NEW MEXICO OIL CONSERVATION COMMISSION GAS WELL TEST DATA SHEET - - SAN JUAN BASIN

(TO BE USED FOR FRUITLAND, PICTURED CLIFFS, MESAVERDE, & ALL DAKOTA EXCEPT BARKER DOME STORAGE AREA)

Purchasing Pipeline	Pool	Blanco Mesa	Verde	Formation_	Mesa Verde	County	San Juan	
Page Natural Case Loase San Juan 32-9 Unit Well No. 55		El Pa	aso Natural			•		
Description								
Unit K Sec. 12 Two 32 Rige. 10 Pay Zone: From 5770 To 5992	Operator	El Paso Natura	l Ges	Lease	an Juan 32-9 Un	it We	_{Il No.} 56	
Casing: OD 5-1/2 WT 15.5 Set At	. K	Sec. 12	Two. 32	10	Pay Zone: From	577 0	E000	
Produced Through: Casing		4					-	5954
Date of Flow Test: From 1-0-58	-		501	7		605		
Office Size				_		u1 eu	Latindted	1
Plowing cosing pressure (Dwt)								
Flowing casing pressure (Dwt)	Meter Run Si	ze	0	rifice Size	Туре	Chart	Type Taps	
Flowing meter pressure (Dwt)				OBSERVE	ED DATA			
Flowing meter pressure (Dwt)								(a)
Flowing meter pressure (meter reading when Dwt, measurement taken: Normal chart reading								(b)
Normal chart reading $\frac{1}{2} \times \frac{1}{2} \times 1$	Flowing meter	pressure (Dwt)			psig ·	+ 12 =	psia	(c)
Square root chart reading (Flowing meter	pressure (meter readi						
Meter error (c) - (d) or (d) - (c)	Normal cha	ırt reading	. 2		psig	+ 12 =	psia	(d)
Fiction loss, Flowing column to meter: (b) - (c) Flow through tubing: (a) - (c) Flow through costing Seven day overage static meter pressure (from meter chart): Normal chart average reading) ² x sprin					(d)
(b) - (c) Flow through tubing; (a) - (c) Flow through casing =				1		=	psi	(e)
Seven day average static meter pressure (from meter chart): Normal chart average reading (7.10) 2 x sp. const. 10 psig + 12 = 504 psia Corrected seven day avge, meter press, (p_f) (g) + (e) = 504 psia psia Pf = 504 psia psia psig + 12 = 972 psia psia psia psig + 12 = 972 psia psia psia psia psia psia psia psia	-			uah oasina		_	nei	(f)
Normal chart average reading $\frac{7.10}{10} \cdot 2x \text{ sp. const.} = \frac{504}{504} \text{psid}$ Square root chart average reading $\frac{7.10}{10} \cdot 2x \text{ sp. const.} = \frac{504}{504} \text{psid}$ Corrected seven day average. (pgt) (gt) + (e) = $\frac{504}{504} \text{psid}$ Pt = (h) + (f) = $\frac{504}{504} \text{psid}$ Wellhead casing shut-in pressure (Dwt) = $\frac{960}{960} \text{psig} + 12 = \frac{972}{972} \text{psid}$ Wellhead thisting shut-in pressure (Dwt) = $\frac{960}{960} \text{psig} + 12 = \frac{972}{972} \text{psid}$ Pc = (j) or (k) whichever well flowed through Flowing Temp. (Meter Run) = $\frac{523}{100} \text{shape} = \frac{523}{100} \text{shape} = \frac{523}{100} $						-		(-)
$\begin{array}{c} SQuint Notice to Vertice Latting Vertice Latting Vertice Latting Scholar Scho$	Normal cha	rage static meter pres art average reading	sure (moin mere		psig	+ 12 =	psia	(g)
Corrected seven day avge, meter press, $(p_f)(g) + (e)$ $P_f = (h) + (f)$ $P_f = (f) + (f)$ $P_f = (f$	Square root	t chart average readin	7.10	2 x sp. const.	10	=50 ¹		
P _c = (h) + (f) 960			• • • • • • • • • • • • • • • • • • • •	•			psia	
Wellhead casing shut-in pressure (Dwt) 960 psig + 12 = 972 psig Wellhead tubing shut-in pressure (Dwt) 960 psig + 12 = 972 psig Pc = (j) or (k) whichever well flowed through Flowing Temp. (Meter Run) Pd = ½ Pc = ½ (1)		• •			^		psid	(i)
Wellhed tubing shut-in pressure (Dw) Poc = (1) or (k) whichever well flowed through Flowing Temp. (Meter Run) Flowing Temp. (Meter Run	•	ng shut-in pressure (D)wt)	•	nsia	· • •		(j)
Flowing Temp. (Meter Run)	Wellhead tubir	ng shut-in pressure (D	wt)	96	psig			(k
Plow RATE CALCULATION Plo	$P_c = (j) \text{ or } (k)$	whichever well flower	d through	62				(1)
$Q = \underbrace{\begin{array}{c} SUMARY \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_d^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_w^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_w^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_w^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_w^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_w^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ P_c = P_w^2 \\ Q = \underbrace{\begin{array}{c} SUMARY \\ SUM_c = \underbrace{\begin{array}{c} SUM_c = SUM_c \\ SUM_c = \underbrace{\begin{array}{c} SUM_c \\ SUM_c = $	Flowing Temp	, (Meter Run)			0			s (m
$Q = \underbrace{\begin{array}{c} X \\ \text{(integrated)} \end{array}} X \\ \underbrace{\begin{array}{c} DELIVERABILITY \ CALCULATION \\ \hline \\ P_c - P_d^2 \\ \hline \\ P_c - P_w^2 \\ \hline \end{array}} = \underbrace{\begin{array}{c} 708,588 \\ \hline \\ 587,817 \\ \hline \end{array}}_n \\ \underbrace{\begin{array}{c} 1.0301 \\ \hline \\ 1.0225 \\ \hline \end{array}} = \underbrace{\begin{array}{c} 390 \\ \hline \\ 390 \\ \hline \\ MCF/da \\ \hline \\ SUMMARY \\ P_c = \underbrace{\begin{array}{c} 972 \\ \hline \\ 92 \\ \hline \\ \hline \\ 92 \\ \hline \\ \hline \\ 94 \\ \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $	$P_d = \frac{1}{2} P_c = \frac{1}{2}$	<u>(</u> (1)				= 400)psia	(n
$Q = \frac{1}{(\text{integrated})} \times \frac{1}{\sqrt{(d)}} = \frac{1}{\sqrt{(d)}} = \frac{1}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt{(d)}} = \frac{1.0301}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt{(d)}} = \frac{1.0301}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt{(d)}} = \frac{1.0301}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt{(d)}} = \frac{1.0301}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt{(d)}} = \frac{1.0301}{\sqrt{(d)}} \times \frac{1.0301}{\sqrt$			/ FI	OW BATE CAL	CIII ATION	\		
SUMMARY Pc			/ 	OW HATE CAL	COLATION	\ ,		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 =	x	Vic	<u>) </u>	=	\	381	F/da
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$D = Q \qquad \begin{array}{ c c c c c c c c c c c c c c c c c c c$,	,	\ \V(d)					
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SUMMARY SUMMARY Signed Summary Summary Summary Signed Signe		381 (¹	2 - Pá)=	708,588 r	1.0301	_	390	271-
SUMMARY SUMMARY Signed Summary Summary Summary Signed Signe	D = Q	†	2 2	687,817	1.0225	=	мсғ	/da.
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		072			El F	aso Natural	LGas	
Pw = 507 psia Title Lewis D. Galloway Pd = 486 psia Witnessed by Company. * This is date of completion test. * Meter error correction factor REMARKS OR FRICTION CALCULATIONS GL (1-e-s) (FcQ)2 (1-e-s) Pt2 Pt2 Pt2 Pt2 Pt2 Pt2 Pt3	-	2Ω1	,	•				
Pd = 486 psia Witnessed by Lewis D. Galloway D = 390 Mcf/day Company. * This is date of completion test. * Meter error correction factor REMARKS OR FRICTION CALCULATIONS GL (1-e-s) (FcQ)2 (1-e-s) Pt2 Pt2 Pt2 Pt2 Pt2 Pt2 Pt2 Pt3		E07		_	Title			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	**	100		•		# Pwie D 4	Galloway	
• This is date of completion test. • Meter error correction factor REMARKS OR FRICTION CALCULATIONS GL (1-e^-s) $(F_cQ)^2$ $(1-e^{-s})$ Pt^2 $Pt^2 + R^2$ Pt^2	-	700		-				
* Meter error correction factor REMARKS OR FRICTION CALCULATIONS	-							
GL (1-e ^{-s}) $(F_cQ)^2$ $(1-e^{-s})$ P_t^2 $P_t^2 + R^2$ P_t^2		•						
GL $(1-e^{-s})$ $(F_cQ)2$ R^2 $(Column i)$ $P_t^2 + R^2$ P_t	r		REM.					
R ² (Column i)	GI.	(1-e ^{-s})	(F_0)2	(FcQ)	2 (1-e-s)	Pt ²	P.2 + R2	Pw
7600 070 10 971		<u></u>	- 54/2		R ²	(Column i)	,	w
I DOME 1 (200) 1 12 DAI 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3602	.230	12.831	2	051	254.016	256 967	507

D at 500 = 378



