

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65



Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special					Test Date 9/19/68						
Company SOUTHERN UNION PRODUCTION CO.				Connection SOUTHERN UNION GAS COMPANY							
Pool BASIN				Formation DAKOTA		Unit					
Completion Date 9/7/68		Total Depth 8240		Plug Back TD 8196		Elevation 7146					
Frog Size 7.625		Wt. 26.40	d 6.969	Set At 4054	Perforations: From 7982 To 8176						
Tbg. Size 5.500		Wt. 15.50	d 4.950	Set At 3897-8196	Perforations: From 8099 To 8107						
Frog Size 1.900		Wt. 2.90	d 1.610	Set At 8107	Perforations: From 8099 To 8107						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple DUAL - GAS - GAS					Packer Set At 7900						
Producing Thru TUBING		Reservoir Temp. °F @		Mean Annual Temp. °F		Baro. Press. - P _a 12					
L 8087		H	Gg .700	% CO ₂	% N ₂	% H ₂ S					
Prover		Meter Run		Taps							
FLOW DATA				TUBING DATA		CASING DATA					
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2"		3/4"				2172				8 DAYS
1.							260	60°			3 HOURS
2.											
3.											
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd				
1	12.3650		272	1.0000	.9258	1.032	3,213				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
2.					Specific Gravity Separator Gas _____ X X X X X X X X						
3.					Specific Gravity Flowing Fluid _____ X X X X X						
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
$P_c = 2184$ $P_c^2 = 4,769,356$											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2708$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1969$						
1	73,984		1,016,549	3,753,307	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3,846$						
2											
3											
4											
5											
Absolute Open Flow 3,846 Mcfd @ 15.025					Angle of Slope θ _____			Slope, n .75			
Remarks: _____											
Approved By Commission:			Conducted By: KENNETH E. RODDY			Calculated By: KENNETH E. RODDY			Checked By: KENNETH E. RODDY		