

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

1. P. Test - Gallup #303

RECEIVED

DEC 27 1984

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		11/15/84	
Company				Connection							
Blackwood & Nichols Co., Ltd.				Northwest Pipeline							
Pool				Formation				Unit			
Undesignated				Gallup							
Completion Date		Total Depth		Plug Back TD		Elevation		Farm or Lease Name			
11-4-84		8011'		7962'		6337' G.L.		Northeast Blanco			
Csg. Size	Wt.	d	Set At	Perforations:				Well No.			
4.500	11.60	4.000	8011'	From 7014' To 7228'				No. 303			
Tbg. Size	Wt.	d	Set At	Perforations:				Unit Sec. Twp. Rye.			
2.375	4.70	1.995	7893'	From To				P 20 31N 6W			
Type Well - Single - Brodenhead - G.G. or G.O. Multiple						Packer Set At		County			
Dual Gas						7264'		Rio Arriba			
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press. - P _a		State			
Casing		°				12.0		New Mexico			
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run	Taps			
7014		.585				3/4"					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	Gallup Csg.								2835		
1.											
2.											
3.	3/4" Choke		127			53 ⁰					3 hrs.
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1							
2							
3	12.365		139	1.0068	1.012	1.011	1,770
4							
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 2847	P _c ² 8,105,409	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0040$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0030$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1				
2	19,321	180	32,400	8,073,009
3				
4				
5				

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1775$

Absolute Open Flow	1775	Mcfd @ 15.025	Angle of Slope @	Slope, n .75
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Remarks: No liquids produced; light mist

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Clark	Clark	