OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENT

P. O. BOX 2088
SANTA FE, NEW MEXICO 87501

Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 3-14-81	
Company: SUPRON ENERGY CORPORATION	Connection: Southern Union Gathering Company			Unit
Pool: Basin	Formation: Dakota			
Completion Date: 3-4-81	Total Depth: 6365	Plug Back TD: 6310	Elevation: 5522	Farm or Lease Name: Angel Peak
Csg. Size: 4.500 / Wt.: 10.50 / d: 4.052 / Set At: 6354	Perforations: From 6055 To 6203			Well No.: 23-E
Tbg. Size: 2.375 / Wt.: 4.70 / d: 1.995 / Set At: 6165	Perforations: From No Perforations To			Unit: O / Sec.: 10 / Twp.: 28N / Rge.: 11W
Type Well – Single – Bradenhead – G.C. or G.O. Multiple: Single		Packer Set At: ----		County: San Juan
Producing Thru: Tubing	Reservoir Temp. °F: 0	Mean Annual Temp. °F	Baro. Press. – P_a: 12	State: New Mexico
L: 6155 / H: / Gg: 0.650	% N_2	% H_2S	Prover	Meter Run / Taps

FLOW DATA

NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press. p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press. p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI	2"	3/4"				1091		1101		7 days
1.						58	67°	449		3 hours
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	12.3650		70	0.9933	0.9608	1.000	826
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 1113 P_c^2 1,238,769

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		461	212,521	1,026,248
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.2071$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1515$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 951

Absolute Open Flow 951 Mcfd @ 15.025 Angle of Slope θ _____ Slope, n 0.75

Remarks: _____

Approved By Division	Conducted By:	Calculated By:	Checked By:
	David Roark	Kenneth E. Roddy	

MAR 25 1981
OIL CON. COM.
DIST. 3