

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

-122
5-1-65

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 6-2-67								
Company Tenneco Oil Co.			Connection									
Pool Blanco Mesa Verde			Formation Mesa Verde		Unit							
Completion Date		Total Depth	Plug Back TD 7445	Elevation 6728	Farm or Lease Name Dawson "A"							
Csg. Size 4.5	Wt. d	Set At 7464	Perforations: From 5138 To 5365		Well No. 1							
Tbg. Size 2.375	Wt. d	Set At 7250	Perforations: From To		Unit Sec. Twp. Rge. N 4 27 8							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual Gas				Packer Set At 7250	County San Juan							
Producing Thru		Reservoir Temp. °F	Average Annual Temp. °F	Baro. Press. - P _g 12.0	State New Mexico							
L	H	Gg	% CO ₂	% N ₂	% H ₂ S							
Prover			Meter Run	Taps								
FLOW DATA			TUBING DATA		CASING DATA							
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow	
1.	2 x 3/4						Pkr.		929		3 hrs	
2.							Pkr.		348	60		
3.												
4.												
5.												
RATE OF FLOW CALCULATIONS												
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd					
1.	12.3650		360	1.000	.9608	1.037	4439					
2.												
3.												
4.												
5.												
NO.	P _t	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.									
1.			A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.									
2.			Specific Gravity Separator Gas _____						X X X X X X X X X X			
3.			Specific Gravity Flowing Fluid _____						X X X X X			
4.			Critical Pressure _____ P.S.I.A.			_____ P.S.I.A.			_____ P.S.I.A.			
5.			Critical Temperature _____ R			_____ R			_____ R			
P _c	941	P _c ²	885481									
NO.	F _t ²	P _w	R _w ²	P _c ² - R _w ²	(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.2783$							
1.	129600		192755	692726	(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.2022$							
2.												
3.												
4.					AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 5337$							
5.												
Absolute Open Flow				5337	Mcf/d @ 15.025				Angle of Slope θ	Slope, n .75		
Remarks:												
Approved By Commission:			Conducted By:			Calculated By: Neil Tefteller			Checked By: <i>[Signature]</i>			

RECEIVED

JUN 19 1967

**TENNECO OIL COMPANY
DURANGO, COLORADO**

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