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appropriate district office
See Rule 401 & Rule 1122

OIL CONSERVATION DIVISION

P.O. Box 2088

Santa Fe, New Mexico 87504-2088

OIL CONDIV.

Form C-122
Revised 4-1-91

FEB 29 1996

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator TEXACO EXPLORATION						Lease or Unit Name E.J. LEVERS FEDERAL NCT-1					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-13-96			Well No. 2		
Completion Date 1-8-96		Total Depth 10600		Plug Back TD 10550		Elevation			Unit Lr. - Sec. - TWP - Rge. F 12-21S-25E		
Csg. Size 5 1/2	Wt. 17	d 4.892	Set At 10600	Perforations: From: 10236 To: 10272			County EDDY				
Tbg. Size 2-3/8	Wt. 4.7	d 1.995	Set At 10180	Perforations: From: To:			Pool Edwards				
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single						Packer Set At 10180			Formation MORROW		
Producing Thru 186		Reservoir Temp. °F 175		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2			Connection ATMOSPHERE		
L 10236	H 10236	G _g .585	% CO ₂ .85	% N ₂ .50	% H ₂ S	Prover		Meter Run 4.026	Taps 6lg.		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						2900				
1.	4.026 X	2.250	490	4	82	2755		PKR		60 min
2.	4.026 X	2.250	480	8	81	2690				60 min
3.	4.026 X	2.250	540	18	69	2460				60 min
4.	4.026 X	2.250	540	32	61	2160				60 min
5.	4.026 X	2.250	570	44	60	1955				30 min

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	25.64	44.86	503.2	.9795	1.307	1.040	1531
2.	25.64	62.81	493.2	.9813	1.307	1.039	2146
3.	25.64	99.79	553.2	.9915	1.307	1.044	3462
4.	25.64	133.05	553.2	.9990	1.307	1.044	4650
5.	25.64	160.19	583.2	1.0000	1.307	1.046	5615

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.75	542	1.55	.925	152.047	48.1	.585	.7883	672	350
2.	.73	541	1.55	.927						
3.	.82	529	1.51	.918						
4.	.82	521	1.49	.918						
5.	.87	520	1.49	.914						

P_c 2913.2 P_c² 8486.7

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.	2770.8	7677.5	809.2	
2.	2728.4	7444.1	1042.7	
3.	2543.4	6468.7	2018.0	
4.	2313.4	5352.3	3134.4	
5.	2188.6	4790.0	3696.7	

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.708$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.040$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 9,484$

Absolute Open Flow **9,484** Mcfd @ 15.025 Angle of Slope θ **54.5°** Slope, n **.71557**

Remarks: **4 BBLS 48.1 API GRAV. OIL MADE DURING TEST**

Approved By Division	Conducted By: PRO WELL TESTER	Calculated By: KS	Checked By: BM
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