



STATE OF NEW MEXICO  
ENERGY, MINERALS and NATURAL RESOURCES DEPARTMENT  
OIL CONSERVATION DIVISION  
AZTEC DISTRICT OFFICE

1000 RIO BRAZOS ROAD  
AZTEC, NEW MEXICO 87410  
(505) 334-6178

November 5, 1991

Mr. Joe H. Cox  
Mallon Oil Company  
1099 18th St  
Suite 2740  
Denver CO 80202

Re: Deliverability Test

Dear Joe:

The conditions you described for the Davis-Federal Com 3 #15 are not unusual for many wells in the Blanco Mesaverde Pool. The calculated deliverability is not intended to equal the tested flow rate. The big difference between your calculated deliverability and your producing rate is caused by the difference in your shut-in and flowing pressures.

I have attached an example of how the test is to be calculated.

Sincerely,

A handwritten signature in dark ink, appearing to read "Frank Chavez".

Frank Chavez, District Supervisor

FC:sh

Enc

**RECEIVED**

OCT 28 1991

State of New Mexico  
Energy, Minerals and Natural Resources Department

APR 25 1991

Form C-122-A  
Revised 4-1-91**OIL CON. DIV**  
DIST. 3**OIL CONSERVATION DIVISION****OIL CON. DIV.**  
DIST. 3

P.O. Box 2088

Santa Fe, New Mexico 87504-2088

RECEIVED JUL 29 1991

WELL DELIVERABILITY TEST REPORT FOR 1990 (Re-Test)

POOL NAME <u>Blanco - Mesaverde</u>	POOL SLOPE <u>0.75</u>	FORMATION <u>Mesaverde</u>	COUNTY <u>Rio Arriba</u>
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OPERATOR <u>Mallon Oil Company</u>				WELL NAME AND NUMBER <u>Davis - Federal Comm. 3 #15</u>		
UNIT LETTER <u>0</u>	SECTION <u>3</u>	TOWNSHIP <u>25 N</u>	RANGE <u>2 W</u>	PURCHASING PIPELINE <u>Phelps Dodge Refining Company</u>		
CASING O.D. - INCHES <u>5.5</u>	CASING I.D. - INCHES <u>4.892</u>	SET AT DEPTH - FEET <u>8277</u>		TUBING O.D. - INCHES <u>2.875</u>	TUBING I.D. - INCHES <u>2.441</u>	TOP - TUBING PERF. - FEET <u>3481</u>
GAS PAY ZONE FROM <u>5433'</u> TO <u>5798'</u>		WELL PRODUCING THRU <u>Casing</u>		GAS GRAVITY <u>0.684</u>		GRAVITY X LENGTH <u>3481</u>
DATE OF FLOW TEST FROM <u>12/16/90</u> TO <u>12/23/90</u>				DATE SHUT-IN PRESSURE MEASURED <u>12/31/90</u>		

## PRESSURE DATA - ALL PRESSURES IN PSIA

(a) Flowing Casing Pressure (DWt) <u>97.77</u>	(b) Flowing Tubing Pressure (DWt) <u>N/A</u>	(c) Flowing Meter Pressure (DWt) <u>67.9</u>	(d) Flow Chart Static Reading <u>67.9</u>	(e) Meter Error (Item c - Item d) <u>0</u>	(f) Friction Loss (a - c) or (b - c) <u>29.87</u>	(g) Average Meter Pressure (Integr.) <u>67.9</u>
(h) Corrected Meter Pressure (g + e) <u>67.9</u>	(i) Avg. Wellhead Press. $P_1 = (h + f)$ <u>97.77</u>	(j) Shut-in Casing Pressure (DWt) <u>1307</u>	(k) Shut-in Tubing Pressure (DWt) <u>1307</u>	(l) $P_c$ = higher value of (j) or (k) <u>1307</u>	(m) Del. Pressure $P_d = 70\% P_c$ <u>(914.9)</u>	(n) Separator or Dehydrator Pr. (DWt) for critical flow only

## FLOW RATE CORRECTION ( METER ERROR)

Integrated Volume - MCF/D <u>326.6</u>	Quotient of $\frac{\text{Item c}}{\text{Item d}} = 1$	$\sqrt{\frac{\text{Item c}}{\text{Item d}}} = 1$	Corrected Volume <u>Q = 326.6 MCF/D</u>
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## WORKING PRESSURE CALCULATION

$(1 - e^{-R})$ <u>0.292344</u>	$(F_c Q_m)^2 (1000)$ <u>439.192</u>	$R^2 = (1 - e^{-R}) (F_c Q_m)^2 (1000)$ <u>128.3949</u>	$P_i^2$ <u>996,112.5854</u>	$P_w^2 = P_i^2 + R^2$ <u>996,241</u>	$P_w = \sqrt{P_w^2}$ <u>998.1187</u>
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## DELIVERABILITY CALCULATION

$$D = Q \left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n = 326.6 \left[ \frac{1,708,249 - 837,042.01}{1,708,249 - 996,241} \right]^n = \left( \frac{871,206.99}{712,008.0} \right)^n = 1.2236 = 1.1634 = 379.97 \text{ MCF/D}$$

## REMARKS:

Pressure adjusted for wellbore liquids per Gas Testing Manual

SUMMARY	
Item h <u>67.9</u>	Psia
$P_c$ <u>1307</u>	Psia
Q <u>326.6</u>	MCF/D
$P_w$ <u>998.12</u>	Psia
$P_d$ <u>914.90</u>	Psia
D <u>379.97</u>	MCF/D

Company Mallon Oil Company  
 By Joe H. Cox, Jr. (Joe H. Cox, Jr.)  
 Title Production Manager  
 Witnessed By Charles Oleson  
 Company Contract Pumper for Mallon Oil Co.

# MALLON OIL COMPANY

1099 18th Street, Suite 2750, Denver, Colorado 80202  
(303) 293-2333

October 25, 1991

**RECEIVED**  
OCT 28 1991.  
**OIL CON. DIV**  
**DIST. 3**

New Mexico Conservation Division  
1000 Rio Brazos Road  
Aztec, NM 87410

Attention: Mr. Frank Chavez  
District III Supervisor

Re: Davis-Federal Comm. 3 #15, Unit O, Section 3, T25N, R2W  
Rio Arriba County, New Mexico  
1990 Deliverability Re-Test

Dear Mr. Chavez:

As we have discussed, regarding the above referenced well, Mallon's deliverability calculations include adjustments for the effects of liquid columns in the tubing and casing. In our latest conversation of October 17, we discussed the adjustment for liquids and you stated that the tests, as used by your district, neglect this factor. I would like to give you a little more background on the Davis well, and what appear to me to be significant factors for using the adjusted test figures.

As I mentioned over the phone, the tests we have conducted so far have been flowed up the casing-tubing annulus. The tests were conducted during the colder months, and that, combined with the fact that the well has a string of rods in the tubing, thus creating a change in the effective inner diameter at the tubing head, has caused freezing conditions when tubing flow has been attempted. With casing flow, our  $P_w$  has been obtained from the tubing, which, due to the periodic pumping of the well to reduce the buildup of liquids, has a higher than normal liquid column and a resulting lower surface pressure. (The well has not been pumped during the conditioning or test periods). This artificially low  $P_w$ , when applied without adjustment to the deliverability equation, results in a substantially lower deliverability factor.

Mr. Frank Chavez  
Davis-Federal cComm. 3 #15, Unit O  
Page 2 of 2

Before adjustment for liquids the ratio of  $P_w/P_c$  in the Davis well 1990 re-test is 0.075 versus an average ratio of 0.64 for all of the 3977 wells tested in the Blanco Mesaverde pool. The resulting "deliverability factor"  $((P_c^2 - P_d^2 / P_c^2 - P_w^2)^n)$  from the deliverability equation is 0.61 for the Davis well and 1.22 for the pool average. The result is a deliverability value that is nearly 40% below the actual flow rate during the test and 14.4% below the average daily sales during the nine months since the test was run.

The adjusted values of  $P_f$  and  $P_w$  were based on the depth to the gas/liquid interface as determined by sonic fluid level shooting, and the specific gravities of the produced fluids as measured at the surface. The calculations were based on formulae and examples in the Gas Well Testing Manual For Northwest New Mexico.

I feel that it should not be the intention of the Commission to penalize a well for unusual well bore conditions, such as the annular flow and high liquid level due to the rods and pump in the Davis well. I would like to request that the adjusted test be used in this case.

If I can help you with any further information, please feel free to contact me.

Sincerely,

MALLON OIL COMPANY



Joe H. Cox, Jr.  
Production Manager

JHC/tm

Attachment