## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

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	ialX	Ar	nual		Sp <b>ec</b> :	ial	<del></del>	_Date of	Test	May 25.	1960
mp	any Pan Ame	rican P	troleum	Corp.	Lease	E, H. P.	lekin	We	ll No	5	
it	<b>B</b> Se	c. <u>36</u>	Twp	Rg_Rg	e. <u>11W</u>	Purch	aser <u>s</u>	ntiern U	nion Ga	a Company	<u> </u>
si	ng_ <b>_6_1/2</b> _Wt	. 9.5	I.D. 4.	<b>090</b> Se	t at <b>62</b>	Per	·f •	53	_To	6171	
biı	ng <b>2-3/8</b> Wt	4.7	_I.D <u>1.</u>	<b>995</b> Se	t at 61	N Per	·f		Kone To		
s l	Pay: From_	<u> </u>	6171	L <b>6</b>	143 x	- <b>700</b> (	est.)GL	4300	_Bar.Pre	ess. <u>12</u>	
od1	ucing Thru:	Casing		Tu	bing		_Type We	113 <u>i</u>	ngl <b>o-</b> ga	6	
ıte	of Completi	.on: <b>5</b> -	-17-60	Packe	r Mon	Sing ●	le-Brade Reservo	nhead-G. ir Temp.	G. or (	3.0. Dual	
	-			<del></del>	OBSERVE		<del></del>				
ste	ed Through	(P10000)	(Choke)	( Martiners )				Type Ta	าร		
			Data		· 7	Tubing	Dat a	Casing		Τ	
$\top$	(PERSONAL)	(Choke)	Press	• Diff.	Temp.					Dur	
0 0	(Line) Size			h <sub>w</sub>	o <sub>F</sub> .	psig	°F.	psig	□F.	H	Flow
	Shut in		135		40 (0-4)	2011		2011			
$\top$		3/4-	425		60 (est	327		1052		3 hr	
-									<u> </u>		
	Coefficie	n+			FLOW CALC			Compa		Rate of	Flow
						cor	Factor	Factor F <sub>pv</sub>		Q-MCFPD @ 15.025 psia	
+-							F <sub>g</sub>				
1											
					<del></del>						
											<u> </u>
				PRI	ESSURE CA	TTCOLATIO	INS				
	.quid Hydroc y of Liquid		rbons_		c:/bbl. deg.		Speci	fic Gravi	ity_Flow	arator Ga ving Flui	
vit		Hydroca					Speci		ity_Flow		
vit	y of Liquid	Hydroca	rbons_		deg.		Speci	fic Gravi	ity_Flow	ving Flui	
vit	y of Liquid	Hydroca	rbons_	(F <sub>c</sub> Q) <sup>2</sup>	deg.	Q) <sup>2</sup>	Speci	fic Gravi	ity Flov	ving Fluid .092.529	i
vit	y of Liquid	Hydroca	rbons_(1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	deg.	Q) <sup>2</sup> -e <sup>-s</sup> )	Speci Pc—— Pw2	fic Gravi	Pc Ca	ving Fluid 092.529	i
vit	y of Liquid	Hydroca	rbons_(1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	deg.	Q) <sup>2</sup> -e <sup>-s</sup> )	Speci Pc—— Pw2	fic Gravi <b>2023</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Pc Ca	ving Fluid .092.529	i
vit	y of Liquid	Hydroca	rbons_(1-e <sup>-s</sup> )	(F <sub>c</sub> Q) <sup>2</sup>	deg.	Q) <sup>2</sup> e-s)	Speci Pc—— Pw2	fic Gravi <b>2023</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Pc Ca	ving Fluid .092.529	i
vit	Pw Pt (psia)	Pt Pt	F <sub>c</sub> Q 6720		(Fc (1-	n75	Speci Pc—— Pw2	fic Gravi <b>2023</b> P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Pc Ca	ving Fluid .092.529	i
sol MPA	Pw Pt (psia)  Oute Potenti	Pt al:	F <sub>c</sub> Q	Corporat	deg.  (Fo (1-	n75	Speci Pc- Pw2	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Pc Ca	ving Fluid .092.529	i
sol MPA DRE	Pw Pt (psia)	Pt al:	F <sub>c</sub> Q	Corporat	deg.  (Fo (1-	n75	Speci Pc—— Pw2	P <sub>c</sub> -P <sub>w</sub> <sup>2</sup>	Pc Ca	ving Fluid .092.529	i

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure  $(P_w)$ . MCF/da. @ 15.025 psia and 60° F.
- $P_c$  72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwI Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fnv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_W$  cannot be taken because of manner of completion or condition of well, then  $P_W$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_+$ .