NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 8-22-73	
Company: Keesee & Thomas		Connection: Waiting on Pipeline			
Pool: Ballard P. C.		Formation: Pictured Cliffs Ext.		Unit:	
Completion Date: 8-6-73	Total Depth: 3287'	Plug Back TD: 3194'	Elevation: 7401'GR	Farm or Lease Name: Chacon Jicarilla	
Csg. Size: 4.500 / Wt.: 9.500 / d: 4.090 / Set At: 3266		Perforations: From 3118 To 3178		Well No.: 4	
Tbg. Size: 1.900 / Wt.: 2.900 / d: 1.610 / Set At: 3157		Perforations: From 3154 To 3157		Unit: C / Sec.: 22 / Twp.: 23N / Rge.: 3W	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: None		County: Sandoval	
Producing Thru: Tubing	Reservoir Temp. °F: 109 @ 3287	Mean Annual Temp. °F: --	Baro. Press. – P_a: 12.0	State: New Mexico	
L: 3154 / H: 3154 / Gg: 0.600	% CO_2: --	% N_2: --	% H_2S: --	Prover: --	Meter Run: -- / Taps: --

FLOW DATA

NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI						730		730		8 da.
1.	3/4"T.C.				60	130		530		3 hr.
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		142	1.0000	1.0000	1.0000	1,756
2.							
3.							
4.							
5.							

AUG 24 1973
OIL CON. COM.
DIST. 3

NO.	P_t	Temp. °R T_r	Z
1.			
2.			
3.			
4.			
5.			

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 742 P_c^2 550,564

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		542	293,764	256,800
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.1439$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.9121$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3,358$

Absolute Open Flow 3,358 Mcfd @ 15.025 | Angle of Slope θ _____ | Slope, n 0.85

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Ewell N. Walsh	Ewell N. Walsh	