

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual		RECEIVED Special 1-7-74	
Company Texas Oil & Gas Corp.		Connection None	
Pool Burton Flat		Formation Morrow	
Completion Date 1-7-74	Total Depth 11,760	Plug Back Pressure 11,659	Elevation 3279 GL
Farm or Lease Name Williamson Federal		Well No. 1	
Csg. Size 4 1/2"	Wt. 13.5	Set At 11,735	Perforations: From 11,412 To 11,552
Tub. Size 2 3/8"	Wt. 4.7	Set At 11,367	Perforations: From To
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single		Packer Set At 11,367	County Eddy
Producing Thru Tubing	Reservoir Temp. °F @	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2
State New Mexico		Unit Sec. Twp. Rge. E 9 20-S 29-E	
L 11,367	H 11,367	G _g 0.588	% CO ₂ 0.10
% N ₂ 0.91	% H ₂ S -	Proven Positive	Meter Run Taps
Choke			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X Orifice size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	0					2595		Packer		72 hrs
1.	15/64		1990	1.483	74	2003				60"
2.	19/64		1832	1.494	78	1845				60"
3.	11/32		1667	1.489	76	1680				60"
4.	13/32		1543	1.50	79	1556				60"
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Choke Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.9165		2003	.9868	1.304	1.136	2683
2	1.484		1845	.9831	1.304	1.129	3962
3	1.999		1680	.9850	1.304	1.125	4853
4	2.794		1556	.9822	1.304	1.115	6208
5							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcfd/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	Dry	Deg.
2.					Specific Gravity Separator Gas	0.588	XXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXX	
4.					Critical Pressure	672	P.S.I.A.
5.					Critical Temperature	360	R

P _c	3595	P _c ²	12,924	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	4012	3244.7	10,528	2396
2	3404	3086.1	9,524	3400
3	2822	2920.4	8,529	4395
4	2421	2797.1	7,824	5100
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.801$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 15060$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right] = 3.801$

Absolute Open Flow	15,060	Mcfd @ 15.025	Angle of Slope θ	45	Slope, n	1
Remarks:						

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
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