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appropriate district office
See Rule 401 & Rule 1122

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Nearburg Producing Company						Lease or Unit Name Black River 3 Federal Com					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 04/08/97		Well No. 1			
Completion Date 01/24/97		Total Depth 11832		Plug Back TD 11730		Elevation 3340' GL		Unit Ltr. - Sec. - TWP - Rge. K 3 24s 26e			
Csg. Size 5 1/2	Wt. 23#	d 4.670	Set At 11832	Perforations: From: 11310 To: 11406				County Eddy			
Tbg. Size 2 7/8	Wt. 6.5#	d 2.441	Set At 11237	Perforations: From: OPEN To: ENDED				Pool <i>Morrow</i> South Carlsbad			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 11237		Formation Morrow			
Producing Thru Tbg		Reservoir Temp. °F 186 @ 11237		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection EPNG			
L 11237	H 11237	Gg 0.580	% CO ₂ 1.14	% N ₂ 0.16	% H ₂ S	Prover		Meter Run 4.026		Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice X Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						1556		PACKER		24 Hrs
1.	4.026 x 2.500		359	2.89	82	1519				1 Hr
2.	4.026 x 2.500		384	13.00	82	1423				1 Hr
3.	4.026 x 2.500		397	24.01	78	1293				1 Hr
4.	4.026 x 2.500		410	38.40	78	1113				1 Hr
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv} .	Rate of Flow Q, Mcfd
1.	32.64	32.80	372.2	.9795	1.313	1.026	1413
2.	32.64	71.86	397.2	.9795	1.313	1.028	3101
3.	32.64	99.24	410.2	.9831	1.313	1.028	4298
4.	32.64	127.48	423.2	.9831	1.313	1.030	5532
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.	.55	542	1.55	.950	A.P. I. Gravity of Liquid Hydrocarbons	Dry	Deg.
2.	.58	542	1.55	.947	Specific Gravity Separator Gas	.580	XXXXXXXXXX
3.	.60	538	1.54	.946	Specific Gravity Flowing Fluid	XXXXXX	
4.	.62	538	1.54	.943	Critical Pressure	* 676	P.S.I.A. P.S.I.A.
5.					Critical Temperature	* 349	R R

P_c 1569.2 P_c² 2462.4

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.		1539.5	2370.1	92.3
2.		1473.5	2171.2	291.2
3.		1384.2	1916.1	546.2
4.		1272.9	1620.2	842.2
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.924$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 10.682$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.931$

Absolute Open Flow	10,682	Mcf @ 15.025	Angle of Slope θ	58.46	Slope, n	.6135
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Remarks: * Corrected To 1.14% CO₂

No Fluid Produced

Approved By Division	Conducted By: Jarrel Services, Inc.	Calculated By: Bob Murray	Checked By: Bob Murray
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