

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special					Test Date 11-24-81		RECEIVED				
Company Mesa Petroleum Co.				Connection Unconnected			JAN 4 1982				
Pool Undesignated ABO				Formation ABO			O. C. D.				
Completion Date 11-24-81		Total Depth 4814		Plug Back TD 4794		Elevation 3738		ARJESIA OFFICE			
Csg. Size 4 1/2		Wt. 1.5#		Set At 4810		Perforations: From 4404 To 4777		Well No. 6			
Tbg. Size 2 3/8		Wt. 4.7#		Set At 4290		Perforations: From open ended To		Unit Sec. Twp. Rge. J 29 8S 26E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single					Packer Set At None		County Chaves				
Producing Thru tubing 4290		Reservoir Temp. *F 102 @ 4814		Mean Annual Temp. *F 60		Baro. Press. - P _a 13.2		State New Mexico			
L 4290		H 4290		G _g .65		% CO ₂ 1		% N ₂ 1			
						% H ₂ S		Prover 2" ORIFICE WELL TESTER			
								Meter Run Taps			
FLOW DATA					TUBING DATA			CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.		Temp. *F
SI							900		860		48 hr SI
1.	2" ORIFICE		1 1/4	10		20	790	58	760		1 hr.
2.	Well		1 1/4	22		20	650	61	635		1 hr.
3.	Tester		1 1/4	23		40	360	62	530		1 hr.
4.			1 1/4	24		47	250	63	450		1 hr.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcid				
1	753	2" ORIFICE	WELL	1.0409	.9608		753				
2	1320	TESTER		1.04708	.9608		1320				
3	1348			1.0198	.9608		1321				
4	1390			1.0127	.9608		1352				
5											
NO.	P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.		A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.				
1					Specific Gravity Separator Gas _____		X X X X X X X X X				
2					Specific Gravity Flowing Fluid _____		X X X X X				
3					Critical Pressure _____ P.S.I.A.		_____ P.S.I.A.				
4					Critical Temperature _____ R		_____ R				
5											
P _c 873		P _c ² 762		(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3905$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1792$					
NO.	P _w	P _w ²	P _w ²	P _c ² - P _w ²							
1	773	598	164								
2	648	420	342								
3	543	295	467								
4	463	214	548								
5											
Absolute Open Flow 1600 Mcid @ 15.025					Angle of Slope θ 63.5°		Slope, n .5				
Remarks: Plot of P _c ² - P _w ² vs. Q yielded a straight line with a θ greater than 63.5°. Drew 63.5° line through highest point.											
Approved By Commission:			Conducted By: James Craig			Calculated By: E.L. Buttross, Jr.			Checked By:		