

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special				Test Date 9-29-76	
Company Dugan Production			Connection New well		
Pool Blanco			Formation Mesa Verde		Unit
Completion Date		Total Depth	Plug Back To	Elevation	Form or Lease Name Sherman-Edwards
Csg. Size 5.500	Wt. d	Set At 5764	Perforations: From 5222 To 5606		Well No. #2A MV
Tbg. Size 1.660	Wt. 2.4	d 1.380	Set At 5550	Perforations: From To	Unit Sec. Twp. Rge. E 3 29 5
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Gas - dual completion				Packer Set At 5200	County Rio Arriba
Producing Thru tubing		Reservoir Temp. *F @	Mean Annual Temp. *F	Baro. Press. - P _a 12.0	State New Mexico
L	H	Gg .586	% CO ₂ 1.18	% N ₂ .12	% H ₂ S sweet
Prover 2"		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	Temp. *F	of Flow
SI							1150				SIP
1.	2"	X	1/8"	1088		56°	1088		*1110		2 hr.
2.	2"	X	3/16"	961		62°	961		1018		2 hr.
3.	2"	X	1/4"	788		66°	788		908		2 hr.
4.	2"	X	5/16"	545		60°	545		719		2 hr.
5.	2"	X	5/16"	472		60°	472		623		12 hr.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	0.265		1100	1.004	1.306	1.095	419
2	0.608		973	.998	1.306	1.080	833
3	1.087		800	.994	1.306	1.064	1201
4	1.672		557	1.000	1.306	1.046	1272
5	1.672		484	1.000	1.306	1.040	1099

NO.	P _t	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	1.63	516	1.46	.834	A.P.I. Gravity of Liquid Hydrocarbons	Deq.
2.	1.44	522	1.48	.858	Specific Gravity Separator Gas	X X X X X X X X
3.	1.18	526	1.49	.883	Specific Gravity Flowing Fluid	0.8 x x x x 376
4.	.82	520	1.47	.914	Critical Pressure 672 + 4	P.S.I.A. 676
5.	.72	520	1.47	.924	Critical Temperature 354 - 1	R 353

P _c 1162 P _c ² 1350244				(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$	
NO	P _t ²	P _w	P _w ²	P _c ² - P _w ²			
1		1110	1232100	118144			
2		1018	1036324	313920			
3		908	824464	525780			
4		719	516961	833283			
5		623	388129	962115			

Absolute Open Flow 1,425 Mcfd @ 15.025		Angle of Slope 36°	Slope, n .73
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Remarks: Flow rates were calculated using NMOCC factors. * Working pressure (PW) was calculated.

Approved By Commission:	Conducted By: F.S. Hamrick	Calculated By: B.J. Broughton	Checked By:
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