MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

| Pool | ol <u>Sesia Sebota</u> | | | Formation Dakets | | | | County San Juan | | | | 9 |
|---|------------------------|---------------|---------------------------------------|------------------|---------------------|----------------------|--|--|--|--|----------------|----------------------------------|
| Init | ial | X | _Annual_ | | | Spec | ial | | _Date of | Test | 11-11 | 1-63 |
| Compa | any All All | RICAN I | TROLIU | CORP. | L | ease 💁 | alleges | Canyon th | itWel | 1 No | 146 | |
| Unit | I | Sec | Twp | 271 | Rge | 1 | Purc | haser | <u>.</u> | | | |
| Casir | ng 4-1/1 | Wt. 10 | 5_I.D. | 1.052 | Set | at_ 597 (| Pe: | rf 5872 | -76 | To | 685-9 | <u> </u> |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| Date of Completion: 11-4-4 | | | | 3 | Packer None | | | Type Well Single-Bradenhead-G. G. or G.O. Dual Reservoir Temp. | | | |)ual |
| OBSERVED DATA | | | | | | | | | | | | |
| m 4 . | and only and a large | 45 | (Chal | \ 444 | <u></u> | ODOLINA | up para | | Туре Тар | , a | Floor | |
| Tested Through (Chol | | | | | | | | Data | | | | |
| | (Dunamar) | (Cho | , , | | Diff. | Temp. | Tubing Press. | Temp. | Casing D | | 1 | Duration |
| No. | (Line) Size | | ize p | sig | h _w | °F. | p sig | °F. | psig | °F. | | of Flow Hr. |
| SI | 7 days | | 730 4 | 44 | | | 2060 667 | 440 | 2063 2. 1217 | 400 | | 9 bre. |
| 1. 2. | 2" | | ,,,, | | | | | | | | | |
| 3. 4. | | - | | | | | | | | | \pm | |
| 5. | | | | | | | | | | 1 | | |
| FLOW CALCULATIONS Coefficient Pressure Flow Temp. Gravity Compress. Rate of Flow | | | | | | | | | | | | |
| No. | Coefficient | | Fa | | Fact | Temp. Gravity factor | | Factor | | Q-MCFPD | | |
| - | (24-Hour) | | √ h _w p _f | ps | | | t | Fg | F _{pv} | | | |
| 1. 2. 3. | 12.3459 | | | | | 1,660 | | 17074 | | | | |
| 3. | | | | <u></u> | | | | | | | | |
| 4. 5. | | | | | | | | | | | | |
| | | | | | PRE | SSURE C | alcut at i | ONS | | | | |
| | iquid Hydr | | | | | cf/bbl. | | | fic Gravi | | | |
| Gravity of Liquid Hydrocarbons Fc(1-e | | | | | deg. | | | | Specific Gravity Flowing Fluid P _C 2075 P _C 4,305,625 | | | |
| · c | | | · · · · · · · · · · · · · · · · · · · | | | | • | <u> </u> | | | _ | |
| | $P_{\mathbf{W}}$ | P | 2 F.O | | $(\mathbf{F_cQ})^2$ | (F | 0)2 | P _w 2 | P _c ² -P _w ² | | al. | P |
| No. | Pt (psia) |) 1 | F _c Q | ' | L CM) | (1 | cQ) ² -e ^{-s}) | | | | P _W | P _w P _c |
| 1. 2. 3. | | | | | | | 13. | HALL | [| - | | |
| 3. | | | | | | | | | | | | |
| 4. 5. | | | | | | | | | | | | |
| Abso | lute Poter | ntial: | 8061 | | | MCFPD; | n | .75 | | e de la companya de l | | |
| COMP: | ESS | AN ARES | | | New Munico | | | | (af FIVEN) | | | |
| AGEN | T and TIT | LE . | h, Neber | n, M | strict | -1000 | ME | | /W | LULI | V ED | 1 |
| WITN | ESSED ANY_ | - 37 | 7- Eul | Pooli | ~~~~ | | | | | TVOV | 3 1963 | |
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INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_W). MCF/da. @ 15.025 psia and 600 F.
- P_c 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- F_t Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.