

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-68

RECEIVED

Type Test ☐ Initial ☒ Annual ☒ Special				Test Date 1-28-73		FEB 12 1973	
Company Hanagan Petroleum Corp.				Connection Llano Gas Co.		O.C.C.	
Pool Catclaw Draw				Formation Morrow		Unit ARTESIA, OFFICE	
Completion Date 8-4-72		Total Depth 10770		Plug Back TD 10701		Elevation 3375 GL	
Csg. Size 5 1/2		Wt. 17 -20		Perforations: From 10633 To 10698		Well No. 4	
Thg. Size 2 7/8		Wt. 6.5#		Perforations: From To		Unit Sec. Twp. Rge. G 24 21S 25E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10584		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 179 @ 10500		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2	
L 10666		H 10666		Gg 0.600		% CO ₂ % N ₂ % H ₂ S Prover X	
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Duration of Flow
SI							
1.	4"	X	2.250	725	4.5	96	60 min.
2.	4"	X	2.250	740	12.5	80	60 min.
3.	4"	X	2.250	760	26	69	60 min.
4.	4"	X	2.250	800	53	66	60 min.
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.	25.64	57.6	738.2	.9671	1.291	1.049	1934.3
2.	25.64	97.0	753.2	.9813	1.291	1.056	3327.2
3.	25.64	141.8	773.2	.9915	1.291	1.059	4928.4
4.	25.64	207.6	813.2	.9943	1.291	1.061	7249.4
5.							
NO.	P _t	Temp. °R	T _t	Z	Dry Gas		
1.	Simplified				Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.		
2.	Supercompressibility				A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.		
3.	Tables Used				Specific Gravity Separator Gas 0.600 XXXXXXXXXX		
4.					Specific Gravity Flowing Fluid XXXXXX		
5.					Critical Pressure 671 P.S.I.A. _____ P.S.I.A.		
					Critical Temperature 358 R _____ R		
$P_f = 3975.2$ $P_f^2 = 15802$							
NO.	P_t^2	P_s^2	$P_s^2 - P_t^2$	$(1) \frac{P_c^2}{P_c^2 - P_w^2} =$			
1.	3765.2	14177	1625	$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$			
2.	3593.2	12911	2891	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$			
3.	3301.2	10898	4904				
4.	2809.2	7892	7910				
5.							
Absolute Open Flow 13,000 Mcfd @ 15.025				Angle of Slope @ 50° 10'		Slope, n 0.83438	
Remarks: BHP measured with Amerada RPG-3 gauge.							
Approved By Commission:		Conducted By:		Calculated By:		Checked By:	
		Tefteller, Inc.		F. Tefteller			