

**NEW MEXICO OIL CONSERVATION COMMISSION**  
**INITIAL WELL DELIVERABILITY TEST REPORT FOR 19 74**

Form C122-A  
 Revised 1-1-66

POOL NAME <b>Basin Dakota</b>	POOL SLOPE $n = .75$	FORMATION <b>Dakota</b>	COUNTY <b>San Juan</b>
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COMPANY <b>Shell Oil Co.</b>			WELL NAME AND NUMBER <b>Carson 113 - 17</b>		
UNIT LETTER	SECTION <b>17</b>	TOWNSHIP <b>25</b>	RANGE <b>11</b>	PURCHASING PIPELINE <b>E.P.N.G.</b>	
CASING O.D. - INCHES <b>5.5</b>	CASING I.D. - INCHES	SET AT DEPTH - FEET <b>5950</b>	TUBING O.D. - INCHES <b>2.375</b>	TUBING I.D. - INCHES <b>1.990</b>	TOP - TUBING PERF. - FEET <b>5600</b>
GAS PAY ZONE FROM <b>5807</b> TO		WELL PRODUCING THRU CASING TUBING <b>X</b>		GAS GRAVITY <b>.707</b>	GRAVITY X LENGTH <b>3959</b>
DATE OF FLOW TEST FROM <b>8-6-74</b> TO <b>8-14-74</b>			DATE SHUT-IN PRESSURE MEASURED <b>7-1-74</b>		

**PRESSURE DATA - ALL PRESSURES IN PSIA**

(a) Flowing Casing Pressure (DWt) <b>Pkr.</b>	(b) Flowing Tubing Pressure (DWt) <b>372</b>	(c) Flowing Meter Pressure (DWt) <b>202</b>	(d) Flow Chart Static Reading <b>202</b>	(e) Meter Error (Item c - Item d) <b>0</b> ✓	(f) Friction Loss (a - c) or (b - c) <b>170</b> ✓	(g) Average Meter Pressure (Integr.) <b>208</b>
(h) Corrected Meter Pressure (g + e) <b>208</b> ✓	(i) Avg. Wellhead Press. $P_t = (h + f)$ <b>378</b> ✓ <i>* 372</i>	(j) Shut-in Casing Pressure (DWt) <b>Pkr</b>	(k) Shut-in Tubing Pressure (DWt) <b>1529</b>	(l) $P_c =$ higher value of (j) or (k) <b>1529</b> ✓	(m) Del. Pressure $P_d =$ <b>50</b> ✓ <del>202</del> <i>765</i>	(n) Separator or Dehydrator Pr. (DWt) for critical flow only

**FLOW RATE CORRECTION (METER ERROR)**

Integrated Volume - MCF/D <b>275</b>	Quotient of $\frac{\text{Item c}}{\text{Item d}}$ <b>1.0000</b>	$\sqrt{\frac{\text{Item c}}{\text{Item d}}}$ <b>1.00000</b>	Corrected Volume Q = <b>275</b> ✓ MCF/D
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**WORKING PRESSURE CALCULATION**

$(1 - e^{-s})$ <b>.250</b> ✓	$(F_c Q_m)^2 (1000)$ <b>6687</b>	$R^2 = (1 - e^{-s}) (F_c Q_m)^2 (1000)$ <b>1692</b>	$P_t^2$ <b>138384</b> <del>142884</del>	$P_w^2 = P_t^2 + R^2$ <b>140056</b> <del>144556</del>	$P_w = \sqrt{P_w^2}$ <b>374</b> <del>382</del>
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**DELIVERABILITY CALCULATION**

$D = Q \left[ \frac{P_c^2 - P_d^2}{P_c^2 - P_w^2} \right]^n$	<b>275</b> ✓	$\left[ \frac{1752.616}{842112} \right]^n$	$(.3842)^n$	<b>.4880</b>	<b>134</b> <del>232</del> MCF/D
		<b>2191917</b>	<b>.7974</b>	<b>.8439</b>	

REMARKS:

*2,197,785*  
*\* Critical flow exists*



**SUMMARY**

Item h	<b>208</b>	Psia
$P_c$	<b>1529</b> ✓	Psia
Q	<b>275</b> ✓	MCF/D
$P_w$	<del>382</del> <b>374</b>	Psia
$P_d$	<del>202</del> <b>765</b>	Psia
D	<del>232</del> <b>232</b>	MCF/D

Company	<b>Shell Oil Co.</b>
By	<b>Neil Tefteller</b>
Title	<b>Agent</b>
Witnessed By	
Company	

*ok*