



MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 6-24-82							
Company Southland Royalty Company			Connection Southern Union Gathering								
Pool Bloomfield			Formation Chacra		Unit						
Completion Date 6-18-82		Total Depth 3160'	Plug Back TD 3147'	Elevation 5727' GL	Farm or Lease Name McClanahan						
Csq. Size 2.875	Wt. 6.5#	d 2.441	Set At 3157'	Perforations: From 2911' To 3039'							
Tbg. Size ---	Wt. ---	d ---	Set At ---	Perforations: From To							
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At ---							
Producing Thru Casing			Reservoir Temp. *F #	Mean Annual Temp. *F	Baro. Press. - P _a 12.2						
L	H	G _g .700	% CO ₂	% N ₂	% H ₂ S						
Prover	Meter Run	Taps	County San Juan								
State New Mexico											
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	Duration of Flow
SI									1031		
1.	2"	X	3/4"						227		1 hr
2.									185		2 hrs
3.									163		3 hrs
4.											
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow O. Mcfd				
1	12.365		175.2	1.0000	.9258	1.0000	2006				
2.											
3.											
4.											
5.											
NO.	P _t	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	Specific Gravity Separator Gas _____ X X X X X X X X X				
1					Specific Gravity Flowing Fluid _____ X X X X X	Critical Pressure _____ P.S.I.A.	Critical Temperature _____ R				
2.											
3.											
4.											
5.											
NO.	P _t ²	P _w ²	R _w ²	P _c ² - R _w ²	(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.0290$	(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.02169$					
1		175.2	30695.0	1057571	2						
2											
3											
4											
5											
AOF = Q						$\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 2050$					
Absolute Open Flow	2050	Mcf/d @ 15.025	Angle of Slope @	Slope, n .75							
Remarks:											
Approved By Division		Conducted By: Steve Kelleners		Calculated By: James Smith		Checked By: R. E. Fielder					