Agreement name: Keep application confidential? NO APD Operator: CHISHOLM ENERGY OPERATING LLC Permitting Agent? NO Operator letter of designation:

Operator Info

Operator Organization Name: CHISHOLM ENERGY OPERATING LLC

Operator Address: 801 Cherry St., Suite 1200 Unit 20

Operator PO Box:

Operator City: Fort Worth State: TX

Operator Phone: (817)469-1104

Operator Internet Address:

Section 2 - Well Information

Well in Master Development Plan? NO

Well in Master SUPO? EXISTING

Well in Master Drilling Plan? EXISTING

Well Name: ASTEROID 20-29 FED COM WCA

Mater Development Plan name:

Master SUPO name: ASTEROID

Well Number: 2H

Master Drilling Plan name: ASTEROID BS

Zip: 76102

Well API Number:

Field/Pool or Exploratory? Field and Pool

Field Name: PURPLE SAGE Pool Name: WOLFCAMP

Is the proposed well in an area containing other mineral resources? USEABLE WATER, NATURAL GAS, OIL

)

Well Name: ASTEROID 20-29 FED COM WCA Well Number: 2H

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Desc	cribe c	other	miner	als:				•				•		2				
ls th	e prop	oosed	well	in a H	elium	prod	uctio	n area?	N Use I	Existing W	ell Pa	d? NO	Ne	ew :	surface o	distur	bance	? ?
Туре	e of W	ell Pa	d։ MՍ	ILTIPL	.E WE	ELL			Multi	ple Well P	ad Nar	ne:	N	uml	ber: 1H, 2	2H, 3ł	4	
Well	Class	: HOF	RIZON	ITAL						ROID 20-2 ber of Leg		COM						
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	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	ease Type	Lease Number	Elevation	QW	TVD
SHL	120	FNL	133	FEL	23S	26E	20	Lot		- '	EDD	NEW	NEW		NMNM	338	0	0
Leg #1			0	,				В	8 ·	104.3112 731	Y	MEXI CO	MEXI CO		070200	6		
KOP Leg #1	120	FNL	133 0	FEL	235	26E	20	Lot B	32.29655 8	- 104.3112 731	EDD Y		NEW MEXI CO	F	NMNM 070200	- 455 0	793 6	793 6
PPP Leg #1	330	FNL	400	FEL	235	26 <u>E</u>	20	Lot . A	32.29598 52	- 104.3082 611	EDD [®] Y	NEW	NEW MEXI CO	F	NMNM 070200	- 528 3	953 3	866 9

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Well Name: ASTEROID 20-29 FED COM WCA Well Number: 2H

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	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	DM	TVD
PPP	330	FNL	400	FEL	23S	26E	20	Lot	32.28963	-	EDD	1		F	NMNM	-	118	866
Leg								1		101.0002	Y	MEXI			069578	528	43	9
#1										27		со	со			3		
EXIT	330	FSL	400	FEL	23S	26E	29	Lot	32.26877	-	EDD	NEW	NEW	F	NMNM	-	190	863
Leg								Р	55	104.3081	Y		MEXI		094838	524	86	5
#1										808		co	со			9		
BHL	330	FSL	400	FEL	23S	26E	29	Lot	32.26877	-	EDD	NEW	NEW	F	NMNM	-	190	863
Leg		1						Р	55	104.3081	Y	MEXI	MEXI		094838	524	86	5
#1										808		co	со			9		

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Section 3 - Casing

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	Casing ID	String Type	Hole Size.	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
	1	SURFACE	17.5	13.375	NEW	API	N	0	420	0	420			420	J-55	48	STC	3.85	12.3 3	BUOY	18.4 5	BUOY	24.8 2
		INTERMED IATE	12.2 5	9.625	NEW	API	N	0	1900	0	1900			1900	J-55	36	STC	3.01	3.49	BUOY	9.77	BUOY	9.77
•		PRODUCTI ON	8.75	5.5	NEW	API	N	0	19086	0	8635	-		19086	P- 110	20	BUTT	2.86	2.96	BUOY	4.34	BUOY	4.34

Casing Attachments

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Casing_Calculator_20180726120050.pdf

Well Name: ASTEROID 20-29 FED COM WCA

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Well Number: 2H

Casing ID: 2	tring Type:INTERMEDIATE			
Inspection Document:				
Spec Document:				
Tapered String Spec:	· · · ·			
Casing Design Assumptio	ns and Worksheet(s):			
Casing_Calculator_20	180726120031.pdf			
Casing ID: 3 S	tring Type: PRODUCTION			
			•	
Inspection Document:			·	
			·	
Inspection Document: Spec Document: Tapered String Spec:				
Spec Document:	ns and Worksheet(s):	 ·		

Section	4 - Ce	emen	t				,				
String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	420	455	1.24	14.8	564	85	Class C Premium Plus	Cellophane Flakes

INTERMEDIATE	Lead	 0	1550	560	2.28	11.5	1277	150	Plus	Sodium Metasilicate, Defoamer, KCL, Kol- Seal, Cellophane Flakes, ROF SealCheck
INTERMEDIATE	Tail	1550	1900	300	1.33	14.8	399	150	Class C Premium Plus	NA

Operator Name: CHISHOLM ENERGY OPERATING LLC **Well Name:** ASTEROID 20-29 FED COM WCA

Well Number: 2H

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
PRODUCTION	Lead		0	7900	875	2.28	11.5	1995	10	Liteweight	Fluid Loss, Expanding Agent, Retarder, Defoamer, Dispersant, Extender, Viscosifier
PRODUCTION	Tail		7900	1908 6	2395	1.18	14.5	2826	10	Class H Premium	Extender, Fluid Loss, Retarder, Defoamer, Dispersant

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

Describe what will be on location to control well or mitigate other conditions: Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times

Describe the mud monitoring system utilized: PVT, Pason/CanRig, Visual Monitoring

Circulating Medium Table

Top Depth	Bottom Depth	Mud Type	Min Weight (Ibs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	Hd	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics	
0	420	WATER-BASED MUD	8.4	8.6								
420	1900	SALT SATURATED	9.8	10.1								
1900	1908 6	OIL-BASED MUD	. 9	9.5								

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures: N/A

List of open and cased hole logs run in the well:

CBL,DS,GR,MWD,MICROLO

Coring operation description for the well:

N/A

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 4317

Anticipated Surface Pressure: 2409.81

Anticipated Bottom Hole Temperature(F): 160

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards attachment:

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations plan:

Eddy_County_H2S_plan_20180726120405.pdf

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

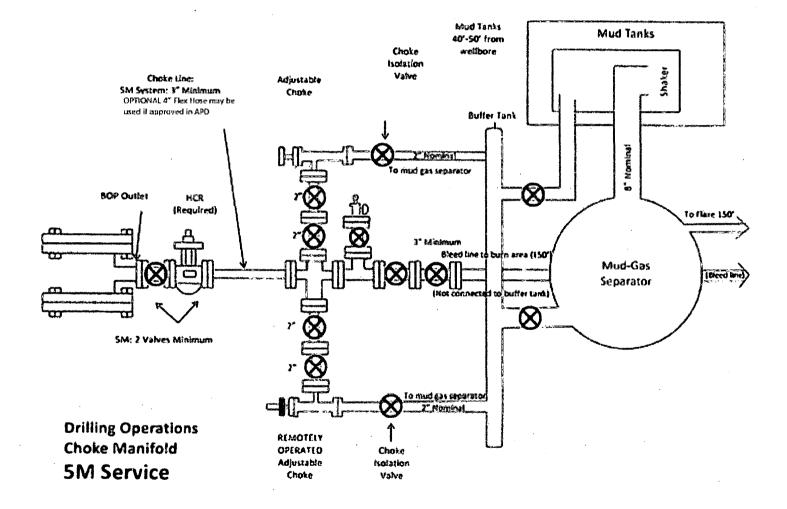
Asteroid_20_29_Fed_Com_WCA_2H_Plan_1_AC_Report__20180726120756.pdf Asteroid_20_29_Fed_Com_WCA_2H_Plan_1_20180726120756.pdf

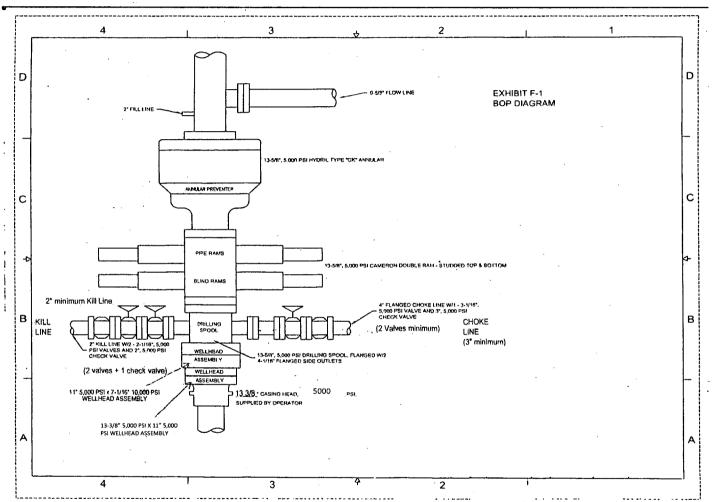
Other proposed operations facets description:

Other proposed operations facets attachment:

Other Variance attachment:

Cactus_Speed_Head_Installation_Procedure_20180726120717.pdf Cactus_Speed_Head_Pressure_Testing_Statement_20180726120717.pdf Cactus_Speedhead_Diagram_20180726120718.pdf Choke_Hose_M55_1_07102017_145204_66_1225_04_14_2014__20180726120718.pdf Choke_Hose_M55_2_07102017_145421_66_1042_05_03_2013__20180726120718.pdf





Casing Program: Asteroid 20-29 Fed Com WCA (13 3/8" x 9 5/8" x 5 1/2")

Open Hole Size (Inches)	Casing Depth; From (ft)	Casing Setting Depth (ft) MD	Casing Setting Depth (ft) TVD	Casing Size (inches)	Casing Weight (Ib/ft)	Casing Grade	Thread	Condition	Anticipated Mud Weight (ppg)	Burst (psi)	Burst SF (1.125)	Collapse (psi)	Collapse SF (1.125)	Pipe Body Tension (klbs)	_ Joint Tension (klbs)	Air Weight (Ibs)		Pipe Body Tension SF (1.8)	
Surface															•				
17.5"	0'	420'	420'	13 3/8"	48.0	J-55	STC	New	8.8	2370	12.33	740	3.85	433,000	322,000	20,160	17,449	24.82	18.45.
Intermediate																			
12.25"	0'	1,900'	1,900'	9 5/8"	36	J-55	LTC'	. New	10.2 ·	3520	3.49	· 2020	3.01	564,000	564,000	68,400	57,739	9.77	9.77
Production																			
8.75"	0'	19,086'	8,635'	5 1/2"	20	P-110	BTC	New	9.5	12640	2.96	12200	.2.86	641,000	641,000	172,700	147,629	4.34	4.34

Casing Design Criteria and Casing Loading Assumptions:	
Surface	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	8.8 ppg
Collapse A 1.125 design factor with full internal evacuation and collapse force equal to a mud gradient of:	8.8 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	8.8 ppg
Intermediate	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	10.2 ppg
Collapse A 1.125 design factor with 1/3 TVD internal evacuation and collapse force equal to a mud gradient of:	10.2 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	10.2 ppg
Production	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	9.5 ppg
. Collapse A 1.125 design factor with full internal evacuation and collapse force equal to a mud gradient of:	9.5 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	9.5 ppg

Casing Program: Asteroid 20-29 Fed Com WCA (13 3/8" x 9 5/8" x 5 1/2")

Open Hole Size (Inches)	Casing Depth; From (ft)	Casing Setting Depth (ft) MD	Casing Setting Depth (ft) TVD	Casing Size (inches)	Casing Weight (lb/ft)	Casing Grade	Thread	Condition	Anticipated Mud Weight (ppg)	Burst (psi)	Burst SF (1.125)	Collapse (psi)	Collapse SF (1.125)	Pipe Body Tension (klbs)	Joint Tension (klbs)	Air Weight (lbs)	Bouyant Weight (Ibs)	Pipe Body Tension SF (1.8)	Joint Tension SF (1.8)
Surface																		· ·	
17.5"	0'	420'	420'	13 3/8"	48.0	J-55	STC	New	8.8	2370	12.33	740	3.85	433,000	322,000	20,160	17,449	24.82	18.45
Intermediate																			
12.25"	0'	1,900'	1,900'	9 5/8"	36	J-55	LTC	New	10.2	3520	3.49	2020	3.01	564,000	564,000	68,400	57,739	9.77	9.77
Production																			
8.75"	0'	19,086	8,635'	5 1/2"	20	P-110	BTC	New	9.5	12640	2.96	12200	2.86	641,000	641,000	172,700	147,629	4.34	4.34

Casing Design Criteria and Casing Loading Assumptions:	
Surface	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	8.8 ppg
Collapse A 1.125 design factor with full internal evacuation and collapse force equal to a mud gradient of:	8.8 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	8.8 ppg
Intermediate	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	10.2 ppg
Collapse A 1.125 design factor with 1/3 TVD internal evacuation and collapse force equal to a mud gradient of:	10.2 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	10.2 ppg
Production	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	9.5 ppg
Collapse A 1.125 design factor with full internal evacuation and collapse force equal to a mud gradient of:	9.5 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	9.5 ppg

Casing Program: Asteroid 20-29 Fed Com WCA (13 3/8" x 9 5/8" x 5 1/2")

Open Hole Size (Inches)	Casing Depth; From (ft)	Casing Setting Depth (ft) MD	Casing Setting Depth (ft) TVD	Casing Size (inches)	Casing Weight (Ib/ft)	Casing Grade	Thread	Condition	Anticipated Mud Weight (ppg)	Burst (psi)	Burst SF (1.125)	Collapse (psi)	Collapse SF (1.125)	Pipe Body Tension (klbs)	Joint Tension (klbs)	Air Weight (lbs)	Bouyant Weight (Ibs)	Pipe Body Tension SF (1.8)	Joint Tension SF (1.8)
Surface																			
17.5"	0'	420'	420'	13 3/8"	48.0	J-55	STC	New	8.8	2370	12.33	740	3.85	433,000	322,000	20,160	17,449	24.82	18.45
Intermediate																			
12.25"	0'	1,900'	1,900'	9 5/8"	36	J-55	LTC	New	10.2	3520	3.49	2020	3.01	564,000	564,000	68,400	57,739	9.77	9.77
Production																			
8.75"	0'	19,086'	8,635'	5 1/2"	20	P-110	BTC	New	9.5	12640	2.96	12200	2.86	641,000	641,000	172,700	147,629	4.34	4.34

Casing Design Criteria and Casing Loading Assumptions:	
Surface	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	8.8 ppg
Collapse A 1.125 design factor with full internal evacuation and collapse force equal to a mud gradient of:	8.8 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	8.8 ppg
ntermediate	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	10.2 ppg
Collapse A 1.125 design factor with 1/3 TVD internal evacuation and collapse force equal to a mud gradient of:	10.2 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	10.2 ppg
Production	
Tension A 1.8 design factor with effects of buoyancy with a fluid equal to a mud weight of:	9.5 ppg
Collapse A 1.125 design factor with full internal evacuation and collapse force equal to a mud gradient of:	9.5 ppg
Burst A 1.125 design factor with full external evacuation and burst force equal to a mud gradient of:	9.5 ppg

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Chisholm Energy Operating, LLC

801 Cherry St., Suite 1200-Unit 20 Fort Worth, TX 76102

H2S Contingency Plan Eddy County, NM

Escape

Crews shall escape upwind of escaping gas in the event of an emergency release of gas. Escape can be facilitated from the location entrance road. Crew should then block entrance to the location from the lease road so as not to allow anyone traversing into a hazardous area. The blockade should be at a safe distance outside of the ROE. <u>There are NO homes or buildings in or near the ROE.</u>

Assumed 100 ppm ROE = 3000' 100 ppm H2S concentration shall trigger activation of this plan

Emergency Procedures

In the event of a release of gas containing H2S, the first responder(s) must:

« Isolate the area and prevent entry by other persons into the 100 ppm ROE.

- « Evacuate any public places encompassed by the 100 ppm ROE.
- « Be equipped with H2S monitors and air packs in order to control the release.
- « Use the "buddy system" to ensure no injuries occur during the response.

« Take precautions to avoid personal injury during this operation.

« Contact operator and/or local officials to aid in operation. See list of phone numbers attached. « Have received training

in the: Detection of

H2S, and

Measures for protection against the gas,

Equipment used for protection and emergency response.

Ignition of Gas Source

Should control of the well be considered lost and ignition considered, take care to protect against exposure to Sulfur Dioxide (S02). Intentional ignition must be coordinated with the NMOCD and local officials. Additionally, the NM State Police may become involved. NM State Police shall be the Incident Command on scene of any major release. Take care to protect downwind whenever there is an ignition of the gas.

Common	Chemical	Specific	Threshold	Hazardous	Lethal
Name	Formula	Gravity	Limit	Limit	Concentration
Hydrogen Sulfide	H2S	1.189 Air=1	10 ppm	100 ppm/hr	600 ppm

Characteristics of H2S and SO,

		SO2	2.21 Air=1		N/A	1000 ppm
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Contacting Authorities

Chisholm Energy Operating personnel must liaise with local and state agencies to ensure **a** proper response to a major release. Additionally, the OCD must be notified of the release as soon **as** possible but no later than 4 hours. Agencies will ask for information such as type and volume of release, wind direction, location of release, etc. Be prepared with all information available including directions to sit e. The following call list of essential and potential responders has been prepared for use during a release. Chisholm Energy Operating, LLC response must be in coordination with the State of New Mexico's "Hazardous Materials Emergency Response Plan" (HMERP).

Hydrogen Sulfide Drilling Operations Plan

- 1 <u>All Company and Contract personnel admitted on location must be trained</u> by a qualified H2S safety instructor to the following:
 - A. Characteristics of H2S
 - B. Physical effects and hazards
 - C. Principal and operation of H2S detectors, warning system and briefing areas.
 - D. Evacuation procedure, routes and first aid.
 - E. Proper use of safety equipment & life support systems
 - F. Essential personnel meeting Medical Evaluation criteria will receive additional training on the proper use of 30-minute pressure demand air packs.

2 H2S Detection and Alarm Systems:

- A. H2S sensors/detectors to be located on the drilling rig floor, in the base of the sub structure/cellar area, on the mud pits in the shale shaker area. Additional H2S detectors may play placed as deemed necessary.
- B. An audio alarm system will be installed on the derrick floor and in the top doghouse.

3 Windsock and/or wind streamers:

- A. Windsock at mudpit area should be high enough to be visible.
- B. Windsock on the rig floor and/ or top doghouse should be high enough to be visible.

4 <u>Condition Flags and Signs</u>

- A. Warning sign on access road to location.
- B. Flags to be displayed on sign at entrance to location. Green flag

indicates normal safe condition. Yellow flag indicates potential pressure and danger. Red flag indicates danger (H2S present in dangerous concentration). Only H2S trained and certified personnel admitted to location.

5 Well control equipment:

A. See exhibit BOP and Choke Diagrams

6 Communication:

- A. While working under masks chalkboards will be used for communication.
- B. Hand signals will be used where chalk board is inappropriate.
- C. Two-way radio will be used to communicate off location in case of emergency help is required. In most cases, cellular telephones will be available at most drilling foreman's trailer or living quarters.

7 Drill stem Testing:

No DSTs are planned at this time.

- 8 Drilling contractor supervisor will be required to be familiar with the effects H2S has on tubular goods and other mechanical equipment.
- 9 If H25 is encountered, mud system will be altered if necessary to maintain control of formation. A mud gas separator will be brought into service along with H2S scavengers if necessary.

Emergency Assistance Telephone List

Chisholm Energy Holdings, LLC

Chisholm Energy Operating, LLC	Office:	(817)953-6063
Vice President of Operations-Brad Grandstaff	Office:	(817)953-3150
	Cell:	(972)977-9221
Drilling Superintendent-Russell Simons	Cell:	(830)285-7501
Production Superintendent-Paul Martinez	Cell:	(325)206-1722

	Public Safety:			911 or	
	Eddy County Sheriff's Department		Number:	(575)887-7551	
	Eddy County Emergency Managemen	it	Number:	(575)628-5450	
	Lea County Fire Service	,	Number:	(575)628-5450	
	Fire Department:		No contra a su		
	Artesia Fire Department	1	Number:	(575)746-5060	
	Sun Country Volunteer Fire D	•	Number:	(505)484-3599	
	Riverside Volunteer Fire Depa		Number:	(505)365-7900	
	Cottonwood Volunteer Fire D	repartment	Number:	 (505)748-7344 (505)746,0562 	
	Atoka Fire Department	·	Number:	(505)746-9562	
	Queen Volunteer Fire Depart		Number:	(505)981-2498	
	Joel Volunteer Fire Departme	int	Number:	(505)885-4966	
	Otis Fire Rescue	., ,	Number:	(575)236-6113	
	La Huerta Volunteer Fire Dep	artment	Number:	(505)887-6353	
	Carlsbad Fire Department	- 4	Number:	(575)885-3125	
	Hope Volunteer Fire Departm	ient	Number:	(505)484-3351	
	Loco Hills Fire Department		Number:	(505)677-2349	
	Loving Fire Department	L ,	Number:	(505)745-3600	
	White's City Fire Department		Number:	(505)785-2219	
	Hospital:		Number	/F7E)740 2020	
	Artesia General Hospital	·	Number:	(575)748-3333	
	Carlsbad Medical Center AirMed: Medevac		Number:	(575)887-4100	
	Dept. of Public Safety		Number: Number:	(888)303-9112	
	New Mexico OCD-Dist. 2-Artesia	Office	Number: Number:	(505)827-9000	
			Number: Number:	(575)748-1283	
	Eddy County Road Department-South	Emergency	Number:	(575)626-0830 (575)885-4835	
	Eddy County Road Department-South			(575)746-9540	
	NMDOT	•	Number: Number:	(505)827-5100	
:			Number.	(505/027-5100	
•				N	
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Job# Rig: Latshaw 17

Chisholm Energy Holdings

Eddy County, NM (NAD 83) Asteroid 20-29 Fed Com API# WCA 2H

Wellbore #1

Sperry Drilling Services

Ellipse Separation Anticollision Report

Minimum Magnetic Interference Warning level is 50' center to center

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference) Reference Design: Asteroid 20-29 Fed Com - WCA 2H - Wellbore #1 - Plan 1

Well Coordinates:

32° 17' 47.61" N 104° 18' 40.58" W North American Datum 1983 New Mexico Eastern Zone 471,621.09 N 548,153.80 E

Ground Level: 3,386.40 usft

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

Version: 5000.1 Build: 81E

Report Version: Midcon Ellipse v1.50

HALLIBURTON

Anticollision Summary

Reference Design: Asteroid 20-29 Fed Com - WCA 2H - Wellbore #1 - Plan 1

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference) Scan Range: 0.00 to 19,086.20 usft, Measured Depth,

Site Name Comparison Well Name - Wellbore Name - Design	Measured Depth (usft)	Minimum Distance (usft)	@Measured Depth (usft)	Ellipse Separation (usft)	@Measured Depth usft	Clearance Factor	Summary Based on Minimum
Asteroid 20-29 Fed Com			• •				
3BS 3H - Wellbore #1 - Plan 1							
	503.92	29.96	503.92	26.45	503.72	8.545	Centre Distance
	19.036.20	192.75	19,086.20	-41.29	18,861.90	0.824	Ellipse Separation / Clearance Factor
WCB 1H - Wellbore #1 - Plan 1							
	1,000.00	29.94	1,000.00	24.32	1,000.30	5.331	Centre Distance
	7,988,44	48,97	7,936.44	12.53	7,936.43	1.344	Ellipse Separation / Clearance Factor

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

	Uncertaint	y Data for Refer	ence Well		,	Uncertainty	Data for Compa	rison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse Co +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
100.00	100.00	0.00	0.00	0.51	99.80	99.80	0.10	29.96	0.51	29.96	27.66	89.81	13.025
200.00	200.00	0.00	0.00	0.59	199.80	199.80	0.10	29.96	0.59	29.96	27.50	89.81	12.176
300.00	300.00	0.00	0.00	0.73	299.80	299.80	0.10	29.96	0.73	29.96	27.21	89.81	10.905
400.00	400.00	0.00	0.00	0.91	399.80	399.80	0.10	29.96	0.91	29.96	26.86	89.81	9.661
500.00	500.00	0.00	0.00	1.10	499.80	499.80	0.10	29.96	1.10	29.96	26.47	89.81	8.584
503.92	503.92	0.00	0.00	. 1.11	503.72	503.72	0.10	2,9.96	1.11	29.96	26.45	89.81	8.545
600.00	600.00	0.00	0.00	1.31	599.43	599.43	-0.20	30.26	1.29		26.38	90.38	7.783
700.00	700.00	0.00	0.00	1.52	698.99	698.94	-2.34	32.40	1.47	32.50	28.22	94.14	7.603
800.00	800.00	0.00	0.00	1.73	798.93	798.82	-4.81	34.87	1.66	35.21	30.54	97.85	7.533
900.00	900.00	0.00	0.00	1.95	898.87	898.70	-7.28	37.34	1.86	38.05	32.97	101.03	7.483
1,000.00	1,000.00	0.00	0.00	2.16	998.81	998.58	-9.74	39.80	2.06	40.99	35.49	103.75	7.446
1,100.00	1,099.98	1.23	1.23	2.38	1,098.73	1,098.43	-12.21	42.27	2.27	43.20	37.27	63.10	7.290
1,200.00	1,199.92	3.70	3.70	2.60	1,198.61	1,198.25	-14.67	44.73	2.49	44.98	38.63	69.07	7.087
1,300.00	1,299.86	6.17	6.17	2.81	1,298.48	1,298.07	-17.14	47.20	2.71	47.21	40.44	74.54	6.969
1,400.00	1,399.80	8.64	8.64	3.03	1,400.03	1,399.60	-18.41	48.47	2.92	48.15	40.94	79.18	6.684
1,500.00	1,499.74	11.11	11.11	3.25	1,499.97	1,499.54	-18.41	48.47	3.13	47.61	39.99	83.31	6.243
1,600.00	1,599.68	13.57	13.57	3.48	1,599.91	1,599.48	-18.41	48.47	3.33	47.33	39.28	87.51	5.878
1,659.05	1,658.69	15.03	15.03	3.61	1,658.92	1,658.49	-18.41	48.47	3.45	47.29	38.98	90.00	5.693
1,700.00	1,699.61	16.04	16.04	3.70	1,699.85	1,699.41	-18.41	48.47	3.53	47.31	38.83	91.73	5.577
1,750.00	1,749.58	17.27	17.27	3.81	1,749.82	1,749.38	-18.41	48.47	3.63	47.40	38.70	93.84	5.448
1,800.00	1,799.57	18.20	18.20	3.91	1,799.80	1,799.37	-18.41	48.47	3.74	47.50	38.60	95.41	5.335
1,850.00	1,849.56	18.51	18.51	4.00	1,849.80	1,849.36	-18.41	48.47	3.84	47.54	38.45	140.94	. 5.227
1,900.00	1,899.56	18.51	18.51	4.10	1,899.80	1,899.36	-18.41	48.47	3.95	47.54	38.25	140.94	5.113
2,000.00	1,999.56	18.51	18.51	4.32	1,999.80	1,999.36	-18.41	48.47	4.16	47.54	37.81	140.94	4.886
2,100.00	2,099.56	18.51	18.51	4.54	2,099.80	2,099.36	-18.41	48.47	4.37	47.54	37.38	140.94	4.677
2,200.00	2,199.56	18.51	18.51	4.76	2,199.80	2,199.36	-18.41	48.47	4.58	47.54	36.94	140.94	4.485
2,300.00	2,299.56	18.51	18.51	4.98	2,299.80	2,299.36	-18.4 1	48.47	4.80	47.54	36.51	140.94	4.308
2,400.00	2,399.56	18.51	18.51	5.20	2,399.80	2,399.36	-18.41	48.47	5.01	47.54	36.07	140.94	4.143
2,500.00	2,499.56	18.51	18.51	5.42	2,499.80	2,499.36	-18.41	48.47	5.23	47.54	35.63	140.94	3.991
2,600.00	2,599.56	18.51	18.51	5.65	2,599.80	2,599.36	-18.41	48.47	5.44	47.54	35.19	. 140.94	3.849

25 June, 2018 - 10:18

COMPASS

Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

	Uncertainty	Data for Refere	ence Well	,		Uncertainty	Data for Comp	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse Ce +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
2,700.00	2,699.56	18.51	18.51	5.87	2,699.80	2,699.36	-18.41	48.47	5.66	47.54	34.75	140.94	3.716
2,800.00	2,799.56	18.51	18.51	6.09	2,799.80	2,799.36	-18.41	48.47	5.88	47.54	34.31	140.94	3.592
2,900.00	2,899.56	18.51	18.5 1	6.31	2,899.80	2,899.36	-18.41	48.47	6.10	47.54	33.87	140.94	3.476
3,000.00	2,999.56	18.51	18.51	6.54	2,999.80	2,999.36	-18.41	48.47	6.32	47.54	33.43	140.94	3.368
3,100.00	3,099.56	18.51	· 18.51	6.76	3,099.80	3,099.36	-18.41	48.47	6.53	47.54	32.98	140.94	3.265
3,200.00	3,199.56	18.51	18.5 1	6.98	3,199.80	3,199.36	-18.41	48.47	6.75	47.54	32.54	140.94	3.169
3,300.00	3,299.56	18.51	18.51	7.21	° 3,299.80	3,299.36	-18.41	48.47	6.97	47,54	32.10	140.94	3.078
3,400.00	3,399.56	18.51	18.51	7.43	3,399.80	3,399.36	-18.41	48.47	7.19	47.54	31.65	140.94	2.992
3,500.00	3,499.56	18.51	18.51	7.65	3,499.80	3,499.36	-18.41	48.47	7.41	47.54	31.21	140.94	2.910
3,600.00	3,599.56	18.51	18.51	7.88	3,599.80	3,599.36	-18.41	48.47	7.64	47.54	30.76 .	140.94	2.833
3,700.00	3,699.56	18.51	1 8 .51	8.10	3,699.80	3,699.36	-18.41	48.47	7.86	47.54	30.32	140.94	2.760
3,800.00	3,799.56	18.51	18.5 1	8.32	3,799.80	3,799.36	-18.41	48.47	8.08	47.54	29.87	140.94	2.691
3,900.00	3,899.56	18.51	18.5 1	8.55	3,899.80	3,899.36	-18.41	48.47	8.30	47.54	29.43	140.94	2.624
4,000.00	3,999.56	18.51	18,51	8.77	3,999.80	3,999.36	-18.41	48.47	8.52	47.54	28.98	140.94	2.561
4,100.00	4,099.56	18.51	18.51	8.99	4,099.80	4,099.36	-18.41	48.47	8.74	47.54	28.54	140.94	2.501
4,200.00	4,199.56	18.51	18.51	9.22	-4,199.80	4,199.36	-18.41	48.47	8.96	47.54	28.09	140.94	2.444
4,300.00	4,299.56	18.51	18.51	9.44	4,299.80	4,299.36	-18.41	48.47	9.19	47.54	27.65	140.94	2.389
4,400.00	4,399.56	18.51	18.51	9.67	4,399.80	4,399.36	-18.41	48.47	9.41	47:54	27.20	140.94	2.337
4,500.00	4,499.56	18.51	18.51	9.89	4,499.80	4,499.36	-18.41	48.47	9.63	47.54	26.75	140.94	2.287
4,600.00	4,599.56	18.51	18.51	10.11	4,599.80	4,599.36	-18.41	48.47	9.85	47.54	26.31	140.94	2.239
4,700.00	4,699.56	18.51	18.51	10.34	4,699.80	4,699.36	-18.41	48.47	10.08	47.54	25.86	140.94	2.192
4,800.00	4,799.56	18.51	18:51	10.56	4,799.80	4,799.36	-18.41	48.47	10.30	47.54	25.41	140.94	2.148
4,900.00	4,899.56	18.51 -	18.51	10.79	4,899.80	4,899.36	-18.41	48.47	10.52	47.54	24.97	140.94	2.106
5,000.00	4,999.56	18.51	18:51	11.01	4,999.80	4,999.36 ·	-18.41	48.47	10.74	47,54	24.52	140.94	2.065
5,100.00	5,099.56	18.51	18.51	11.24	5,099.80	5,099.36	-18.41	48.47	10.97	47.54	24.07	140.94	2.025
5,200.00	5,199.56	18.51	18.51	11.46	5,199.80	5,199.36	-18.41	48.47	11.19	47.54	23.62	140.94	1.988
5,300.00	5,299.56	18.51	18.51	11.68	5,299.80	5,299.36	-18.41	48.47	11.41	47.54	23.18	140.94	1.951
5,400.00	5,399.56	18.51	18.51	11.91	5,399.80	5,399.36	-18.41	48.47	11.64	47.54	22.73	140.94	1.916
5,500.00	5,499.56	18.51	18.51	12.13	5,499.80	5,499.36	-18.41	48.47	11.86	47.54	22.28	140.94	1.882

25 June, 2018 - 10:18

Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertaint	y Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
5,600.00	5,599.56	18.51	18.51	12.36	5,599.80	5,599.36	-18.41	48.47	12.08	47.54	21.83	140.94	1.849
5,700.00	5,699.56	18.51	18.51	12.58	5,699.80	5,699.36	-18.41	48.47	12.30	47.54	· 21.39	140.94	1.818
5,800.00	5,799.56	18.51	18.51	12.81	5,799.80	5,799.36	-18.41	48.47	12.53	47.54	20.94	140.94	1.787
5,900.00	5,899.56	18.51	18.51	13.03	5,899.80	5,899.36	-18.41	48.47	12.75	47.54	20.49	140.94	1.757
6,000.00	5,999.56	18.51	18.51	13.25	5,999.80	5,999.36	-18.41	48.47	12.97	47.54	20.04	140.94	1.729
6,100.00	6,099.56	18.51	18.51	13.48	6,099.80	6,099.36	-18.41	48.47	13.20	47-54	19.60	140.94	1.701
6,200.00	6,199.56	18.51	18.51	13.70	6,199.80	6,199.36	-18.41	48.47	13. 42	47:54	19.15	140.94	1.674
6,300.00	6,299.56	18.51	18.51	13.93	6,299.80	6,299.36	-18.41	48.47	13.65	47.54	18.70	140.94	1.648
6,400.00	6,399.56	18.5 1	18.51	14.15	6,399.80	6,399.36	-18.41	48.47	13.87	47.54	18.25	140.94	1.623
6,500.00	6,499.56	18.51	18.51	14.38	6,499.80	6,499.36	-18.41	48.47	14.09	47/54	17.80	140.94	1.599
6,600.00	6,599.56	18.51	18.51	14.60	6,599.80	6,599.36	-18.41	48.47	14.32	47/54	17.36	140.94	1.575
6,700.00	6,699.56	18.51	18.51	14.82	6,699.80	6,699.36	-18.41	48.47	14.54	47.54	16.91	140.94	1.552
6,800.00	6,799.56	18.51	18.51	15.05	6,799.80	6,799.36	-18.41	48.47	14.76	47.54	16.46	140.94	1.529
6,900.00	6,899.56	18.51	18.51	15.27	6,899.80	6,899.36	-18.41	48.47	14.99	47.54	16.01	140.94	1.508
7,000,00	6,999.56	18.51	18.51	15.50	6,999.80	6,999.36	-18.41	48.47	15.21	47.54	15.56	140.94	1,437
7,100.00	7,099.56	18.51	18.51	15.72	7,099.80	7,099.36	-18.41	48.47	15.43	47,54	15.11	140.94	1.466
7,200.00	7,199.56	18.51	18.51	15.95	7,199.80	7,199.36	-18.41	48.47	15.66	47.54	14.67	. 140.94	1,446
7,300.00	7,299.56	18.51	18.51	16.17	7,299.80	7,299.36	-18.41	48.47	15.88	47.54	14.22	140.94	1,427
7,400,00	7,399.56	18.51	18.51	16.40	7,399.80	7,399.36	-18.41	48.47	16.11	47.54	13.77	140.94	1,408
7,500,00	7,499.56	18.51	18.51	16.62	7,499.80	7,499.36	-18.41	48.47	16.33	47.54	13.32	140.94	1.339
7,600,00	7,599.56	18.51	18.51	16.85	7,599.80	7,599.36	-18.41	48.47	16.55	47/54	12.87	140.94	1.371
7,700.00	7,699.56	18.51	18.51	17.07	7,699.80	7,699.36	-18.41	48.47	16.78	47.54	12.42	140.94	1.354
7,800.00	7,799.56	18.51	18.51	17.29	`7,799.80	7,799.36	-18.41	48.47	17.00	- 47.54	11.97	140.94	1,337
7,200.00	7,899.56	18.51	18.51	17.52	7,899.80	7,899.36	-18.41	48.47	17.23	47,54	11.53	140.94	1.320
7,986.AA	7,936.00	18.51	18.51	17.60	7,934.26	7,933.80	-18.41	49.46	17.30	48.22	12.07	140.02	1.334
7,950.00	7,949.56	18.51	18.67	17.63	7,946.95	7,946.46	-18.41	50.45	17.33	48.80	12.62	49.22	1.349
8,000,00	7,999.43	18.51	22.03	17.73	7,993.54	7,992.57	-18.41	56.94	17.43	51.25	15.06	46.17	1.416
8,050.00	8,048.82	18.51	29.73	17.84	8,039.73	8,037.45	-18.41	67.7 9	17.53	54.19	18.17	43.05	1.505
8,100.00	8,097.35	18.51	41.70	17.95	8,085.50	8,080.69	-18.41	82.76	17.63	57.62	21.98	39.97	1.617
8,150.00	8,144.65	18.51	57.85	18.06	8,130.82	8,121.89	-18.41	101.60	17.75	61.53	26.48	37.02	1.755

Eddy County, NM (NAD 83)

HALLIBURTON

Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

	Uncertaint	y Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. >	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	centre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
8,200.00	8,190.37	18.51	78.07	18.19	8,175.00	8,160.16	-18.41	123.6 4	17.87	65.88	31.75	34.28	1.930
8,250.00	8,234.14	18.51	102.19	18.33	8,220.02	8,196.89	-18.41	149.63	18.02	70.62	37.36	31.69	2.124
8,300.00	8,275.65	18.51	130.04	18.50	8,263.87	8,230.17	-18.41	178.18	18.19	75.70	43.61	29.36	2.359
8,350.00	8,314.58	18.51	161.40	18.69	8,307.22	8,260.35	-18.41	209.27	. 18.39	81.08	50.27	27.26	2.632
8,400.00	8,350.62	18.51	196.03	18.93	8,350.00	8,287.25	-18. 41	242.51	18.63	86.69	57.25	25.39	2.945
8,450.00	8,383.51	18.51	233.67	19.21	8,392.43	8,310.89	-18.41	277.74	18.91	92.46	64.40	23.70	3.295
8,500.00	8,412.99	18.51	274.03	19.55	8,434.31	8,331.06	-18.41	314.42	19.24	98.35	71.64	22.21	3.681
8,550.00	8,438.84	1,8.51	316.81	19.96	8,475.00	8,347.51	-18.41	351.62	19.61	104.30	. 78.94	20.90	4.113
8,600.00	8,460.86	18.51	361.68	20.44	8,518.64	8,361.86	-18.72	392.83	20.07	110.08	85.43	19.87	4.465
8,633,94	8,473.54	18.51	393.16	20.80	8,550.00	8,371.65	-20.88	422.53	20.42	112.95	88.14	20.46	4.553
8,650.00	8,479.10	18.28	408.22	20.99	8,564.60	8,376.18	-22.59	436.30	20.59	114.07	89.11	20.59	4.571
8,700.00	8,496.34	14.70	455.00	21.58	8,610.05	8,390.15	-30.73	478.76	21.15	117.75	92.24	21.06	4.616
8,750.00	8,513.39	6.79	501.32	22.22	8,654.98	8,403.64	-42.91	519.84	21.74	121.72	95.61	21.57	4.662
8,800.00	8,530.12	-5.39	546.82	22.89	8,700.00	8,416.72	-59.14	559.72	22.35	125.98	99.16	22.14	4.697
8,850.00	8,546.41	-21.75	591.15	23.59	8,743.25	8,428.76	-78.38	596.51	22.94	130.50	103.12	22.68	4.767
8,900.00	8,562.12	-42.16	633.99	24.30	8,786.57	8,440.22	-101.09	.631.56	23.54	135.23	107.25	23.25	4.833
8,950.00	8,577.13	-66.48	675.00	25,02	8,829.36	8,450.85	-126.71	664.13	24.12	140.16	111.62	23.83	4.911
9,000.00	8,591.35	-94.51	713.87	25.72	8,871.63	8,460.58	-154.93	694.04	24.68	145.23	116.20	24.41	5.003
9,050.00	8,604.64	-126.03	750.30	26.42	8,913.39	8,469.39	-185.43	721.14	25.21	150.39	120.96	24.99	5.110
9,100.00	8,616.93	-160.82	784.03	27.08	8,954,65	8,477.23	-217.90	745.35	25.71	155.61	125.87	25.58	5.233
9,150.00	8,628.10	-198.61	814.78	27.73	8,995.45	8,484.08	-252.04	766.58	26.18	160.83	130.88	26.18	5.371
9,200.00	8,638.08	-239.10	842.34	28.33	9,035.79	8,489.92	-287.56	784.78	26.60	165.99	135.94	26.80	5.523
9,250.00	8,646.79	-281.99	866.48	28.90	9,075.00	8,494.67	-323.50	799.68	26.99	171.07	141.08	27.42	5.704
9,300.00	8,654.17	-326.96	887.02	29.42	9,115.23	8,498.57	-361.58	812.00	27.35	176.00	145.96	28.11	5.860
9,350.00	8,660.15	-373.65	903.82	29.90	9,154.37	8,501.38	-399.55	821.03	27.66	180.74	150.80	28.82	6.037
9,400.00	8,664.69	-421.73	916.73	30.33	9,193.16	8,503.19	-437.82	827.04	27.94	185.26	155.44	29.56	6.213
9,450.00	8,667.77	-470.81	925.67	30.72	9,231.63	8,504.02	-476.15	830,07	28.18	189.51	159.80	, 30.34	6.379
9,500.00	8,669.34	-520.53	930.56	31.05	9,275.72	8,503.99	-520.24	830.55	28.42	193.07	163.00	31.17	6.420
9,533.16	8,669.56	-553.67	931.55	31.25	9,308.86	8,503.87	-553.38	830.65	28.61	193.82	163.31	31.37	6.353

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Eddy County, NM (NAD 83)

HALLIBURTON

Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

	Uncertainty	/ Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > (Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
9,600.00	8,669.32	-620.51	931.73	31.64	9,375.71	8,503.64	-620.22	830.84	29.02	193.81	162.52	31.37	• 6.195
9,700.00	8,668.97	-720.51	932.01	32.27	9,475.71	8,503.29	-720.22	831.12	29.69	193.80	161.27	31.37	5.958
9,800.00	8,668.61	-820.50	932.28	32.98	9,575.71	8,502.95	-820.22	831.41	30.45	193.79	159.90	31.37	5.719
9,900.00	8,668.26	-920.50	932.56	33.76	9,675.71	8,502.60	-920.22	831.69	31.28	193.78	158.44	31.37	5.483
10,000.00	8,667.90	-1,020.50	932.83	34.61	9,775.71	8,502.25	-1,020.22	831.98 ·	32.20	193.77	156.89	31.36	5.254
10,100.00	8,667.55	-1,120.50	933.11	35.53	9,875.71	8,501.91	-1,120.22	832.26	33.19	193.76	155.26	31.36	5.033
10,200.00	8,667.20	-1,220.50	933.38	36.52	9,975.71	8,501.56	-1,220.21	832.55	34.25	193.74	153.56	31.36	4.822
10,300.00	8,666.84	-1,320.50	933.66	37 .57	10,075.71	8,501.21	-1,320.21	832.83	35.38	193.73	151.81	31.36	4.621
10,400.00	8,666.49	-1,420.50	933.93	38.68	10,175.71	8,500.87	-1,420.21	833.12	36.57	193.72	150.01	31.36	4.432
10,500.00	8,666.13	-1,520.50	934.21	39.84	10,275.71	8,500.52	-1,520.21	833.41	37.81	. 193.71	148.16	31.36	4.253
10,600.00	8,665.78	-1,620.50	934.48	41.06	10,375.71	8,500.17	-1,620.21	833.69	39.11	193.70	146.27	31.36	4.084
10,700.00	8,665.43	-1,720.50	934.76	42.32	10,475.71	8,499.82	-1,720.21	833.98	40.45	193.69	144.35	31.35	3.926
10,800.00	8,665.07	-1,820.49	935.04	43.63	10,575.71	8,499.48	-1,820.21	834.26	41.83	193.68	142.40	31.35	3.777
10,900.00	8,664.72	-1,920.49	935.31	44.98	10,675.71	8,499.13	-1,920.21	834.55	43.25	193.67	140.42	31.35	3.637
11,000.00	8,664.36	-2,020.49	935.59	46.36	10,775.71	8,498.78	-2,020.21	834.83	44.70	193.66	138.41	31.35	3.506
11,100.00	8,664.01	-2,120.49	935.86	47.78	10,875.71	8,498.44	-2,120.21	835.12	46.18	193.64	136.39	31.35	3.382
11,200.00	8,663.65	-2,220.49	936.14	49.23	10,975.71	8,498.09	-2,220.20	835.40	47.69	193.63	134.34	31.35	3.266
11,300.00	8,663.30	-2,320.49	936.41	50.71	11,075.71	8,497.74	-2,320.20	835.69	49.22	193.62	132.28	31.35	3.156
11,400.00	8,662.95	-2,420.49	936.69	52.21	11,175.71	8,497.39	-2,420.20	835.97	50.77	193.61	130.20	31.35	3.053
11,500.00	8,662.59	-2,520.49	936.96	53.73	11,275.71	8,497.05	-2,520.20	836.26	52.34	193.60	128.11	31.34	2,956
11,600.00	8,662.24	-2,620.49	937.24	55.27	11,375.71	8,496.70	-2,620.20	836.54	53.93	193.59	126.00	31.34	2.864
11,700.00	8,661.88	-2,720.49	937.51	56.83	11,475.71	8,496.35	-2,720.20	836.83	55.54	193.58	123.89	31.34	2.778
11,800.00	8,661.53	-2,820.48	937.79	58.41	11,575.71	8,496.01	-2,820.20	837.11	57.16	193.57	121.76	31.34	2.696
11,900.00	8,661.17	-2,920.48	938.07	60.01	11,675.71	8,495.66	-2,920.20	837.40	58.80	193.55	119.62	31.34	2.618
12,000.00	8,660.82	-3,020.48	938.34	61.62	11,775.71	8,495.31	-3,020.20	837.68	60.44	193.54	117.48	31.34	2.544
12,100.00	8,660.47	-3,120.48	938.62	63.24	11,875.71	8,494.96	-3,120.19	837.97	62.10	193.53	115.32	31.34	2.474
12,200.00	8,660.11	-3,220.48	938.89	64.88	11,975.71	8,494.62	-3,220.19	838.25	63.77	193.52	113.16	31.33	2.408
12,300.00	8,659.76	-3,320.48	939.17	66.52	12,075.71	8,494.27	-3,320.19	838.54	65.45	193.51	110.99	31.33	2.345
12,400.00	8,659.40	-3,420.48	939.44	68.18	12,175.71	8,493.92	-3,420.19	838.82	67.13	193.50	108.82	31.33	2.285
12,500.00	8,659.05	-3,520.48	939.72	69.84	12,275.71	8,493.58	-3,520.19	839.11	68.83	193.49	106.64	31.33	2.228

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Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

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	Uncertainty	/ Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
12,600.00	8,658.70	-3,620.48	939.99	71.52	12,375.71	8,493.23	-3,620.19	839.39	70.53	193.48	104.45	31.33	2.173
12,700.00	8,658.34	-3,720.48	940.27	73.20	12,475.71	8,492.88	-3,720.19	839.68	72.24	193.47	102.26	31.33	2.121
12,800.00	8,657.99	-3,820.47	940.54	74.89	12,575.71	8,492.54	-3,820.19	839.96	73.95	193.45	100.07	31.33	2.071
12,900.00	8,657.63	-3,920.47	940.82	76.59	12,675.71	8,492.19	-3,920.19	840.25	75.67	193.44	97.87	31.32	2.024
13,000.00	8,657.28	-4,020.47	941.10	78.29	12,775.71	8,491.84	-4,020.19	840.54	77.40	193.43	95.66	31.32	1.978
13,100.00	8,656.92	-4,120.47	941.37	80.00	12,875.71	8,491.49	-4,120.18	840.82	79.13	193.42	93.46	31.32	1.935
13,200.00	8,656.57	-4,220.47	941.65	81.71	12,975.71	8,491.15	-4,220.18	841.11	80.86	193.41	91.24	31.32	1.893
13,300.00	8,656.22	-4,320.47	941.92	83.43	13,075.71	8,490.80	-4,320.18	841.39	82.60	193.40	89.03	31.32	1.853
13,400.00	8,655.86	-4,420.47	942.20	85.16	13,175.71	8,490.45	-4,420.18	841.68	84.35	193.39	86.81	31.32	1.815
13,500.00	8,655.51	-4,520.47	942.47	86.89	13,275.71	8,490.11	-4,520.18	841.96	86.09	193.38	84.59	31.32	1.778
13,600.00	8,655.15	-4,620.47	942.75	88.62	13,375.71	8,489.76	-4,620.18	842.25	87.84	193.36	82.37	31.32	1.742
13,700.00	8,654.80	-4,720.47	943.02	90.36	13,475.71	8,489.41	-4,720.18	842.53	89.60	193.35	80.15	31.31	1.708
13,800.00	8,654.44	-4,820.46	943.30	92.10	13,575.71	8,489.06	-4,820.18	842.82	91.36	193.34	77.92	31.31	1.675
13,900.00	8,654.09	-4,920.46	943.57	93.85	13,675.71	8,488.72	-4,920.18	843.10	93.12	193.33	75.69	31.31	1.643
14,000.00	8,653.74	-5,020.46	943.85	95.60	13,775.71	8,488.37	-5,020.18	843.39	94.88	193.32	73.46	31.31	1.613
- 14,100.00	8,653.38	-5,120.46	944.13	97.35	13,875.71	8,488.02	-5,120.17	843.67	96.64	193.31	71.23	31.31	1.583
14,200.00	8,653.03	-5,220.46	944.40	99.10	13,975.71	8,487.68	-5,220.17	843.96	98.41	193.30	68.99	31.31	1.555
14,300.00	8,652.67	-5,320.46	944.68	100.86	14,075.71	8,487.33	-5,320.17	844.24	100.18	193.29	66.76	31.31	1.528
14,400.00	8,652.32	-5,420.46	944.95	102.62	14,175.71	8,486.98	-5,420.17	844.53	101.96	193.28	64.52	31.30	1.501
14,500,00	8,651.97	-5,520.46	945.23	104.39	14,275.71	8,486.64	-5,520.17	844.81	103.73	193.26	62.28	31.30	1,475
14,800.00	8,651.61	-5,620.46	945.50	106.15	14,375.71	8,486.29	-5,620.17	845.10	105.51	193.25	60.04	31.30	1.451
14,700.00	8,651.26	-5,720.46	945.78	107.92	14,475.71	8,485.94	-5,720.17	845.38	107.29	193.24	57.79	31.30	1.427
14,800.00	8,650.90	-5,820.45	946.05	109.69	14,575.71	8,485.59	-5,820.17	845.67	109.07	193.23	55.55	31.30	1.408
14,900.00	8,650.55	-5,920.45	946.33	111.46	14,675.71	8,485.25	-5,920.17	845.95	110.85	193.22	53.30	31.30	1,331
15,000,00	8,650.19	-6,020.45	946.60	113.24	14,775.71	8,484.90	-6,020.17	846.24	112.63	193.21	51.06	31.30	1.352
15,100.00	8,649.84	-6,120.45	946.88	115.01	14,875.71	8,484.5 5	-6,120.16	846.52	114.42	193.20	48.81	31.29	1.338
15,200.00	8,649.49	-6,220.45	947.16	116.79	14,975.71	8,484.21	-6,220.16	846.81	116.21	193.19	46.56	31.29	1.318
15,300,00	8,649.13	-6,320.45	947.43	118.57	15,075.71	8,483.86	-6,320.16	847.10	117.99	193.17	44.31	31.29	1.298
15,400,00	8,648.78	-6,420.45	947.71	120.35	15,175.71	8,483.51	-6,420.16	847.38	119.78	193.16	42.06	31.29	1.278

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

	Uncertainty	y Data for Refer	rence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth	Vertical Depth	Ellipse C +N/-S	+E/-W	Ellipse Major	Measured Depth	Vertical Depth	Ellipse C +N/-S	+E/-W	Ellipse Major	Between Centres	Between Ellipsoids	Relative Highside	Clearance
(usft)	(usft)	(usft)	(usft)	Axis/2	(usft)	(usft)	(usft)	(usft) _	Axis/2	(usft)	(usft)	Bearing	Factor
15,500.00	8,648.42	-6,520.45	947.98	122.13	15,275.71	8,483.16	-6,520.16	847.67	121.57	193.15	39.81	31.29	1.260
15,600.00	8,648.07	-6,620.45	948.26	123.92	15,375.71	8,482.82	-6,620.16	847.95	123.37	193.14	37.56	31.29	1,241
15,700.00	8,647.71	-6,720.45	948.53	125.70	15,475.71	8,482.47	-6,720.16	848.24	125.16	193.13	35.30	31.29	1.224
15,800.00	8,647.36	-6,820.44	948.81	127.49	15,575.71	8,482.12	-6,820.16	848.52	126.95	193.12	33.05	31.29	1.208
15,900.00	8,647.01	-6,920.44	949.08	129.28	15,675.71	8,481.78	-6,920.16	848.81	128.75	193.11	30.79	31.28	1.190
16,000,00	8,646.65	-7,020.44	949.36	131.07	15,775.71	8,481.43	-7,020.16	849.09	130.55	193.10	28.54	31.28	1.178
16,100.00	8,646.30	-7,120.44	949.63	132.86	15,875.71	8,481.08	-7,120.15	849.38	132.34	193.09	26.28	· 31.28	1.158
16,200.00	8,645.94	-7,220.44	949.91	134.65	15,975.71	8,480.73	-7,220.15	849.66	134.14	193.07	24.03	31.28	1.142
16.300.00	8,645.59	-7,320.44	950.19	136.44	16,075.71	8,480.39	-7,320.15	849.95	135.94	193.06	21.77	31.28	1.127
16,400,00	8,645.23	-7,420.44	950.46	138.23	<u>16,175.71</u>	8,480.04	-7,420.15	850.23	137.74	193.05	19.51	31.28	1.112
16,500.00	8,644.88	-7,520.44	950.74	140.03	16,275.71	8,479.69	-7,520.15	850.52	139.54	193.04	17.25	31.28	1.098
16.600.00	8,644.53	-7,620.44	951.01	141.82	16,375.71	8,479.35	-7,620.15	850.80	141.34	193.03	14.99	31.27	1.084
16,700.00	8,644.17	-7,720.44	951.29	143.62	16,475.71	8,479.00	-7,720.15	851.09	143.15	193.02	12.73	31.27	1.071
16,800,00	8,643.82	-7,820.43	951.56	145.42	16,575.71	8,478.65	-7,820.15	851.37	144.95	193.01	10.47	31.27	1.057
16,000.00	8,643.46	-7,920.43	951.84	147.22	16,675.71	8,478.31	-7,920.15	851.66	146.75	193.00	8.21	31.27	1.044
17,000,00	8,643.11	-8,020.43	952.11	149.02	16,775.71	8,477.96	-8,020.15	851.94	148.56	192.98	5.95	31.27	1.032
17,100.00	8,642.76	-8,120.43	952.39	150.82	16,875.71	8,477.61	-8,120.14	852.23	150.36	192.97	3.69	31.27	1.019
17,200.00	8,642.40	-8,220.43	952.66	152.62	16,975.71	8,477.26	-8,220.14	852.51	152.17	192.96	1.43	31.27	1.007
17,300.00	8,642.05	-8,320.43	952.94	154.42	17,075.71	8,476.92	-8,320.14	852.80	153.98	192.95	< 0	31.26	0.996
17,000.00	8,641.69	-8,420.43	953.22	156.22	17,175.71	8,476.57	-8,420.14	853.08	155.78	192.94	< 0	31.26	0.984
17,500.00	8,641.34	-8,520.43	953.49	158.02	17,275.71	8,476.22	-8,520.14	853.37	157.59	192.93	< 0	31.26	0.972
17,000.00	8,640.98	-8,620.43	953.77	159.83	17,375.71	8,475.88	-8,620.14	853.65	159.40	192.92	< 0	31.26	0.962
17,700,00	8,640.63	-8,720.43	954.04	161.63	17,475.71	8,475.53	-8,720.14	853.94	161.21	192.91	< 0	31.26	0.931
17,800,00	8,640.28	-8,820.42	954.32	163.44	17,575.71	8,475.18	-8,820.14	854.23	163.02	192.90	< 0	31.26	0.941
17,900.00	8,639.92	-8,920.42	954.59	165.24	17,675.7 1	8,474.83	-8,920.14	854.51	164.83	192.88	< 0	31.26	0.980
18,000.00	8,639.57	-9,020.42	954.87	167.05	17,775.71	8,474.49	-9,020.14	854.80	166.64	192.87	< 0	31.25	0,920
18,100.00	8,639.21	-9,120.42	955.14	168.85	17,875.71	8,474.14	-9,120.13	855.08	168.45	192.86	< 0	31.25	0.911
18,200.00	8,638.86	-9,220.42	955.42	170.66	17,975.71	8,473.79	-9,220.13	855.37	170.26	192.85	< 0	31.25	0.901
18,300.00	8,638.50	-9,320.42	955.69	172.47	18,075.71	8,473.45	-9,320.13	855.65	172.07	192.84	< 0	31.25	0.391
18,400.00	8,638.15	-9,420.42	955.97	174.28	18,175.71	8,473.10	-9,420.13	855.94	173.88	192.83	< 0	31.25	0.832

25 June, 2018 - 10:18

COMPASS

Offset Design: Asteroid 20-29 Fed Com - 3BS 3H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertaint	y Data for Refe	rence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. >	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	Centre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth <u>(</u> usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
18,500.00	8,637.80	-9,520.42	956.25	176.08	18,275.71	8,472.75	-9,520.13	856.22	175.69	192.82	< 0	31.25	0.378
18,600.00	8,637.44	-9,620.42	956.52	177.89	18,375.71	8,472.41	-9,620.13	856.51	177.51	192.81	< 0	31.25	0.864
18,700.00	8,637.09	-9,720.42	956.80	179.70	18,475.71	8,472.06	-9,720.13	856.79	179.32	192.79	< 0	31.25	0.356
18,800.00	8,636.73	-9,820.41	957.07	181.51	18,575.71	8,471.71	-9,820.13	857.08	181.13	192.78	< 0	31.24	0.847
18,900.00	8,636.38	-9,920.41	957.35	183.32	18,675.71	8,471.36	-9,920.13	857.36	182.95	192.77	< 0	31.24	0.83E
19,000,00	8,636.03	-10,020.41	957.62	185.13	18,775.71	8,471.02	-10,020.13	857.65	184.76	192.76	< 0	31.24	0.831
19,036,20	8,635.72	-10,106.61	957.86	186.69	18,861.90	8,470.72	-10,106.32	857.89	186.33	192.75	< 0	31.24	0.824

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertaint	y Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
100.00	100.00	0.00	0.00	0.51	100.30	100.30	-0.03	-29.94	0.51	29.94	27.64	-90.06	13.016
200.00	200.00	0.00	0.00	0.59	200.30	200.30	-0.03	-29.94	0.59	29.94	27.48	-90.06	12.165
300.00	300.00	0.00	0.00	0.73	300.30	300.30	-0.03	-29.94	0.73	-29.94	27.19	-90.06	10.895
400.00	400.00	0.00	0.00	0.91	[,] 400.30	400.30	-0.03	-29.94	0.91	29.94	26.84	-90.06	9.651
500.00	500.00	0.00	0.00	1.10	500.30	500.30	-0.03	-29.94	1.10	29:94	26.45	-90.06	8.575
600.00	600.00	0.00	0.00	1.31	600.30	600.30	-0.03	-29.94	1.31	29.94	26.04	-90.06	7.677
700.00	700.00	0.00	0.00	1.52	700.30	700.30	-0.03	-29.94	1.52	29.94	25.62	-90.06	6.930
800.00	800.00	0.00	0.00	1.73	800.30	800.30	-0.03	-29.94	1.73	29.94	25.19	-90.06	6.306
900.00	900.00	0.00	0.00	1.95	900.30	900.30	-0.03	-29.94	1.95	29.94	24.76	-90.06	5.780
1,000.00	1,000.00	· 0.00	0.00	2.16	1,000.30	1,000.30	-0.03	-29.94	2.17	29.94	24.32	-90.06	5,331
1,100.00	1,099.98	1.23	1.23	2.38	1,100.28	1,100.28	-0.03	-29.94	2.38	31.20	25.15	-137.30	5.156
1,200.00	1,199.92	3.70	3.70	2.60	1,200.22	1,200.22	-0.03	-29.94	2.60	33.85	27.36	-141.31	5.220
1,300.00	1,299.86	6.17	6.17	2.81	1,300.16	1,300.16	-0.03	-29.94	2.83	36.64	29.72	-144.73	5.295
1,400.00	1,399.80	8.64	8.64	3.03	1,400.10	1,400.10	-0.03	-29.94	3.05	39:54	32.18	-147.65	5.374
1,500.00	1,499.74	11.11	11.11	3.25	1,500.04	1,500.04	-0.03	-29.94	3.27	42.53	34.73	-150.16	5.454
1,600.00	1,599.68	13.57	13.57	3.48	1,599.98	1,599.98	-0.03	-29.94	3.49	45.59	37.35	-152.35	5.533
1,700.00	1,699.61	16.04	16.04	3.70	1,699.91	1,699.91	-0.03	-29.94	3.71	48.71	40.03	-154.25	5.611
1,750.00	1,749.58	17.27	17.27	3.81	1,749.88	1,749.88	-0.03	-29.94	3.82	50.29	41.38	-155.11	5.648
1,800.00	1,799.57	18.20	18.20	3.91	1,799.87	1,799.87	-0.03	-29.94	3.94	51.48	42.36	-155.74	5.649
1,850.00	1,849.56	18.51	18.51	4.00	1,849.86	1,849.86	-0.03	-29.94	4.05	51.87	42.56	-110.94	5.572
1,900.00	1,899.56	18.51	18.51	4.10	1,899.86	1,899.86	-0.03	-29.94	4.16	51.87	42.35	-110.94	5.449
2,000.00	1,999.56	18.51	· 18.51	4.32	1,999.86	1,999.86	-0.03	-29.94	4.38	51.87	41.91	-110.94	5.206
2,100.00	2,099.56	18.51	18.5 1	4.54	2,100.56	2,100.54	-1.28	-28.69	4.58	51.18	40.80	-112.74	4.928
2,200.00	2,199.56	18.51	18.5 1	4.76	2,200.50	2,200.42	-3.74	-26.23	4.76	49.97	39.18	-116.45	4.633
2,300.00	·2,299.56	18.51	18.51	4.98	2,300.22	2,300.09	-5.8 9	-24.08	4.95	49.08	37.88	-119.81	4.383
2,365.64	2,365.21	18.51	18.51	5.12	2,365.64	2,365.51	-6.20	-23.77	5.08	48.97	37.50	-120.30	4.269
2,400.00	2,399.56	18.51	18.51	5.20	2,400.00	2,399.86	-6.20	-23.77	5.15	48.97	37.35	-120.30	4.216
2,500.00	2,499.56	18.51	18.51	5.42	2,500.00	2,499.86	-6.20	-23.77	5.37	48.97	36.91	-120.30	4.060
2,600.00	2,599.56	18.51	18.51	5.65	2,600.00	2,599.86	-6.20	-23.77	5.59	48.97	36.46	-120.30	3.915
2,700.00	2,699.56	18.51	18.51	5.87	2,700.00	2,699.86	-6.20	-23.77	5.82	48.97	36.02	-120.30	3.780

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertainty	y Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
2,800.00	2,799.56	18.51	18.51	6.09	2,800.00	2,799.86	-6.20	-23.77	6.04	48:97	35.57	-120.30	3.654
2,900.00	2,899.56	18.51	18.51	6.31	2,900.00	2,899.86	-6.20	-23.77	6.26	48.97	35.12	-120.30	3.536
3,000.00	2,999.56	18.51	18.51	6.54	3,000.00	2,999.86	-6.20	-23.77	6.49	48.97	34.68	-120.30	3.426
3,100.00	3,099.56	18.51	18.51	6.76	3,100.00	3,099.86	-6.20	-23.77	6.71	48.97	34.23	-120.30	3.322
3,200.00	3,199.56	18.51	18.51	6.98	3,200.00	3,199.86	-6.20	-23.77	6.94	48.97	33.78	-120.30	3.224
3,300.00	3,299.56	18.51	18.51	7.21	3,300.00	3,299.86	-6.20	-23.77	7.16	48.97	33.33	-120.30	3.132
3,400.00	3,399.56	18.51	18.51	7.43	3,400.00	3,399.86	-6.20	-23.77	7.38	48.97	32.89	-120.30	3.045
3,500.00	3,499.56	18.51	18.51	7.65	3,500.00	3,499.86	-6.20	-23.77	7.61	48.97	32.44	-120.30	2.962
3,600.00	3,599.56	18.51	18.51	7.88	3,600.00	3,599.86	-6.20	-23.77	7.83	48.97	31.99	-120.30	2.884
3,700.00	3,699.56	18.51	18.51	8.10	3,700.00	3,699.86	-6.20	-23.77	8.05	48:97	31.54	-120.30	2.810
3,800.00	3,799.56	18.51	18.51	8.32	3,800.00	3,799.86	-6.20	-23.77	8.28	48.97	31.10	-120.30	2.740
3,900.00	3,899.56	18.51	. 18.51	8.55	3,900.00	3,899.86	-6.20	-23.77	8.50	48.97	30.65	-120.30	2.673
4,000.00	3,999.56	18.51	18.51	8.77	,4,000.00	3,999.86	-6.20	-23.77	8.73	48.97	30.20	-120.30	2.609
4,100.00	4,099.56	18.51	18.51	8.99	4,100.00	4,099.86	-6.20	-23.77	8.95	48.97	29.75	-120.30	2.548
4,200.00	4,199.56	18.51	18.51	9.22	4,200.00	4,199.86	-6.20	-23.77	. 9.18	48.97	29.30	-120.30	2.490
- 4,300.00	4,299.56	18.51	18.51	9.44	4,300.00	4,299.86	-6.20	-23.77	9.40	48.97	28.86	-120.30	2.435
4,400.00	4,399.56	18.51	18.51	9.67	4,400.00	4,399.86	-6.20	-23.77	9.62	48.97	28.41	-120.30	2.381
4,500.00	4,499.56	18.51	18.51	9.89	4,500.00	4,499.86	-6.20	-23.77	9.85	48.97	27.96	-120.30	2.331
4,600.00	4,599.56	18.51	18.51	10.11	4,600.00	4,599.86	-6.20	-23.77	10.07	48.97	27.51	-120.30	2.282
4,700.00	4,699.56	18.51	18.51	10.34	4,700.00	4,699.86	-6.20	-23.77	10.30	48.97	27.06	-120.30	2,235
4,800.00	4,799.56	18.51	18.51	10.56	4,800.00	4,799.86	-6.20	-23.77	10.52	48:97	26.61	-120.30	2.190
4,900.00	4,899.56	18.51	18.51 ·	10.79	4,900.00	4,899.86	-6.20	-23.77	10.75	48.97	26.16	-120.30	2.147
5,000.00	4,999.56	18.51	18.51	11.01	5,000.00	4,999.86	-6.20	-23.77	10.97	48.97	25.72	-120.30	2.106
5,100.00	5,099.56	18.51	18.51	11.24	5,100.00	5,099.86	-6.20	-23.77	11.19	48.97	25.27	-120.30	2.066
5,200.00	5,199.56	18.51	18.51	11.46	5,200.00	5,199.86	-6.20	-2 3.77	11.42	48.97	24.82	-120.30	2.028
5,300.00	5,299.56	18.51	18.51	11.68	5,300.00	5,299.86	-6.20	-23.77	11.64	48.97	24.37	-120.30	1.991
5,400.00	5,399.56	18.51	18.51	11.91	5,400.00	5,399.86	-6.20	-23.77	11.87	48.97	23.92	-120.30	1.955
5,500.00	5,499.56	18.51	18,51	12.13	5,500.00	5,499.86	-6.20	-23.77	12.09	48.97	23.47	-120.30	1.921
5,600.00	5,599.56	18.51	18.51	12.36	5,600.00	5,599.86	-6.20	-23.77	12.32	48.97	23.02	-120.30	1.887

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

-	Uncertainty	y Data for Refer	ence Well		3	Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
5,700.00	5,699.56	18.51	18.51	12.58	5,700.00	5,699.86	-6.20	-23.77	12.54	48:97	22.57	-120.30	1.855
5,800.00	5,799.56	18.51	18.51	12.81	5,800.00	5,799.86	-6.20	-23.77	12.77	48.97	22.13	-120.30	1.824
5,900.00	5,899.56	18.51	18.51	13.03	5,900.00	5,899.86	-6.20	-23.77	12.99	48.97	21.68	-120.30	1.794
6,000.00	5,999.56	18.51	18.51	13.25	6,000.00	5,999.86	-6.20	-23.77	13.21	48.97	21.23	-120.30	1.765
6,100.00	6,099.56	18.51	18.51	13.48	6,100.00	6,099.86	-6.20	-23.77	13.44	48.97	20.78	-120.30	1.737
6,200.00	6,199.56	18.51	18.51	13.70	6,200.00	6,199.86	-6.20	-23.77	13.66	48.97	20.33	-120.30	1.710
6,300.00	6,299.56	18.51	18.51	13.93	6,300.00	6,299.86	-6.20	-23.77	13.89	48.97	19.88	-120.30	1.683
6,400.00	6,399.56	18.51	18.51	14.15	6,400.00	6,399.86	-6.20	-23.77	14.11	48.97	19.43	-120.30	1.658
6,500.00	6,499.56	18.51	18.51	14.38	6,500.00	6,499.86	-6.20	-23.77	14.34	48.97	18.98	-120.30	1.633
6,600.00	6,599.56	18.51	18.51	14.60	6,600.00	6,599.86	-6.20	-23.77	14.56	48.97	18.53	-120.30	1.609
6,700.00	6,699.56	18.51	18.51	14.82	6,700.00	6,699.86	-6.20	-23.77	14.79	48.97	18.09	-120.30	1.586
6,800.00	6,799.56	18.51	18.51	15.05	6,800.00	6,799.86	-6.20	-23.77	15.01	48:97	17.64	-120.30	1.563
6,900.00	6,899.56	18.51	18.51	15.27	6,900.00	6,899.86	-6.20	-23.77	15.24	48.97	17.19	-120.30	1.541
7,000.00	6,999.56	18.51	18.51	15.50	7,000.00	6,999.86	-6.20	-23.77	15.46	48.97	16.74	-120.30	1.519
7,100.00	7,099.56	18.51	18.51	15.72	7,100.00	7,099.86	-6.20	-23.77	15.68	48.97	16.29	-120.30	1,493
7,200.00	7,199.56	18.51	18.51	15.95	7,200.00	7,199.86	-6.20	-23.77	15.91	48.97	15.84	-120.30	1,478
7.300.00	7,299.56	18.51	18.51	16.17	7,300.00	7,299.86	-6.20	-23.77	16.13	48.97	15.39	-120.30	1,458
7,400,00	7,399.56	18.51	18.51	16.40	7,400.00	7,399.86	-6.20	-23.77	16.36	48.97	14.94	-120.30	1,430
7,500.00	7,499.56	18.51	18.51	16.62	7,500.00	7,499.86	-6.20	-23.77	16.58	48.97	14.49	-120.30	1.420
7,600.00	7,599.56	18.51	18.51	16.85	7,600.00	7,599.86	-6.20	-23.77	16.81	48.97	14.04	-120.30	1,402
7,700.00	7,699.56	18.51	18.51	17.07	7,700.00	7,699.86	-6.20	-23.77	17.03	48.97	13.59	-120.30	1.384
7,300.00	7,799.56	18.51	18.51	17.29	7,800.00	7,799.86	-6.20	-23.77	17.26	48.97	13.15	-120.30	1.367
7,900.00	7,899.56	18.51	18.51	17.52	7,900.00	7,899.86	-6.20	-23.77	17.48	48.97	12.70	-120.30	1.350
7,933.AA	7,936.00	18.51	18.51	17.60	7,936.43	7,936.30	-6.20	-23.77	17.56	48.97	12.53	-120.30	1.344
7,950.00	7,949.56	18.51	18.67	17.63	7,949.99	7,949.86	-6.20	-23.77	17.59	49.11	12.61	149.79	1.346
8,000.00	7,999.43	18.51	22.03	17.73	7,999.87	7,999.73	-6.20	-23.77	17.71	52.04	15.33	151.51	1.418
8,050.00	8,048.82	18.51	29.73	17.84	8,049.25	8,049.12	-6.20	-23.77	17.82	58.93	22.01	154.78	1.596
8,100.00	8,097.35	18.51	41.70	17.95	8,097.78	8,097.65	-6.20	-23.77	17.93	69.97	32.85	158.53	1.885
8,150.00	8,144.65	18.51	57.85	18.06	8,145.08	8,144.95	-6.20	-23.77	18.03	85.28	47.95	161.99	2.284
8,200.00	8,190.37	18.51	78.07	18.19	8,190.80	8,190.67	-6.20	-23.77	18.13	104.79	67.26	-164.85	2.792

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertaint	y Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well	•	Sepa	ration (Ref. > (Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
8,250.00	8,234.14	18.5 1	102.19	18.33	8,234.58	8,234.44	-6.20	-23.77	18.23	128.36	90.64	167.06	3.403
8,300.00	8,275.65	18.51	130.04	18.50	8,276.08	8,275.95	-6.20	-23.77	18.33	155.78	117.87	168.72	4.110
8,350.00	8,314.58	18.51	161.40	18.69	8,315.01	8,314.88	-6.20	-23.77	18.41	186.81	148.73	169.92	4,906
8,400.00	8,350.62	18.51	196.03	18.93	8,351.05	8,350.92	-6.20	-23.77	18.49	221.18	182.94	170.75	5.784
8,450.00	8,383.51	18.51	233.67	19.21	8,383.94	8,383.81	-6.20	-23.77	18.57	258.62	220.24	171.26	6.738
8,500.00	8,412.99	18.51	274.03	19.55	8,413.42	8,413.29	-6.20	-23.77	18.63	298.83	260.31	171.48	7.759
8,550.00	8,438.84	18.51	316.81	19.96	° 8,439.27	8,439.14 [.]	-6.20	-23.77	18.69	341.48	302.85	171.39	8.840
8,600.00	8,460.86	18.51	361.68	20.44	8,461.29	8,461.16	-6.20	-23.77	18.74	386.24	347.52	170.92	9.974
8,633.94	8,473.54	18.51	393.16	20.80	8,473.98	8,473.84	-6.20	-23.77	18.77	417.66	378.88	170.28	10.769
8,650.00	8,479.10	18.28	408.22	20.99	8,479.53	8,479.40	-6.20	-23.77	18.78	432.69	393.88	165.93	11.150
8,700.00	8,496.34	14.70	455.00	21.58	8,496.78	8,496.64	-6.20	-2 3.77	18.82	479.23	440.36	153.93	12.329
8,750.00	8,513.39	6.79	501.32	22.22	8,513.83	8,513.69	-6.20	-23.77	18.86	525.25	486.32	144.09	13.491
8,800.00	8,530.12	-5.39	546.82	22.89	8,530.56	8,530.42	-6.20	-23.77	18.90	570.59	531.59	135.99	14.632
8,850.00	8,546.41	-21.75	591.15	23.59	8,546.84	8,546.71	-6.20	-23.77	18.93	615.12	576.06	129.22	15.748
8,900.00	8,562.12	-42.16	633.99	24.30	8,562.55	8,562.42	-6.20	-23.77	18.97	658.74	619.62	123.48	16.839 [·]
8,950.00	8,577.13	-66.48	675.00	25.02	8,577.57	8,577.43	-6.20	-23.77	19.00	701.36	662.18	118.52	17.900
9,000.00	8,591.35	-94.51	713.87	25.72	8,591.78	8,591.65	-6.20	-23.77	19.03	742.91	703.66	114.19	18.932
9,050.00	8,604.64	-126.03	750.30	26.42	8,605.08	8,604.94	-6.20	-23.77	19.06	783.29	744.00	110.38	19.932
9,100.00	8,616.93	-160.82	784.03	27.08	9,750.50	9,404.41	-50.72	594.57	25.78	817.11	791.84	175.19	32.330
9,150.00	8,628.10	-198.61	814.78	27.73	9,810.22	9,419.94	-76.63	646.05	26.64	818.46	792.97	175.62	32.106
9,200.00	8,638.08	-239.10	842.34	28.33	9,873.23	9,435.36	-109.87	697.27	27.53	820.31	794.62	176.14	31.925
9,250.00	8,646.79	-281.99	866.48	28.90	9,939.80	9,450.36	-151.15	747.26	28.46	822.54	796.67	176.72	31.793
9,300.00	8,654.17	-326.96	887.02	29.42	10,010.15	9,464.57	-201.02	794.73	29.40	825.01	798.99	177.36	31,704
9,350.00	8,660.15	-373.65	903.82	29.90	10,084.35	9,477.48	-259.77	838.08	30.31	827.54	801.39	178.01	31.643
9,400.00	8,664.69	-421.73	916.73	30.33	10,162.31	9,488.52	-327.24	875. 4 0	31.18	829.96	803.67	` 178.65	31.572
9;450.00	8,667.77	-470.81	925.67	30.72	10,243.68	9,497.08	-402.62	904.65	31.96	832.08	805.60	179.22	31.423
9,500.00	8,669.34	-520.53	930.56	31.05	10,327.85	9,502.56	-484.31	923.86	32.63	833.73	806.93	179.68	31.110
9,533.16	8,669.56	-553.67	931.55	31.25	10,384.79	9,504.26	-540.84	930.27	33.01	834.50	807.38	179.91	30.770
9,600.00	8,669.32	-620.51	931.73	31.64	10,467.44	9,504.32	-623.46	931.66	33.48	834.70	806.88	179.99	30.002

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertainty	y Data for Refer	rence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
9,700.00	8,668.97	-720.51	932.01	32.27	10,567.44	9,503.96	-723.46	931.94	34.07	834.70	805.90	179.99	28.977
9,800.00	8,668.61	-820.50	932.28	32.98	10,667.44	9,503.61	-823.46	932.22	34.73	834.70	804.87	179.99	27.982
9,900.00	8,668.26	-920.50	932.56	33.76	10,767.44	9,503.26	-923.46	932.49	35.46	834.70	803.81	179.99	27.021
10,000.00	8,667.90	-1,020.50	932.83	34.61	10,867.44	9,502.90	-1,023.46	932.77	36.26	834.70	802.72	180.00	26.096
10,100.00	8,667.55	-1,120.50	933.11	35.53	10,967 <i>.</i> 44	9,502.55	-1,123.46	933.04	37.12	834.70	801.59	180.00	25.210
10,200.00	8,667.20	-1,220.50	933.38	36.52	11,067.44	9,502.19	-1,223.46	933.32	38.05	834.70	800.44	180.00	24.362
10,300.00	8,666.84	-1,320.50	933.66	37.57	11,167.44	9,501.84	-1,323.46	933.60	39.04	834.70	799.26	180.00	23.554
10,400.00	8,666.49	-1,420.50	933.93	38.68	11,267.44	9,501.48	-1,423.46	933.87	40.09	834.70	798.07	180.00	22.785
10,500.00	8,666.13	-1,520.50	934.21	39.84	11,367.44	9,501.13	-1,523.46	934.15	41.20	834.70	796.85	180.00	22.052
10,600.00	8,665.78	-1,620.50	934.48	41.06	11,467.44	9,500.78	-1,623.45	934.43	42.36	834.70	795.62	180.00	21.356
10,700.00	8,665.43	-1,720.50	934.76	42.32	11,567.44	9,500.42	-1,723.45	934.70	43.58	834.70	794.37	180.00	20.694
10,800.00	8,665.07	-1,820.49	935.04	43.63	11,667.44	9,500.07	-1,823.45	934.98	44.83	834.70	793.10	180.00	20.065
10,900.00	8,664.72	-1,920.49	935.31	44.98	11,767.44	9,499.71	-1,923.45	935.25	46.13	834.70	791.82	180.00	19.467
11,000.00	8,664.36	-2,020.49	935.59	46.36	11,867.44	9,499.36	-2,023.45	935.53	47.47	834.70	790.53	180.00	18.898
11,100.00	8,664.01	-2,120.49	935.86	47.78	11,967.44	9,499.00	-2,123.45	935.81	48.85	834.70	789.23	180.00	18.357
11,200.00	8,663.65	-2,220.49	936.14	49.23	12,067.44	9,498.65	-2,223.45	936.08	50.25	834.70	787.92	180.00	17.843
11,300.00	8,663.30	-2,320.49	936.41	50.71	12,167.44	9,498.30	-2,323.45	936.36	51.69	834.70	786.60	180.00	17.353
11,400.00	8,662.95	-2,420.49	936.69	52.21	12,267.44	9,497.94	-2,423.45	936.64	53.15	834.70	785.27	180.00	16.886
11,500.00	8,662.59	-2,520.49	936.96	53.73	12,367.44	9,497.59	-2,523.45	936.91	54.64	834.70	783.93	180.00	16.442
11,600.00	8,662.24	-2,620.49	937.24	55.27	12,467.44	9,497.23	-2,623.44	937.19	56.15	834.70	782.59	180.00	16.018
11,700.00	8,661.88	-2,720.49	937.51	56.83	12,567.44	9,496.88	-2,723.44	937.46	57.68	834.70	781.24	180.00	15.613
11,800.00	8,661.53	-2,820.48	937.79	58.41	12,667.44	9,496.52	-2,823.44	937.74	59.23	834.70	779.88	180.00	15.227
11,900.00	8,661.17	-2,920.48	938.07	60.01	12,767.44	9,496.17	-2,923.44	938.02	60.79	834.70	778.52	180.00	14.858
12,000.00	8,660.82	-3,020.48	938.34	61.62	12,867.44	9,495.82	-3,023.44	938.29	62.38	834.70	777.15	180.00	14.505
12,100.00	8,660.47	-3,120.48	938.62	63.24	12,967.44	9,495.46	-3,123.44	938.57	63.97	834.70	775.78	180.00	14.167
12,200.00	8,660.11	-3,220.48	938.89	64.88	13,067.44	9,495.11	-3,223.44	938.85	65.58	834.70	774.40	180.00	13.843
12,300.00	8,659.76	-3,320.48	939.17	66.52	13,167.44	9,494.75	-3,323.44	939.12	67.20	834.70	773.02	180.00	13.533
12,400.00	8,659.40	-3,420.48	939.44	68.18	13,267.44	9,494.40	-3,423.44	939.40	68.84	834.70	771.64	180.00	13.236
12,500.00	8,659.05	-3,520.48	939.72	69.84	13,367.44	9,494.04	-3,523.44	939.67	70.48	834.70	770.25	180.00	12.951
12,600.00	8,658.70	-3,620.48	939.99	71.52	13,467.44	9,493.69	-3,623.43	939.95	72.14	834.70	768.86	180.00	12.677

Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1 0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

	Uncertaint	y Data for Refe	rence Well			Uncertainty Data for Comparison Well				Separation (Ref. > Comp.)				
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor	
12,700.00	8,658.34	-3,720.48	940.27	73.20	13,567.44	9,493.34	-3,723.43	940.23	73.80	834.70	767.46	180.00	12.414	
12,800.00	8,657.99	-3,820.47	940.54	74.89	13,667.44	9,492.98	-3,823.43	940.50	75.47	834.70	766.06	180.00	12.161	
12,900.00	8,657,63	-3,920.47	940.82	76.59	13,767.44	9,492.63	-3,923.43	940.78	77.15	834.70	764.66	180.00	11.918	
13,000.00	8,657.28	-4,020:47	941.10	78.29	13,867.44	9,492.27	-4,023.43	941.06	78.84	834.70	763.26	180.00	11.684	
13,100.00	8,656.92	-4,120.47	941.37	80.00	13,967.44	9,491.92	-4,123.43	941.33	80.53	834.70	761.85	180.00	11.458	
13,200.00	8,656.57	-4,220.47	941.65	81.71	14,067.44	9,491.56	-4,223.43	941.61	82.23	834.70	760.44	180.00	11.241	
13,300.00	8,656.22	-4,320.47	941.92	83.43	14,167.44	9,491.21	-4,323.43	941.88	83.94	834.70	759.03	180.00	11.031	
13,400.00	8,655.86	-4,420.47	942.20	85.16	14,267.44	9,490.86	-4,423.43	942.16	85.65	834.70	757.62	180.00	10.829	
13,500.00	8,655.51	-4,520.47	942.47	86.89	14,367.44	9,490.50	-4,523.42	· 942.44	87.37	834.70	756.20	180.00	10.634	
13,600.00	8,655.15	-4,620.47	942.75	88.62	14,467.44	9,490.15	-4,623.42	942.71	89.09	834.70	754,79	180.00	10.445	
13,700.00	8,654.80	-4,720.47	943.02	90.36	14,567.44	9,489.79	-4,723.42	942.99	90.81	834.70	753.37	180.00	10.263	
13,800.00	8,654.44	-4,820.46	943.30	92.10	14,667.44	9,489.44	-4,823.42	943.27	92.54	834.70	751.95	180.00	10.087	
13,900.00	8,654.09	-4,920.46	943.57	93.85	14,767.44	9,489.08	-4,923.42	943.54	94.28	834.70	750.52	180.00	9.916	
14,000.00	8,653.74	-5,020.46	943.85	95.60	14,867,44	9,488.73	-5,023.42	943.82	96.02	834.70	749.10	180.00	9.751	
14,100.00	8,653.38	-5,120.46	944.13	97.35	14,967.44	9,488.38	-5,123.42	944.09	97.76	834.70	747.68	180.00	9.592	
14,200.00	8,653.03	-5,220.46	944.40	99.10	15,067.44	9,488.02	-5,223.42	944.37	99.50	834.70	746.25	180.00	9.437	
14,300.00	8,652.67	-5,320.46	944.68	100.86	15,167.44	9,487.67	-5,323.42	944.65	101.25	834.70	744.82	180.00	9.287	
14,400.00	8,652.32	-5,420.46	944.95	102.62	15,267.44	9,487.31	-5,423.42	944.92	103.00	834.70	743.39	180.00	9.142	
14,500.00	8,651.97	-5,520.46	945.23	104.39	15,367.44	9,486.96	-5,523.41	945.20	104.76	834.70	741.96	180.00	9.001	
14,600.00	8,651.61	-5,620.46	945.50	106.15	15,467.44	9,486.60	-5 ,623. 4 1	945.48	106.51	834.70	. 740.53	180.00	8.864	
14,700.00	8,651.26	-5,720.46	945.78	107.92	15,567.44	9,486.25	-5,723.41	945.75	108.27	834.70	739.10	180.00	8.731	
14,800.00	8,650.90	-5,820.45	946.05	109.69	15,667.44	9,485.90	-5,823.41	946.03	110.03	834.70	737.66	180.00	8.602	
14,900.00	8,650.55	-5,920.45	946.33	111.46	15,767.44	9,485.54	-5,923.41	946.30	111.80	834.70	736.23	180.00	8.477	
15,000.00	8,650.19	-6,020.45	946.60	113.24	15,867.44	9,485.19	-6,023.41	946.58	113.56	834.70	734.79	180.00	8.355	
15,100.00	8,649.84	-6,120.45	946.88	115.01	15,967.44	9,484.83	-6,123.41	946.86	115.33	834.70	733.36	180.00	8.237	
15,200.00	8,649.49	-6,220.45	947.16	116.79	16,067.44	9,484.48	-6,223.41	947.13	117.10	834.70	731.92	180.00	8.121	
15,300.00	8,649.13	-6,320.45	947.43	118.57	16,167.44	9,484.12	-6,323.41	947.41	118.88	834.70	730.48	180.00	8.009	
15,400.00	8,648.78	-6,420.45	947.71	120.35	16,267.44	9,483.77	-6,423.41	947.69	120.65	834.70	729.04	180.00	7.900	
15,500.00	8,648.42	-6,520.45	947.98	122.13	16,367.44	9,483.42	-6,523.40	947.96	122.43	834.70	727.60	180.00	7.794	

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Eddy County, NM (NAD 83)

HALLIBURTON

Anticollision Report for WCA 2H - Plan 1

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

	Uncertainty	/ Data for Refer	ence Well			Uncertainty	Data for Compa	arison Well		Sepa	ration (Ref. > 0	Comp.)	•
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
15,600.00	8,648.07	-6,620.45	948.26	123.92	16,467.44	9,483.06	-6,623.40	948.24	124.20	834.70	726.16	180.00	7.691
15,700.00	8,647.71	-6,720.45	948.53	125.70	16,567.44	9,482.71	-6,723.40	948.51	125.98	834.70	724.72	180.00	7.590
15,800.00	8,647.36	-6,820.44	948.81	127.49	16,667.44	9,482.35	-6,823.40	948.79	127.76	834.70	723.28	180.00	7.492
15,900.00	8,647.01	-6,920.44	949.08	129.28	16,767.44	9,482.00	-6,923.40	949.07	129.55	834.70	721.84	180.00	7.396
16,000.00	8,646.65	-7,020.44	949.36	131.07	16,867.44	9,481.64	-7,023.40	949.34	131.33	834.70	720.39	180.00	7.303
16,100.00	8,646.30	-7,120 .44	949.63	132.86	16,967.44	9,481.29	-7,123:40	949.62	133.12	834.70	718.95	180.00	7.211
16,200.00	8,645.94	-7,220.44	949.91	134.65	17,067.44	9,480.94	-7,223.40	949.90	134.90	834.70	717.51	180.00	7.123
16,300.00	8,645.59	-7,320.44	950.19	136.44	17,167.44	9,480.58	-7,323.40	950.17	136.69	834.70	716.06	180.00	7.036
16,400.00	8,645.23	-7,420.44	950.46	138.23	17,267.44	9,480.23	-7,423.40	950.45	138.48	834.70	714.62	180.00	6.951
16,500.00	8,644.88	-7,520.44	. 950.74	140.03	17,367.44	9,479.87	-7,523.39	950.72	140.27	834.70	713.17	180.00	6.868
16,600.00	8,644.53	-7,620.44	951.01	141.82	17,467.44	9,479.52	-7,623.39	951.00	142.06	834.70	711.72	180.00	6.788
16,700.00	8,644.17	-7,720.44	951.29	143.62	17,567.44	9,479.16	-7,723.39	951.28	143.85	834.70	710.28	180.00	6.709
16,800.00	8,643.82	-7,820.43	951.56	145.42	17,667.44	9,478.81	-7,823.39	951.55	145.64	834.70	`708.83	180.00	6.632
16,900.00	8,643.46	-7,920.43	951.84	147.22	17,767.44	9,478.46	-7,923.39	951.83	147.44	834.70	707.38	180.00	6.556
17,000.00	8,643.11	-8,020.43	952.11	149.02	17,867.44	9,478.10	-8,023.39	952.11	149.23	834.70	705.93	180.00	6.482
17,100.00	8,642.76	-8,120.43	952.39	150.82	17,967.44	9,477.75	-8,123.39	952.38	151.03	834.70	704.48	180.00	6.410
17,200.00	8,642.40	-8,220.43	952.66	152.62	18,067.44	9,477.39	-8,223.39	952.66	152.82	834.70	703.04	180.00	6.340
17,300.00	8,642.05	-8,320.43	952.94	154.42	18,167.44	9,477.04	-8,323.39	952.93	154.62	834.70	701.59	180.00	6.271
17,400.00	8,641.69	-8,420.43	953.22	156.22	18,267.44	9,476.68	-8,423.39	953.21	156.42	834.70	700.14	180.00	6.203
17,500.00	8,641.34	-8,520.43	953.49	158.02	18,367.44	9,476.33	-8,523.38	953.49	158.22	834.70	698.69	180.00	6.137
17,600.00	8,640.98	-8,620.43	953.77	159.83	18,467.44	9,475.98	-8,623.38	953.76	160.02	834.70	697.24	180.00	6.072
17,700.00	8,640.63	-8,720.43	954.04	161.63	18,567 .44	9,475.62	-8,723.38	954.04	161.82	834.70	695.78	180.00	6.009
17,800.00	8,640.28	-8,820.42	954.32	163.44	18,667.44	9,475.27	-8,823.38	954.32	163.62	834.70	694.33	180.00	5.947
17,900.00	8,639.92	-8,920.42	954.59	165.24	18,767.44	9,474.91	-8,923.38	954.59	165. 4 2	834.70	692.88	180.00	5.886
18,000.00	8,639.57	-9,020.42	954.87	167.05	18,867.44	9,474.56	-9,023.38	954.87	167.22	834.70	691.43	180.00	5.826
18,100.00	8,639.21	-9,120.42	955.14	168.85	18,967.44	9,474.20	-9,123.38	955.14	169.03	834.70	689.98	180.00	5.768
18,200.00	8,638.86	-9,220.42	955.42	170.66	19,067. 44	9,473.85	-9,223.38	955.42	170.83	834.70	688.53	180.00	5.710
18,300.00	8,638.50	-9,320.42	955.69	172.47	19,167.44	9,473.49	-9,323.38	955.70	172.64	834.70	687.07	180.00	5.654
18,400.00	8,638.15	-9,420.42	955.97	174.28	19,267.44	9,473.14	-9,423.38	955.97	174.44	834.70	685.62	180.00	5.599
18,500.00	8,637.80	-9,520.42	956.25	176.08	19,367.44	9,472.79	-9,523.37	956.25	176.25	834.70	684.17	180.00	5.545

Offset Design: Asteroid 20-29 Fed Com - WCB 1H - Wellbore #1 - Plan 1

0-MWD

Closest Approach 3D Proximity Scan on Current Survey Data (Highside Reference)

Scan Range: 0.00 to 19,086.20 usft. Measured Depth.

Scan Radius is 10,000.00 usft . Clearance Factor cutoff is Unlimited. Max Ellipse Separation is Unlimited

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	Uncertaint	y Data for Refe	rence Well			Uncertainty	Data for Comp	arison Well		Sepa	ration (Ref. >	Comp.)	
Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Measured Depth (usft)	Vertical Depth (usft)	Ellipse C +N/-S (usft)	entre +E/-W (usft)	Ellipse Major Axis/2	Between Centres (usft)	Between Ellipsoids (usft)	Relative Highside Bearing	Clearance Factor
18,600.00	8,637.44	-9,620.42	956.52	177.89	19,467.44	9,472.43	-9,623.37	956.53	178.05	834.70	682.71	180.00	5.492
18,700.00	8,637.09	-9,720.42	956.80	179.70	19,567.44	9,472.08	-9,723.37	956.80	179.86	834.70	681.26	180.00	5.440
18,800.00	8,636.73	-9,820.41	957.07	181.51	19,667.44	9,471.72	-9,823.37	957.08	181.67	834.69	679.80	180.00	5.389
18,900.00	8,636.38	-9,920.41	957.35	183.32	19,767.44	9,471.37	-9,923.37	957.35	183.47	834.69	678.35	180.00	5.339
19,000.00	8,636.03	-10,020.41	957.62	185.13	19,867.44	9,471.01	-10,023.37	957.63	185.28	834.69	676.90	180.00	5.290
19,082.75	8,635.73	-10,103.16	957.85	186.63	19,950.19	9,470.72	-10,106.11	957.86	186.78	834.69	675.69	180.00	5.250
19,086.20	8,635.72	-10,106.61	957.86	186.69	19,950.69	9,470.72	-10,106.61	957.86	186.79	834.70	675.68	180.00	5.249

Eddy County, NM (NAD 83)

HALLIBURTON

Anticollision Report for WCA 2H - Plan 1

	Reference Well Surve	y tool program	• .			
	From (usft) 0.00	To (usft) 19,086.20 Plan 1	Survey/Plan		Survey Tool MWD	
	<u>Anticollision Info</u> Error Model:	ISCWSA		Output errors are at	2.00 sigma	
	Scan Method:	Closest Approach 3D		·	-	
•	ns are correlated across surve	, ,			•	
•	es incorporate surface errors					
Separation is the	e actual distance between elli	psoids.				
Distance Betwee	en centres is the straight line o	distance between wellbore centres.				
Clearance Facto	or = Distance Between Profiles	s / (Distance Between Profiles - Ellips	se Separation).			
All station coord	inates were calculated using t	the Minimum Curvature method.	$(0, 1) \in \mathbb{R}^{n}$	•		

Eddy County, NM (NAD 83)

Anticollision Report for WCA 2H - Plan 1

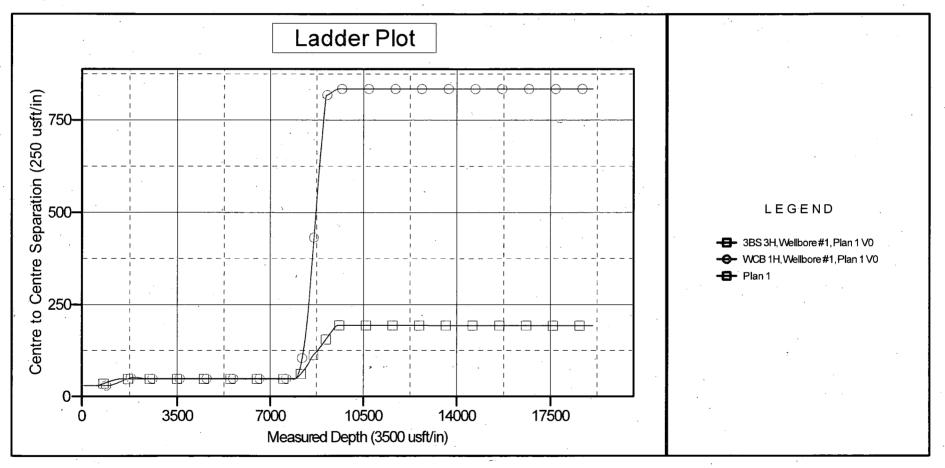
Direction and Coordinates are relative to Grid North Reference.

Vertical Depths are relative to GE 3386.40 + 26 KB @ 3412.40usft (Latshaw 17). Northing and Easting are relative to WCA 2H.

Coordinate System is US State Plane 1983, New Mexico Eastern Zone.

Central Meridian is -104.00°, Grid Convergence at Surface is: 0.01°.

Summary is based on Minimum Centre Distance

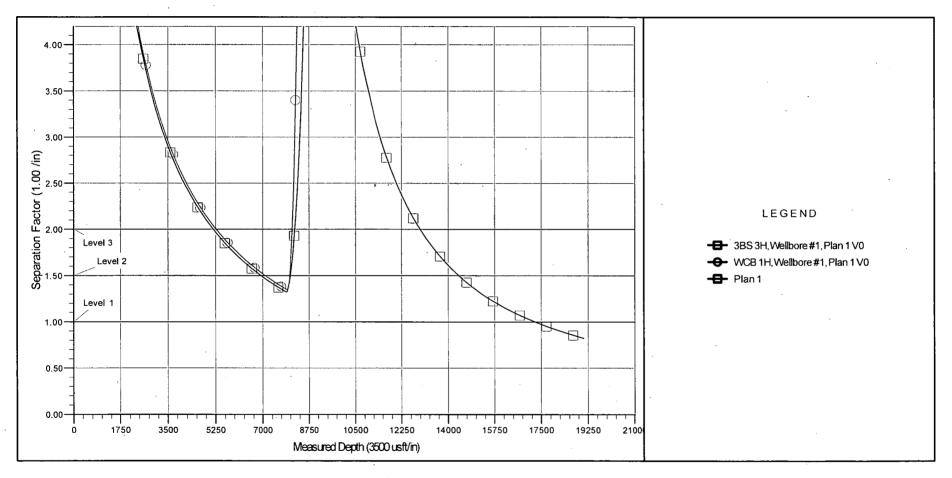


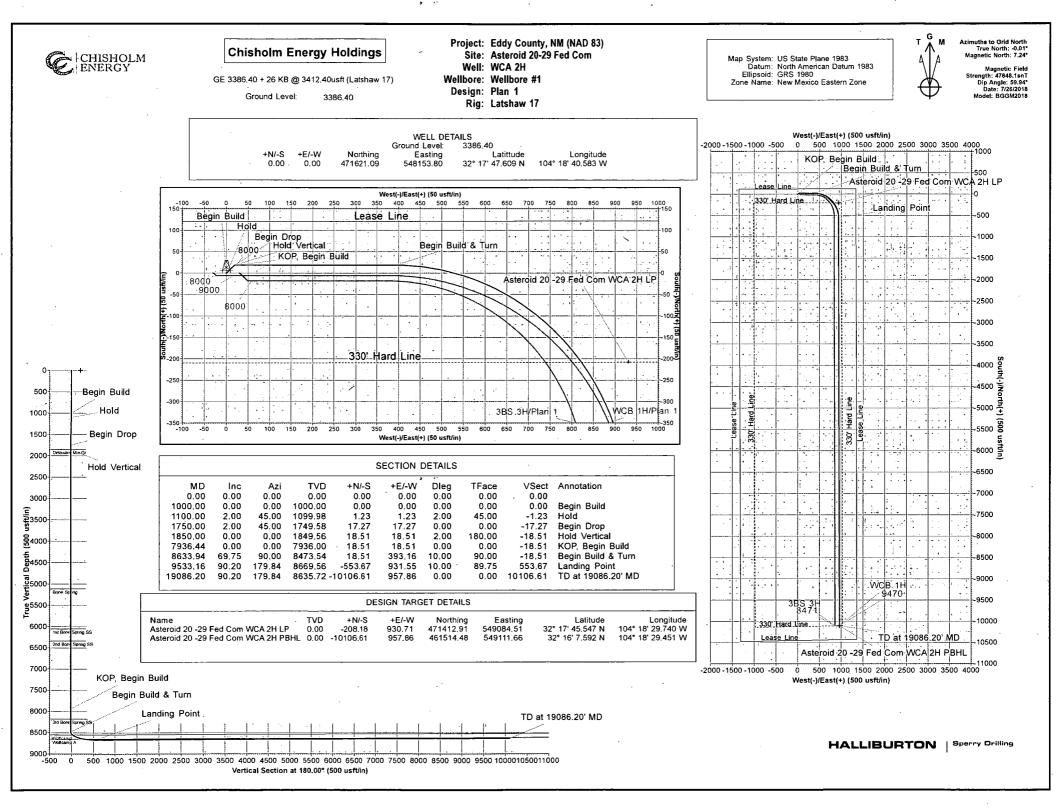
Chisholm Energy Holdings

Eddy County, NM (NAD 83)

Anticollision Report for WCA 2H - Plan 1

Clearance Factor Plot: Measured Depth versus Separation(Clearance) Factor





Latshaw 17

Chisholm Energy Holdings

Eddy County, NM (NAD 83) Asteroid 20-29 Fed Com API# WCA 2H

Wellbore #1 Plan: Plan 1

Sperry Drilling Services Combo Report

25 June, 2018

Well Coordinates:

32° 17' 47.61" N 104° 18' 40.58" W North American Datum 1983 New Mexico Eastern Zone 471,621.09 N 548,153.80 E

Ground Level: 3,386.40 usft

Local Coordinate Origin: Viewing Datum: TVDs to System: **North Reference:** Unit System:

Version: 5000.1 Build: 81E

Report Version: Midcon Combo v1.12

Centered on Well WCA 2H GE 3386.40 + 26 KB @ 3412.40usft (Latshaw 17) N **Grid** API US Survey Feet

HALLIBURTON

Plan Report for WCA 2H - Plan 1

Measured Depth (usft)	Inclination (°)	Grid Azimuth (°)	Vertical Depth (usft)	Local Coo Northing (usft)	rdinates Easting (usft)	Map Coord Northing (usft)	Easting	Dogleg Rate (°/100usft)	Vertical Section (usft)	Toolface Angle (°)	Comments	
0.0			0.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
100.0	0.00	0.00	100.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
200.0	0.00 [°]	0.00	200.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00	•	
300.0	0.00	0.00	300.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
400.0	0.00	0.00	400.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
500.0	0.00 C	0.00	500.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	÷0.00	0.00		
600.0	0.00	0.00	600.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
700.0	0.00	0.00	700.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
800.0	0.00	0.00	800.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00	v	
900.0	0.00 c	0.00	900.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00		
1,000.00	0.00	0.00	1,000.00	0.00 N	0.00 E	471,621.09	548,153.80	0.00	0.00	0.00	Begin Build	·
1,100.00	2.00	45.00	1,099.98	1.23 N	1.23 E	471,622.32	548,155.03	2.00	-1.23	45.00		
1,200.0	0 2.00	45.00	1,199.92	3.70 N	3.70 E	471,624.79	548,157.50	0.00	-3.70	0.00		
1,300.00	2.00	45.00	1,299.86	6.17 N	6.17 É	471,627.26	548,159.97	0.00	-6.17	0.00		
1,400.00	2.00	45.00	1,399.80	8.64 N	8.64 E	471,629.73	548,162.44	0.00	-8.64	0.00		
1,500:00	2.00	45.00	1,499.74	11.11 N	11.11 E	471,632.20	548,164.91	0.00	-11.11	0.00		•
1,600.00	0 2.00	45.00	1,599.68	13.57 N	13.57 E	471,634.66	548,167.37	0.00	-13.57	0.00		
1,700.00	2.00	45.00	1,699.61	16.04 N	16.04 E	471,637.13	548,169.84	0.00	-16.04	0.00		
1,750.00	2.00	45.00	1,749.58	17.27 N	17.27 E	471,638.36	548,171.07	0.00	-17.27	0.00	Begin Drop	
1,800.00	D 1.00	45.00	1,799.57	18.20 N	18.20 E	471,639.29	548,172.00	2.00	-18.20	180.00		
1,850.00	0.00	0.00	1,849.56	18.51 N	18.51 E	471,639.60	548,172.31	2.00	-18.51	-180.00	Hold Vertical	
1,900.00	0.00	0.00	1,899.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	.0.00		
2,000.00	0.00	0.00	1,999.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,100.00	0.00	0.00	2,099.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,200.00	0.00	0.00	2,199.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,300.00	0.00	0.00	2,299.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,400.00	0.00	0.00	2,399.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,500.00	0.00	0.00	2,499.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,600.00	0.00 C	0.00	2,599.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,700.00	0.00	0.00	2,699.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,800.00	0.00	0.00	2,799.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
2,900.00	0.00	0.00	2,899.56	18.51 N	18.51 E	471,639.60	548,172.31	/ 0.00	-18.51	0.00		
3,000.00	0.00 ⁻	0.00	2,999.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
3,100.00	0.00 C	0.00	3,099.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		•
3,200.00	0.00	0.00	3,199.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
3,300.00	0.00	0.00	3,299.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		

Chisholm Energy Holdings

Eddy County, NM (NAD 83)

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Plan Report for WCA 2H - Plan 1

Measured	~	Grid	Vertical	Local Cod	ordinates	Map Coor	dinates	Dogleg	Vertical	Toolface		
	Inclination (°)		Depth (usft)	Northing (usft)	Easting (usft)	Northing (usft)	Easting (usft)	Rate (°/100usft)	Section (usft)	Angle (°)	Comments	
3,400.00		0.00	3,399.56	• •	18.51 E	471,639.60	548,172.31		-18.51	0.00		
3,500.00		0.00	3,499.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
3,600.00		0.00	3,599.56	18.51 N	18.51 E	471,639.60	548,172.31		-18.51	0.00		
3,700.00	0.00	0.00	3,699.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
3,800.00	0.00	0.00	3,799.56	18.51 N	18.51 E	471,639.60	548,172.31	. 0.00	-18.51	0.00		
3,900.00		0.00	3,899.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,000.00	0.00	0.00	3,999.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,100.00	0.00	0.00	4,099.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,200.00	0.00	0.00	4,199.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,300.00	0.00	0.00	4,299.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,400.00	0.00	0.00	4,399.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,500.00	0.00	0.00	4,499.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,600.00	0.00	0.00	4,599.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,700.00	0.00	0.00	4,699.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,800.00	0.00	0.00	4,799.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
4,900.00	0.00	0.00	4,899.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,000.00	0.00	0.00	4,999.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,100.00	0.00	0.00	5,099.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,200.00	0.00	0.00	5,199.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,300.00	0.00	0.00	5,299.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,400.00	0.00	0.00	5,399.56	18.51 N	18.51 E	471,639.60	548,172.31	· 0.00	-18.51	0.00		
5,500.00	0.00	0.00	5,499.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,600.00	0.00	0.00	5,599.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,700.00	0.00	0.00	5,699.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,800.00	0.00	0.00	5,799.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
5,900.00	0.00	0.00	5,899.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,000.00	0.00	0.00	5,999.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,100.00	0.00	0.00	6,099.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,200:00	0.00	0.00	6,199.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,300.00	0.00	0.00	6,299.56	18.51 N	18.51 E	, 471,639.60	548,172.31	0.00	-18.51	0.00		
6,400.00	0.00	0.00	6,399.56	18.51 N	18.51 E	471,639.60	548,172.31	0,00	-18.51	0.00		
6,500.00	0.00	0.00	6,499.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,600.00	0.00	0.00	6,599.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,700.00	0.00	0.00	6,699.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,800.00	0.00	0.00	6,799.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
6,900.00	0.00	0.00	6,899.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00		
7,000.00					18.51 E	471,639.60	548,172.31			0.00		

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COMPASS

Chisholm Energy Holdings

Eddy County, NM (NAD 83)

Plan Report for WCA 2H - Plan 1

Measured		Grid	Vertical	Local Coordinates		Map Coor	dinates	Dogleg	Vertical	Toolface	
Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	Northing (usft)	Easting (usft)	Northing (usft)	Easting (usft)	Rate (°/100usft)	Section (usft)	Angle (°)	Comments
7,100.00	0.00		7,099.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,200.00	0.00	0.00	7 <u>,</u> 199.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,300.00	0.00	0.00	7,299.56	18.51 N	18.51 E	47 1,639.60	548,172.31	0.00	-18.51	0.00	
7,400.00	0.00	0.00	7,399.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,500.00	0.00	0.00	7,499.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	-
7,600.00	0.00	0.00	7,599.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,700.00	0.00	0.00	7,699.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,800.00	0.00	0.00	7,799.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,900.00	0.00	0.00	7,899.56	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	
7,936.44	0.00	0.00	7,936.00	18.51 N	18.51 E	471,639.60	548,172.31	0.00	-18.51	0.00	KOP, Begin Build
7,950.00) 1.36	90.00	7,949.56	18.51 N	18.67 E	471,639.60	548,172.47	10.00	-18.51	90.00	
8,000.00	6.36	90.00	7,999.43	18.51 N	22.03 E	471,639.60	548,175.83	10.00	-18.51	0.00	· · ·
8,050.00) 11.36	90.00	8,048.82	18.51 N	29.73 E	471,639.60	548,183.53	10.00	-18.51	0.00	
8,100.00) 16.36	90.00	8,097.35	18.51 N	41.70 E	471,639.60	548,195.50	10.00	-18.51	0.00	
8,150.00			8,144.65	18.51 N	57.85 E	471,639.60	548,211.65	10.00	-18.51	0.00	
8,200.00	26.36	90.00	8,190.37	18.51 N	78.07 E	471,639.60	548,231.87	10.00	-18.51	0.00	
8,250.00) 31.36	90.00	8,234.14	18.51 N	102.19 E	471,639.60	548,255.99	10.00	-18.51	0.00	
8,300.00	36.36	90.00	8,275.65	18.51 N	130.04 E	471,639.60	548,283.84	10.00	-18.51	0.00	
8,350.00	41.36	90.00	8,314.58	18.51 N	161.40 E	471,639.60	548,315.20	10.00	-18.51	0.00	
8,400.00	46.36	90.00	8,350.62	18.51 N	196.03 E	471,639.60	548,349.83	10.00	-18.51	0.00	
8,450.00			8,383.51	18.51 N	233.67 E	471,639.60	548,387.47	10.00	-18.51	0.00	
8,500.00	56.36	90.00	8,412.99	18.51 N	274.03 E	471,639.60	548,427.83	10.00	-18.51	0.00	
8,550.00	61.36	90.00	8,438.84	18,51 N	316,81 E	471,639.60	548,470.61	10.00	-18.51	0.00	
8,600.00	66.36	90.00	8,460.86	18.51 N	361.68 E	471,639.60	548,515.48	10.00	-18.51	0.00	
8,633.94	69.75	90.00	8,473.54	18.51 N	393.16 E	471,639.60	548,546.96	10.00	-18.51	0.00	Begin Build & Turn
8,650.00			8,479.10	18.28 N	408.22 E	471,639.37	548,562.02	10.00	-18.28	89.75	
8,700.00	69.92	97.04	8,496.34	14.70 N	455.00 E	471,635.79	548,608.80	10.00	-14.70	89.16	
8,750.00	70.23	102.34	8,513.39	6.79 N	501.32 E	471,627.88	548,655.12	10.00	- 6.79	87.33	
8,800.00	70.70	107.63	8,530.12	5.39 S	546.82 E	471,615.70	548,700.62	10.00	5.39	85.52	
8,850.00			8,546.41	21.75 S	591.15 E	471,599.34	548,744.95	10.00	21.75	83.75	
8,900.00		118.08	8,562.12	42.16 S	633.99 E	471,578.93	548,787.79	10.00	42.16	82.04	
8,950.00	72.98	123.24	8,577.13	66.48 S	675.00 E	471,554.61	548,828.80	10.00	66.48	80.40	
9,000.00		128.34	8,591.35	94.51 S	713.87 E	471,526.58	548,867.67	10.00	94.51	78.86	
9,050.00	75.16	133.39	8,604.64	126.03 S	750.30 E	471,495.06	548,904.10	10.00	126.03	77.41	
9,100.00		138.38	8,616.93	160.82 S	784.03 E	471,460.27	548,937.83	10.00	160.82	76.06	
9,150.00		143.32	8,628.10	198.61 S	814.78 E	471,422.48	548,968.58	10.00	198.61	74.84	
9,200.00) 79.21	148.20	8,638.08	239.10 S	842.34 E	471,381.99	548,996.14	10.00	239.10	73.73	

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Chisholm Energy Holdings

Eddy County, NM (NAD 83)

Plan Report for WCA 2H - Plan 1

Measured	· · ·	Grid	Vertical	Local Cod		Map Coord		Dogleg	Vertical	Toolface	· ·		
Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	Northing (usft)	Easting (usft)	Northing (usft)	Easting (usft)	Rate (°/100usft)	Section (usft)	Angle (°)	Comments		
9,250.00		153.04	8,646.79	281.99 S	866.48 E	471,339.10	549,020.28	10.00	281.99	72.76			
9,300.00		157.84	8,654.17	326.96 S	887.02 E	471,294.13	549,040.82	10.00	326.96	71.91			
9,350.00		162.60	8,660.15		903.82 E	471,247.44	549,057.62	10.00	373.65	71.21			
9,400.00		167.33	8,664.69		916.73 E	471,199.36	549,070.53		421.73	70.64			
9,450.00	87.33	172.04	8,667.77	470.81 S	925.67 E	471,150.28	549,079.47	10.00	470.81	70.21			
9,500.00		176.73	8,669.34	520.53 S	930.56 E	471,100.56	549,084.36	· 10.00	520.53	69.92			
9,533.16	90.20	179.84	8,669.56	553.67 S	931.55 E	471,067.42	549,085.35	10.00	553.67	69.77	Landing Point		
9,600.00		179.84	8,669.32		931.73 E	471,000.58	549,085.53	0.00	620.51	0.00	· ·		
9,700.00		179.84	8,668.97		932.01 E	470,900.58	549,085.81	0.00	720.51	0.00			
9,800.00	90.20	179.84	8,668.61	820.50 S	932.28 E	470,800.59	549,086.08	0.00	820.50	0.00			
9,900.00	90.20	179.84	8,668.26	920.50 S	932.56 E	470,700.59	549,086.36	0.00	920.50	0.00			
10,000.00	90.20	179.84	8,667.90	1,020.50 S	932.83 E	470,600.59	549,086.63	0.00	1,020.50	0.00			
10,100.00	90.20	179.84	8,667.55	1,120.50 S	933.11 ⁻ E	470,500.59	549,086.91	0.00	1,120.50	0.00			
10,200.00	90.20	179.84	8,667.20	1,220.50 S	933.38 E	470,400.59	549,087.18	0.00	1,220.50	0.00			
10,300.00	90.20	179.84	8,666.84	1,320.50 S	933.66 E	470,300.59	549,087.46	0.00	1,320.50	0.00			
10,400.00	90.20	179.84	8,666.49	1,420,50 S	933.93 E	470,200.59	549,087.73	0.00	1,420.50	0.00			
10,500.00	90.20	179.84	8,666.13	1,520.50 S	934.21 E	470,100.59	549,088.01	0.00	1,520.50	0.00			
10,600.00	90.20	179.84	8,665.78	1,620.50 S	934.48 E	470,000.59	549,088.28	0.00	1,620.50	0.00			
10,700.00	90.20	179.84	8,665.43	1,720.50 S	934.76 E	469,900.59	549,088.56	0.00	1,720.50	0.00			
10,800.00	90.20	179.84	8,665.07	1,820.49 S	935.04 E	469,800.60	549,088.84	0.00	1,820.49	0.00			
10,900.00	90.20	179.84	8,664.72	1,920.49 S	935.31 E	469,700.60	549,089.11	0.00	1,920.49	0.00			
11,000.00	90.20	179.84	8,664.36	2,020.49 S	935.59 E	469,600.60	549,089.39	0.00	2,020.49	0.00			
11,100.00	90.20	179.84	8,664.01	2,120.49 S	935.86 E	469,500.60	549,089.66	0.00	2,120.49	0.00			
11,200.00	90.20	179.84	8,663.65	2,220.49 S	936.14 E	469,400.60	549,089.94	0.00	2,220.49	0.00			
11,300.00	90.20	179.84	8,663.30	2,320.49 S	936.41 E	469,300.60	549,090.21	0.00	2,320.49	0.00			
11,400.00	90.20	179.84	8,662.95	2,420.49 S	936.69 E	469,200.60	549,090.49	0.00	2,420.49	0.00			
11,500.00	90.20	179.84	8,662.59	2,520.49 S	936.96 E	469,100.60	549,090.76	0.00	2,520.49	0.00			
11,600.00	90.20	179.84	8,662.24	2,620.49 S	937.24 E	469,000.60	549,091.04	0.00	2,620.49	0.00	,		
11,700.00	90.20	179.84	8,661.88	2,720.49 S	937.51 E	468,900.60	549,091.31	0.00	2,720.49	0.00			
11,800.00	90.20	179.84	- 8,661.53	2,820.48 S	937.79 E	468,800.61	549,091.59	0.00	2,820.48	0.00			
11,900.00	90.20	179.84	8,661.17	2,920.48 S	938.07 E	468,700.61	549,091.87	0,00	2,920.48	0.00			
12,000.00	90.20	179.84	8,660.82	3,020.48 S	938.34 E	468,600.61	549,092.14	0.00	3,020.48	0.00			
12,100.00	90.20	179.84		3,120.48 S	938.62 É	468,500.61	549,092.42		3,120.48	0.00			
12,200.00	90.20	179.84	8,660.11	3,220.48 S	938.89 E	468,400.61	549,092.69	0.00	3,220.48	0.00			
12,300.00	90.20	179.84	8,659.76	3,320.48 S	939.17 E	468,300.61	549,092.97	0.00	3,320.48	0.00			
12,400.00	90.20	179.84	8,659.40	3,420.48 S	939.44 E	468,200,61	549,093.24	0.00	3,420,48	0.00	4		
			.,				,	2.20	-,	0.00			

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Chisholm Energy Holdings

Eddy County, NM (NAD 83)

4

Plan Report for WCA 2H - Plan 1

	Measured		Grid	Vertical	Local Coordinates		Map Coord	linates	Dogleg	Vertical	Toolface	
	Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	Northing (usft)	Easting (usft)	Northing (usft)	Easting (usft)	Rate (°/100usft)	Section (usft)	· Angle (°)	Comments
	12,500.00	90.20	179.84	8,659.05	3,520.48 S	939.72 E	468,100.61	549,093.52	0.00	3,520.48	0.00	
	12,600.00		179.84		3,620.48 S	939.99 E	468,000.61	549,093.79	0.00	3,620.48	0.00	
•	12,700.00	90.20	179.84	8,658.34	3,720.48 S	940.27 E	467,900.61	549,094.07	0.00	3,720.48	0.00	
	12,800.00	90.20	179.84	8,657.99	3,820.47 S	940.54 E	467,800.62	549,094.34	0.00	3,820.47	0.00	
	12,900.00	90.20	179.84	8,657.63	3,920.47 S	940.82 E	,467,700.62	549,094.62	0.00	3,920.47	0.00	
	13,000.00	90.20	179.84	8,657.28	4,020.47 S	941.10 E	467,600.62	549,094.90	0.00	4,020.47	0.00	
	13,100.00	90.20	179.84	8,656.92	4,120.47 S	941.37 E	467,500.62	549,095.17	0.00	4,120.47	0.00	
	13,200.00	90.20	179.84	8,656.57	4,220.47 S	941.65 E	467,400.62	549,095.45	0.00	4,220.47	0.00	
	13,300.00	90.20	179.84	8,656.22	4,320.47 S	941.92 E	467,300.62	549,095.72	0.00	4,320.47	0.00	
	13,400.00	90.20	179.84	8,655.86	4,420.47 S	942.20 E	467,200.62	549,096.00	0.00	4,420.47	0.00	
	13,500.00	90.20	179.84	8,655.51	4,520.47 S	942.47 E	467,100.62	549,096.27	0.00	4,520.47	0.00	
	13,600.00	90.20	179.84	8,655.15	4,620.47 S	942.75 E	467,000.62	549,096.55	0.00	4,620.47	0.00	
	13,700.00	90.20	179.84	8,654.80	4,720.47 S	943.02 E	466,900.62	549,096.82	0.00	4,720.47	0.00	
	13,800.00	90.20	179.84	8,654.44	4,820.46 S	943.30 E	466,800.63	549,097.10	0.00	4,820.46	0.00	
	13,900.00	90.20	179.84	8,654.09	4,920.46 S	943.57 E	466,700.63	549,097.37	0.00	4,920.46	0.00	
	14,000.00	90.20	179.84	8,653.74	5,020.46 S	943.85 E	466,600.63	549,097.65	0.00	5,020.46	0.00	
	14,100.00	90.20	179.84	8,653.38	5,120.46 S	944.13 E	466,500.63	549,097.93	0.00	5,120.46	0.00	
	14,200.00	90.20	179.84	8,653.03	5,220.46 S	944.40 E	466,400.63	549,098.20	0.00	5,220.46	0.00	
	14,300.00	90.20	179.84	8,652.67	5,320.46 S	944.68 E	466,300.63	549,098.48	0.00	5,320.46	0.00	
	14,400.00	90.20	179.84	8,652.32	5,420.46 S	944.95 E	466,200.63	549,098.75	0.00	5,420.46	0.00	
	14,500.00	90.20	179.84	8,651.97	5,520.46 S	945.23 E	466,100.63	549,099.03	0.00	5,520.46	0.00	
•	14,600.00	90.20	179.84	8,651.61	5,620.46 S	945.50 E	466,000.63	549,099.30	0.00	5,620.46	0.00	
	14,700.00	90.20	179.84	8,651.26	5,720.46 S	945.78 E	465,900.63	549,099.58	0.00	5,720.46	0.00	
	14,800.00	90.20	179.8 4	8,650.90	5,820.45 S	946.05 E	465,800.64	549,099.85	0.00	5,820.45	0.00	
	14,900.00	90.20	179.84	8,650.55	5,920.45 S	946.33 E	465,700.64	549,100.13	0.00	5,920.45	0.00	
	15,000.00	90.20	179.84	8,650.19	6,020.45 S	946.60 E	465,600.64	549,100.40	0.00	6,020.45	0.00	
	15,100.00	90.20	179.84	8,649.84	6,120.45 S	946.88 E	465,500.64	549,100.68	0.00	6,120.45	0.00	
	15,200.00	90.20	179.84	8,649.49	6,220.45 S	947.16 E	465,400.64	549,100.96	0.00	6,220.45	0.00	
	15,300.00	90.20	179.84	8,649.13	6,320.45 S	947.43 E	465,300.64	549,101.23	0.00	6,320.45	0.00	
	15,400.00	90.20	179.84	8,648.78	6,420.45 S	947.71 E	465,200.64	549,101.51	0.00	6,420.45	0.00	
	15,500.00	90.20	179.84	8,648.42	6,520.45 S	947.98 E	465,100.64	549,101.78	0.00	6,520.45	0.00	
	15,600.00	. 90.20	179.84	8,648.07	6,620.45 S	948.26 E	465,000.64	549,102.06	0.00	6,620.45	0.00	
	15,700.00	90.20	179.84	8,647.71	6,720.45 S	948.53 E	464,900.64	549,102.33	0.00	6,720.45	0.00	
	15,800.00	90.20	179.84	8,647.36	6,820.44 S	948.81 E	464,800.65	549,102.61	0.00	6,820.44	0.00	
ř	15,900.00	90.20	179.84	8,647.01	6,920.44 S	949.08 E	464,700.65	549,102.88	0.00	6,920.44	0.00	
	16,000.00	90.20	179.84	8,646.65	7,020.44 S	949.36 E	464,600.65	549,103.16	0.00	7,020.44	0.00	
_	16,100.00	90.20	179.84	8,646.30	7,120.44 S	949.63 E	,464,500.65	549,103.43	0.00	7,120.44	0.00	

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COMPASS

Chisholm Energy Holdings

Eddy County, NM (NAD 83)

Plan Report for WCA 2H - Plan 1

	Measured		Grid	Vertical	Local Cod	ordinates	Map Coord	dinates	Dogleg	Vertical	Toolface	
	Depth (usft)	Inclination (°)	Azimuth (°)	Depth (usft)	Northing (usft)	Easting (usft)	Northing (usft)	Easting (usft)	Rate (°/100usft)	Section (usft)	Angle (°)	Comments
	16,200.00	90.20	179.84	8,645.94	7,220.44 S	949.91 E	464,400.65	549,103.71	0.00	7,220.44	0.00	
	16,300.00	90.20	179.84	8,645.59	7,320.44 S	950.19 E	464,300.65	549,103.99	0.00	7,320.44	0.00	
	16,400.00	90.20	179.84	8,645.23	7,420.44 S	950.46 E	464,200.65	549,104.26	0.00	7,420.44	0.00	
	16,500.00	90.20	179.84	8,644.88	7,520.44 S	950.74 E	464,100.65	549,104.54	0.00	7,520.44	0.00	
	16,600.00	90.20	179.84	8,644.53	7,620.44 S	951.01 E	464,000.65	549,104.81	0.00	7,620.44	0.00	
•	16,700.00	90.20	179.84	8,644.17	7,720.44 S	951.29 E	463,900.65	549,105.09	0.00	7,720.44	0.00	
	16,800.00	90.20	179.84	8,643.82	7,820.43 S	951.56 E	463,800.66	549,105.36	0.00	7,820.43	0.00	
•	16,900.00	90.20	179.84	8,643.46	7,920.43 S	951.84 E	463,700.66	549,105.64	0.00	7,920.43	0.00	
	17,000.00	90.20	179.84	8,643.11	8,020.43 S	952.11 E	463,600.66	549,105.91	0.00	8,020.43	0.00	
	17,100.00	90.20	179.84	8,642.76	8,120.43 S	952.39 E	463,500.66	549,106.19	0.00	8,120.43	0.00	
	17,200.00	90.20	179.84	8,642.40	8,220.43 S	952.66 E	463,400.66	549,106.46	0.00	8,220.43	0.00	•
	17,300.00	90.20	179.84	8,642.05	8,320.43 S	952.94 E	463,300.66	549,106.74	0.00	8,320.43	0.00	
	17,400.00	90.20	179.84	8,641.69	8,420.43 S	953.22 E	463,200.66	549,107.02	0.00	8,420.43	0.00	
	17,500.00	90.20	179.84	8,641.34	8,520.43 S	953.49 E	463,100.66	549,107.29	0.00	8,520.43	0.00	
	17,600.00	90.20	179.84	8,640.98	8,620.43 S	953.77 E	463,000.66	549,107.57	0.00	8,620.43	0.00	
	17,700.00	90.20	179.84	8,640.63	8,720.43 S	954.04 E	462,900.66	549,107.84	0.00	8,720.43	0.00	
	17,800.00	90.20	179.84	8,640.28	8,820.42 S	954.32 E	462,800.67	549,108.12	. 0.00	8,820.42	0.00	
	17,900.00	90.20	179.84	8,639.92	8,920.42 S	954.59 E	462,700.67	549,108.39	0.00	8,920.42	0.00	
	18,000.00	90.20	179.84	8,639.57	9,020.42 S	954.87 E	462,600.67	549,108.67	0.00	9,020.42	0.00	
	18,100.00	90.20	179.84	8,639.21	9,120.42 S	955.14 E	462,500.67	549,108.94	0.00	9,120.42	0.00	
	18,200.00	90.20	179.84	8,638.86	9,220.42 S	955,42 E	462,400.67	549,109.22	0.00	9,220.42	0.00	
	18,300.00	90.20	179.84	8,638.50	9,320.42 S	955.69 E	462,300.67	549,109.49	0.00	9,320.42	0.00	
	18,400.00	90.20	179.84	8,638.15	9,420.42 S	955.97 E	462,200.67	549,109.77	0.00	9,420.42	0.00	
	18,500.00	90.20	179.84	8,637.80	9,520.42 S	956.25 E	462,100.67	549,110.05	0.00	9,520.42	0.00	
	18,600.00	90.20	179.84	8,637.44	9,620.42 S	956.52 E	462,000.67	549,110.32	0.00	9,620.42	0.00	
	18,700.00	90.20	179.84	8,637.09	9,720.42 S	956.80 E	461,900.67	549,110.60	0.00	9,720.42	0.00	
	18,800.00	90.20	179.84	8,636.73	9,820.41 S	957.07 E	461,800.68	549,110.87	0.00	9,820.41	0.00	•
	18,900.00	90.20	179.84	8,636.38	9,920.41 S	957.35 E	461,700.68	549,111.15	0.00	9,920.41	0.00	
	19,000.00	90.20	179.84		10,020.41 S	957.62 E	461,600.68	549,111.42		-	0.00	
	19,086.20		179.84		10,106.61 S	957.86 E	461,514.48	549,111.66		10,106.61		TD at 19086.20
					•							

Chisholm Energy Holdings

Eddy County, NM (NAD 83)

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Plan Report for WCA 2H - Plan 1

Plan Annotations

Measured	Vertical	Local Coor	dinates	
Depth (usft)	Depth (usft)	+N/-S (usft)	+E/-W (usft)	Comment
1,000.00	1,000.00	0.00	0.00	Begin Build
1,100.00	1,099.98	1.23	1.23	Hold
1,750.00	1,749.58	17.27	17.27	Begin Drop
1,850.00	1,849.56	18.51	18.51	Hold Vertical
7,936.44	7,936.00	18.51	18.51	KOP, Begin Build
8,633.94	8,473.54	18.51	393.16	Begin Build & Turn
9,533.16	8,669.56	-553.67	931.55	Landing Point
19,086.20	8,635.72	-10,106.61	957.86	TD at 19086.20' MD

Vertical Section Information

		Ångle			Origin	Orig	jin	Start
		Туре	Target	Azimuth (°)	Туре	+N/_S (usft)	+E/-W (usft)	TVD (usft)
	User		No Target (Freehand)	180.00	Slot	0.00	0.00	0.00
<u>Surv</u>	<u>ey tool pro</u>	<u>gram</u>					•	
	From (usft)	To (usft)		Survey/Plan			Surve	ey Tool
	Ó.00	19,086.20	Plan 1			. · · · ·	MWD	

Casing Details

Measured Depth (usft)	Vertical Depth (usft)		Name	Casing Diameter ('')	Hole Diameter ('')	
2,500.00	2,499.56	13 3/8"		13-3/8	17-1/2	

Chisholm Energy Holdings

Eddy County, NM (NAD 83)

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Plan Report for WCA 2H - Plan 1

Measured Depth (usft)	Vertical Depth (usft)		TVDSS (usft)	Name		Lithology	Dip (°)	Dip Direction (°)	
1,849.90	1,849.	40	-1,563.00	Delaware Mtn Gr	•		-0.20	179.84	
5,114.90	5,114.	40	1,702.00	Bone Spring			-0.20	179.84	
6,055.90	6,055.	40	2,643.00	1st Bone Spring	SŚ		-0.20	179.84	
6,339.90	6,339.	40	2,927.00	2nd Bone Spring	SS		-0.20	179.84	
8,186.79	8,178.	40	4,766.00	3rd Bone Spring	SS		-0.20	179.84	
8,868.51	8,552.	40	5,140.00	Wolfcamp			-0.20	179.84	
9,266.37	8,650.	40	5,238.00	Wolfcamp A			-0.20	179.84	
sign Targets jet Name	Dip	Dip							
hit/miss target Shape		Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
teroid 20 -29 Fe	d Com WC	A 2H F	PBHL ()						
Daint			5.72usft at	00 -10,106.61 19086.20usft MD(461,514.48 , -10106.61 N, 957.86 E	549,111.6 E)	6 32° 16' 7.592	N 104° 18' 29.451 W
teroid 20 -29 Fe	d Com WC	A 2H L	-P ()						
- plan misses tai - Point	0.00 rget center	0.00 by 953		00 -208.18 .00usft MD (0.00 T	930.71 VD, 0.00 N, 0	471,412.91 .00 E)	549,084.5	32° 17' 45.547	N 104° 18' 29.740 W

Directional Difficulty Index

Average Dogleg over Survey:	0.86 °/100usft	Maximum Dogleg over Survey:	10.00 °/100usft at 9,533.16 usft
Net Tortousity applicable to Plans:	0.86 °/100usft	Directional Difficulty Index:	6.683

<u>Audit Info</u>

Eddy County, NM (NAD 83)

North Reference Sheet for Asteroid 20-29 Fed Com - WCA 2H - Wellbore #1

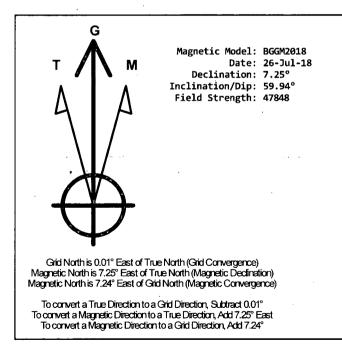
All data is in US Feet unless otherwise stated. Directions and Coordinates are relative to Grid North Reference. Vertical Depths are relative to GE 3386.40 + 26 KB @ 3412.40usft (Latshaw 17). Northing and Easting are relative to WCA 2H

Coordinate System is US State Plane 1983, New Mexico Eastern Zone using datum North American Datum 1983, ellipsoid GRS 1980 Projection method is Transverse Mercator (Gauss-Kruger) Central Meridian is 104° 20' 0.000 W°, Longitude Origin:0° 0' 0.000 E°, Latitude Origin:0° 0' 0.000 N°

False Easting: 541,337.50usft, False Northing: 0.00usft, Scale Reduction: 0.99990914

Grid Coordinates of Well: 471,621.09 usft N, 548,153.80 usft E Geographical Coordinates of Well: 32° 17' 47.61" N, 104° 18' 40.58" W Grid Convergence at Surface is: 0.01°

Based upon Minimum Curvature type calculations, at a Measured Depth of 19,086.20usft the Bottom Hole Displacement is 10,151.90usft in the Direction of 174.59° (Grid). Magnetic Convergence at surface is: -7.24° (26 July 2018, BGGM2018)





Installation Procedure Prepared For:

Chisholm Energy

13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead System With CTH-HPS-F MOD Tubing Head

Publication # IP0571

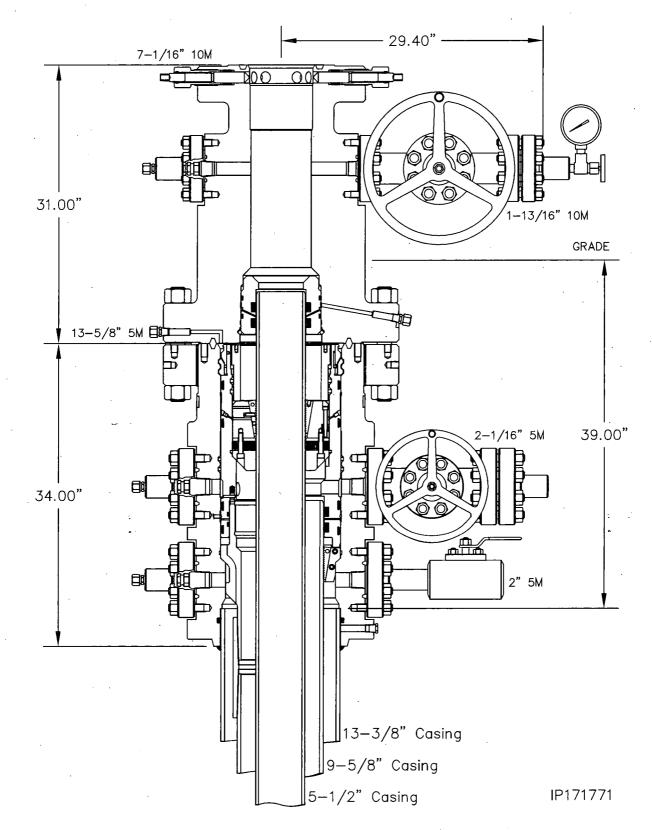
May, 2017

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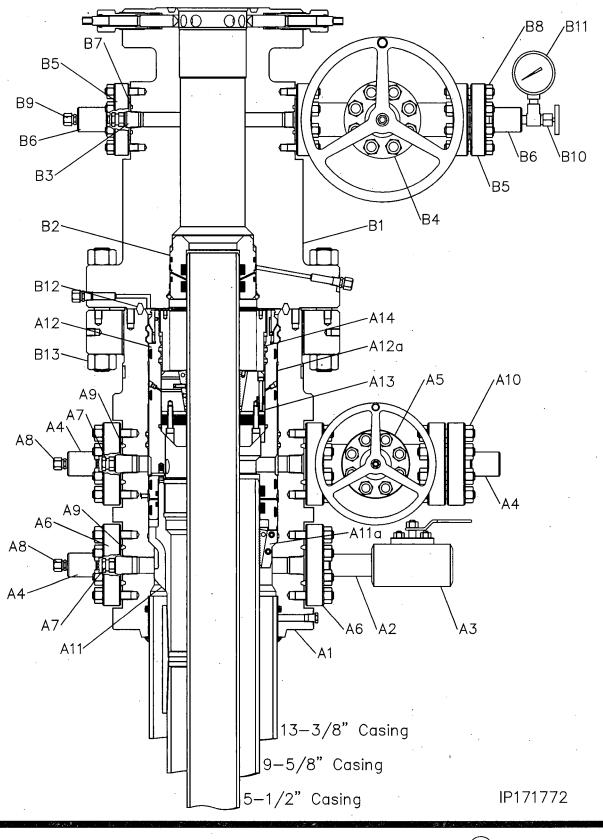
System Drawing





Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Bill of Materials



IP 0571 Page 2



MBU-	3T HOUSING ASSEMBLY	MBU	-3T HOUSING ASSEMBLY		TUBING HEAD ASSEMBLY				
Item Qty	Description	Item Qty	Description	Item	Qty	Description			
A1 1	Housing, CW, MBU-3T, 13.5/8" 5M x 13-3/8" SOW, with two 2-1/16" 5M studded upper and lower outlets with o-ring, 6A-PU-AA-1-2 Part # 117620	A11 1	Casing Hanger, CW, MBU3T-LWR-TP, fluted, 13-5/8" x 9-5/8" (40#) LC bottom x 10.250" 4 Stub Acme 2G RH box top, with 11-1/2" OD neck, 6A-U-AA-1-2 Part # 120251	B1	1	Tubing Head, CW, CTH-HPS-F, 9" (MOD), 13-5/8" 5M x 7-1/16" 10M, with two 1-13/16" 10M studded outlets, round bar, 17-4PH lockscrews, 6A-PU-EE- 0,5-2-1 Part #			
A2 1 A3 1	Nipple, 2" line pipe x 6" long Part # NP6A Ball Valve, TV, 2" RP, 5M x 2" LP, WCB body SS trim, Delrin	A12 1	Packoff, CW, MBU-3T, Mandrel, 13-5/8" nested x 11" with 11.250" 4 Stub Acme 2G LH box top, 1/8" NPT test ports,	B2	1	Secondary Seal, CW, HPS-F, 9 MOD x 5-1/2", 6A-PU-DD- NL-1-2 Part # 110503			
	seats, HNBR seats, nace with locking handle Part # 115184	A13 1	6A-U-AA-1-1 Part # 117152 Casing Hanger, C2, 11" x	В3	1	VR Plug, 1-1/4" Sharp Vee x 1-1/4" hex Part # VR1			
A4 3	Bull Plug, 2" line pipe x 1/2" line pipe, 4130 60K Part # BP2T		5-1/2" Part # 108067	B4	1	Gate valve, AOZE, 1-13/16" 10M, flanged end, handwheel			
A5 1	Gate valve, CW1, 2-1/16" 3/5M, flanged end, handwheel operated, AA/DD-NL trim,	A14 1	Hold Down Ring, for C2 hanger, 11" x 7 through 4-1/2", arranged for packoff MBU-3T, 13-5/8" with 11.250" 4 Stub Acme 2G			operated, EE-0,5 trim, (6A-LU-EE-0,5-3-1) Part # 103188			
A6 4	(6A-LU-AA/DD-NL-1-2) Part # 610003 Companion Flange, 2-1/16″ 5M		LH pin x 9.06" ID x 6.25" long, with 2.12" thread length, 4140 110K Part # 117418	B5	2	Companion Flange, 1-13/16" 10M x 2" LP, 5000 psi max WP, 6A-KU-EE-NL-1 Part # 200010			
	x 2" line pipe, 4130 CMS-102, CMS-002 Part # 200002		· ·	B6	2	Bull Plug, 2" line pipe x 1/2" line pipe, 4130 60K Part # BP2T			
A7 2	VR Plug, 1-1/2" Sharp Vee x 1-1/4" hex Part # VR2			B7	3	Ring Gasket, BX151, 1-13/16" 10M Part # BX-151			
A8 2	Fitting, grease, vented cap, 1/2" NPT alloy non-nace Part # FTG1			B8	8	Studs, all thread with two nuts, black, 3/4" x 5-1/2" long, B7/2H Part # 780080			
A9 ⁵ 5	Ring Gasket, R-24, 2-1/16" 3/5M Part # R24			B9	1	Fitting, grease, vented cap, 1/2" NPT alloy non-nace Part # FTG1			
A10 8	Studs, all thread with two nuts, black, 7/8" x 6-1/2" long, B7/2H Part # 780067			B10	1	Needle Valve, MFA, 1/2" NPT 10M service Part # NVA			
				B11	1	Pressure Gauge, 5M, 4-1/2" face, liquid filled, 1/2" NPT PG5M			
				B12	1	Ring Gasket, BX-160, 13-5/8" 15M Part # BX-160			
				B13	16	Studs, all thread with two nuts, black, 1-5/8" x 12-3/4" long, B7/2H Part # 780087			
		L	·						



RECON	IMENDED SERVICE TOOLS	F	ENTAL EQUIPMENT	EMERGENCY EQUIPMENT			
tem Qty	Description	ltem Qty	Description	Item Qty	Description		
ST1 1	Test Plug/Retrieving Tool, CW, 13-5/8" x 4-1/2" IF (NC-50), 1-1/4" LP bypass and spring loaded lift dogs Part # 104467	R1 1	Threaded Hub, CW, MBU-3T, 13-5/8" 5M With 19.000" 2 Stub Acme-2G Left Hand Box Thread Part # 117268	A11a 1 A12a 1	Casing Hanger, CW, MBU-3T, 13-5/8" x 9-5/8" 6A-PU-DD-3-1 Part # 116998 Packoff, CW, MBU-3T,		
ST2 1	Wear Bushing, CW, MBU-3T-LWR, 13-5/8" x 12.31" ID x 27.0" long with 3/8" o-ring Part # 116974	R2 1	Drilling Adapter, CW, MBU-3T, 13-5/8" 5M Quick Connect Bottom x 13-5/8" 5M Studded Top, Temp Rating PU Part # 117278		Emergency, 13-5/8" nested x 11" with 11.250" 4 Stub Acme 2G LH box top, 1/8" NPT test ports, 6A-U-AA-1-1 Part # 117184		
ST3 1	Casing Hanger Running Tool, CW, MBU-3T-LR-TP, 13-5/8" x 9-5/8" LC box top x 10.250" 4 Stub Acme 2G RH pin bottom, max load capacity 1000K, max torque 18000 ft-lbs. spec for rotating casing Part # 105845	R3 1	TA Cap, CW, MBU-3T-HPS, 13-5/8" 5M quick connect, with one 2" LPO & 1/2" NPT port, with 1/2" NPT needle valve and 2" LP nipple and valve, 6A-U-AA-1-1 Part # 117317				
ST4 1	Torque Collar, CW, for use with running tool, TP, 10.250 4 stub Acme 2G RH pin bottom and arranged for 11.50" OD x	1	Secondary Seal Bushing, CW, HPS, 9" x 5-1/2 Part # 109026				
	5.00" long box hanger neck, maximum torque 18,000 ft-lbs Part # 118906	R4 4	Lift Eyes, 3/4", side pull hoist ring Part # 115542				
ST5 1	Wash Tool, CW, Casing Hanger, MBU-LR/MBS2, fluted, 13-5/8" x 4-1/2" IF (NC-50) box top threads, with brushes Part # 106277			!	· .		
ST6 1	Packoff Running Tool, CW, MBU-3T UPR, 13-5/8" nested, with 11.250" 4 Stub Acme 2G LH pin bottom x 4-1/2" IF (NC-50) box top with seal sleeve Part # 117310						
ST7 1	^ Test Plug, CW, MBU-2LR Inner, 11" x 4-1/2" IF, 1-1/4" LP bypass Part # 108848		•	· .			
ST8 1	Wear Bushing, MBU-3T-UPR, nested, 13-5/8" x 11" x 9.00" I.D. x 20.0" long, arranged for 13-5/8" tool Part # 117158				· ·		
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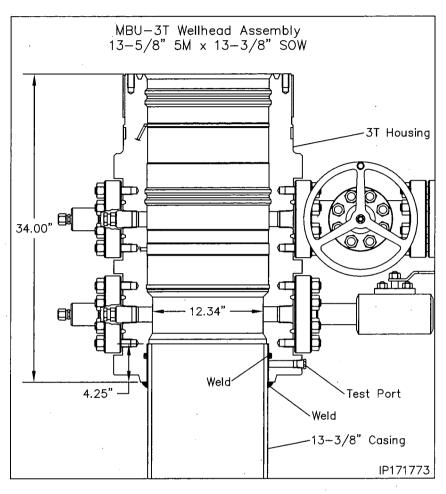


Stage 1 — Install the MBU-3T Housing

- 1. Run the conductor and 13-3/8" surface casing to the required depth and cement as required.
- 2. Cut the conductor pipe off level with the cellar floor.
- 3. Final cut the 13-3/8" surface casing at 39.00" below ground level (grade). Ensure the cut is level and square with the horizon.
- 4. Place an 3/16" x 3/8" bevel on the OD of the stub.

Note: The slip on and weld preparation is 4.25" in depth.

- 5. Examine the 13-5/8" 5M x 13-3/8" SOW x 19.00" 2 Stub Acme LH (Left Hand Thread) MBU-3T Wellhead Housing (Item A1). Verify the following:
 - internal bore is clean and in good condition
 - external Acme thread is clean and in good condition
 - thread flange is in place and rotates freely
 - valves are intact and in good condition
 - weld socket is clean and free of grease and debris and o-ring is in place and in good condition
- Align and level the Wellhead Assembly over the casing stub, orienting the outlets so they will be compatible with the drilling equipment.
- 7. Remove the pipe plug from the port on the bottom of the Head.
- 8. Slowly and carefully lower the assembly over the casing stub, weld and test the MBU-3T wellhead to the surface casing.
- 9. Replace the pipe plug in the port on the bottom of the wellhead.



Note: The weld should be a fillet-type weld with legs no less than the wall thickness of the casing. Legs of 1/2" to 5/8" are adequate for most jobs.

Refer to the back of this publication for the **Recommended Procedure for Field Welding Pipe to Wellhead Parts for Pressure Seal** and for field testing of the weld connection.



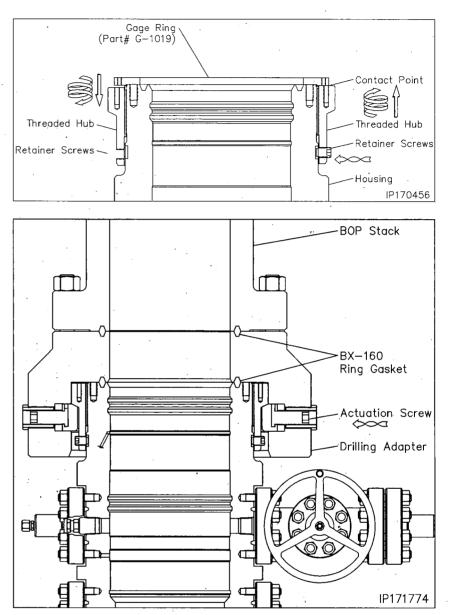
Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 2 — Nipple Up The BOP Stack

- Examine the 13-5/8" 5M x 19.00"
 4 Stub Acme Threaded Hub (Item R1). Verify the following:
 - Acme thread are clean and in good condition
 - remove the (4) retainer set screws an place them in a safe place
- Thoroughly clean and lightly lubricate the mating threads of the housing and the Thread Hub with Copper Coat or Never Seize.
- Pick up the Hub and carefully thread it onto the top of the housing with counter clockwise rotation until the top of the ring is approximately a 1/4" below the top of the housing.
- Position the hub gage ring on top of the housing with the counter bore down as indicated. Ensure the gage ring is level and straight.
- 5. Rotate the Hub clockwise (UP) until it contacts the gage ring.

WARNING: Do not off seat the gage ring.

- 6. Locate the retainer screw holes in the threaded hub.
- 7. Rotate the Hub up or down to align the holes in the hub with the notches in the housing.
- 8. Install the set screws and tighten securely. Remove gage ring.
- Make up the 13-5/8" 5M Quick Connect x 13-5/8" 5M Studded Adapter (Item R2) to the bottom of the BOP stack using a new BX-160 Ring Gasket.
- Thoroughly clean the MBU-3T hub, ring groove and the mating clamp segments and ring groove of the Adapter attached to the BOP stack.
- 11. Install a new **BX-160 Ring Gasket** into the ring groove of the housing.
- 12. Pick up the BOP stack and carefully lower it over the top of the housing and land it on the ring gasket.



- 13. Ensure the BOP is level and then carefully run in all of the drive screws of the upper adapter to contact point.
- 14. Ensure the assembly remains level, run in one actuation and torque to 100 ft lbs.
- 15. Locate the screw 180° from the first and torque it to 100 ft lbs.
- Locate the screws 90° to the right and left and torque them to 100 ft lbs.

- 17. Position the second 4 point sequence 90° from the first and torque each screw to 200 ft lbs.
- Run in all remaining screws to contact and then torque each screw to 400 ft lbs.
- 19. Make one additional round until a stable torque of 400 ft lbs on all (16) screws is achieved.

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Stage 3 — Test the BOP Stack

Immediately after making up the BOP stack and periodically during the drilling of the well for the next casing string the BOP stack (connections and rams) must be tested.

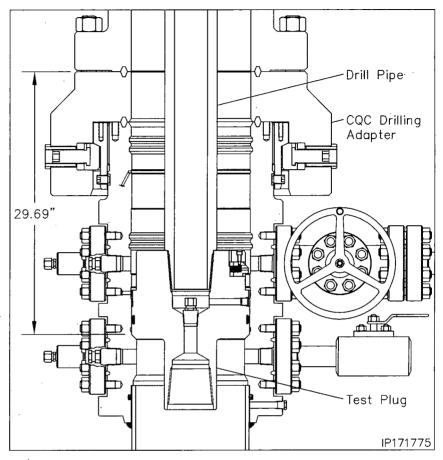
- Examine the 13-5/8" Nominal x 4-1/2" IF (NC-50) CW Test Plug/ Retrieving Tool (Item ST1). Verify the following:
 - 1-1/4" VR plug and weep hole plug are in place and tightened securely
 - elastomer seal is in place and in good condition
 - retractable lift lugs are in place, clean, and free to move
 - drill pipe threads are clean and in good condition
- Position the test plug with the elastomer seal down and the lift lugs up and make up the tool to a joint of drill pipe.

WARNING: Ensure that the lift lugs are up and the elastomer seal is down

- Remove the 1/2" NPT pipe plug from the weep hole if pressure is to be supplied through the drill pipe.
- 4. Open the housing lower side outlet valve.
- 5. Lightly lubricate the test plug seal with oil or light grease.
- Carefully lower the test plug through the BOP and land it on the load shoulder in the housing, 29.69" below the top of the drilling adapter.
- 7. Close the BOP rams on the pipe and test the BOP to 5000 psi or as required by site supervisor.

Note: Any leakage past the test plug will be clearly visible at the open side outlet valve.

 After a satisfactory test is achieved, release the pressure and open the rams.



 Remove as much fluid as possible from the BOP stack and the retrieve the test plug with a straight vertical lift.

Note: When performing the BOP blind ram test it is highly recommended to suspend a stand of drill pipe below the test plug to ensure the plug stays in place while disconnecting it from the drill pipe.

10. Repeat this procedure as required during the drilling of the hole section.



Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 4 — Run the Lower Wear Bushing

Note: Always use a Wear Bushing while drilling to protect the load shoulders from damage by the drill bit or rotating drill pipe. The Wear Bushing **must be retrieved** prior to running the casing.

- 1. Examine the 13-5/8" Nominal MBU-3T-LWR Wear Bushing (Item ST2). Verify the following
 - internal bore is clean and in good condition
 - upper trash o-ring is in place and in good condition
 - shear o-ring cord is in place and in good condition
 - paint anti-rotation lugs white and allow paint to dry

Run the Wear Bushing Before Drilling

- Orient the 13-5/8" Nominal x 4-1/2" IF (NC-50) CW Test Plug/Retrieving Tool (Item ST1) with drill pipe connection up.
- 3. Attach the Retrieving Tool to a joint of drill pipe.

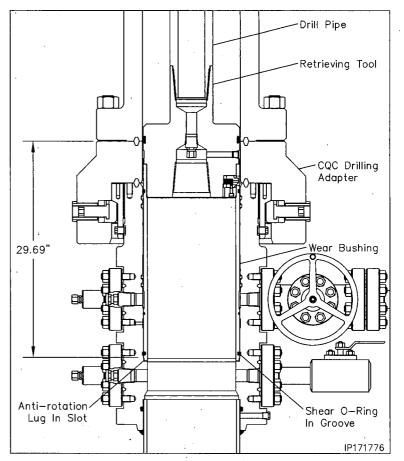
WARNING: Ensure that the lift lugs are down and the elastomer seal is up

4. Align the retractable lift lugs of the tool with the retrieval holes of the bushing and carefully lower the tool into the Wear Bushing until the lugs snap into place.

Note: If the lugs did not align with the holes, rotate the tool in either direction until they snap into place.

- 5. Apply a heavy coat of grease, not dope, to the OD of the bushing.
- 6. Ensure the BOP stack is drained and free of any debris from previous test.
- 7. Slowly lower the Tool/Bushing Assembly through the BOP stack and land it on the load shoulder in the housing, 29.69" below the top of the drilling adapter.
- 8. Rotate the drill pipe clockwise (right) to locate the stop lugs in their mating notches in the head. When properly aligned the bushing will drop an additional 1/2".

Note: The Shear O-Ring on bottom of the bushing will locate in a groove above the load shoulder in the head to act as a retaining device for the bushing.



- 9. Remove the tool from the Wear Bushing by rotating the drill pipe counter clockwise (left) 1/4 turn and lifting straight up.
- 10. Drill as required.

Note: It is highly recommended to retrieve, clean, inspect, grease, and reset the wear bushing each time the hole is tripped during the drilling of the hole section.

Retrieve the Wear Bushing After Drilling

- 11. Make up the Retrieving Tool to the drill pipe.
- 12. Drain BOP stack and wash out if necessary.
- 13. Slowly lower the tool into the Wear Bushing.
- 14. Rotate the Retrieving Tool clockwise until a positive stop is felt. This indicates the lugs have snapped into the holes in the bushing.
- 15. Using the top drive, slowly pick up on the landing joint in 1000 lbs increments until the busing starts to rise. This action should take a minimum of 3000 lbs pull. Do Not Exceed 60,000 lbs.
- 16. Retrieve the Wear Bushing, and remove it and the Retrieving Tool from the drill string.

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Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head



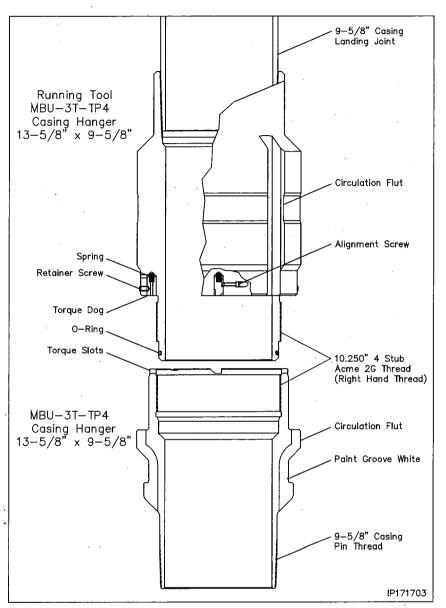
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Stage 5 — Hang Off the 9-5/8" Casing

- Examine the 13-5/8" x 9-5/8" CW-MBU-3T-TP4 Casing Hanger Running Tool (Item ST3). Verify the following:
 - internal bore and threads are clean and in good condition
 - o-ring seal is clean and in good condition
 - torque dogs are in place, in upper most position and retainer set screws are tightened securely
- 2. Make up a landing joint to the top of the Running Tool and torque connection to thread manufacturer's maximum make up torque.
- 3. Lay down the landing joint on the pipe rack.
- On the pipe rack, examine the 13-5/8" x 9-5/8" CW-MBU-3T-TP4 Mandrel Casing Hanger (Item A11). Verify the following:
 - internal bore and threads are clean and in good condition
 - neck seal area is clean and undamaged
 - torque slots are clean and in good condition
 - pin threads are clean and in good condition. Install thread protector
 - paint indicator groove white as indicated and allow paint to dry
- Liberally lubricate the mating threads, seal areas and o-ring of the hanger and running tool with a oil or light grease.
- 6. <u>Using chain tongs only</u>, thread the Running Tool into the hanger, with right hand rotation, until it shoulders out on the Hanger body.

WARNING: Do Not apply torque to the Hanger/Tool connection.

Note: If steps 1 through 6 were done prior to being shipped to location, the running tool should be backed off 1 turn and made back up to ensure it will back off freely.

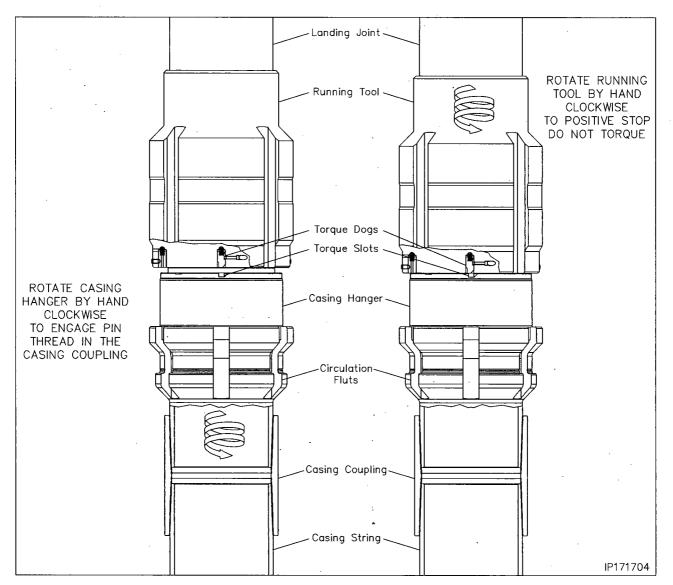


- 7. Calculate the total landing dimension by adding the previously determined RKB dimension and 29.69", the depth of the wellhead.
- 8. Starting at the top of the 45° angle load shoulder of the casing hanger measure up the landing joint and place a paint mark on the joint. Mark **HANGER LANDED**.
- 9. Place a second mark 30" below the first and mark STOP ROTATING.
- 10. Run the 9-5/8" casing as required and space out appropriately for the mandrel casing hanger.



Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 5 — Hang Off the 9-5/8" Casing



Note: If the 9-5/8" casing becomes stuck and the mandrel casing hanger cannot be landed, Refer to **Stage 5A** for the emergency slip casing hanger procedure.

- 11. Pick up the casing hanger/running tool joint assembly.
- 12. Remove the casing hanger thread protector and carefully thread the hanger into the last joint of casing ran. Rotate the hanger clockwise, by hand, to a positive stop.
- 13. Rotate the running tool clockwise by hand to a positive stop.

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Stage 5 — Hang Off the 9-5/8" Casing

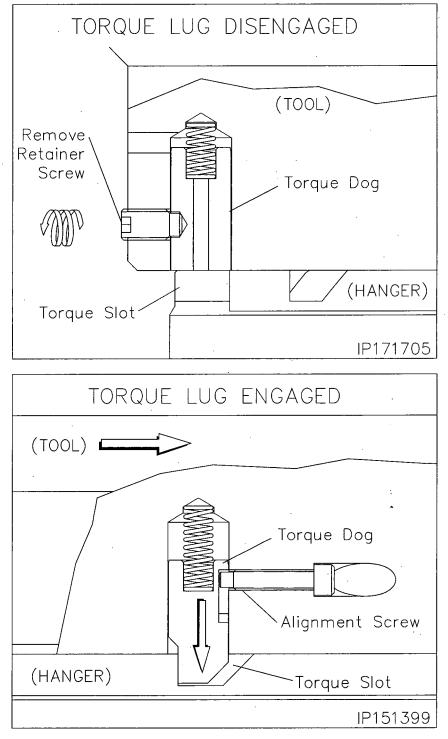
14. Locate the (4) 3/8" socket head set screws in the side of the hanger running tool and remove the screws.

WARNING: Place the screws in a safe place to reinstall in the tool when the job is completed.

Note: This will release the running tool torque dogs allowing them to move downward.

15. Using only chain tongs, rotate the running tool to the left to allow the torque dogs to engage the torque slots in the top of the hanger.

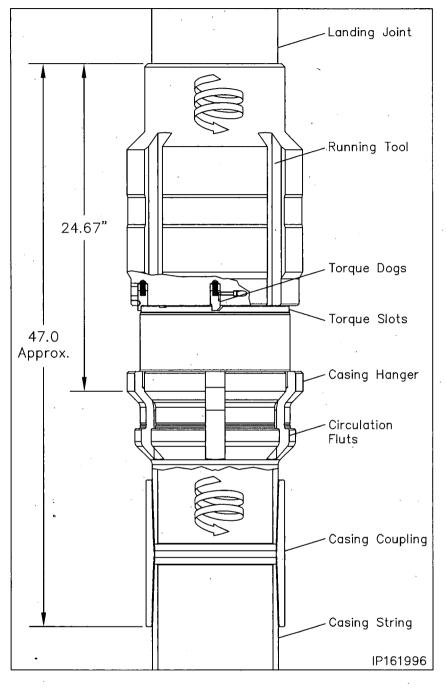
WARNING: Do not rotate the running tool more than 1/4 turn to the left. Doing so will decrease the torque dog engagement





Stage 5 — Hang Off the 9-5/8" Casing

16. Engage the CRT tool on the landing joint and torque the casing hanger in the casing string to thread manufacturer's maximum make up torque.



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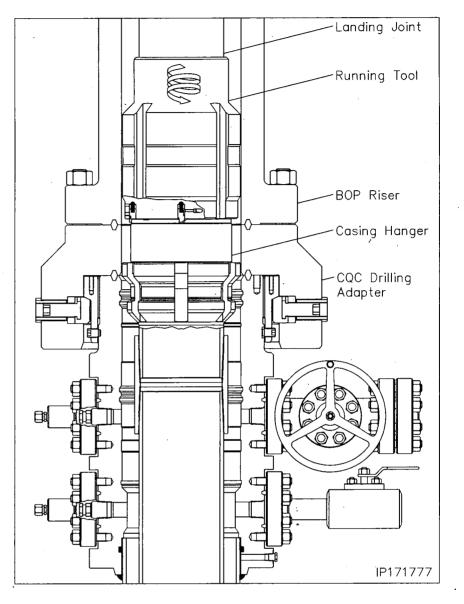


Stage 5 — Hang Off the 9-5/8" Casing

- Pick up the casing string and remove the floor slips and rotary bushings.
- Carefully lower the hanger completely through the BOP annular and then engage the top drive to allow the casing to be rotated clockwise.
- 19. While rotating the casing clockwise, carefully lower the casing string until the **STOP ROTATING** mark on the landing joint is level with the rig floor.

Note: The torque dogs have a maximum rated capacity of 18,000 ft lbs.







Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 5 — Hang Off the 9-5/8" Casing

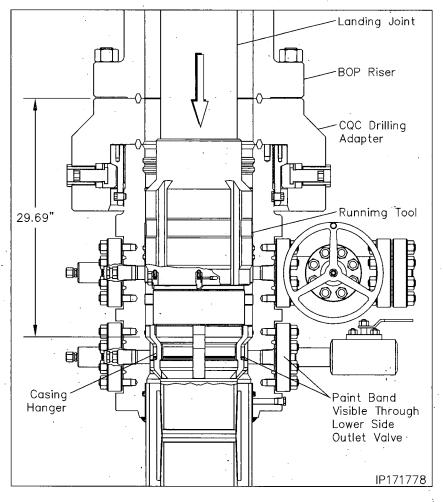
WARNING: Torque wrap can build in the casing string as it is rotated. Ensure the string comes to a neutral position, by allowing it to back off slowly counter clockwise, before the casing hanger is fully landed.

- 20. Cease rotation and continue carefully lowering the hanger through the wellhead and land it on the load shoulder in the MBU-3T housing, 29.69" below the top of the drilling adapter.
- 21. Slack off all weight on the casing and verify that the **HANGER LANDED** paint mark has aligned with the rig floor.
- 22. Open the MBU-3T housing lower outlet valve and drain the BOP stack.
- 23. Sight through the valve bore to confirm the hanger is properly landed. The white painted indicator groove will be clearly visible in the center of the open outlet valve.
- 24. Close the open valve and place a vertical paint mark on the landing joint to verify if the casing string rotates during the cementing process.
- 25. Cement the casing as required.

Note: Returns may be taken through the circulation slots and out the BOP or out the side outlets on the housing.

- With cement in place, bleed off all pressure and remove the cementing head.
- 27. <u>Using Chain Tongs Only located</u> <u>180° apart</u>, retrieve the Running Tool and landing joint by rotating the landing joint counter clockwise (left) approximately 13 turns or until the tool comes free of the hanger.

WARNING: The rig floor tong may be used to break the connection but under no circumstances is the top drive to be used to rotate or remove the casing hanger running tool.



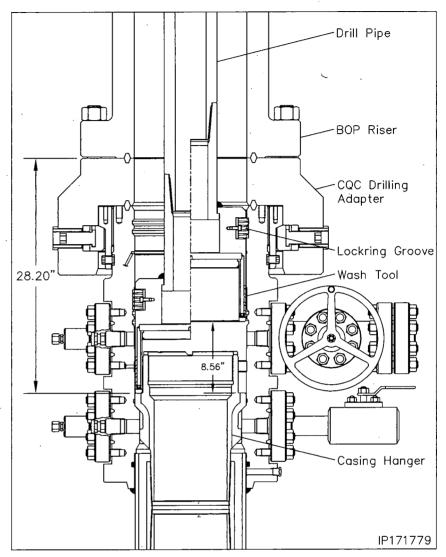
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Stage 5 — Hang Off the 9-5/8" Casing

Running the 13-5/8" Wash Tool

- Examine the 13-5/8" x 4-1/2" IF Wash Tool (Item ST5). Verify the following:
 - drill pipe threads and bore are clean and in good condition
 - all ports are open and free of debris
- Orient the Wash Tool with drill pipe box up. Make up a joint of drill pipe to the tool.
- Carefully lower the Wash Tool through the BOP and land it on top of the 9-5/8" casing hanger, 28.20" below the top flange of the wellhead housing.
- 4. Place a paint mark on the drill pipe level with the rig floor.
- 5. Open the housing lower side outlet valve and drain the BOP stack.
- Using chain tongs, rotate the tool clockwise approximately 6 turns to loosen any debris that may be on top of the hanger flutes.
- Pick up on the tool approximately 1" and attach a high pressure water line or the top drive to the end of the drill pipe and pump water (at approximately 200 to 300 PSI on the rig pump) through the tool and up the BOP stack.
- While flushing, raise and lower the tool the full length of the wellhead and BOP stack. The drill pipe should be slowly rotated (approximately 20 RPM) while raising and lowering to wash the inside of the housing and BOP stack to remove all caked on debris.
- 9. Once washing is complete, land the wash tool on the hanger flutes.
- 10. Shut down pumps and allow the BOP stack to drain.



 Reengage the pump and fully wash the inside of the wellhead and the entire BOP one additional cycle ensuring the stopping point is with the was tool resting on top of the hanger flutes.

Note: Observe the returns at the open outlet valve. If returns are not clean, continue flushing until they are.

- 12. Once the returns are clean and free of debris, retrieve the tool to the rig floor.
- 13. Using a bright light, sight through the bore of the BOP stack and observe the top of the hanger neck and flutes. Ensure that there are no dark areas on top of the flutes of the hanger.

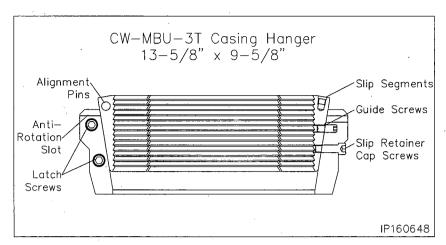
WARNING: Continue washing until all debris is removed.

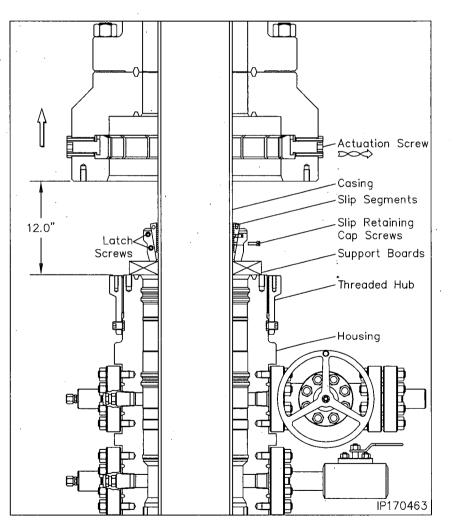


Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 5A — Hang Off the 9-5/8" Casing (Emergency)

- 1. Cement the hole as required.
- 2. Drain the BOP stack through the housing side outlet valve.
- 3. Locate the actuation screw on the OD of the drilling adapter.
- Using a hex drive, fully retract the actuation screws until they are slightly over flush with the glandnuts.
- Pick up on the BOP stack a minimum of 12" above the housing hub and secure with safety slings.
- 6. Washout as required.
- 7. Examine the 13-5/8" x 9-5/8" MBU-3T Slip Casing Hanger (Item A11a). Verify the following:
 - slips and internal bore are clean and in good condition
 - all screws are in place
- There are two latch screws located in the top of the casing hanger. Using a 5/16" Allen wrench, remove the two latch screws located 180° apart and separate the hanger into two halves.
- Place two boards on the lower adapter against the casing to support the Hanger.
- Pick up one half of the hanger and place it around the casing and on top of the boards.
- 11. Pick up the second hanger half and place it around the casing adjacent the first half.
- 12. Slide the two hanger halves together ensuring the slip alignment pins properly engage the opposing hanger half.
- 13. Reinstall the latch screws and tighten securely.
- 14. Prepare to lower the hanger into the housing bowl.





Chisholm Energy 71 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, 16 With CTH-HPS-F MOD Tubing Head



Stage 5A — Hang Off the 9-5/8" Casing (Emergency)

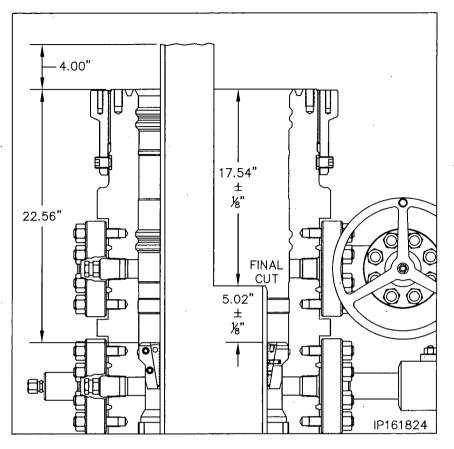
WARNING: Do Not Drop the Casing Hanger!

- Grease the Casing Hanger's body and remove the slip retaining screws.
- 16. Remove the boards and allow the hanger to slide into the housing bowl. When properly positioned the top of the hanger will be approximately 22.56" below the top of the housing.
- 17. Pull tension on the casing to the desired hanging weight and then slack off.

Note: A sharp decrease on the weight indicator will signify that the hanger has taken weight and at what point, If this does not occur, pull tension again and slack off once more.

WARNING: Because of the potential fire hazard and the risk of loss of life and property, It is highly recommended to check the casing annulus and pipe bore for gas with an approved sensing device prior to cutting off the casing. If gas is present, do not use an open flame torch to cut the casing. It will be necessary to use a air driven mechanical cutter which is spark free.

- Rough cut the casing approximately 4" above the top of the housing and move the excess casing out of the way.
- 19. Using the Wach's internal casing cutter, final cut the casing at 17.54" \pm 1/8" below the top of the lower adapter or 5.02" \pm 1/8" above the hanger body.
- 20. Remove the internal casing cutter assembly and reconfigure the assembly to bevel the casing. Reinstall the cutter assembly and then place a 3/16" x 3/8" bevel on the O.D. and a I.D. chamfer to match the minimum bore of the packoff to be installed.



Note: There must not be any rough edges on the casing or the seals of the Packoff will be damaged.

- 21. Thoroughly clean the housing bowl, removing all CEMENT AND CUTTING DEBRIS.
- 22. Locate the two anti-rotation notches in the top of the sip bowl.
- 23. Place a straight edge on top of the slip bowl and in line with the center of one of the notches.
- 24. Ensure the straight edge is vertical and then place a paint mark on top of the housing in line with the notch in the slip bowl.



Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

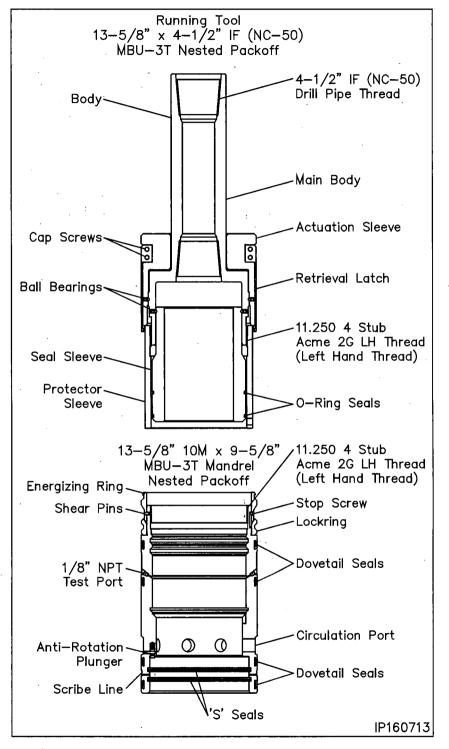
Stage 6 — Install the MBU-3T Mandrel Hanger Packoff

The following steps detail the installation of the MBU-3T Nested Packoff Assembly for the mandrel hanger. If the casing was landed using the emergency slip hanger, skip this step and proceed with Stage 6A for installing the emergency MBU-3T Nested packoff.

- 1. Examine the 13-5/8" x 11.250" 4 Stub Acme 2G LH box top MBU-3T Mandrel Hanger Nested Packoff Assembly (Item A12). Verify the following:
 - all elastomer seals are in place and undamaged
 - internal bore, and ports, are clean and in good condition
 - lockring is fully retracted
 - energizer ring is in its upper most position and retained with shear pins and stop screws are loose
 - anti-rotation plungers are in place, free to move
- 2. Inspect the ID and OD seals for any damage and replace as necessary.
- 3. Examine the 13-5/8" Nominal x 11.250" 4 Stub Acme 2G LH, MBU-3T Nested Packoff Running Tool (Item ST6). Verify the following:
 - Acme threads are clean and in good condition
 - retrieval latch is in position and retained with cap screws
 - Remove seal sleeve protector sleeve
 - seal sleeve is in position and rotates freely
 - seal sleeve o-rings are in place and in good condition
 - reinstall seal sleeve protector

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4. Remove the retrieval latch and set aside.



IP 0571 Page 18 Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

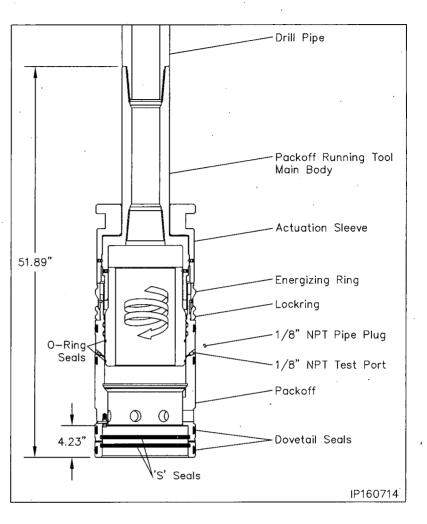


Stage 6 — Install the MBU-3T Mandrel Hanger Packoff

- Make up the running tool to 4-1/2" IF (NC-50) drill pipe and torque the connection to optimum make up torque.
- 6. Pick up the Running Tool with landing joint and suspend it above the packoff.
- 7. Remove the tool protector sleeve with counter clockwise rotation and set the sleeve aside.
- 8. Thoroughly clean and lightly lubricate the mating Acme threads of the running tool and packoff with oil or light grease.
- 9. Lightly lubricate the seal sleeve o-rings with oil or a light grease.
- 10. Carefully lower the tool into the packoff and thread them together by first rotating the tool clockwise (RIGHT) to locate the thread start and then counter clockwise (LEFT) until the tool upper body makes contact with the packoff Energizing Ring. Approximately 4 turns.
- 11. Install (1) 1/8" NPT pipe plug in the OD test port of the packoff and tighten securely.
- Attach a test pump to the remaining open port and inject test fluid between the seal sleeve o-rings until a stable test pressure of 5000 psi is achieved.
- If the test fails, remove the tool and replace the leaking o-rings.
- 14. After a satisfactory test is achieved remove the test pump and the 1/8" pipe plug from the opposite test port.

WARNING: All 1/8" pipe plugs must be removed prior to installing the packoff

15. Pick up the assembly and thoroughly clean and lightly lubricate the packoff ID 'S' seals and the OD dovetail seals with oil or light grease.



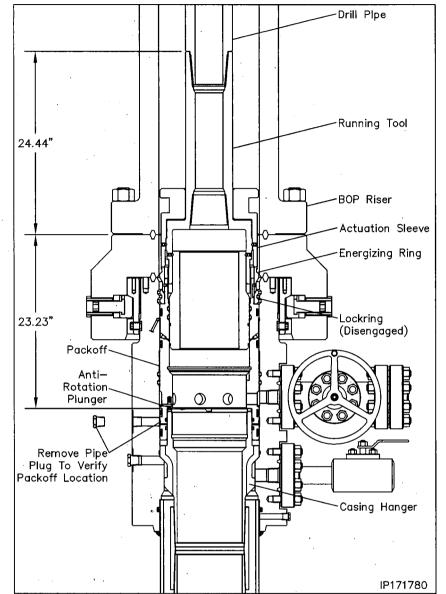


Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 6 — Install the MBU-3T Mandrel Hanger Packoff

Landing the Packoff

- 16. Remove the hole cover.
- Measure up 5 foot from the paint mark on the OD of the packoff and place a paint mark on the drill pipe.
- Pick up the packoff/running tool assembly and carefully lower the assembly through the BOP marking the landing joint every five feet until the calculated dimension is reached.
- Place a paint mark on the landing joint at that dimension and mark land off. Place an additional mark 1-1/2" above the first one and mark engaged.
- Continue lowering the packoff until it passes over the neck of the hanger and lands on the casing hanger neck, 23.23" below the top of the drilling adapter.
- 21. Locate the upper 1" sight port pipe plug and remove the plug
- 22. Look through the port to verify that the packoff is properly landed. The white paint scribe line will be clearly visible in the center of the open port.
- 23. Reinstall the pipe plug and tighten securely.



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Stage 6 — Install the MBU-3T Mandrel Hanger Packoff

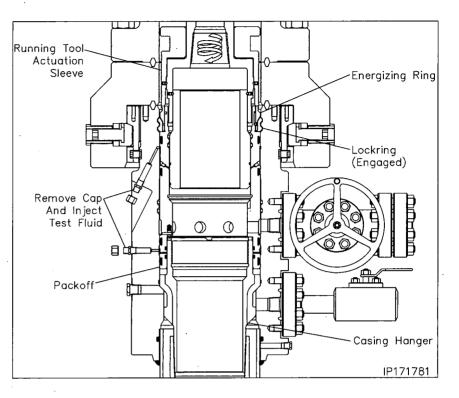
Seal Test

- 24. Locate the upper and lower seal test fittings on the O.D. of the housing and remove the dust cap from the fittings.
- Attach a test pump to the open lower fitting and pump clean test fluid between the seals until a stable test pressure of 5,000 psi is achieved.
- 26. Hold test pressure for 5 minutes.
- 27. If a leak develops, bleed off test pressure, remove the packoff from the wellhead and replace the leaking seals.
- 28. Repeat steps 24 through 27 for the remaining seal test.
- 29. After satisfactory tests are achieved, bleed off the test pressure but leave the test manifolds in place.

Engaging the Lockring

- 30. Using chain tongs only located 180° apart, slowly rotate the drill pipe counter clockwise until the anti-rotation plungers align with the slots in the top of the hanger. Expect torque of approximately 400 ft lbs. to rotate the packoff.
- 31. Using only chain tongs, rotate the landing joint approximately 6 to 6-1/2 turns counter clockwise to engage the packoff lockring in its mating groove in the bore of the MBU-LR housing.

Note: Approximately 800 to 900 ft. lbs. of torque will be required to break over the shear pins in the packoff. The torque will drop off and then increase slightly when the energizing ring pushes the lockring out. A positive stop will be encountered when the lockring is fully engaged.



Note: When properly engaged the second paint mark on the landing joint will align with the rig floor. VERIFY PAINT MARKS.

WARNING: It is imperative that the landing joint remain concentric with the well bore when rotating to engage the lockring. This can be accomplished with the use of the air hoist.

WARNING: If the required turns to engage the lockring are not achieved or excessive torque is encountered, remove the packoff and first call local branch and then Houston Engineering.

- 32. Back off the landing joint/running tool approximately three turns. Using the top drive, exert a 40,000 lbs. pull on the landing joint.
- 33. Reattach the test pump to the open test manifolds and retest the packoff seals to 5,000 psi for 15 minutes. This will also verify that the packoff is in place.
- 34. After satisfactory test is achieved, bleed off all test pressure, remove test pump and reinstall the dust cap on the open fittings.
- 35. Using only chain tongs, rotate the landing joint clockwise until the tool comes free of the packoff (approximately 9 to 9-1/2 turns) and then retrieve the tool with a straight vertical lift.



Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 6 — Install the MBU-3T Mandrel Hanger Packoff

In the event the packoff is required to be removed after the lockring is engaged the following procedure is to be followed.

Retrieving the Packoff

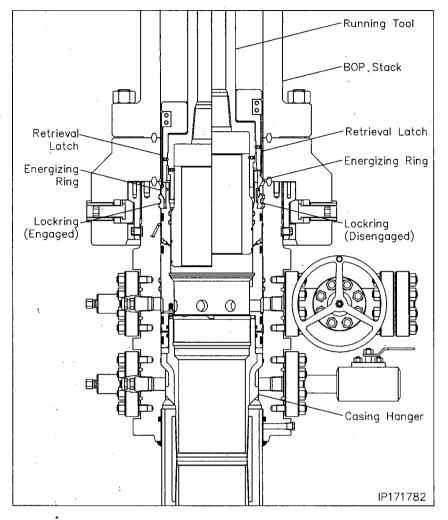
- 1. Position the retrieval latch so the latch finger extend from the bottom of the running tool body.
- 2. Reinstall the cap screws and tighten them securely.
- 3. Ensure the retrieval latch freely rotates on the running tool body.
- Carefully lower the running tool through the BOP stack and into the packoff.
- Rotate the drill pipe clockwise (Right) to locate the thread start and then counter clockwise (Left) (approximately 9 to 9-1/2 turns) to a positive stop.

Note: At this point the retrieval latches will have passed over the energizing ring and snapped into place.

 Rotate the drill pipe clockwise (right) approximately 6 turns to a positive stop. The drill pipe should rise approximately 1-1/2".

Warning: Do not exceed the 6 turns or the packoff may be seriously damaged.

- Carefully pick up on the drill pipe and remove the packoff from the MBU-3T wellhead with a straight vertical lift.
- 8. Rotate the packoff 1 turn clockwise to relax the retrieval latch.
- 9. Remove the (4) 1/2" cap screws and remove the latch assembly.



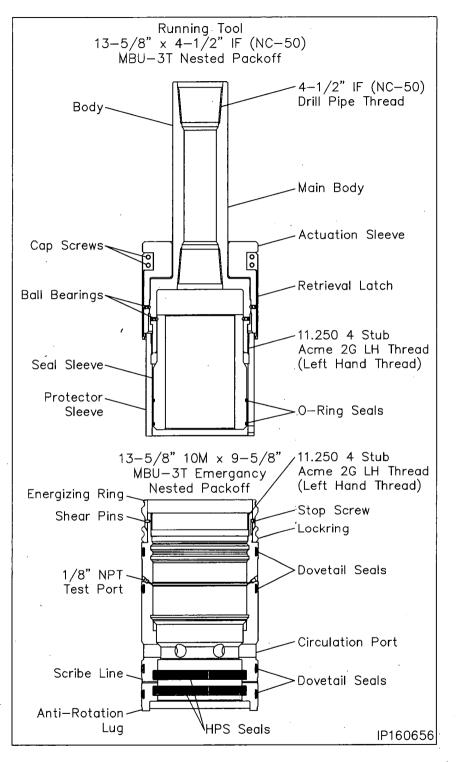
- 10. Redress the Packoff and reset as previously outlined.
- 11. Once the packoff is properly set, reinstall the retrieval latch on the tool.

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Stage 6A — Install the MBU-3T Emergency Packoff

- 1. Examine the 13-5/8" 10M x 9-5/8" x 11.250" 4 Stub Acme 2G LH box top MBU-3T Emergency Nested Packoff Assembly (Item A12a). Verify the following:
 - all elastomer seals are in place and undamaged
 - internal bore, and ports, are clean and in good condition
 - lockring is fully retracted
 - energizer ring is in its upper most position and retained with shear pins
- 2. Inspect the ID and OD seals for any damage and replace as necessary.
- 3. Examine the 13-5/8" Nominal x 11.250" 4 Stub Acme 2G LH, MBU-3T Nested Packoff Running Tool (Item ST6). Verify the following:
 - Acme threads are clean and in good condition
 - retrieval latch is in position and retained with cap screws
 - seal sleeve is in position and rotates freely
 - seal sleeve o-rings are in place and in good condition
 - reinstall seal sleeve protector
- Make up a joint 4-1/2" IF (NC-50) drill pipe to the top of the Running Tool and tighten connection to thread manufacturer's maximum make up torque.
- 5. Run in the hole with two stands of drill pipe and set in floor slips.



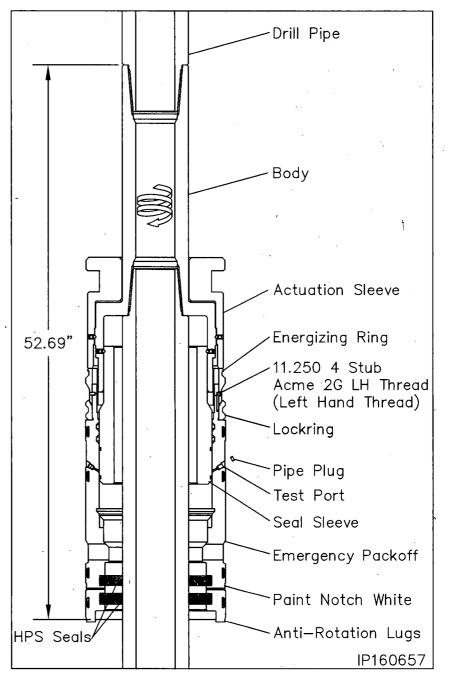


Stage 6A — Install the MBU-2LR Emergency Packoff

- Pick up the packoff and carefully pass it over the drill pipe and set it on top of the floor slips.
- Pick up the running tool with landing joint and remove the tool protector sleeve with counter clockwise rotation and set the sleeve aside.
- 8. Thoroughly clean and lightly lubricate the mating acme threads of the running tool and packoff with oil or light grease.
- 9. Lightly lubricate the seal sleeve o-rings with oil or a light grease.
- Make up the running tool to the drill pipe in the floor slips using the appropriate length pip x pin sub.
- 11. Pick up the packoff and thread it onto the running tool with clockwise (Right) rotation until the Energizing Ring makes contact with the lower body of the tool. (Approximately 4 turns).
- 12. Install (1) 1/8" NPT pipe plug in the OD test port of the packoff and tighten securely
- Attach a test pump to the remaining open port and inject test fluid between the seal sleeve o-rings until a stable test pressure of 5,000 psi is achieved.
- 14. If the test fails, remove the tool and replace the leaking o-rings.
- After a satisfactory test is achieved remove the test pump and the 1/8" pipe plug from the opposite test port.

WARNING: All 1/8" pipe plugs must be removed prior to installing the packoff

16. Thoroughly clean and lightly lubricate the packoff ID 'HPS' seals and the OD dovetail seals with oil or light grease.



17. Using a straight edge positioned vertically and centered on the anti-rotation lug on the bottom of the packoff, place a white paint mark up the side of the packoff in line with the lug.

Note: The line will be used to guide the packoff anti-rotation lug into its mating notch in the slip bowl.



Stage 6A — Install the MBU-2LR Emergency Packoff

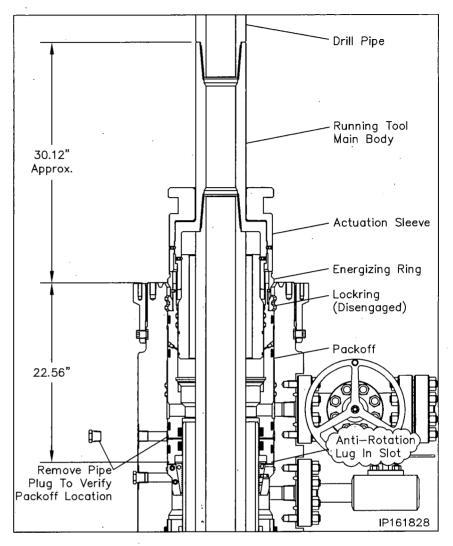
Landing the Packoff

- 18. Pick up the drill string and remove the floor slips.
- 19. Carefully lower the packoff through the rig floor and position it just above the housing.
- 20. Align the white paint line with the existing paint mark on top of the housing.
- 21. While holding the packoff to maintain alignment, carefully lower the packoff into the housing until it lands on top of the slip hanger.

Note: When properly positioned the top of the running tool will be approximately 30.12" above the top of the MBU-3T Housing.

22. Remove the upper 1" LP pipe plug from the sight port to verify the packoff is properly landed. The 5/16" scribe line should be clearly visible in the center of the port.

With landing verified, reinstall the pipe plug and tighten securely.





Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 6A — Install the MBU-2LR Emergency Packoff

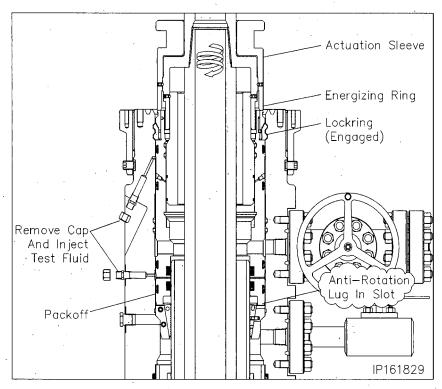
Seal Test

- Locate the upper and lower seal test fittings on the O.D. of the housing and remove the dust cap from the fittings.
- Attach a test pump to the open lower fitting and pump clean test fluid between the seals until a stable test pressure of 5,000 psi is achieved.
- 3. Hold test pressure for 5 minutes.
- 4. If a leak develops, bleed off test pressure, remove the packoff from the wellhead and replace the leaking seals.
- 5. After satisfactory test is achieved, bleed off the test pressure but leave the test manifold in place.
- 6. Repeat steps 1 through 5 for the upper seal test port.

Engaging the Lockring

 Using only chain tongs, rotate the landing joint approximately 6 to 6-1/2 turns counter clockwise (Left) to engage the packoff lockring in its mating groove in the bore of the MBU-3T housing.

Note: Approximately 800 to 900 ft. lbs. of torque will be required to break over the shear pins in the packoff. The torque will drop off and then increase slightly when the energizing ring pushes the lockring out. A positive stop will be encountered when the lockring is fully engaged.



WARNING: It is imperative that the drill pipe landing joint remain concentric with the well bore when rotating to engage the lockring. This can be accomplished with the use of the air hoist.

WARNING: If the required turns to engage the lockring are not achieved or excessive torque is encountered, remove the packoff and first call local branch and then Houston Engineering.

- 8. Back off the landing joint/running tool approximately three turns. Using the top drive, exert a 40,000 lbs. pull on the landing joint.
- Reattach the test pump to the open test manifolds and retest the packoff seals to 5,000 psi for 15 minutes. This will also verify that the packoff is in place.
- After satisfactory test is achieved, bleed off all test pressure, remove test pump and reinstall the dust cap on the open fittings.
- 11. Using only chain tongs, rotate the landing joint clockwise until the tool comes free of the packoff (approximately 9 to 9-1/2 turns) and then retrieve the tool with a straight vertical lift.
- 12. Reinstall and nipple up the BOP stack.

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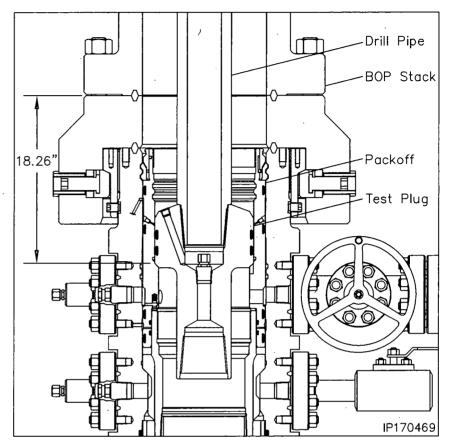
Stage 7 — Test the BOP Stack

Immediately after making up the BOP stack and periodically during the drilling of the well for the next casing string the BOP stack (connections and rams) must be tested.

- Examine the 11" Nominal x 4-1/2" IF (NC-50) CW Test Plug/ Retrieving Tool (Item ST7). Verify the following:
 - 1-1/4" VR plug and weep hole plug are in place and tightened securely
 - elastomer seal is in place and in good condition
 - retractable lift lugs are in place, clean, and free to move
 - drill pipe threads are clean and in good condition
- Position the test plug with the elastomer seal down and the lift lugs up and make up the tool to a joint of drill pipe.

WARNING: Ensure that the lift lugs are up and the elastomer seal is down

- Remove the 1/2" NPT pipe plug from the weep hole if pressure is to be supplied through the drill pipe.
- 4. Open the housing upper side outlet valve.
- 5. Lightly lubricate the test plug seal with oil or light grease.
- Carefully lower the test plug through the BOP and land it on the load shoulder in the packoff, 18.26" below the top of the drilling adapter.
- 7. Close the BOP rams on the pipe and test the BOP to 5,000 psi.



Note: Any leakage past the test plug will be clearly visible at the open side outlet valve.

- 8. After a satisfactory test is achieved, release the pressure and open the rams.
- Remove as much fluid as possible from the BOP stack and the retrieve the test plug with a straight vertical lift.

Note: When performing the BOP blind ram test it is highly recommended to suspend a stand of drill pipe below the test plug to ensure the plug stays in place while disconnecting from it with the drill pipe.

10. Repeat this procedure as required during the drilling of the hole section.



Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Stage 8 — Run the Upper Wear Bushing

Note: Always use a Wear Bushing while drilling to protect the load shoulders from damage by the drill bit or rotating drill pipe. The Wear Bushing **must be retrieved** prior to running the casing.

- 1. Examine the 13-5/8" x 11" x 9.00" ID MBU-3T-UPR Wear Bushing (Item ST8). Verify the following
 - internal bore is clean and in good condition
 - o-ring is in place and in good condition
 - shear o-ring cord is in place and in good condition
 - paint anti-rotation lugs white and allow paint to dry

Run the Wear Bushing Before Drilling

- Orient the 13-5/8" Nominal x 4-1/2" IF (NC-50) CW Test Plug/ Retrieving Tool (Item ST1) with drill pipe connection up.
- 3. Attach the Retrieving Tool to a joint of drill pipe.

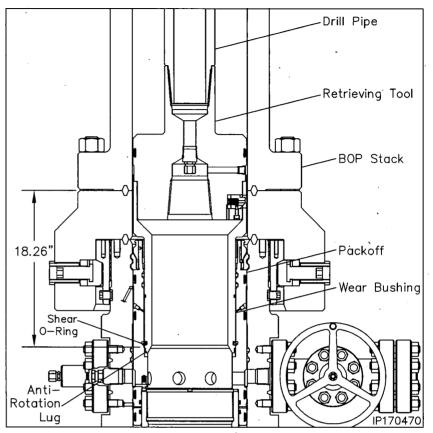
WARNING: Ensure that the lift lugs are down and the elastomer seal is up

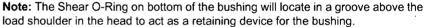
 Align the retractable lift lugs of the tool with the retrieval holes of the bushing and carefully lower the tool into the Wear Bushing until the lugs snap into place.

Note: If the lugs did not align with the holes, rotate the tool in either direction until they snap into place.

5. Apply a heavy coat of grease, not dope, to the OD of the bushing.

- 6. Ensure the BOP stack is drained and free of any debris from previous test.
- Slowly lower the Tool/Bushing Assembly through the BOP stack and land it on the load shoulder in the housing, 18.26" below the top of the drilling adapter.
- 8. Rotate the drill pipe clockwise (right) to locate the stop lugs in their mating notches in the head. When properly aligned the bushing will drop an additional 1/2".





- 9. Remove the tool from the Wear Bushing by rotating the drill pipe counter clockwise (left) 1/4 turn and lifting straight up.
- 10. Drill as required.

Note: It is highly recommended to retrieve, clean, inspect, grease, and reset the wear bushing each time the hole is tripped during the drilling of the hole section.

Retrieve the Wear Bushing After Drilling

- 11. Make up the Retrieving Tool to the drill pipe.
- 12. Drain BOP stack and wash out if necessary.
- 13. Slowly lower the tool into the Wear Bushing.
- 14. Rotate the Retrieving Tool clockwise until a positive stop is felt. This indicates the lugs have snapped into the holes in the bushing.
- 15. Using the top drive, slowly pick up on the landing joint in 1000 lbs increments until the busing starts to rise. This action should take a minimum of 3000 lbs pull. Do Not Exceed 60,000 lbs.
- 16. Retrieve the Wear Bushing, and remove it and the Retrieving Tool from the drill string.

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Stage 9 — Hang Off the 5-1/2" Casing

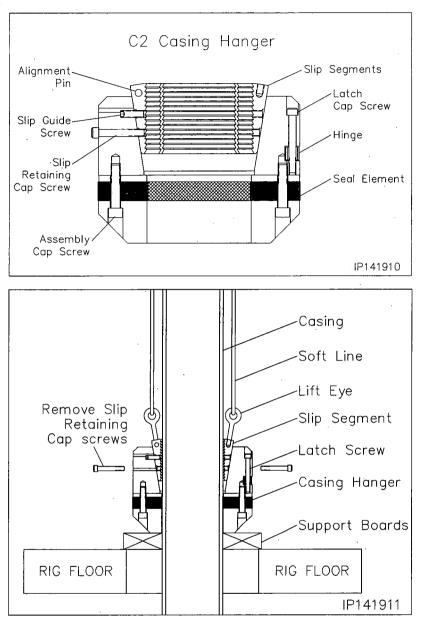
- 1. Run and cement the 5-1/2" casing string as required.
- 2. Open the housing upper side outlet valve to drain the BOP stack.
- Clean the ID of the BOP stack and OD of the casing with a high pressure water hose until returns through the open side outlet valve are clean and free of debris.
- 4. Thoroughly inspect the BOP stack to ensure all rams are fully retracted into their respective ram bores, the annular rubber is fully relaxed, all drilling adapters/spools are full opening and there are no casing collars between the rig floor and the wellhead.

Note: Side outlet valve to remain open while setting the casing hanger.

- Examine the 11" x 5-1/2" C2 Slip Casing Hanger (Item A13). Verify the following:
 - slips and internal bore are clean and in good condition
 - all screws are in place
 - packoff rubber is in good condition

Note: Ensure that the packoff rubber does not protrude beyond the O.D. of the casing hanger body. If it does, loosen the cap screws in the bottom of the hanger.

- 6. Measure the distance from the rig floor to the top of the wellhead flange and record this measurement.
- 7. Pour a light oil through the BOP stack to thoroughly coat the OD of the casing.
- Using a 5/16" Allen wrench, remove the two latch screws located 180° apart on top of the hanger and separate the hanger into two halves.
- 9. Place two boards on the housing flange against the casing to support the hanger.
- Pick up one half of the hanger and place it around the casing and on top of the boards.
- 11. Pick up the second hanger half and place it around the casing adjacent the first half.



- 12. Slide the two hanger halves together ensuring the slip guide pins properly engage the opposing hanger half.
- 13. Reinstall the latch screws and tighten securely.
- 14. Using a 5/16" allen wrench, remove the slip retainer cap screws and discard them.
- 15. Lubricate the OD of the Casing Hanger liberally with a light grease or oil.
- 16. Prepare to lower the hanger through the BOP stack.



Stage 9 — Hang Off the 5-1/2" Casing

WARNING: Do not drop or allow the hanger to fall through the BOP stack.

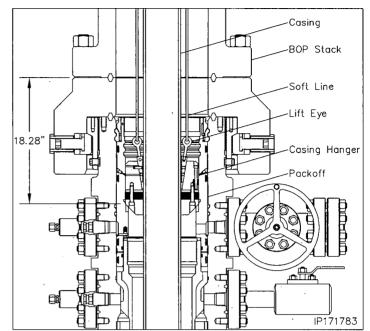
One method commonly used is to loop or tie four lengths of soft line through the hanger eye bolts as shown. Tie a knot in the soft line at the measurement noted in step six (6).

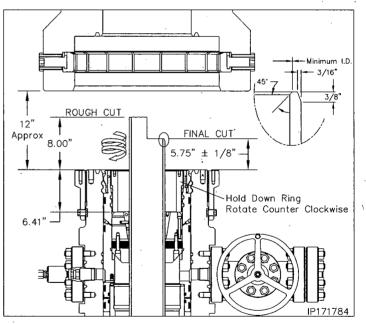
Note: The soft line may stretch and give an imprecise indication of the Casing Hanger's location.

- 17. Remove the boards and allow the Casing Hanger to slide through the BOP and into the MBU-3T packoff bowl using the cat line to center that casing if necessary.
- 18. When the Casing Hanger is down as indicated by the knots in the soft line, pull tension to the desired hanging weight and slack off.

Note: A sharp decrease on the weight indicator will signify that the Hanger has taken weight and at what point.

- 19. Untie the soft lines and pull them back through the lift eyes or drop them inside the BOP stack.
- 20. Prior to nippling down the BOP the integrity of the slip hanger seal can be verified by closing the BOP annular on the casing string and applying customer specific pressure through the kill line.
- 21. Once a satisfactory test is achieved, bleed off all test pressure, and drain the BOP stack.
- 22. Locate the actuation screws on the OD of the lower drilling adapter.
- 23. Using a hex drive, fully retract the (16) actuation screws until they are slightly over flush with the glandnuts.
- 24. Pick up on the BOP stack a minimum of 12" above the housing and secure with safety slings.
- 25. Remove the four lift eyes.
- 26. Rough cut the casing approximately 8" above the top of the housing and move the excess casing out of the way.
- 27. Final cut the casing at $5-3/4" \pm 1/8"$ above the top flange of the housing.
- Grind the casing stub level and then place a 3/16" x 3/8" bevel on the O.D. and a I.D. chamfer to match the minimum bore of the tubing head to be installed.





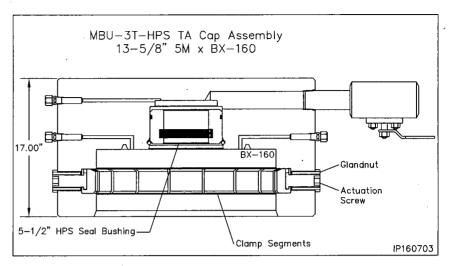
- 29. Thoroughly clean the top of the housing and Casing Hanger. Ensure all cutting debris are removed.
- Thoroughly clean and lightly lubricate the mating acme threads of the MBU-3T packoff and the slip *Hold Down Ring (Item A14).*
- 31. Thread the ring into the packoff with counter clockwise rotation to a positive stop on top of the slip hanger.
- 32. Re-land the BOP stack and prepare to remove the upper adapter with the BOP stack

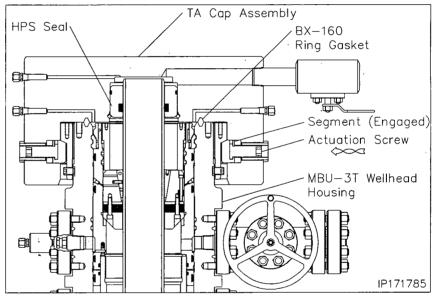
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Stage 10 — Install the 'Quick Connect' TA Cap Assembly

- 1. Examine the 13-5/8" 5M 'Quick Connect' TA Cap Assembly (Item R3). Verify the following:
 - bore is clean and free of debris
 - ring groove is clean and
 - undamaged
 - (16) drive screws and clamp segments are properly installed and fully retracted
 - 5-1/2" HPS seal bushing is in place and properly retained with the square snap wire
- Thoroughly clean the top of the MBU-3T housing, thread hub, and the mating seal surfaces of the TA Cap.
- 3. Install a new *BX-160 Ring Gasket* into the ring groove of the housing.
- Using a suitable lifting devise with weight rated slings, pick up the TA Cap assembly and carefully lower it over the casing stub and land it on the ring gasket.
- Ensure the TA Cap is level and then carefully run in all of the drive screws of the TA Cap to contact point.
- Ensure the assembly remains level, run in one actuation and torque to 100 ft lbs.
- 7. Locate the screw 180° from the first and torque to 100 ft lbs.
- 8. Locate the screws 90° to the right and left and torque to 100 ft lbs.
- 9. Position the second 4 point sequence 90° from the first and torque each screw to 200 ft lbs
- 10. Run in all remaining screws to contact and then torque each screw to 400 ft lbs.
- 11. Make one additional round until a stable torque of 400 ft lbs on all (16) screws is achieved.







Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

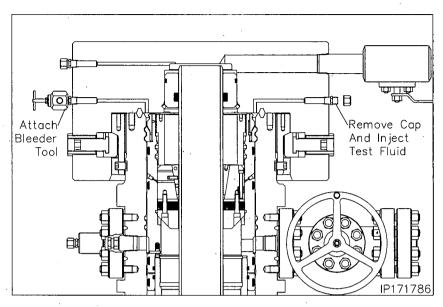
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Stage 10 — Install the 'Quick Connect' TA Cap Assembly

Connection Test

- 1. Open the TA Cap ball valve and the housing upper side outlet valve to monitor leakage.
- Locate the two test fittings marked flange test and remove the dust caps from the fittings.
- 3. Attach a bleeder tool to one of the open fitting and open the tool.
- Attach a test pump to the remaining open fitting and pump clean test fluid into the void area until a continuous stream flows from the open bleeder tool.
- Close the tool and continue pumping fluid until a stable test pressure of 5,000 psi or 80% of casing collapse is achieved, whichever is less.
- 6. Hold test pressure for 15 minutes.
- After a satisfactory test is achieved, bleed off the test pressure, drain the fluid, remove the bleeder tool and re install the dust cap on the open fittings.
- 8. Close all open valves.

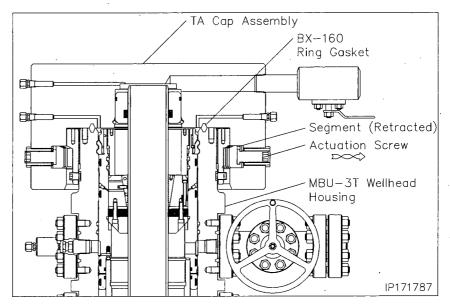


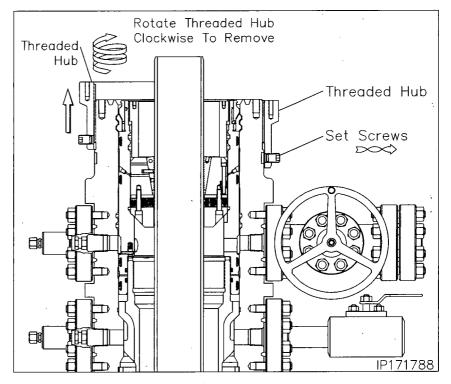
IP 0571 Page 32 Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head



Stage 11 — Remove the TA Cap Assembly

- 1. Open the ball valve on the TA cap to check for trapped pressure above the casing hanger.
- 2. Locate the actuation screws on the OD of the TA Cap Assembly.
- Using a hex drive, fully retract the actuation screws until they are slightly over flush with the glandnuts.
- Install a lift eye with pick up sling to the top of the TA Cap and lift the cap free of the wellhead.
- 5. Remove the thread hub set screws.
- 6. Remove the thread hub from the top of the housing with clockwise rotation.





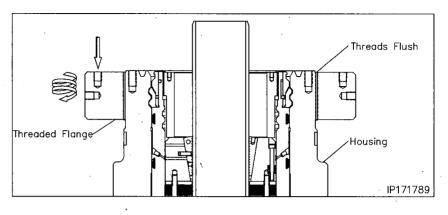


Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

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Stage 11 — Remove the TA Cap Assembly

- 7. Examine the 13-5/8" 5M Thread Flange. Verify the following:
 - Acme thread are clean and in . good condition
- 8. Thoroughly clean and lightly lubricate the mating threads of the housing and the Thread Flange with Copper Coat or Never Seize.
- 9. Pick up the flange and carefully thread it onto the top of the housing with counter clockwise rotation until the top of the flange is level with the top of the Acme thread of the housing.
- 10. Rotate the flange in either direction to two hole.
- 11. Prepare to install the tubing head.



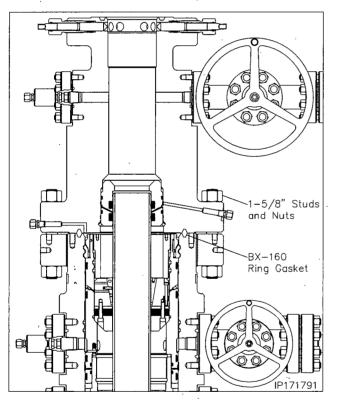
Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

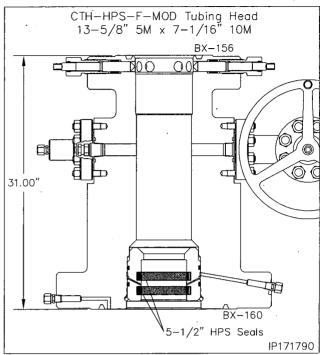


Stage 12 — Install the Tubing Head

Note: The tubing head may be shipped to location with the lower frac valve pre installed and tested.

- Examine the 13-5/8" 5M x 7-1/16" 10M CW, CTH-HPS-F MOD Tubing Head With 5-1/2" DBLHPS Bottom (Item B1) Verify the following:
 - seal area and bore are clean and in good condition
 - HPS-F MOD Secondary Seal Bushing is in place and properly retained with a square snap wire
 - all peripheral equipment is intact and undamaged
- 2. Clean the mating ring grooves of the MBU-3T Housing and tubing head.
- 3. Lightly lubricate the I.D. of the tubing head 'HPS' seals and the casing stub with a light oil or grease.





Note: Excessive oil or grease may prevent a good seal from forming!

- 4. Install a new *BX-160 Ring Gasket (Item B12)* in the ring groove of the housing.
- 5. Pick up the tubing head and suspend it above the housing.
- Orient the head so that the outlets properly align with the housing upper outlets and then carefully lower the head over the casing stub and then land it on the ring gasket.

Warning: Do Not damage the 'HPS' seals or their sealing ability will be impaired!

7. Make up the flange connection using the appropriate size *studs and nuts (Item B13)*; tightening them in an alternating cross pattern.



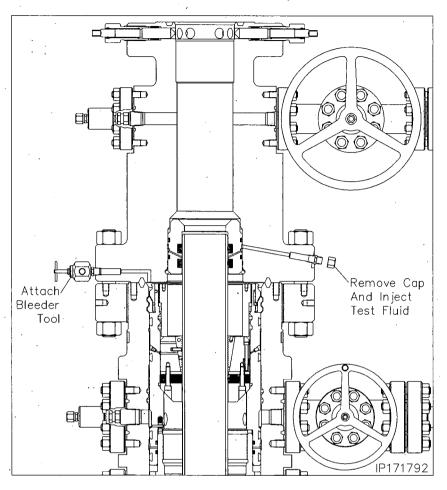
Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

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Stage 12 — Install the Tubing Head

Seal Test

- Locate the seal test fitting and one flange test fitting on the Tubing Head lower flange and remove the dust cap from both fittings.
- 2. Attach a Bleeder Tool to one of the open flange test fittings and open the Tool.
- 3. Attach a test pump to the seal test fitting and pump clean test fluid between the HPS Seals until a test pressure of 10,000 psi or 80% of casing collapse Whichever is less.
- 4. Hold test pressure for 15 minutes.
- 5. If pressure drops, a leak has developed. Bleed off test pressure and take the appropriate action in the adjacent table.
- After a satisfactory test is achieved, remove the Test Pump, drain test fluid and reinstall the dust cap on the open seal test fitting.



Seal Test				
Leak Location	Appropriate Action			
Open bleeder tool - Lower HPS seal is leaking	replace leaking seals. Re			
Into the tubing head bore - Upper HPS seal is leaking	land and retest seals			

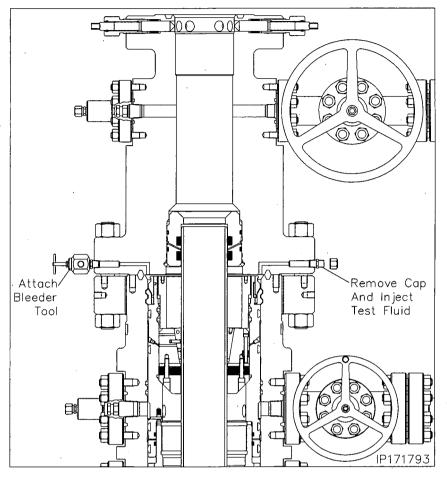
IP 0571 Page 36 Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head



Stage 12 — Install the Tubing Head

Flange Test

- 1. Locate the remaining flange test fitting on the Tubing Head lower flange and remove the dust cap from the fitting.
- Attach a test pump to the open flange test fitting and inject test fluid into the flange connection until a continuous stream flows from the opposite flange test bleeder tool.
- 3. Close the bleeder tool and continue to pumping test fluid to 5,000 psi or 80% of casing collapse -Whichever is less..
- 4. Hold test pressure for 15 minutes.
- 5. If pressure drops a leak has developed. Take the appropriate action from the adjacent chart.
- 6. Repeat this procedure until a satisfactory test is achieved.
- Once a satisfactory test is achieved, remove the test pump and bleeder tool, drain all test fluid, and reinstall the dust caps.



Flange [^] Test				
Leak Location	Appropriate Action			
Between flanges - Ring gasket is leaking	Verify flange bolt torque. If correct, remove tubing head to clean, inspect and possibly replace damaged ring gasket.			



Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

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Recommended Procedure for Field Welding Pipe to Wellhead Parts for Pressure Seal

 Introduction and Scope. The following recommended procedure has been prepared with particular regard to attaining pressure-tight weld when attaching casing heads, flanges, etc., to casing. Although most of the high strength casing used (such as N-80) is not normally considered field weldable, some success may be obtained by using the following or similar procedures.

<u>Caution:</u> In some wellheads, the seal weld is also a structural weld and can be subjected to high tensile stresses. Consideration must therefore be given by competent authority to the mechanical properties of the weld and its heat affected zone.

- a. The steels used in wellhead parts and in casing are high strength steels that are susceptible to cracking when welded. It is imperative that the finished weld and adjacent metal be free from cracks. The heat from welding also affects the mechanical properties. This is especially serious if the weld is subjected to service tension stresses.
- b. This procedure is offered only as a recommendation. The responsibility for welding lies with the user and results are largely governed by the welder's skill. Weldability of the several makes and grades of casing varies widely, thus placing added responsibility on the welder. Transporting a qualified welder to the job, rather than using a less-skilled man who may be at hand, will, in most cases, prove economical. The responsible operating representative should ascertain the welder's qualifications and, if necessary, assure himself by instruction or demonstration, that the welder is able to perform the work satisfactorily.
- 2. Welding Conditions. Unfavorable welding conditions must be avoided or minimized in every way possible, as even the most skilled welder cannot successfully weld steels that are susceptible to cracking under adverse working conditions, or when the work is rushed. Work above the welder on the drilling floor should be avoided. The weld should be protected from dripping mud, water, and oil and from wind, rain, or other adverse weather conditions. The drilling mud, water, or other fluids must be lowered in the casing and kept at a low level until the weld has properly cooled. It is the responsibility of the user to provide supervision that will assure favorable working conditions, adequate time, and the necessary cooperation of the rig personnel.

- **3. Welding.** The welding should be done by the shielded metal-arc or other approved process.
- 4. Filler Metal. Filler Metals. For root pass, it's recommended to use E6010, E6011 (AC), E6019 or equivalent electrodes. The E7018 or E7018-A1 electrodes may also be used for root pass operations but has the tendency to trap slag in tight grooves. The E6010, E6011 and E6019 offer good penetration and weld deposit ductility with relatively high intrinsic hydrogen content. Since the E7018 and E7018-A1 are less susceptible to hydrogen induced cracking, it is recommended for use as the filler metal for completion of the weld groove after the root pass is completed. The E6010, E6011 (AC), E6019, E7018 and E7018-A1 are classified under one of the following codes AWS A5.1 (latest edition): Mild Steel covered electrodes or the AWS A5.5 (latest edition): Low Alloy Steel Covered Arc-Welding Electrodes. The low hydrogen electrodes, E7018 and E7018-A1, should not be exposed to the atmosphere until ready for use. It's recommended that hydrogen electrodes remain in their sealed containers. When a job arises, the container shall be opened and all unused remaining electrodes to be stored in heat electrode storage ovens. Low hydrogen electrodes exposed to the atmosphere, except water, for more than two hours should be dried 1 to 2 hours at 600°F to 700 °F (316°C to 371 °C) just before use. It's recommended for any low hydrogen electrode containing water on the surface should be scrapped.
- 5. Preparation of Base Metal. The area to be welded should be dry and free of any paint, grease/oil and dirt. All rust and heat-treat surface scale shall be ground to bright metal before welding.

IP 0571 Page 38 Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head



Recommended Procedure for Field Welding Pipe to Wellhead Parts for Pressure Seal

- Preheating. Prior to any heating, the wellhead member 6. shall be inspected for the presence of any o-rings or other polymeric seals. If any o-rings or seals are identified then preheating requires close monitoring as noted in paragraph 6a. Before applying preheat, the fluid should be bailed out of the casing to a point several inches (>6" or 150 mm) below the weld joint/location. Preheat both the casing and wellhead member for a minimum distance of three (3) inches on each side of the weld joint using a suitable preheating torch in accordance with the temperatures shown below in a and b. The preheat temperature should be checked by the use of heat sensitive crayons. Special attention must be given to preheating the thick sections of wellhead parts to be welded, to insure uniform heating and expansion with respect to the relatively thin casing.
 - a. Wellhead members containing o-rings and other polymeric seals have tight limits on the preheat and interpass temperatures. Those temperatures must be controlled at 200°F to 325°F or 93 °C to 160°C and closely monitored to prevent damage to the o-ring or seals.
 - b. Wellhead members not containing o-rings and other polymeric seals should be maintained at a preheat and interpass temperature of 400°F to 600°F or 200°C to 300°C.
- 7. Welding Technique. Use a 1/8 or 5/32-inch (3.2 or 4.0 mm) E6010 or E7018 electrode and step weld the first bead (root pass); that, weld approximately 2 to 4 inches (50 to 100 mm) and then move diametrically opposite this point and weld 2 to 4 inches (50 to 100 mm) halfway between the first two welds, move diametrically opposite this weld, and so on until the first pass is completed. This second pass should be made with a 5/32-inch (4.0 mm) low hydrogen electrode of the proper strength and may be continuous. The balance of the welding groove may then be filled with continuous passes without back stepping or lacing, using a 3/16-inch (4.8 mm) low hydrogen electrode. All beads should be no undercutting and weld shall be workmanlike in appearance.
 - a. Test ports should be open when welding is performed to prevent pressure buildup within the test cavity.
 - b. During welding the temperature of the base metal on either side of the weld should be maintained at 200 to 300°F (93 to 149°C).
 - c. Care should be taken to insure that the welding cable is properly grounded to the casing, but ground wire should not be welded to the casing or the wellhead. Ground wire should be firmly clamped to the casing, the wellhead, or fixed in position between pipe slips. Bad contact may cause sparking, with resultant hard spots beneath which incipient cracks may develop. The welding cable should not be grounded to the steel derrick, nor to the rotary-table base.

- 8. Cleaning. All slag or flux remaining on any welding bead should be removed before laying the next bead. This also applies to the completed weld.
- **9. Defects.** Any cracks or blow holes that appear on any bead should be removed to sound metal by chipping or grinding before depositing the next bead.
- **10. Postheating.** Post-heating should be performed at the temperatures shown below and held at that temperature for no less than one hour followed by a slow cooling. The post-heating temperature should be in accordance with the following paragraphs.
 - a. Wellhead members containing o-rings and other polymeric seals have tight limits on the post-heating temperatures. Those temperatures must be controlled at 250°F to 300°F or 120 °C to 150°C and closely monitored to prevent damage to the o-ring or seals.
 - **b.** Wellhead members not containing o-rings and other polymeric seals should be post-heated at a temperature of 400°F to 600°F or 200°C to 300°C.
- **11.** Cooling. *Rapid cooling must be avoided.* To assure slow cooling, welds should be protected from extreme weather conditions (cold, rain, high winds, etc.) by the use of suitable insulating material. (Specially designed insulating blankets are available at many welding supply stores.) Particular attention should be given to maintaining uniform cooling of the thick sections of the wellhead parts and the relatively thin casing, as the relatively thin casing will pull away from the head or hanger if allowed to cool more rapidly. The welds should cool in air to less than 200°F (93°C) (measured with a heat sensitive crayon) prior to permitting the mud to rise in the casing.
- **12. Test the Weld.** After cooling, test the weld. The weld must be cool otherwise the test media will crack the weld. The test pressure should be no more than 80% of the casing collapse pressure.

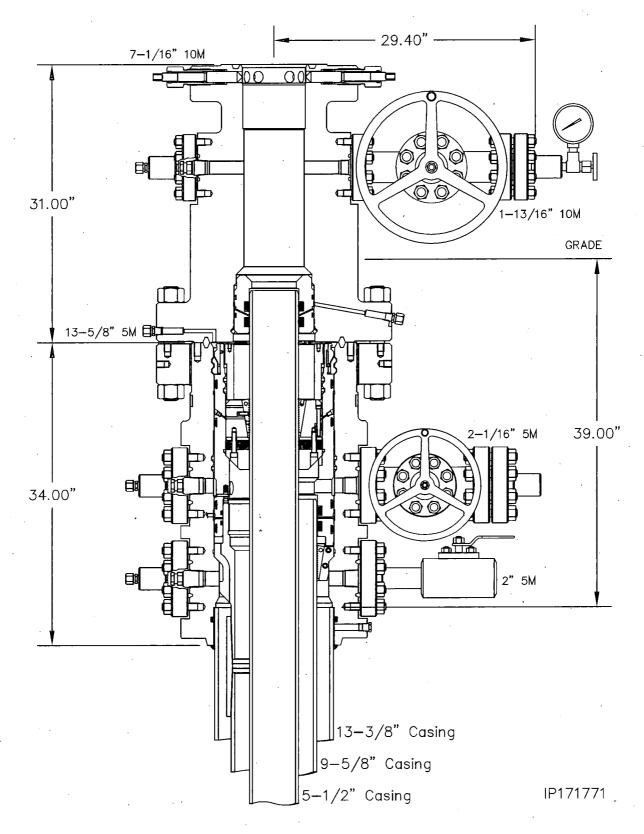


Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

Cactus Speed Head Pressure Testing Statement

Our procedure is to nipple up BOP's to the surface casing, pressure test the BOP's to 5000 psi high and 250 psi low. We do not anticipate breaking any seals on the BOP from that point until rig release, however if we do break any seal, the entire BOP will be retested to 5000 psi high and 250 psi low.

System Drawing





Chisholm Energy 13-3/8" x 9-5/8" x 5-1/2" 5/10M MBU-3T Wellhead, With CTH-HPS-F MOD Tubing Head

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CONTITECH RUBBER	No:QC-DB- 247/ 2014
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ContiTech

QUALITY C			ATE		CERT.	N°:	702	
PURCHASER: Conti	Fech Oil &	Marine Co	orp.		P.Ö. Nº		4500421	193
CONTITECH ORDER N°: 53844	8 ноя	SE TYPE:	3" ।	ID		Choke	& Kill Hose	
HOSE SERIAL Nº: 6755	4 NON	/INAL / AC	TUAL LEN	IGTH:		10,67 r	n / 10,66 m	1
W.P. 68,9 MPa 10000	psi T.P.	103,4	MPa	15000) psi	Duration:	60	mi
Pressure test with water at		·						
ambient temperature								
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ContiTech Rubber Industrial Kft. | Budapesti út 10. H-6728 Szeged | H-6701 P.O.Box 152 Szeged, Hungary Phone: +36 62 566 737 | Fax: +36 62 566 738 | e-mail: info@fluid.contitech.hu | Internet: www.contitech.rubber.hu; www.contitech.hu The Court of Csongrad County as Registry Court Registry Court No: Cg.06-09-002502 | EU VAT No: HU11087209 Bank data Commerzbank Zrt., Budapest | 14220108-26830003 ATTACHMENT OF QUALITY CONTROL INSPECTION AND TEST CERTIFICATE

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ContiTech

Hose Data Sheet

CRI Order No.	538448
Customer	ContiTech Oil & Marine Corp.
Customer Order No	CBC5571164500421193
Item No.	1
Hose Type	Flexible Hose
Standard	API SPEC 16 C
Inside dia in inches	3
Length	35 ft
Type of coupling one end	FLANGE 4.1/16" 10KPSI API SPEC 17D SV SWIVEL FLANGE SOURC/W BX155 ST/ST INLAID R.GR.
Type of coupling other end	FLANGE 4.1/16" 10KPSI API SPEC 17D SV SWIVEL FLANGE SOUR C/W BX155 ST/ST INLAID R.GR.
H2S service NACE MR0175	Yes
Working Pressure	10 000 psi
Design Pressure	10 000 psi
Test Pressure	15 000 psi
Safety Factor	2,25
Marking	USUAL PHOENIX
Cover	NOT FIRE RESISTANT
Outside protection	St.steel outer wrap
Internal stripwound tube	No
Lining	OIL + GAS RESISTANT SOUR
Safety clamp	Yes
Lifting collar	Yes
Element C	Yes
Safety chain	Yes
Safety wire rope	No
Max.design temperature [°C]	100
Min.design temperature [°C]	-20
Min. Bend Radius operating [m]	0,90
Min. Bend Radius storage [m]	0,90
Electrical continuity	The Hose is electrically continuous
Type of packing	WOODEN CRATE ISPM-15



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QUALITY CONTROL INSPECTION AND TEST CERTIFICATE					CERT. N	۷°:	731		
PURCHASER:	ContiTech (Dil & Marine Co	orp.		P.O. N°:		4500300)249	
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HOSE SERIAL Nº:	65346	NOMINAL / AC	TUAL LE	NGTH:		7,62	m / 7,66 m	1	
W.P. 68,9 MPa 10)000 psi	T.P. 103,4	MPa	1500)0 psi	Duration:	60	,	min.
Pressure test with water at ambient temperature \uparrow 10 mm = 10 Min. \rightarrow 10 mm = 20 MPa		See attachme	ent. (1	page	•)				
\rightarrow 10 mm = 20 MPa COUPLINGS Type	-	Serial N°			Quality		· Heat	N° [°]	-
3" coupling with		3428	3433		AISI 413		A103		
4 1/16" API 10K Swivel Fl	ange end				AISI 413	so	034435	5496	51
Hub		·			AISI 413	80	A046	62U	
NOT DESIGN 66 – 1042 All metal parts are flawless							3"		
WE CERTIFY THAT THE ABOVE						THE TERI	MS OF THE OF	RDER	
INSPECTED AND PRESSURE TO STATEMENT OF CONFORMITY conditions and specifications of accordance with the referenced st	: We hereby the above Pure	certify that the abov chaser Order and th	e items/ed	quipmen items/ec	nt supplied	vere fabrica	ted inspected	and teste	ed in
Date:	Inspector		Quality	Contro				<u> </u>	
03. May 2013.			De	ner :	Co	ntiTech R Industrial ality Contro (1)	Kft.	2 es	

ContiTech Rubber Industriai Kft. Budapesti út 10., Szeged H-6728 P.O.Box 152 Szeged H-6701 Hungary

Phone: +36 62 566 737 Fax: +36 62 566 738 e-mail: info@fluid.contitech.hu Interne:: www.contitech-rubber.hu The Court of Csongrád County as Registry Court Registry Court No: HU 06-09-002502 EU VAT No: HU11087209 Bank data Commercial and Creditbank Szeged 10402805-28014250-00000000 ATTACHMENT OF QUALITY CONTROL INSPECTION AND TEST CERTIFICATE

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Hose Data Sheet

CRI Order No.	536555
Customer	ContiTech Oil & Marine Corp.
Customer Order No	4500300249 CBC384527
Item No.	1
Hose Туре	Flexible Hose
Standard	API SPEC 16 C
Inside dia in inches	3
Length	25 ft
Type of coupling one end	FLANGE 4.1/16" 10KPSI API SPEC 17D SV SWIVEL FLANGEC/W BX155 ST/ST INLAID RING GR
Type of coupling other end	FLANGE 4.1/16" 10KPSI API SPEC 17D SV SWIVEL FLANGE C/W BX155 ST/ST INLAID RING GR
H2S service NACE MR0175	Yes
Working Pressure	10 000 psi
Design Pressure	10 000 psi
Test Pressure	15 000 psi
Safety Factor	2,25
Marking	USUAL PHOENIX
Cover	NOT FIRE RESISTANT
Outside protection	St.steel outer wrap
Internal stripwound tube	No
Lining	OIL RESISTANT
Safety clamp	Yes
Lifting collar	Yes
Element C	Yes
Safety chain	Yes
Safety wire rope	No
Max.design temperature [°C]	100
Min.design temperature [°C]	-20
MBR operating [m]	1,60
MBR storage [m]	1,40
Type of packing	WOODEN CRATE ISPM-15

FAFMSS

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

SUPO Data Report

04/02/2019

Highlighted data reflects the most

recent changes

Show Final Text

APD ID: 10400032424

Operator Name: CHISHOLM ENERGY OPERATING LLC

Well Name: ASTEROID 20-29 FED COM WCA

Well Type: CONVENTIONAL GAS WELL

Submission Date: 07/26/2018

Well Number: 2H

Well Work Type: Drill

Section 1 - Existing Roads

Will existing roads be used? YES

Existing Road Map:

ASTEROID_20_29_FED_COM_WCA_2H_ACCESS_ROUTE_MAP_07242018_20180726121129.pdf ASTEROID_20_29_FED_COM_WCA_2H_VICINITY_MAP_07242018_20180726121130.pdf Existing Road Purpose: ACCESS,FLUID TRANSPORT Row(s) Exist? YES

ROW ID(s)

ID: 134601

Do the existing roads need to be improved? NO

Existing Road Improvement Description:

Existing Road Improvement Attachment:

Section 2 - New or Reconstructed Access Roads

Will new roads be needed? YES

New Road Map:

ASTEROID_20_29_FED_COM_WCA_2H_ACCESS_ROUTE_MAP_07242018_20180726121150.pdf ASTEROID_20_29_FED_COM_WCA_2H_SITE_MAP_07242018_20180726121150.pdf

New road type: RESOURCE

Length: 300 Feet Width (ft.): 30

Max slope (%): 2

Max grade (%): 1

Army Corp of Engineers (ACOE) permit required? NO

ACOE Permit Number(s):

New road travel width: 15

New road access erosion control: ROAD WILL BE CROWNED AND DITCHED TO PREVENT EROSION

New road access plan or profile prepared? NO

New road access plan attachment:

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Access road engineering design? NO

Access road engineering design attachment:

Access surfacing type: OTHER

Access topsoil source: BOTH

Access surfacing type description: 6" ROLLED AND COMPACTED CALICHE

Access onsite topsoil source depth: 6

Offsite topsoil source description: SURFACING MATERIAL WILL CONSIST OF NATIVE CALICHE OBTAINED FROM THE WELL SITE IF POSSIBLE. OTHERWISE, CALICHE WILL BE HAULED FROM NEAREST CALICHE PIT Onsite topsoil removal process: GRADING

Access other construction information:

Access miscellaneous information:

Number of access turnouts:

Access turnout map:

Drainage Control

New road drainage crossing: OTHER

Drainage Control comments: WATER WILL BE DIVERTED WHERE NECESSARY TO AVOID PONDING, PREVENT EROSION, MAINTAIN GOOD DRAINAGE, AND BE CONSISTENT WITH LOCAL DRAINAGE PATTERNS **Road Drainage Control Structures (DCS) description:** NO DRAINAGE CONTROL NECESSARY

Road Drainage Control Structures (DCS) attachment:

Access Additional Attachments

Additional Attachment(s):

Section 3 - Location of Existing Wells

Existing Wells Map? YES

Attach Well map:

ASTEROID_20_29_FED_COM_WCA_2H_MILE_RADIUS_MAP_07242018_20180726121206.pdf

Existing Wells description:

Section 4 - Location of Existing and/or Proposed Production Facilities

Submit or defer a Proposed Production Facilities plan? DEFER

Estimated Production Facilities description: If the well is productive, the anticipated facility will consist of a tank battery constructed in accordance with API standards, a flow line will be installed in accordance to the API standards and laid to a 3 phase separator, lines will then be laid from the separator to the tank battery.

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Section 5 - Location and Types of Water Supply

Water Source Table

Water source use type: INTERMEDIATE/PRODUCTION CASING, STIMULATION, SURFACE CASING Describe type:

Source latitude:

Source datum:

Water source permit type: WATER WELL

Source land ownership: PRIVATE

Water source transport method: PIPELINE

Source transportation land ownership: PRIVATE

Water source volume (barrels): 140000

Source volume (acre-feet): 18.045033

Water source type: GW WELL

Source longitude:

Source volume (gal): 5880000

Water source and transportation map:

ASTEROID_20_29_FED_COM_3BS_3H_WATER__MAP_07242018_20180726121300.pdf

Water source comments: Chisholm Energy Operating, LLC has not chosen a water source at this time. Attached is a map showing the #1 option from where we will receive water at this time. New water well? NO

New Water Well I	nfo	
Well latitude:	Well Longitude:	Well datum:
Well target aquifer:		
Est. depth to top of aquifer(ft):	Est thickness	of aquifer:
Aquifer comments:		
Aquifer documentation:	• .	
Well depth (ft):	Well casing type	:
Well casing outside diameter (in.):	Well casing insid	de diameter (in.):
New water well casing?	Used casing sou	Irce:
Drilling method:	Drill material:	· · ·
Grout material:	Grout depth:	
Casing length (ft.):	Casing top dept	h (ft.):
Well Production type:	Completion Mether	nod:
Water well additional information:	· · ·	

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

State appropriation permit:

Additional information attachment:

Section 6 - Construction Materials

Construction Materials description:

Construction Materials source location attachment:

Section 7 - Methods for Handling Waste

Waste type: DRILLING

Waste content description: Drilling Fluids

Amount of waste: 6000 barrels

Waste disposal frequency : Daily

Safe containment description: Steel tanks

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: COMMERCIAL FACILITY Disposal type description:

Disposal location description: Trucked to approved disposal facility. Estimated 6000 bbls total

Waste type: FLOWBACK

Waste content description: Flowback Water

Amount of waste: 25000 barrels

Waste disposal frequency : Daily

Safe containment description: Steel frac tanks

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: COMMERCIAL FACILITY

Disposal type description:

Disposal location description: Haul to approved SWD facility.

Waste type: DRILLING

Waste content description: Cuttings

Amount of waste: 2000 barrels

Waste disposal frequency : Daily

Safe containment description: Steel bins, roll-offs

Safe containmant attachment:

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Waste disposal type: HAUL TO COMMERCIALDisposal location ownership: COMMERCIALFACILITYDisposal type description:

Disposal location description: Truck to an approved disposal facility

Waste type: GARBAGE

Waste content description: Trash and debris

Amount of waste: 200 pounds

Waste disposal frequency : Weekly

Safe containment description: Roll-off bin with netted top

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: COMMERCIAL FACILITY

Disposal type description:

Disposal location description: Truck to commercial waste facility

Waste type: SEWAGE

Waste content description: Human Waste

Amount of waste: 2000 gallons

Waste disposal frequency : Weekly

Safe containment description: Waste will be properly contained and disposed of at a state approve disposal facility

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: COMMERCIAL FACILITY

Disposal type description:

Disposal location description: Haul to a commercial disposal facility

Reserve Pit

Reserve Pit being used? NO

Temporary disposal of produced water into reserve pit?

Reserve pit length (ft.) Reserve pit width (ft.)

Reserve pit depth (ft.)

Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Cuttings Area

Cuttings Area being used? NO

Are you storing cuttings on location? NO

Description of cuttings location

Cuttings area length (ft.)

Cuttings area depth (ft.)

Cuttings area width (ft.)

Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

WCuttings area liner

Cuttings area liner specifications and installation description

Section 8 - Ancillary Facilities

Are you requesting any Ancillary Facilities?: NO

Ancillary Facilities attachment:

Comments:

Section 9 - Well Site Layout

Well Site Layout Diagram:

ASTEROID_20_29_FED_COM_WCA_2H_SITE_MAP_07242018_20180726121521.pdf

Comments:

Section 10 - Plans for Surface Reclamation

Type of disturbance: No New Surface Disturbance Multiple Well Pad Name: ASTEROID 20-29 FED COM

Multiple Well Pad Number: 1H, 2H, 3H

Recontouring attachment:

Drainage/Erosion control construction: Drainage systems, if any, will be reshaped to original configuration with provisions made to alleviate erosion.

Drainage/Erosion control reclamation: Any portion of the site that is not needed for future operations will be reclaimed to the original stat as much as feasible.

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Well pad proposed disturbance	Well pad interim reclamation (acres):	Well pad long term disturbance
(acres): 0 Road proposed disturbance (acres): 0	Road interim reclamation (acres):	(acres): Road long term disturbance (acres):
Powerline proposed disturbance (acres): 0 Pipeline proposed disturbance (acres): 0 Other proposed disturbance (acres): 0	0 Pipeline interim reclamation (acres): Other interim reclamation (acres):	Powerline long term disturbance (acres): 0 Pipeline long term disturbance (acres): Other long term disturbance (acres):
Total proposed disturbance: 0	Total interim reclamation:	Total long term disturbance:
Disturbance Comments:		
•	plans to drill additional wells on the well pa	

planned at this time. Any portion of the site that is not needed for future operation and production operations will be recontoured to the original state as much as possible.

Topsoil redistribution: After the area has been shaped and contoured, topsoil from the stockpile will be placed over the disturbed area to the extent possible.

Soil treatment: NO treatment necessary.

Existing Vegetation at the well pad: Mesquite, shinnery oak

Existing Vegetation at the well pad attachment:

Existing Vegetation Community at the road: Mesquite, shinner oak

Existing Vegetation Community at the road attachment:

Existing Vegetation Community at the pipeline: Mesquite, shinnery oak

Existing Vegetation Community at the pipeline attachment:

Existing Vegetation Community at other disturbances: None.

Existing Vegetation Community at other disturbances attachment:

Non native seed used? NO

Non native seed description:

Seedling transplant description:

Will seedlings be transplanted for this project? NO

Seedling transplant description attachment:

Will seed be harvested for use in site reclamation? NO

Seed harvest description:

Seed harvest description attachment:

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Seed Table			
Seed type: PERENNIAL	GRASS	Seed source: COMMERCIAL	
Seed name: LPC-Seed N	Mix 2		
Source name:		Source address:	
Source phone:	· .		
Seed cultivar:			
Seed use location: WEL	L PAD,WELL PAD		
PLS pounds per acre: 5	; .	Proposed seeding season: SPRING	
Seed S	Summary	Total pounds/Acre: 5	•
Seed Type	Pounds/Acre		
PERENNIAL GRASS	5		
d reclamation attachme	nt.		
u reolamation attaonne			
Operator Contact/	·	ial Contact Info	
Operator Contact/	·		
rst Name: Jennifer	·	Last Name: Elrod	
Operator Contact/ irst Name: Jennifer hone: (817)953-3728	·		
irst Name: Jennifer hone: (817)953-3728	Responsible Offic	Last Name: Elrod	
i rst Name : Jennifer	Responsible Offic	Last Name: Elrod	
i rst Name : Jennifer hone: (817)953-3728 dbed prep: Rip and add t	Responsible Offic	Last Name: Elrod	
i rst Name : Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP:	Responsible Offic topsoil	Last Name: Elrod	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method:	Responsible Offic topsoil	Last Name: Elrod	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species? I	Responsible Offic	Last Name: Elrod	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species? I sting invasive species tr sting invasive species tr	Responsible Offic	Last Name: Elrod	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species? I sting invasive species tr sting invasive species tr	Responsible Offic	Last Name: Elrod Email: jelrod@chisholmenergy.com	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species ? I sting invasive species tr sting invasive species tr sting invasive species tr	Responsible Offic	Last Name: Elrod Email: jelrod@chisholmenergy.com onitored and weeds will be treated.	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species tr sting invasive species tr sting invasive species tr ed treatment plan descri	Responsible Offic	Last Name: Elrod Email: jelrod@chisholmenergy.com onitored and weeds will be treated.	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species? I sting invasive species tr sting invasive species tr ed treatment plan descri ed treatment plan attach	Responsible Offic	Last Name: Elrod Email: jelrod@chisholmenergy.com onitored and weeds will be treated.	
irst Name: Jennifer hone: (817)953-3728 dbed prep: Rip and add t d BMP: d method: sting invasive species? I sting invasive species tr sting invasive species tr ed treatment plan description hitoring plan description	Responsible Offic topsoil NO eatment description: eatment attachment: ption: All areas will be m ment: : Monitor after final reclai	Last Name: Elrod Email: jelrod@chisholmenergy.com onitored and weeds will be treated.	

Well Name: ASTEROID 20-29 FED COM WCA

Well Number: 2H

Section 11 - Surface Ownership

Disturbance type: WELL PAD

Describe:

Surface Owner: BUREAU OF LAND MANAGEMENT

Other surface owner description:

BIA Local Office:

BOR Local Office:

COE Local Office:

DOD Local Office:

NPS Local Office:

State Local Office:

Military Local Office:

USFWS Local Office:

Other Local Office:

Other Local Office:

USFS Region:

USFS Region:

USFS Forest/Grassland:

USFS Ranger District:

Disturbance type: EXISTING ACCESS ROAD Describe: Surface Owner: BUREAU OF LAND MANAGEMENT,STATE GOVERNMENT Other surface owner description: BIA Local Office: BOR Local Office: COE Local Office: DOD Local Office: NPS Local Office: State Local Office: NM SLO Military Local Office: USFWS Local Office: **Operator Name:** CHISHOLM ENERGY OPERATING LLC **Well Name:** ASTEROID 20-29 FED COM WCA

Well Number: 2H

USFS Forest/Grassland:

USFS Ranger District:

Section 12 - Other Information

Right of Way needed? NO

Use APD as ROW?

ROW Type(s):

ROW Applications

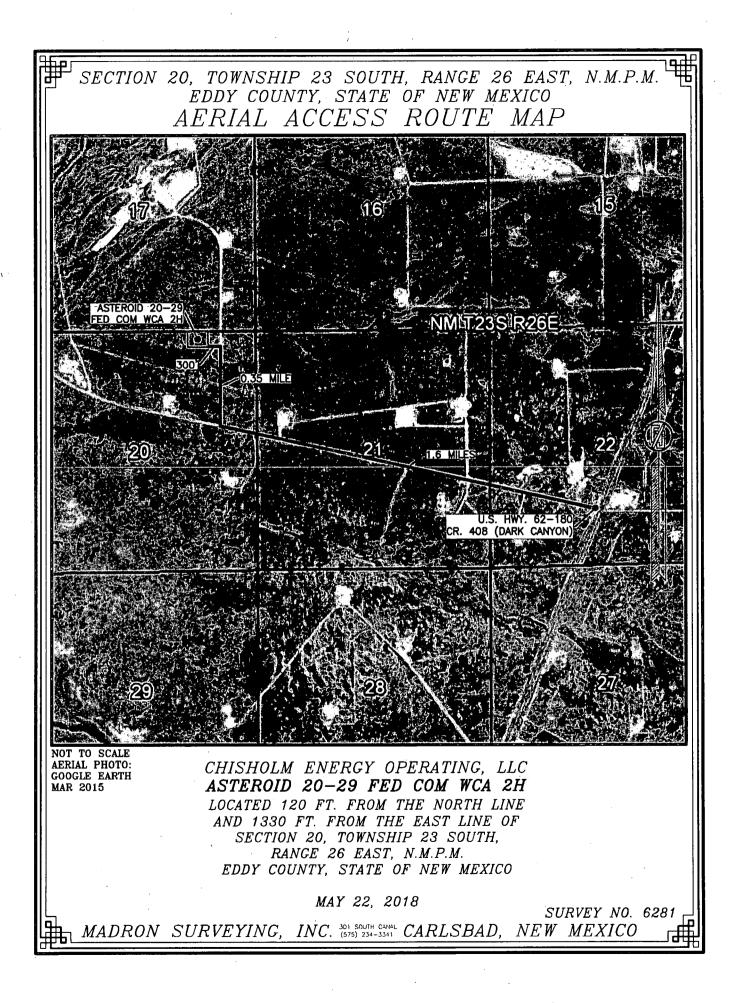
SUPO Additional Information: GCP ATTACHED APD RECEIPT ATTACHED

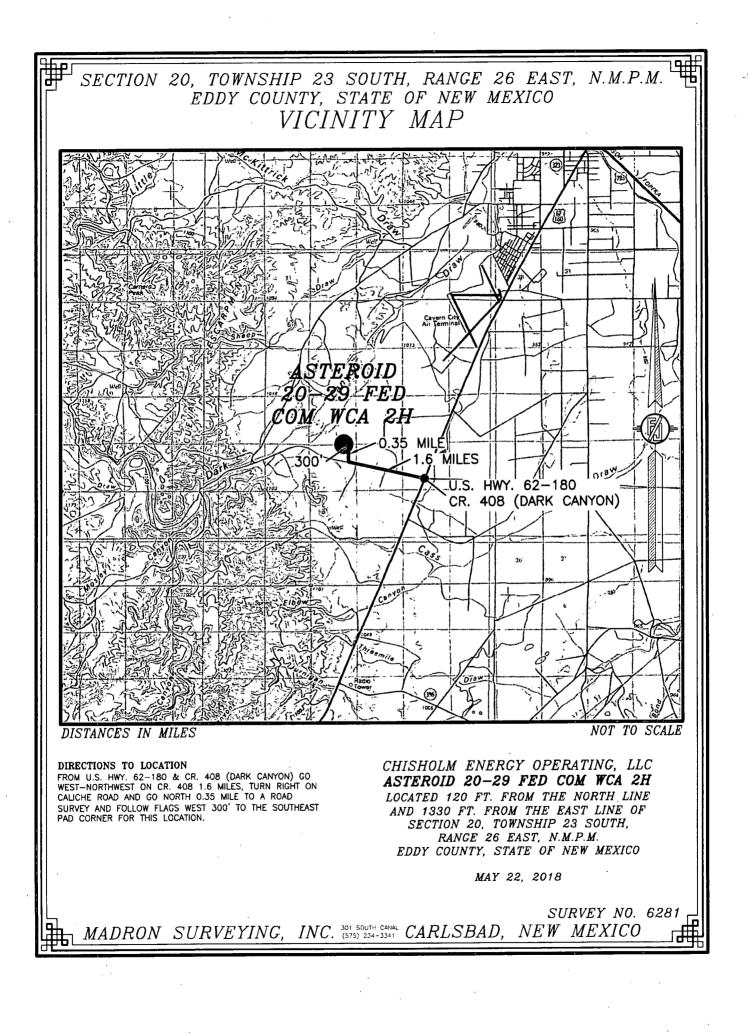
Use a previously conducted onsite? YES

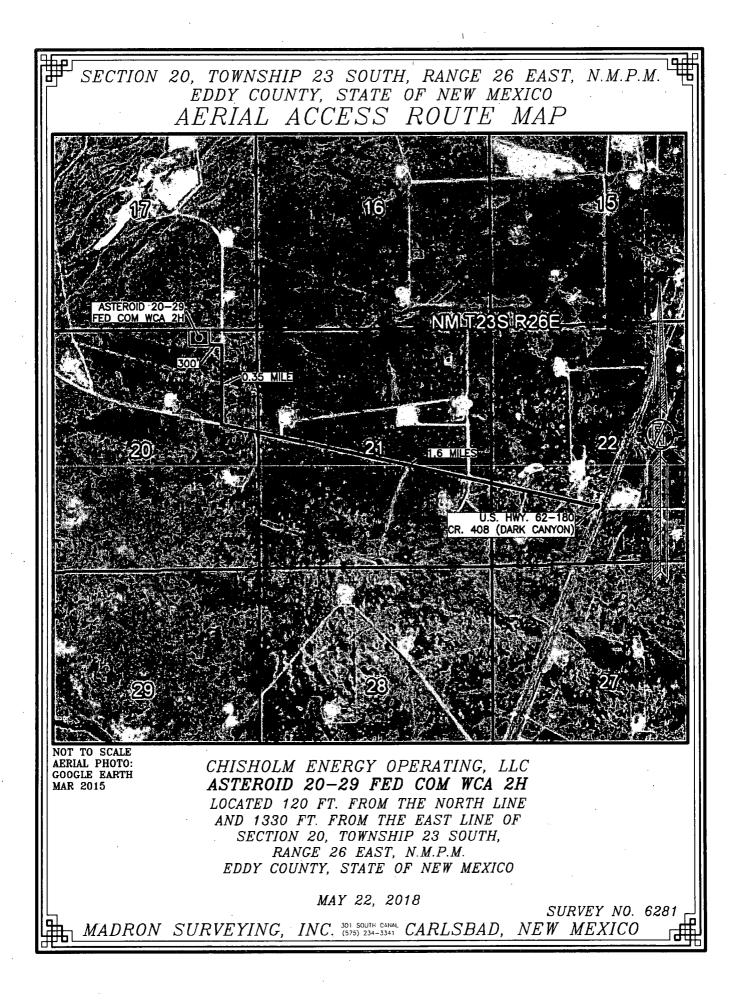
Previous Onsite information: ONSITE CONDUCTED 05/22/2018

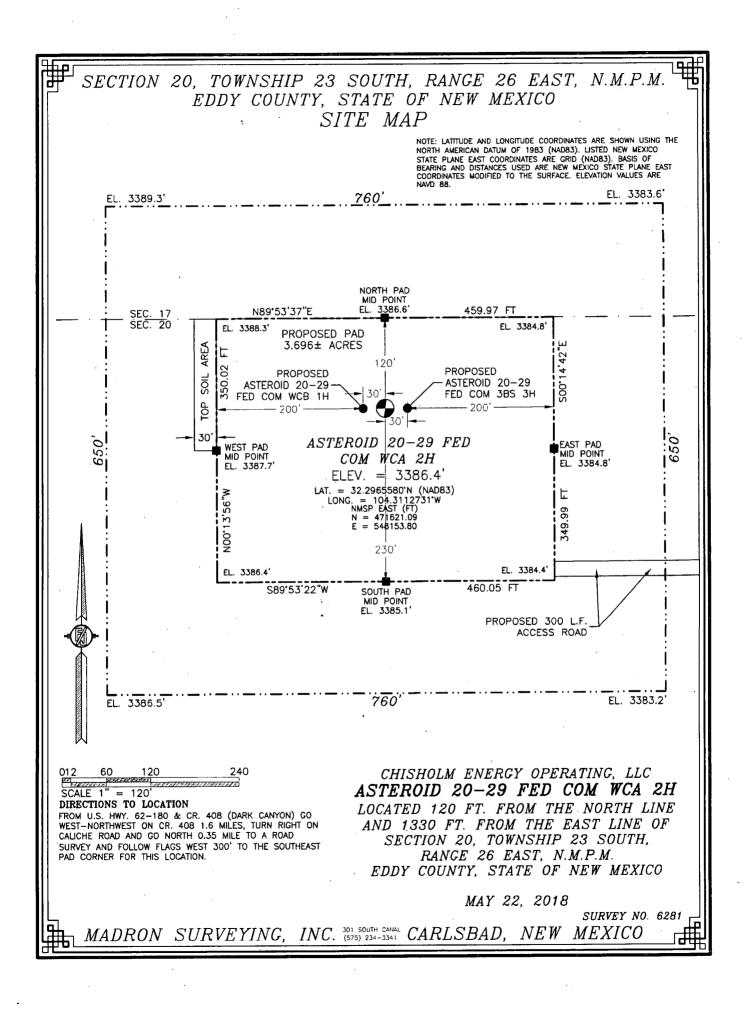
Other SUPO Attachment

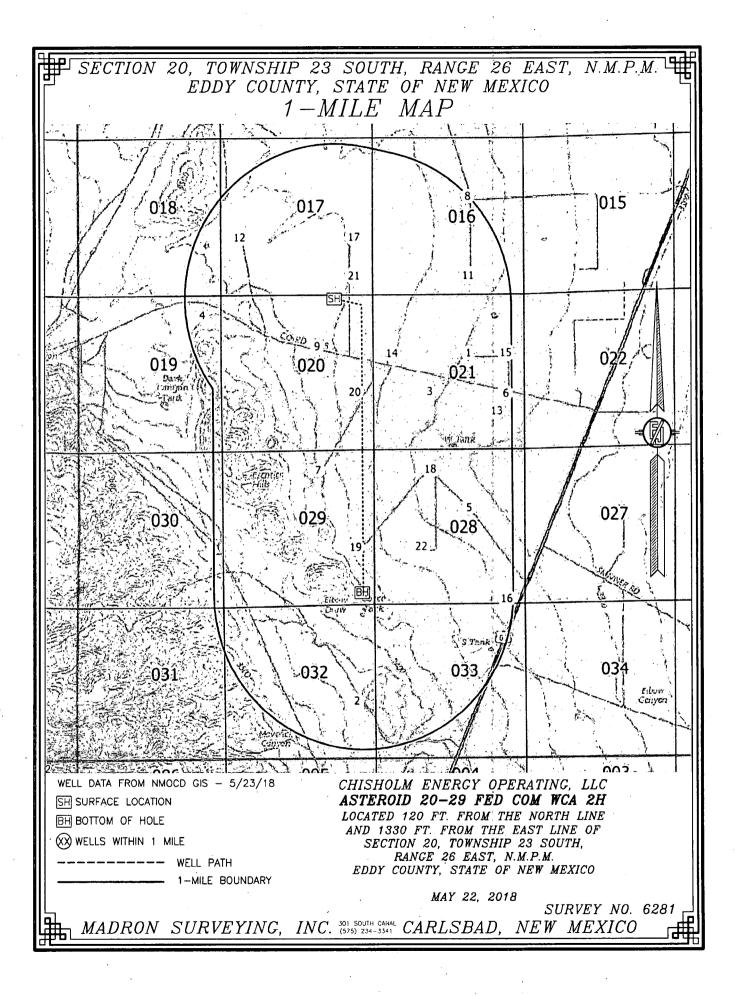
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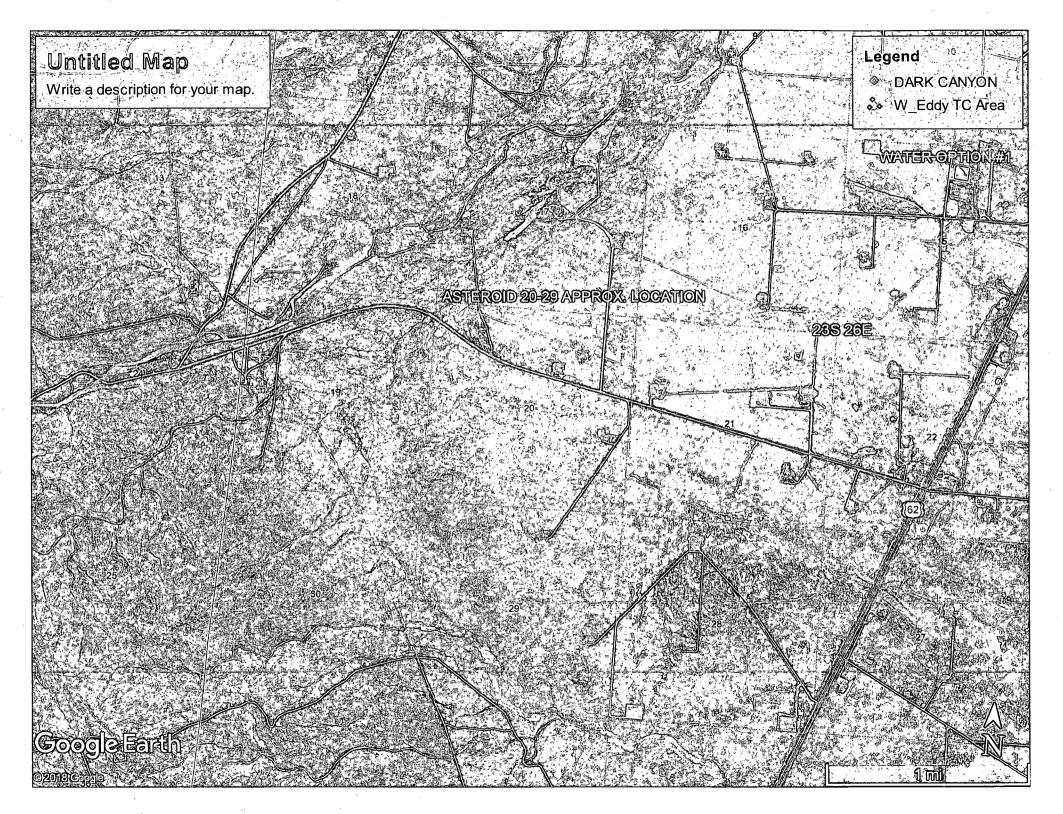


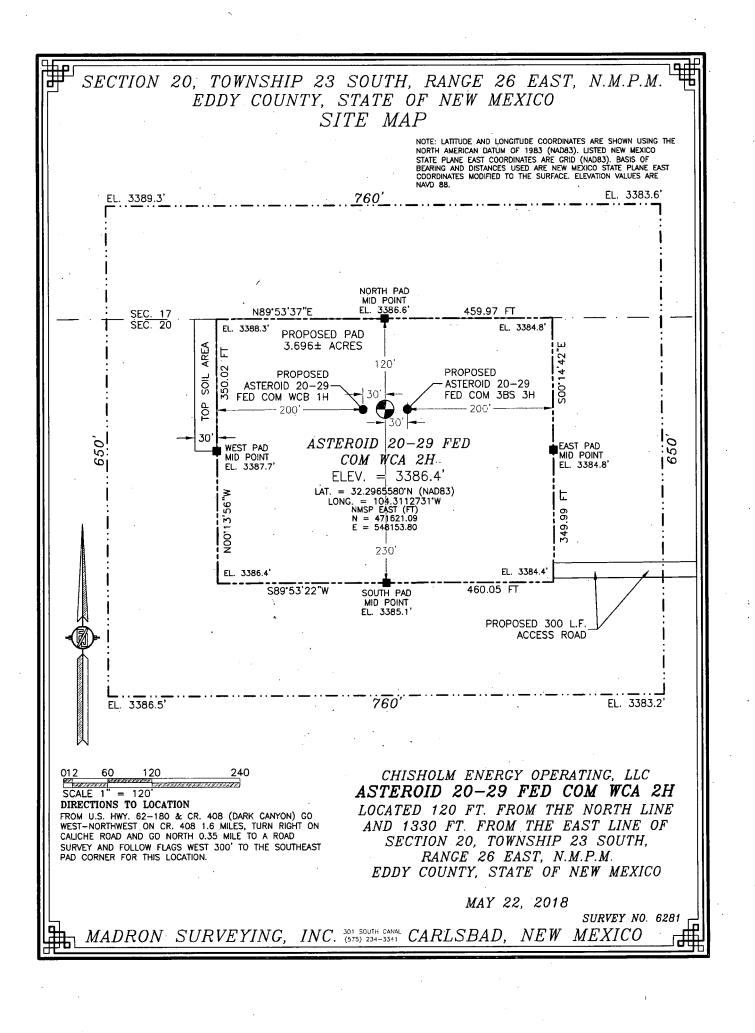


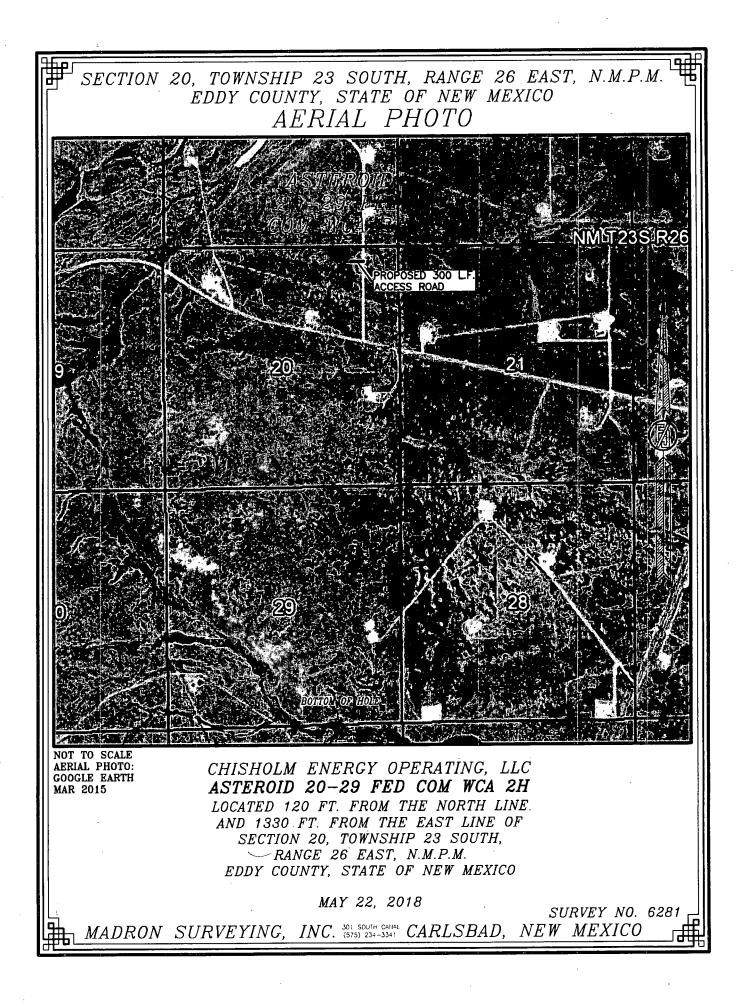














Receipt

Your payment is submitted

Pay.gov Tracking ID: 26B665Q1 Agency Tracking ID: 75537646408 Form Name: Bureau of Land Management (BLM) Application for Permit to Drill (APD) Fee Application Name: BLM Oil and Gas Online Payment

Payment Information

Payment Type: Bank account (ACH) Payment Amount: \$68,530.00 Transaction Date: 07/25/2018 04:09:27 PM EDT Payment Date: 07/26/2018 Company: CHISHOLM ENERGY OPERATING, LLC APD IDs: 10400032174, 10400032218, 10400032219, 10400032423, 10400032424, 10400032426, 10400032427 Lease Numbers: NMNM097120, NMNM097120, NMNM097120, NMNM070200, NMNM070200, NMNM070200, NMNM113944 Well Numbers: 6H, 5H, 4H, 3H, 2H, 1H, 13H

Note: You will need your Pay.gov Tracking ID to complete your APD transaction in AFMSS II. Please ensure you write this number down upon completion of payment.

Account Information

Account Holder Name: CHISHOLM ENERGY OPERATING, LLC Routing Number: 114000093 Account Number: *********************************

Email Confirmation Receipt

Confirmation Receipts have been emailed to: jelrod@chisholmenergy.com amccullough@chisholmengergy.com **FMSS**

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Section 1 - General

Would you like to address long-term produced water disposal? NO

Section 2 - Lined Pits

Would you like to utilize Lined Pit PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Lined pit PWD on or off channel:

Lined pit PWD discharge volume (bbl/day):

Lined pit specifications:

Pit liner description:

Pit liner manufacturers information:

Precipitated solids disposal:

Decribe precipitated solids disposal:

Precipitated solids disposal permit:

Lined pit precipitated solids disposal schedule:

Lined pit precipitated solids disposal schedule attachment:

Lined pit reclamation description:

Lined pit reclamation attachment:

Leak detection system description:

Leak detection system attachment:

Lined pit Monitor description:

Lined pit Monitor attachment:

Lined pit: do you have a reclamation bond for the pit?

Is the reclamation bond a rider under the BLM bond?

Lined pit bond number:

Lined pit bond amount:

Additional bond information attachment:

PWD disturbance (acres):

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Section 3 - Unlined Pits

Would you like to utilize Unlined Pit PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Unlined pit PWD on or off channel:

Unlined pit PWD discharge volume (bbl/day):

Unlined pit specifications:

Precipitated solids disposal:

Decribe precipitated solids disposal:

Precipitated solids disposal permit:

Unlined pit precipitated solids disposal schedule:

Unlined pit precipitated solids disposal schedule attachment:

Unlined pit reclamation description:

Unlined pit reclamation attachment:

Unlined pit Monitor description:

Unlined pit Monitor attachment:

Do you propose to put the produced water to beneficial use?

Beneficial use user confirmation:

Estimated depth of the shallowest aquifer (feet):

Does the produced water have an annual average Total Dissolved Solids (TDS) concentration equal to or less than that of the existing water to be protected?

TDS lab results:

Geologic and hydrologic evidence:

State authorization:

Unlined Produced Water Pit Estimated percolation:

Unlined pit: do you have a reclamation bond for the pit?

Is the reclamation bond a rider under the BLM bond?

Unlined pit bond number:

Unlined pit bond amount:

Additional bond information attachment:

Section 4 - Injection

Would you like to utilize Injection PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Injection PWD discharge volume (bbl/day):

Injection well mineral owner:

PWD disturbance (acres):

PWD disturbance (acres):

Injection well type:

Injection well number:

Assigned injection well API number?

Injection well new surface disturbance (acres):

Minerals protection information:

Mineral protection attachment:

Underground Injection Control (UIC) Permit?

UIC Permit attachment:

Section 5 - Surface Discharge

Would you like to utilize Surface Discharge PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Surface discharge PWD discharge volume (bbl/day):

Surface Discharge NPDES Permit?

Surface Discharge NPDES Permit attachment:

Surface Discharge site facilities information:

Surface discharge site facilities map:

Section 6 - Other

Would you like to utilize Other PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Other PWD discharge volume (bbl/day):

Other PWD type description:

Other PWD type attachment:

Have other regulatory requirements been met?

Other regulatory requirements attachment:

Injection well name:

Injection well API number:

PWD disturbance (acres):

PWD disturbance (acres):

FAFMSS

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Bond Information

Federal/Indian APD: FED

BLM Bond number: NMB001468

BIA Bond number:

Do you have a reclamation bond? NO

Is the reclamation bond a rider under the BLM bond?

Bond Info Data Report

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Is the reclamation bond BLM or Forest Service?

BLM reclamation bond number:

Forest Service reclamation bond number:

Forest Service reclamation bond attachment:

Reclamation bond number:

Reclamation bond amount:

Reclamation bond rider amount:

Additional reclamation bond information attachment: